# QUICK STARTGUIDE FOR DEMONSTRATIO N CIRCUIT1352A LOW QUIESC ENTCURRENT, DUALOUTPUTSYNCHRONOUSBUCK CONVERTER 

## DESCRIPTION

Demonstration circuit 1352A is a Low Quiescent Current, Dual Output Synchronous Buck Converter featuring the LTC3857EGN-1/LTC3858EGN-1. The circuit is single sided layout, while the package style for the LTC3857/8EGN-1 is a 28 -lead narrow plastic SSOP.

The main features of the board include rail tracking (LTC3857EGN-1 only), an internal 5V linear regulator for bias, RUN pins for each output, a PGOOD signal (CH1 only) and a Mode selector that allow the converter to run in CCM, pulse skip or Burst Mode operation. Synchronization to an external clock is also possible.
Two versions of the board are available. DC-1352A-A is for the LTC3857EGN-1, while the DC1352A-B is for the LTC3858EGN-1. The

LTC3857EGN-1 offers lower quiescent current and smaller burst mode ripple, while the LTC3858EGN-1 offers latch-off protection and increased burst mode efficiency.

The wide input voltage range of 4.5 V to 36 V is suitable for automotive or other battery fed application where low quiescent current is important. The LT3857EGN-1 and LTC3858EGN-1 datasheets give a complete description of these parts, operation and application information. The datasheets must be read in conjunction with this quick start guide for demo circuit 1352A.
Design files for this circuit board are available. Call the LTC factory.

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Table 1. Performance Summary ( $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ )

| PARAMETER | CONDITION | VALUE |  |
| :---: | :---: | :---: | :---: |
| Minimum Input Voltage |  | $4.5 \mathrm{~V}^{\text {\# }}$ |  |
| Maximum Input Voltage |  | 36V |  |
| Output Voltage V ${ }_{\text {OUT1 }}$ | $\mathrm{V}_{\text {IN }}=4.5 \mathrm{~V}$ to 36 V , I OUT1 $=0 \mathrm{~A}$ to 5 A | $3.3 \mathrm{~V} \pm 2 \%$ |  |
| Output Voltage $\mathrm{V}_{\text {OUT2 }}$ | $\mathrm{V}_{\text {IN }}=9 \mathrm{~V}$ to 36 V , I ${ }_{\text {OUT2 }}=0 \mathrm{~A}$ to 3 A | $8.5 \mathrm{~V} \pm 2 \%$ |  |
| Nominal Switching Frequency |  | 350 kHz |  |
| Efficiency, DC1352A-A/B <br> See Figures 3 to 6 for efficiency curves |  | $\mathrm{V}_{\text {IN }}=24 \mathrm{~V}$ | $\mathrm{V}_{\text {IN }}=36 \mathrm{~V}$ |
|  | $\mathrm{V}_{\text {OUT1 }}=3.3 \mathrm{~V}, \mathrm{I}_{\text {OUT1 }}=5 \mathrm{~A}$ | 92.5\%* Typical | 90.4\%* Typical |
|  | $\mathrm{V}_{\text {OUT2 }}=8.5 \mathrm{~V}, \mathrm{I}_{\text {OUT1 }}=3 \mathrm{~A}$ | 96.6\%* Typical | 95.4\%* Typical |
| * Measured at bulk output capacitor | \# Minimum input voltage required for 8.5 V out regulation is 9 Vin |  |  |

## QUICK START PROCEDURE

Demonstration circuit 1352A is easy to set up to evaluate the performance of the LTC3857EGN-1/LTC3858EGN-1. Refer to Figure 1 for proper measurement equipment setup and follow the procedure below:

NOTE: When measuring the input or output voltage ripple, care must be taken to avoid a long ground
lead on the oscilloscope probe. Measure the input or output voltage ripple by probing directly across the bulk Vin or Vout capacitor. See Figure 2 for proper scope probe technique.

1. Place jumpers in the following positions:

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| JP2 | Burst Mode |
| :--- | :--- |
| JP3 | On |
| JP4 | On |
| JP5 | SS |
| JP6 | SS |

2. With power off, connect the input power supply to Vin and GND.
3. Turn on the power at the input.
note: Make sure that the input voltage does not exceed 26 V .
4. Check for the proper output voltages.

$$
\begin{aligned}
& \text { Vout1 }=3.234 \mathrm{~V} \text { to } 3.366 \mathrm{~V}, \\
& \text { Vout2 }=8.330 \mathrm{~V} \text { to } 8.670 \mathrm{~V}
\end{aligned}
$$

NOTE: If there is no output, temporarily disconnect the load to make sure that the load is not set too high.
5. Once the proper output voltages are established, adjust the loads within the operating range and observe the output voltage regulation, ripple voltage, efficiency and other parameters.
6. Different operating modes can be evaluated by changing position of jumper JP3.


Figure 1. Proper Measurement Equipment Setup

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Figure 2. Measuring Input or Output Ripple Directly Across Bulk Capacitor

## RAIL TRACKING

Demonstration circuit 1352 is setup for independent soft start without tracking. The soft start ramp-rate is determined by the value of the SS capacitors C1 and C23. This board can also be operated in coincident tracking mode with either
output as master or both can slave an external ramp Refer to Table 2 for tracking options and to the data sheet for more details.

Table 2. Output Tracking Options

|  | TRACKISS JUMPERS |  | TERMINALS |  |
| :--- | :---: | :---: | :---: | :---: |
| CONFIGURATION | JP3 | JP4 | TRACK1 | TRACK2 |
| Soft Start Without Tracking <br> Vout1 <br> Vout2 | SS |  |  |  |
| Coincident Tracking: |  |  | No connection / Don't care |  |
| Vout1 tracking External Ramp | TRACK |  |  |  |
| Vout2 tracking External Ramp |  | TRACK |  |  |
| Vout2 tracking Vout1 | SS | TRACK | No connection / Don't care | Connection / Don't care |
| Vout1 tracking Vout2 | TRACK | SS | Connect to Vout2 | No connecternal ramp |

## INDUCTOR DCR SENSING AND RESISTOR SENSING

The DCR sense circuit uses the resistive voltage drop across the inductor to estimate the current. In contrast to the traditional sense resistor current feedback, the DCR sensing circuit offers lower cost and higher efficiency, but results in less accurate current limit due to the large variation of the inductor DC resistance. Furthermore, this indirect current sensing method cannot detect inductor saturation and requires the use of 'soft' saturating inductors (such as powder
iron) resulting in increased core losses or 'hard' saturating inductors (such as ferrite) with sufficiency high current ratings resulting in increased inductor size.
For modifying the demo board for DCR sensing, please refer to Table 3. A full load efficiency improvement of between $0.25 \%-0.75 \%$ is still possible with optional DCR sensing, but since the inductors are ferrite based, short circuit performance may be compromised.

Table 3. DCR sensing component selection

|  | REMOVE RSENSE NETWORK | DCR NETWORK |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Vout1 | $\mathrm{R} 8, \mathrm{R} 9=$ Open, R10 $=$ Short | $\mathrm{R} 28=1.37 \mathrm{k} \Omega$ | $\mathrm{R} 30=2.74 \mathrm{k} \Omega$ | $\mathrm{R} 29=0 \Omega$ | $\mathrm{C} 6=0.47 \mu \mathrm{~F}$ |
| Vout2 | $\mathrm{R} 20, \mathrm{R} 21=$ Open, R17 = Short | $\mathrm{R} 32=1.91 \mathrm{k} \Omega$ | $\mathrm{R} 31=1.54 \mathrm{k} \Omega$ | $\mathrm{R} 33=0 \Omega$ | $\mathrm{C} 18=0.47 \mu \mathrm{~F}$ |

## FREQUENCY SYNCHRONIZATION

Demonstration circuit 1352's Mode selector allows the converter to run in CCM, pulse skip or Burst Mode operation by changing position of jumper JP2. For synchronizing to an external
clock source, remove jumper JP2 entirely and apply the external clock signal to the PLLIN/MODE pin. Please refer to datasheet for details on external clock signal requirements.

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Figure 3. Typical Efficiency vs. Load Current for A-A board - 24Vin, 3.3Vout and 8.5Vout


Figure 4. Typical Efficiency vs. Load Current for A-A board - 36Vin, 3.3Vout and 8.5Vout

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Figure 5. Typical Efficiency vs. Load Current for A-B board - 24Vin, 3.3Vout and 8.5Vout


Figure 6. Typical Efficiency vs. Load Current for A-B board - 36Vin, 3.3Vout and 8.5Vout




