LT1725 and LTC1693

DESCRIPTION

Demonstration circuit 562A-C is an isolated synchronous forward converter featuring the LT1725 and LTC1693. The design provides an isolated 12V at 12A from 48V (36V to 72V) input. Isolation voltage is 1500VDC. The circuit features low input capacitance, feedback without an opto-isolator, input undervoltage lockout and short circuit cycling protection to minimize thermal stress. Design files for this circuit board are available. Call the LTC factory.

PARAMETER	CONDITION	VALUE	
Minimum Input Voltage		36V	
Maximum Input Voltage		72V	
Output Voltage (V _{OUT)}	V _{IN} = 36V to 72V, I _{OUT} = 0A to 12A	12V±2%	
Maximum Input Current	V _{IN} = 36V, I _{OUT} = 12A	4.3A	
Inrush Transient	V _{IN} = 72V	0.5 A ² s	
Maximum Output Current		12A	
Nominal Switching Frequency		200kHz	
Output Short Circuit Period	Cycling, Auto-restart	300ms	
Dynamic Response	Peak Deviation	1000mV	
	Load Step 50% to 100%		
	Settling Time (to within 10mV of set point)	200µs	
Efficiency	V _{IN} = 48V, I _{OUT} = 12A	93.5% Typical	
Output Ripple	V _{IN} = 48V, I _{OUT} = 12A (20MHz BW)	300mV _{P-P}	
Isolation Voltage		1500 VI	C
Isolation Resistance		10 M	Ω
Isolation Capacitance		2200 pF	

OPERATING PRINCIPLES

CIRCUIT OVERVIEW

This single transistor forward converter operates at a nominal switching frequency of 200 kHz. Pulse width modulation control is done by U1, the LT1725 controller. Galvanic isolation is met with transformer T1,

T2 and L1. C7 is used as a local bypass to reduce common mode currents.

The primary side power path is comprised of T1, C6, C24, C25, Q1 and Q10 the primary switches. Power is transferred during the on time of Q1 and Q10. MOS-FETs Q3, 4, 5, and 6 are the secondary synchronous

rectifiers. L1, C1 and C2 form the secondary output filter. L2, C6, C24 and C25 form the primary input filter. C5 bypasses the input terminals. For large values of input inductance, an external 22uF aluminum electrolytic capacitor will damp the input filter and provide adequate stability. This will however, increase inrush transient current from 0.5A²s to about 3.5 A²s. See Linear Technology Application Note AN19 for a discussion on input filter stability analysis.

An auxiliary winding on L1 performs two functions; it provides output feedback information and supplies bias voltage to the LT1725. U2, the LTC1693, synchronizes with the LT1725 via T2, a small pulse transformer, to provide gate drive to secondary switching MOSFETs.

During an output short circuit, the primary bias supply collapses. This results in the converter harmlessly cycling on and off, reducing power dissipation to a minimum. The cycling rate is nominally 3.3Hz with 48V input. When the short is removed, the converter returns to normal operation.

DC562A-C relies on the pcb area (2.5"x3") and 200 linear feet per minute of airflow to provide full load operation to 50°C ambient without the use of a heat sink. The area might be reduced further (depending on airflow and ambient temperature) when used as part of a larger pcb. The maximum output power is primarily limited by component temperature rise. For example, for continued reliability, temperature should be kept below 105°C and the magnetics temperature rise should be limited to 50°C. Assuming 50°C ambient, this corresponds to 55°C surface mount component temperature rise. Figures 6 through 16 detail the temperature rise for the hottest components in the design with and without airflow. Based on these measurements and assuming a 50°C ambient, it is recommended that the output load current be limited to 8A without airflow and 12A with 200 linear feet per minute of airflow.

When input voltage is applied, R8 provides trickle charge current to C10, resulting in a turn on delay of approximately 1000ms at 36Vin.

Figure 5 shows efficiency. Figures 6 through 16 show hot spot temperature rise.

FORWARD CONVERTER DESIGN EQUATIONS

The single-transistor forward converter is a good choice for 48V telecom applications. This topology is used quite extensively in many modular designs. Unlike the flyback, energy is not intentionally stored in the power transformer. This allows for a much smaller transformer design.

The forward converter has pulsating current in the input capacitor and continuous current in the output capacitor. Worst case ripple current for the input capacitor occurs at 60% duty cycle. Four 0.82μ F ceramic capacitors (C5, C6, C24 and C25) are used for the input filter. The basic single-transistor synchronous forward converter diagram is shown in Figure 3. The idealized equations for duty cycle relationships are shown below.

Basic Duty Cycle Equation:

$$V_{\text{OUT}} = V_{\text{IN}} \bullet DC \bullet \frac{N_{\text{S}}}{N_{\text{P}}}$$

Input Capacitor RMS Current:

$$I_{\text{RMS}} = I_{\text{OUT}} \bullet \frac{N_{\text{S}}}{N_{\text{P}}} \bullet \sqrt{DC - DC^2}$$

Output Capacitor RMS Current:

$$I_{\text{RMS}} = \frac{I_{\text{L}}(pk-pk)}{\sqrt{12}}$$

Inductor Ripple Current:

$$I_{L}(pk-pk) = \frac{(V_{OUT}+V_{D})\bullet(1-DC)\bullet f_{SW}}{L}$$

Primary RMS Current:

$$I_{\text{RMS}} = I_{\text{OUT}} \bullet \frac{N_{\text{S}}}{N_{\text{P}}} \bullet \sqrt{DC}$$

Secondary RMS Current:

$$I_{\rm RMS} = I_{\rm OUT} \bullet \sqrt{\rm DC}$$

SAFETY AND ISOLATION

The demo board is designed to meet the requirements of UL 60950, 3^{rd} edition for basic insulation in secondary circuits. The input is considered to be a TNV-2 circuit, and the output is SELV. The bridging capacitor C7 has an agency file number. A 6A fast blow type fuse must be placed in series with the ungrounded (hot) input line. The transformer is designed to meet the basic insulation requirement with an isolation voltage of 1500VDC. The core is considered part of the secondary circuit.

CONDUCTED EMI

Tests for conducted emissions were performed for the demo board. An external PI filter using a $68 \mu F$

QUICK START PROCEDURE

Demonstration circuit 562A-C is easy to set up to evaluate the performance of the LT1725 and LTC1693. Refer to 0 for proper measurement equipment setup and follow the procedure below:

NOTE: When measuring the input or output voltage ripple, care must be taken to avoid a long ground lead on the oscilloscope probe. Measure the input or output voltage ripple by touching the probe tip directly across the Vin or Vout and GND terminals. See Figure 2 for proper scope probe technique.

- For normal operation, a minimum of 36V must be applied at the input. Input voltages lower than 36V will keep the converter from turning on due to the undervoltage lockout feature in the LT1725.
- **2.** Connect a 36-72V power supply, a 22uF 100V capacitor and meters to the Vin pins, as shown in Figure 1. Observe proper polarity.
- **3.** Connect a 0-12A load and meters to the Vout pins, as shown in Figure 1.
- **4.** After all connections are made, turn on the input power and verify the output voltage, regulation, ripple voltage, efficiency and other parameters.

aluminum electrolytic capacitor, 37μ H inductor and 10μ F film capacitor is required for the CISPR 22 class B limit. No tests for radiated RFI were performed. Proper grounding and layout technique must be observed to minimize radiation. See Figure 4 for EMI test setup. For EMI graphs see Figures 17 and 18.

RELIABILITY

Reliability prediction for the circuit has been calculated using the Telcordia (formerly Bellcore) SR-332. The black box technique was used. The calculation was made assuming a grounded, fixed, controlled environment and quality level II. A 50% electrical stress at 40°C yields an MTBF (mean time between failures) of 1.5 million hours.

NOTE: If there is no output, temporarily disconnect the load to make sure that the load is not set too high.

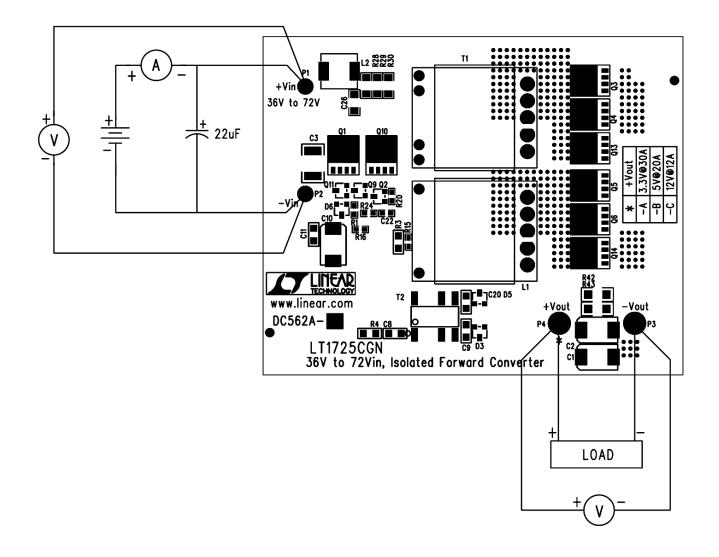


Figure 1. Proper Measurement Equipment Setup

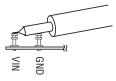


Figure 2. Measuring Input or Output Ripple



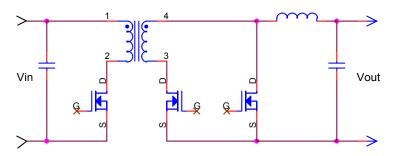


Figure 3. Basic single transistor synchronous forward converter

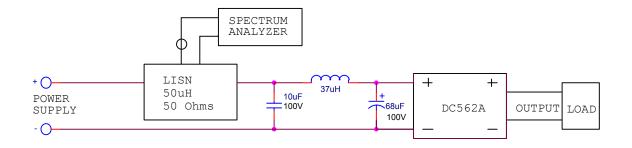


Figure 4. EMI Setup

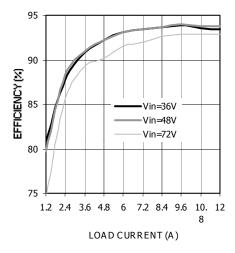


Figure 5. Typical Efficiency

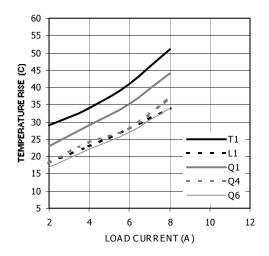


Figure 6. T1 and L1 Core and Q1, Q4, and Q6 Case Temperature Rise at 36Vin, No Airflow

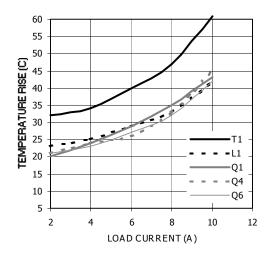


Figure 7. T1 and L1 Core and Q1, Q4, and Q6 Case Temperature Rise at 48Vin, No Airflow

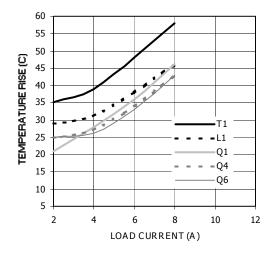


Figure 8. T1 and L1 Core and Q1, Q4, and Q6 Case Temperature Rise at 72Vin, No Airflow

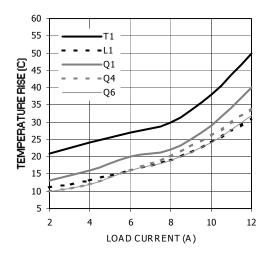


Figure 9. T1 and L1 Core and Q1, Q4, and Q6 Case Temperature Rise at 36Vin with 200LFM of Airflow

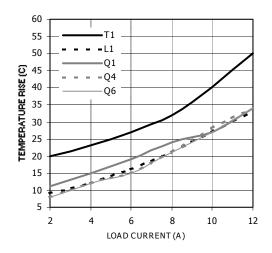


Figure 10. T1 and L1 Core and Q1, Q4, and Q6 Case Temperature Rise at 48Vin with 200LFM of Airflow

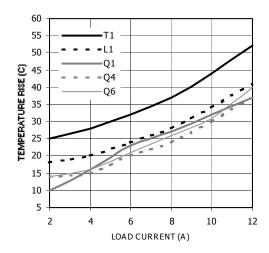


Figure 11. T1 and L1 Core and Q1, Q4, and Q6 Case Temperature Rise at 72Vin with 200LFM of Airflow

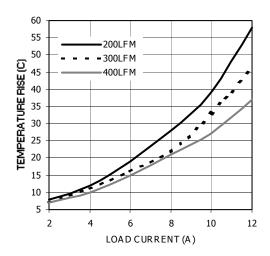


Figure 12. Q6 Case (Hottest component on board) Temperature Rise at 48Vin with 200LFM, 300LFM and 400LFM of Airflow

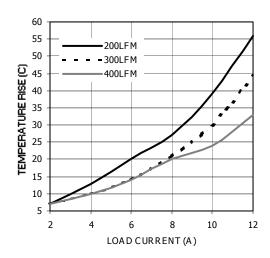


Figure 13. T1 Core Temperature Rise at 48Vin with 200LFM, 300LFM and 400LFM of Airflow

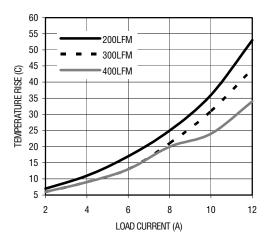


Figure 14. L1 Core Temperature Rise at 48Vin with 200LFM, 300LFM and 400LFM of Airflow

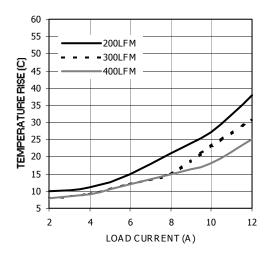


Figure 15. Q1 Case Temperature Rise at 48Vin with 200LFM, 300LFM and 400LFM of Airflow

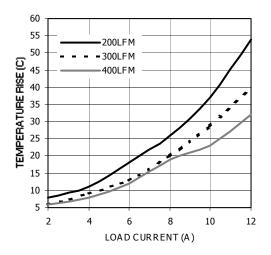


Figure 16. Q4 Case Temperature Rise at 48Vin with 200LFM, 300LFM and 400LFM of Airflow

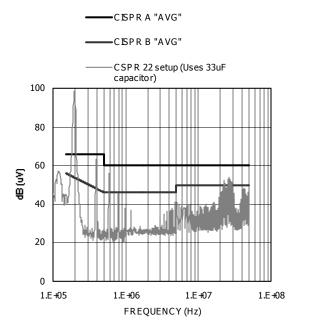


Figure 17. Conducted Emissions at V_{IN} = 48V, 12A load, without input PI Filter

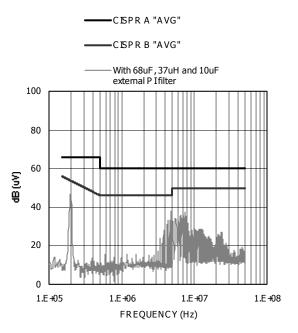
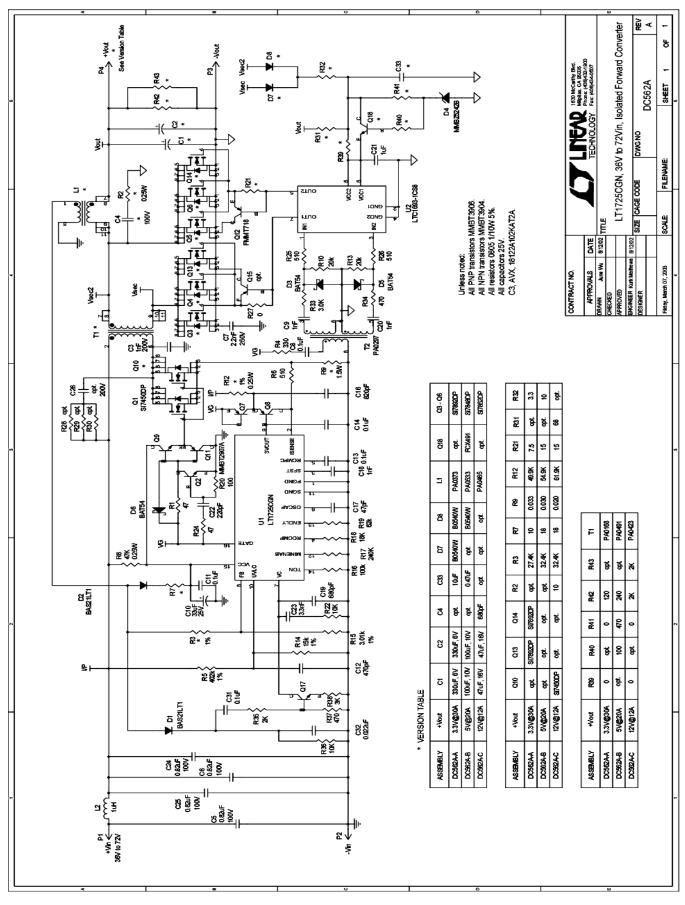


Figure 18. Conducted Emissions at V_{IN} = 48V with External PI Filter, 12A load, with input PI Filter



T