
#### Abstract

Errata

Title \& Document Type: 8559A Spectrum Analyzer Operation and Service Manual

Manual Part Number: 08559-90013

Revision Date: January 1984

\section*{HP References in this Manual}

This manual may contain references to HP or Hewlett-Packard. Please note that HewlettPackard's former test and measurement, semiconductor products and chemical analysis businesses are now part of Agilent Technologies. We have made no changes to this manual copy. The HP XXXX referred to in this document is now the Agilent XXXX. For example, model number HP8648A is now model number Agilent 8648A.


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## Agilent Technologies

# OPERATION AND SERVICE MANUAL 

## 8559A SPECTRUM ANALYZER . $01-21 \mathrm{GHz}$



## OPERATION AND SERVICE MANUAL

## 8559A <br> SPECTRUM ANALYZER <br> 0.1 - 21 GHz

## SERIAL NUMBERS

This manual applies directly to instruments with serial numbers prefixed 2347A.

With modifications described in Section VII, this manual also applies to instruments with serial number prefixes 1909Athrough 2320A.

For additional information about serial numbers, see INSTRUMENTS COVERED BY MANUAL in Section I.

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## SAFETY SYMBOLS

The following safety symbols are used throughout this manual and in the instrument. Familiarize yourself with each of the symbols and its meaning before operating this instrument.


Instruction manual symbol. The instrument will be marked with this symbol when it is necessary for the user to refer to the instruction manual in order to protect the instrument against damage. Location of pertinent information within the manual is indicated by use of this symbol in the table of contents.


Indicates dangerous voltages are present. Be extremely careful.

The CAUTION sign denotes a hazard. It calls attention to a procedure which, if not correctly performed or adhered to, could result in damage to or destruction of the instrument. Do not proceed beyond a CAUTION sign until the indicated conditions are fully understood and met.

## WARNING

The WARNING sign denotes a hazard. It calls attention to a procedure which, if not correctly performed or adhered to, could result in injury or loss of life. Do not proceed beyond a WARNING sign until the indicated conditions are fully understood and met.

## GENERAL SAFETY CONSIDERATIONS

## WARNING

BEFORE THIS INSTRUMENT IS SWITCHED ON, make sure it has been properly grounded through the protective conductor of the ac power cable to a socket outlet provided with protective earth contact. Any interruption of the protective (grounding) conductor, inside or outside the instrument, or disconnection of the protective earth terminal can result in personal injury.

## WARNING

There are voltages at many points in the instrument which can, if contacted, cause personal injury. Be extremely careful. Any adjustments or service procedures that require operation of the instrument with protective covers removed should be performed only by trained service personnel.

## CAUTION

BEFORE THIS INSTRUMENT IS SWITCHED ON, make sure its primary power circuitry has been adapted to the voltage of the ac power source. Failure to set the ac power input to the correct voltage could cause damage to the instrument when the ac power cable is plugged in.


FIGURE 1-1. HP MODEL8559ASPECTRUM ANALYZER AND ACCESSORIES SUPPLIED

## SECTIONI GENERAL INFORMATION

## 1-1. INTRODUCTION

1-2. This Operation and Service manual contains information required to install, operate, test, adjust, and service the Hewlett-Packard 8559A Spectrum Analyzer. Figure 1-1 shows the instrument and accessories supplied. This section covers instrument identification, description, options, accessories, specifications, and other basic information.

## 1-3. DESCRIPTION

1-4. The H P 8559A displays the amplitude and frequency of each component of an input signal on a CRT. This display gives quantitative information often not available from a conventional oscilloscope. The HP 8559A is capable of measuring signals from -112 dBm to +30 dBm over a frequency range of 10 MHz to 21 GHz .

1-5. The complete measuring system includes the HP 8559A Spectrum Analyzer plugged into a compatible Hewlett-Packard display mainframe.

## 1-6. MANUAL ORGANIZATION

1-7. This manual is divided into eight sections as follows:

SECTION I, GENERAL INFORMATION; contains the instrument description and specifications, explains accessories and options, and lists recommended test equipment.

SECTION II, INSTALLATION AND OPERATION VERIFICATION; contains information concerning initial mechanical inspection, preparation for use, operating environment, packaging and shipping, and operation verification.

SECTION III, OPERATION; contains detailed operating instructions for operation of the instrument.

SECTION IV, PERFORMANCE TESTS; contains the necessary tests to verify that the electrical operation of the instrument is in accordance with published specifications.

SECTION V, ADJUSTMENTS; contains the necessary adjustment procedures to properly adjust the instrument after repair.

SECTION VI, REPLACEABLE PARTS; contains the information necessary to order parts and/or assemblies for the instrument.

SECTION VII, MANUAL BACKDATING CHANGES; contains backdating information to make this manual compatible with earlier equipment configurations.

SECTION VIII, SERVICE; contains schematic diagrams, block diagrams, component location illustrations, circuit descriptions, and troubleshooting information to aid in repair of the instrument.

1-8. On the title page of this manual, below the manual part number, is a microfiche part number. This number may be used to order 4- by 6-inch microfilm transparencies of the manual. Each microfiche contains up to 60 photo-duplicates of the manual pages. The microfiche package also includes the latest Manual Updating supplement.

## 1-9. SPECIFICATIONS

1-10. Instrument specifications are listed in Table 1-1. These specifications are the performance standards or limits against which the instrument is tested. Table 1-2 lists supplemental characteristics. Supplemental characteristics are not specifications but are typical characteristics included as additional information for the user.

## NOTE

To ensure that the HP 8559A meets the specifications listed in Table 1-1, performancetests (Section IV) should be performedevery six months.

## 1-11. SAFETY CONSIDERATIONS

1-12. Before operating this instrument, you should familiarize yourself with the safety markings on the instrument and safety instructions in this manual. This instrument has been manufactured and tested according to international safety standards. However, to ensure safe operation of the instrument and personal safety of the user and service personnel, the cautions and warnings in this manual must be followed. Refer to the summary of safety considerations at the beginning of this section. Refer also to individual sections of this manual for detailed safety notation concerning the use of the instrument as described in those individual sections.

## 1-13. INSTRUMENTS COVERED BY MANUAL

## 1-14. Serial Numbers

1-15. Attached to the rear of this instrument is a mylar serial number label. The serial number is in two parts. The first four digits and letter are the serial number prefix; the last five digits are the suffix. (Refer to Figure 1-2.) The prefix is the same for all identical instruments; it changes only when a change is made to the instrument. The suffix, however, is assigned sequentially and is different for each instrument. The contents of this manual apply to

## SERIAL NUMBER

PREFIX SUFFIX
SER 2203AO1726
OPT
$[(h p)]$ HEWLE T T•PACKARD

FIGURE 1-2. TYPICALSERIALNUMBER LABEL
instruments with the serial number prefix(es) listed under SERIAL NUMBERS on the title page.

## 1-16. Manual Updating Supplement

1-17. An instrument manufactured after the printing of this manual might have a serial number prefix that is not listed on the title page. This unlisted serial number prefix indicates the instrument is different from those described in this manual. The manual for this newer instrument is accompanied by a yellow

Manual Updating supplement. This supplement contains change information that explains how to adapt the manual to the newer instrument.

1-18. In addition to change information, the supplement may contain information for correcting errors in the manual. To keep this manual as current and accurate as possible, Hewlett-Packard recommends that you periodically request the latest Manual Updating supplement. The supplement carries a manual identification block that includes the model number, print date of the manual, and manual part number. Complimentary copies of the supplement are available from Hewlett-Packard. Addresses of Hewlett-Packard offices are located at the back of this manual.

## 1-19. Manual Backdating Changes

1-20. Instruments manufactured before the printing of this manual have been assigned serial number prefixes other than those for which this manual was written directly. Manual backdating information is provided in Section VII to adapt this manual to earlier serial number prefixes.

1-21. This information should not be confused with information contained in the yellow Manual Updating supplement, which is intended to adapt this manual to instruments manufactured after the printing of this manual.

## 1-22. ACCESSORIES SUPPLIED

1-23. A type-N male to BNC female adapter, HP Part Number 1250-0780, is supplied with the standard instrument for the use of lightweight cables with BNC connectors.

1-24. Side stop kit, H P Part Number 08558-60131, is supplied to prevent the spectrum analyzer from sliding out of the mainframe. When the side stops are installed, the plug-in cannot be removed from the mainframe. Refer to Section II for installation or removal of the side stops.

1-25. Three graticule overlays provide the operator with reference-level labels for the CRT. HP Part Number 5020-8565 is the overlay for HP 180-series display mainframes. HP Part Number 5020-8566 is the overlay for HP 181-series display mainframes. HP Part Number 5020-8567 is the overlay for HP 182 -series display mainframes. For proper installation of the graticule overlay, refer to Section II.

## SPECIFICATIONS

## FREQUENCYSPECIFICATIONS

## FREQUENCY RANGE

10 MHz to 21 GHz , covered in six pushbuttonselectable ranges:

| Frequency <br> Band | Mixing <br> Mode <br> (n) | Lowest <br> Freq(GHz) <br> [ALTIF] | Highest <br> Freq <br> $(\mathrm{GHz})$ |
| :---: | :---: | :---: | :---: |
| $.01 \mathbf{- 3}$ | $\mathbf{1 -}$ | 0.010 | 3.060 |
|  |  | $[0.025]$ |  |
| $\mathbf{6 - 9}$ | $\mathbf{1 +}$ | 6.035 | 9.060 |
|  |  | $[6.020]$ |  |
| $\mathbf{3 - 9}$ | $\mathbf{2 -}$ | 3.033 | 9.120 |
|  |  | $[3.048]$ |  |
| $\mathbf{9 - 1 5}$ | $\mathbf{2 +}$ | 9.058 | 15.120 |
|  |  | $[9.043]$ |  |
| $\mathbf{6 - 1 5}$ | $\mathbf{3 -}$ | 6.055 | 15.180 |
|  |  | $[6.070]$ | 21.000 |
| $\mathbf{1 2 . 1 - 2 1}$ | $\mathbf{3 +}$ | 12.080 | $[12.065]$ |
|  |  |  |  |
| FREQUENCYSPANS |  |  |  |

## FullSpan(F)

Entire frequency band displayed with frequency of tunable marker indicated by Frequency GHz readout.

## Per Division(MHz/Div, kHz/Div)

14 frequency scale calibrations in 1-2-5 sequence from $10 \mathrm{kHz} /$ div to $200 \mathrm{MHz} /$ div. Center frequency is set with the TUNING control and indicated by the FREQUENCY GHz readout.

## Zero Span (0)

Analyzer functions as a manually tuned receiver, at the frequency indicated by the FREQUENCY GHz readout, for time-domain display of signal modulation.

## FREQUENCYACCURACY

## Tuning Accuracy

Frequency GHz readout (center or marker frequency), after zeroing on the LO feedthrough:
$0.01-3.0 \mathrm{GHz}: \quad \pm(1 \mathrm{MHz}+0.3 \%$ of center frequency) $3.0-21.0 \mathrm{GHz}: \quad \pm(5 \mathrm{MHz}+0.2 \%$ of center frequency)

Frequency Readout Resolution 1 MHz

Frequency Span Accuracy
$\pm 5 \%$ of displayed frequency separation

## SPECTRAL RESOLUTION AND STABILITY <br> ResolutionBandwidths

Eight selectable resolution (3-dB) bandwidths in $1-3$ sequence from 1 kHz to 3 MHz . Bandwidth may be selected independently or coupled with frequency span. Optimum ratio of frequency span to resolution bandwidth is indicated by alignment of markers ( $X$ ) n the two controls.

## Resolution Bandwidth Accuracy:

Individual resolution bandwidth 3-dB points:
$< \pm 15 \%$ ( $< \pm 30 \%$ for $3-\mathrm{MHz}$ bandwidth)

## Selectivity:

$60-\mathrm{dB} / 3-\mathrm{dB}$ resolution bandwidth ratio: <15:1

## Stability

For fundamental mixing ( $\mathrm{n}=1-$ or $1+$ ):

## Residual FM:

$<2 \mathrm{kHz}$ p-p in 0.1 second'

## Noise Sidebands:

$\geq 70 \mathrm{~dB}$ down, $>30 \mathrm{kHz}$ from center of CW signal with 1 kHz resolution bandwidth and video filter at MAX (not in detent).

## Video Filter

Post-detection low-pass filter averages displayed noise for a smooth trace. The MAX (detent) position selects a video filter bandwidth of approximately 1.5 Hz for noise level measurement.

## AMPLITUDESPECIFICATIONS

## AMPLITUDERANGE

-111 dBm to +30 dBm .

[^0]TABLE 1-1. HP MODEL 8559ASPECIFICATIONS(2OF4)

## Maximum Input (without damage) Levels

 Total Power:+20 dBm (O.IW, 2.2 Vrms) with 0 dB input attenuation
+30 dBm (1W, 7.1 Vrms) with $\geq 10 \mathrm{~dB}$ input attenuation
DC: $\pm 7.1 \mathrm{~V}$
AC (<100 Hz): 7.1 Vrms
Peak Pulse Power:
$+50 \mathrm{dBm}(100 \mathrm{~W},<10 \mu \mathrm{sec}$ pulse width, $0.01 \%$ duty cycle) with input attenuation $\geq 30 \mathrm{~dB}$

## Gain Compression

$<0.5 \mathrm{~dB}$ for a -10 dBm input level with 0 dB input attenuation.

## Average Noise Level

The displayed average noise level determines sensitivity (minimum discernible signal). Signals at this input level peak approximately 3 dB above the displayed noise.
Maximum average noise level with 1 kHz resolution bandwidth, 0 dB input attenuation, and video filter at MAX (detent):

| Frequency <br> Band (GHz) | Harmonic <br> Mode | Average Noise <br> Level (dBrn) |
| :---: | :---: | :---: |
| $01-3$ | $1-$ | -111 |
| $6-9$ | $1+$ | -108 |
| $3-9$ | $2-$ | -103 |
| $9-15$ | $2+$ | -98 |
| $6-15$ | $3-$ | -93 |
| $121-18$ | $3+$ | -92 |
| $18-21$ | $3+$ | -90 |

## Calibrated Display Range Log (from Reference Level):

70 dB with $10 \mathrm{~dB} /$ DIV Amplitude Scale 8 dB with $1 \mathrm{~dB} /$ DIV Amplitude Scale
Linear:
8 divisions with LIN Amplitude Scale

## AMPLITUDE ACCURACY

With AUTO sweep time selected, amplitude accuracy is determined by one or more of the following factors, depending on the measurement technique.'

2Whenswitching to or from the Alternate IF, the REF LEVEL CAL and the FREQ CAL should be readjusted. Without readjustment, an additional reference level error of $\pm 1 \mathrm{~dB}$ and an additional frequency readout error of $\pm 1 \mathrm{MHz}$ may result.

## Calibrator Output

$-10 \mathrm{dBm} \pm 0.3 \mathrm{~dB}$ (into $50 \Omega$ )
$35 \mathrm{MHz} \pm 400 \mathrm{kHz}$

## Reference Level

$10-\mathrm{dB}$ steps and a $12-\mathrm{dB}$ vernier for calibrated Reference Level adjustment from -112 dBm to +60 dBm .'
Step Accuracy (with 0 dB input attenuation):
-10 dBm to $-80 \mathrm{dBm}: \quad \pm 0.5 \mathrm{~dB}$
-10 dB mto- $100 \mathrm{dBm}: \quad \pm 1.0 \mathrm{~dB}$
Vernier Accuracy:
$\pm 0.5 \mathrm{~dB}$

## Frequency Response

Frequency response, measured with 0 or 10 dB input attenuation, includes input attenuator flatness, mixer flatness, and band-to-band amplitude variation:

| Frequency Band GHz | Frequency Response <br> $( \pm \mathbf{d B}$ MAX.) |
| :---: | :---: |
| $01-3$ | 10 |
| $6-9$ | 10 |
| $3-9$ | 15 |
| $9-15$ | 18 |
| $6-15$ | 21 |
| $121-18$ | 23 |
| $18-21$ | 30 |

## Input Attenuator

0 dB to 70 dB of input attenuation selectable in $10-$ dB steps

## Step Accuracy:

0 dB to $60 \mathrm{~dB}, 0.01$ to 18.0 GHz : $< \pm 1.0 \mathrm{~dB}$ per $10-\mathrm{dB}$ step

## Maximum Cumulative Step Error:

0 dB to $60 \mathrm{~dB}, 0.01$ to $18.0 \mathrm{GHz}: \quad< \pm 2.4 \mathrm{~dB}$

## Bandwidth Switching (Amplitude Variation)

Bandwidths 3 MHz to $300 \mathrm{kHz}: \quad< \pm 0.5 \mathrm{~dB}$
Bandwidths 3 MHz to $1 \mathrm{kHz}:< \pm 1.0 \mathrm{~dB}$

[^1]
## Display Fidelity

CRT linearity and log or linear fidelity affect amplitude accuracy at levels other than Reference Level.
Log Incremental Accuracy:
$\pm 0.1 \mathrm{~dB}$ per dB from Reference Level
Log Maximum Cumulative Error:
$\leq \pm 1.5 \mathrm{~dB}$ over entire $70-\mathrm{dB}$ range
Linear Accuracy:
$\pm 3 \%$ of Reference Level

## RESIDUAL RESPONSES

$<-90 \mathrm{dBm}(0.01-3.06 \mathrm{GHz})^{4}$ with 0 dB input attenuation and no signal present at input.

## SWEEP SPECIFICATIONS

## SWEEP TIME

## Automatic(AUTO):

Sweep time adjusted automatically to maintain absolute amplitude calibration for any combination of frequency span, resolution bandwidth, and video filter bandwidth.

Calibrated Sweep Times (sec/Div, mSec/Div, $\mu$ Sec/Div):

20 selectable sweep times in 1-2-5 sequence from $2 \mu \mathrm{sec} / \mathrm{div}$ to $10 \mathrm{sec} /$ div (excluding $2 \mathrm{sec} /$ div), provided primarily for time-domain calibration in zero span (0).
Sweep time accuracy: $\pm 10 \%$ ( $\pm 20 \%$ for 5 and $10 \mathrm{sec} / \mathrm{div}$ )

## GENERALSPECIFICATIONS

## TEMPERATURERANGE

Operating: $0^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$
Storage: $-40^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$

## HUMIDITY RANGE

Type-tested from $50 \%$ to $95 \%$ relative humidity $\left(\leq+40^{\circ} \mathrm{C}\right)$ per requirements of MIL-STD-810C, Method 507.1, Procedure IV.

## EMI

Conducted and radiated interference is in compliance with MIL-STD 461A, Methods CEO3 and RE02, CISPR Publication 11 (1975) and Messempfaenger Postverfuegung 526/527/79 (Kennzeichnung Mit F-Nummer/Funkschutzzeichen).

## POWER REQUIREMENTS

## HP Model 853A Display with HP Model 8559A

 Spectrum Analyzer:100 or $120 \mathrm{Vac}+5 \%-10 \%$, 48 to 66 Hz , singlephase. Power consumption less than 200 Voltamperes with plug-in installed.
HP Model 182T/180TR Display with HP Model 8559A Spectrum Analyzer:

115 or $230 \mathrm{Vac} \pm 10 \%, 48-440 \mathrm{~Hz}$. Power consumption less than 200 Volt-amperes with plugin installed, convectioncooled.
HP Model 181T/181TR Display with HP Model 8559A Spectrum Analyzer:

115 or 230 Vac $\pm 10 \%, 48-440 \mathrm{~Hz}$. Power consumption less than 225 Volt-amperes with plugin installed, convection cooled.

## WEIGHT

HP Model 8559A Spectrum Analyzer:
Net: $5.5 \mathrm{~kg}(12.1 \mathrm{lbs})$
Shipping: 9.1 kg (20 lbs)
HP Model 853A Display:
Net: $\quad 15.9 \mathrm{~kg}$ ( 35 lbs )
Shipping: 18.6 kg ( 41 lbs )
HP Model 853A Option 001 Display:
Net: $\quad 14.5 \mathrm{~kg}(32 \mathrm{lbs})$
Shipping: 17.3 kg ( 38 lbs )
HP Model 182T Display:
Net: $12.5 \mathrm{~kg}(27 \mathrm{lbs})$
Shipping: $16.5 \mathrm{~kg}(36 \mathrm{lbs})$
HP Model 181T Display:
Net: $\quad 11.0 \mathrm{~kg}(24 \mathrm{lbs})$
Shipping: 15.5 kg ( 34 lbs )
HP Model 181TR Display:
Net: $\quad 12.0 \mathrm{~kg}(26 \mathrm{lbs})$
Shipping: 17.5 kg ( 38 lbs )
HP Model 180TR Display:
Net: $\quad 12.0 \mathrm{~kg}$ (26lbs)
Shipping: $\quad 17.5 \mathrm{~kg}(38 \mathrm{lbs})$

TABLE 1.1. HP MODEL8559ASPECIFICATIONS(4OF 4)
DIMENSIONS

## HP Model 8559A Spectrum Analyzer:



HP Model 853A Display:


HP Model 853A Option 001 Display:


HP Model 182T Display:


HP Model 181T Display:


HP Model 180TR/181TR Display:


## SUPPLEMENTALCHARACTERISTICS

NOTE: Values in this table are not specifications. They are typical characteristics included for user information.

## FREQUENCY CHARACTERISTICS

## FREQUENCY ACCURACY

## Frequency Cal

Adjusts digital FREQUENCY GHz readout. FREQUENCY CAL control may be used to calibrate the frequency readout on a known signal or on the 35 MHz CAL OUTPUT signal.

## FREQUENCY RANGE

Alternate IF
Regular IF approximately 3.0075 GHz . Alternate IF available at approximately 2.9925 GHz for all frequency bands (minimum frequency 25 MHz ).

## SPECTRAL RESOLUTION AND STABILITY

## Frequency Drift

(Fundamentalmixing-n=1- or 1+)
At fixed center frequency after 2-hour warmup: $< \pm 25 \mathrm{kHz} / 10$ minutes
With temperature changes: $<200 \mathrm{kHz} /{ }^{\circ} \mathrm{C}$

## Resolution Bandwidth Shape

Approximately gaussian (synchronously-tuned, 4 -pole filter).

## Spectral Resolution

The following graph shows typical spectrum analyzer resolution for different resolution bandwidths.


SIGNAL RESOLUTIONVS. FREQUENCYSEPARATION

## AMPLITUDECHARACTERISTICS

## AMPLITUDE RANGE AND ACCURACY

## Dynamic Range

Maximum power ratio of two signals simultaneously present at the input that may be measured within the limits of specified accuracy, sensitivity, and distortion (i.e., spurious responses): $>70 \mathrm{~dB}$.

Frequency Response and Average Noise Level
The following graph shows typical frequency response and average noise level versus frequency.


AVERAGENOISELEVELANDFREQUENCYRESPONSE

## Amplitude Scale Switching

Reference Level variation is typically less than $+/-1 \mathrm{~dB}$ for any change in Amplitude Scale.

## SPURIOUSRESPONSES

(with 0 dB input attenuation)
Second Harmonic Distortion

| Input Power | Relative Distortion |
| :---: | :---: |
| -40 dBm | $<-70 \mathrm{~dB}$ |

## TABLE 1-2. MODEL8559A/180-SERIES SUPPLEMENTAL CHARACTERISTICS(2OF3)

## SUPPLEMENTAL CHARACTERISTICS

NOTE: Values in this table are not specifications. They are typical characteristics included for user information.

## Third Order IntermodulationDistortion

| For Two Input Signals with |  | Relative <br> Disortion |
| :---: | :---: | :---: |
| Input Power | Signal Sep. |  |
| -30 dBm | 50 kHz | $<-70 \mathrm{~dB}$ |

## Signal Identifier

Signal identifier provided over entire frequency range and in all Frequency Span/Div settings. Correct signal response is a 1 MHz shift to the left and approximately a 6 dB lower amplitude.

## SWEEP CHARACTERISTICS

## MANUAL SWEEP

Spectrum analyzer may be swept manually, in either direction, with front panel control.

## SWEEP TRIGGER

## Free Run

End of each sweep triggers new sweep.

## Line

Sweep triggered at ac line frequency.

## Video

Sweep triggered on post-detection video waveform. One-half major division of vertical deflection required to trigger sweep.

## Single

Single sweep started or reset by turning SWEEP TRIGGER clockwise momentarily.

## FRONT PANEL INPUT AND OUTPUT CHARACTERISTICS

## SIGNAL INPUT

## Input Impedance

50 ohms nominal; Precision Type N female connector.

Input SWR<br><2.0 SWR with OdB input attenuation<br><1.3 SWR with $\geq 10 \mathrm{~dB}$ input attenuation<br>LO Emission ( 3.0 - 6.1 GHz)<br>$\leq-8 \mathrm{dBm}$ with 0 dB input attenuation

## REAR PANEL OUTPUT

CHARACTERISTICS'

## VERTICAL, PENLIFTIBLANKING, AND HORIZONTALOUTPUTS(AUX A, B, D)

These outputs are compatible with and may be used to drive HP X-Y Recorders (using positive pencoils or TTL penlift input) and CRT monitors.

## AUX A VERTICAL OUTPUT

BNC output provides detected video signal from a 50 -ohm output impedance. Typical $0-800 \mathrm{mV}$ range corresponds to full 8 -division CRT vertical deflection.

## AUX B PENLIFT/BLANKING OUTPUT

BNC output provides a +15 V penlift/blanking signal from a 10 K -ohm output impedance when CRT trace is blanked. Otherwise, output is low at OV (low impedance, 150 mA max.) for an unblanked trace.
'Rear panel outputs refer to 180T-series display mainframes and other 180-series mainframes with Option 807 installed. Horizontal, vertical, and blanking outputs, attenuated and shifted in dc level, are available on other 180 -series mainframes at the MAIN SWEEP, MAIN GATE, and DELAYED GATE outputs, respectively. DO NOT connect an X-Y recorder to the DELAYED GATE OUTPUT, or damage will result.

TABLE 1-2. MODEL 8559A1180-SERIES SUPPLEMENTALCHARACTERISTICS(30F3)

## SUPPLEMENTALCHARACTERISTICS

NOTE: Values in this table are not specifications. They are typical characteristics included for user information.

## AUX C 21.4 MHz IF OUTPUT

BNC output provides 21.4 MHz IF signal (linearly related to spectrum analyzer RF input) from a 50 -ohm output impedance. Output bandwidth controlled by spectrum analyzer RESOLUTION BW setting; output amplitude controlled by INPUT ATTEN, REFERENCE LEVEL FINE, and first six REFERENCE LEVEL positions (i.e., -10 through -60 dBm
with 0 dB input attenuation). Output level is approximately -10 dBm into 50 ohms with a signal displayed at Reference Level.

## AUX D HORIZONTALOUTPUT

BNC output provides horizontal sweep voltage from a SK-ohm output impedance. -5 V to $+\mathbf{S V}$ range corresponds to full 10-division CRT horizontal deflection.

## 1-26. EQUIPMENT REQUIRED BUT NOT SUPPLIED

## 1-27. Display Mainframe

1-28. An HP 853A digital Spectrum Analyzer Display is recommended for use with the HP 8559A. The rear panel of the HP 853A mainframe provides the following output connections: HORIZ (SWEEP), VERTICAL (VIDEO), BLANK (PENLIFT), 21.4 MHz IF, and HP-IB interface connector.

1-29. An HP 180T-series display mainframe (180TR, 181T, 181TR, or 182T) is also designed for use with the HP 8559A. In the HP 180T-series mainframe, the rear-panel auxiliary output connectors (AUX A, AUX B, AUX C, and AUX D) provide, respectively, Vertical Output, Pen Lift Output, 21.4 MHz IF Output, and Horizontal Output. A standard HP 180-series display mainframe (HP 180A/AR, HP 180C/D, HP 181A/AR, HP 182A/C, or HP 184A/B) provides only horizontal, vertical, and blanking rear panel outputs. Furthermore, these outputs are attenuated and shifted in dc level. Unbuffered rear panel outputs (similar to the HP 180Tseries) are provided only if Option 807 is installed.

### 1.30. Extender Cable Assembly

1-31. An Extender Cable Assembly (Figure 1-3), HP Part Number 5060-0303, allows operation of the HP 8559A outside the display mainframe. This provides access to the HP 8559A for necessary adjustments and some performance tests. This cable is also useful for troubleshooting.

## 1-32. EQUIPMENT AND ACCESSORIES AVAILABLE

## 1-33. Input Limiter



FIGURE 1.3. HP 11683A LIMITER

1-34. The HP 11693A Limiter can be used with the HP 8559A to prevent input mixer damage due to inadvertent application of strong signals. Frequency
response flatness is degraded by less than $\pm 0.5 \mathrm{~dB}$ from 100 MHz to 12.4 GHz ; the limiter is usable from 10 MHz to 18 GHz . Input levels of 1 watt average or 75 watts peak can be tolerated.

### 1.35. Low Pass Filter



FIGURE 1-4. HP 11870A LOW PASS FILTER
1-36. The HP 11870A Low Pass Filter (dc-2.6 GHz ) can be used with the HP 8559A to reject signals above 3 GHz by more than $\mathbf{6 0} \mathrm{dB}$ for image-free measurements over the 10 MHz to 2.6 GHz range.

## 1-37. Modification Kit (Option 807 Connections)

1-38. A modification kit, HP Part Number 0018069503 , provides the materials and information necessary to install unbuffered rear panel connections (formerly included in Option 807) in the following display mainframes: HP 180A/AR, HP 180C/D, HP 181A/AR, HP 182A/C, and HP 184A/B. Refer to Table 1-3 for a description of parts included in the modification kit.

## 1-39. Oscilloscope Camera



FIGURE 1-5. HP 197B Opt 002,006 OSCILLOSCOPECAMERA

1-40. The HP 197B, Option 002, General Purpose Camera can be used with HP 180- and HP 181-series display mainframes to make a permanent record of measurements. The HP 10367A adapter allows the camera to be used with HP 182-series mainframes.

TABLE 1-3. PARTSINCLUDEDIN MODIFICATION KIT 00180-69503

| Quantity | Description | HP Part Number |
| :---: | :--- | :---: |
| 1 | Output Amplifier Assembly (Auxiliary Output Board) | $00180-66551$ |
| 1 | Label | $7120-3116$ |
| 2 | $3 / 4$ inch pieces of shrink tubing | $0890-0720$ |
| 1 | Service Note | $180 \mathrm{~A} / \mathrm{AR}-10,180 \mathrm{C} / \mathrm{D}-2,181 \mathrm{~A} / \mathrm{AR} 8$, <br> similar for all instruments listed) |

## 1-41. SERVICE ACCESSORIES

1-42. Service accessories are shown in Figure 1-6.
1-43. RECOMMENDEDTEST EQUIPMENT

1-44. Table 1-4 lists all of the equipment required for testing, adjusting and troubleshooting the Hewlett-Packard Model 8559A Spectrum Analyzer. Other equipment may be substituted if it meets or exceeds the critical specifications listed in the table.


FIGURE 16. SERVICEACCESSORIES(10F 2)


TABLE1-4. RECOMMENDEDTESTEQUIPMENT (1OF 4)

| Instrument | Critical Specifications | Recommended Model | Use* |
| :---: | :---: | :---: | :---: |
| Display Mainframe | HP 180 Series with Variable Persistence | HP 181 T/TR | P, A, T |
| Sweep Oscillator | Mainframe for RF Plug-Ins below. <br> External Sweep <br> Adjustable Sweep range (Marker Sweep) | HP 8620C | P, A |
| R F Plug-In | Compatible with mainframe above. <br> Output Frequency: 0.01 to 2.4 GHz <br> Output Amplitude: 0 to +10 dBm adjustable <br> FM and Phase Lock <br> Internal and External leveling <br> (both crystal detector and power meter) | HP 86222A/B | P, A |
| RF Plug-In | Compatible with mainframe above. <br> Output Frequency: 2 to 21 GHz <br> Output Amplitude: <br> Band 1,0 to +10 dBm adjustable <br> Band 2,0 to +10 dBm adjustable <br> Band 3, 0 to +3 dBm adjustable <br> Band 4,0 to +3 dBm adjustable <br> FM and Phase Lock <br> Internal and External leveling <br> (both crystal detector and power meter) | HP 86290B-H08 ${ }^{1}$ | P, A |
| Signal Generator | Output Frequency: 21.4 MHz and 321.4 MHz <br> Output Amplitude: -40 to 0 dBm adjustable | HP 8640B | P, A, T |
| Function Generator | Output Frequency: 1 Hz to 1 MHz adjustable Output Amplitude: 0 to 15 V p-p adjustable Triangle-Wave Output | HP 3310A | P, A |
| Comb Generator | 1 MHz comb teeth to 3 GHz 100 MHz comb teeth to 21 GHz | HP 8406A | P, A |
| Spectrum Analyzer | Frequency Range: 20 MHz to 6 GHz <br> Maximum Input Level: $\geqslant 0 \mathrm{dBm}$ <br> Amplitude Scale: Log $10 \mathrm{~dB} /$ DIV and $1 \mathrm{~dB} /$ DIV <br> Minimum Resolution Bandwidth: $\leqslant 300 \mathrm{kHz}$ <br> Adjustable Reference Level | HP 8569B | A, T |
| Synchronizer | Input Frequency: 21.4 MHz <br> Sensitivity: $6 \mathrm{MHz} /$ Volt <br> Error Voltage Output Polarity: <br> + and - Selectable | HP $8709 \mathrm{~A} \cdot \mathrm{H} 10^{2}$ | A |
| * $\mathrm{P}=$ Performance Test; $\mathrm{A}=$ Adjustments; $\mathrm{T}=$ Troubleshooting <br> ${ }^{1}$ Option H08 extends the frequency range of the standard HP 86290 B from 18.6 GHz to 22 GHz . A standard ( 18.6 GHz ) may be used if Option $\mathrm{H} 08(22 \mathrm{GHz}$ ) is not available. <br> ${ }^{2}$ Option H 10 changes input frequency to 21.4 MHz and adds error voltage output polarity selection capability. |  |  |  |

TABLE 1-4. RECOMMENDEDTESTEQUIPMENT (2OF 4)

| instrument | Critical Specifications | Recommended Model | Use" |
| :---: | :---: | :---: | :---: |
| Oscilloscope | Frequency: 500 Hz <br> Display Amplitude: -15 Vdc <br> Single-Channel | HP 1740A | A, T |
| Frequency Counter | Frequency Range: 20 MHz to 23 GHz <br> Sensitivity: -15 dBm <br> Resolution: 0.1 MHz | HP 5342A-005 | P, A, T |
| Universal Counter | Time Interval Measurement from 1 ms to 500 ms | HP 5300B/5302A | P, A |
| Digital Voltmeter | Range: -12 to +15 Vdc Accuracy: $\pm 1 \mathrm{mV}$ | HP 3456A | P, A, T |
| Power Meter | Range: -20 to +10 dBm Resolution: 0.1 dB | HP 435A/B | P, A |
| Power Sensor | $\begin{aligned} & \text { Frequency Range: } 50 \mathrm{MHz} \text { to } 26.5 \mathrm{GHz} \\ & \text { Maximum SWR: } \\ & 1.15,50 \mathrm{MHz} \text { to } 100 \mathrm{MHz} \\ & 1.10,100 \mathrm{MHz} \text { to } 2 \mathrm{GHz} \\ & 1.15,2 \text { to } 12.4 \mathrm{GHz} \\ & 1.20,12.4 \text { to } 18 \mathrm{GHz} \\ & 1.25,18 \text { to } 26.5 \mathrm{GHz} \end{aligned}$ | HP 8485A | $\mathrm{P}, \mathrm{A}$ |
| Power Sensor | Frequency Range: 10 MHz to 18 GHz Maximum SWR: $\begin{aligned} & \text { 1.40, } 10 \mathrm{MHz} \text { to } 30 \mathrm{MHz} \\ & 1.18,30 \mathrm{MHz} \text { to } 50 \mathrm{MHz} \\ & 1.10,50 \mathrm{MHz} \text { to } 2 \mathrm{GHz} \\ & 1.18,2 \text { to } 12.4 \mathrm{GHz} \\ & 1.28,12.4 \text { to } 18 \mathrm{GHz} \end{aligned}$ | HP 8481A | $\mathrm{P}, \mathrm{A}$ |
| Power Splitter | Frequency Range: 10 MHz to 18 GHz <br> Tracking between output arms: $\leqslant 0.25 \mathrm{~dB}$ Connectors: <br> Type $N(f)$ input, Type $N(m)$ outputs | HP 11667A-C16 ${ }^{3}$ | P, A |
| Step Attenuator | Frequency Range: 20 MHz to 350 MHz <br> Attenuation Range: 0 to 90 dB in 10 dB steps <br> Step Accuracy: kO.1 dB <br> Overall Accuracy ( 0 to 90 dB ): $\pm 0.2 \mathrm{~dB}$ | HP 355D-H82 ${ }^{4}$ | $\mathrm{P}, \mathrm{A}$ |
| Step Attenuator | Frequency Range: 20 MHz to 350 MHz <br> Attenuation Range: 0 to 12 dB in 1 dB steps <br> Step Accuracy: k0.05 dB <br> Overall Accuracy ( 0 to 12 dB ): kO.l dB | HP 355C-H80 ${ }^{5}$ | P, A |
| ${ }^{*} \mathrm{P}=$ Performance Test; $\mathrm{A}=$ Adjustments; $\mathrm{T}=$ Troubleshooting <br> ${ }^{3}$ Option C16 provides Type $\mathrm{N}(\mathrm{m})$ output connectors to eliminate the use of adapters. <br> ${ }^{4}$ Option H82 is selected for best attenuation accuracy and provides calibration data at 30 MHz and 280 MHz . <br> ${ }^{5}$ Option H 80 is selected for best attenuation accuracy and provides calibration data at 100 MHz . |  |  |  |

TABLE 1-4. RECOMMENDED TEST EQUIPMENT (3OF 4)

| Instrument | Critical Specifications | $\begin{aligned} & \text { Recommended } \\ & \text { Model } \end{aligned}$ | Use* |
| :---: | :---: | :---: | :---: |
| Fixed Attenuator (2 required) | Frequency Range: 10 MHz to 18 GHz Attenuation: $20 \mathrm{~dB} \pm 1.0 \mathrm{~dB}$ Connectors: Type $\mathrm{N}(\mathrm{m})(f)$ | $\begin{aligned} & \text { HP 8491B } \\ & \text { Option } 020^{6} \end{aligned}$ | P, A |
| Fixed Attenuator | Frequency Range: 10 MHz to 18 GHz Attenuation: $10 \mathrm{~dB} \pm 0.5 \mathrm{~dB}$ Connectors: Type $\mathrm{N}(\mathrm{m})$ (f) | HP 8491B <br> Option $010^{6}$ | P, A |
| Crystal Detector | Frequency Range: 10 MHz to 21 GHz <br> Frequency Response: $\pm 0.6 \mathrm{~dB}, .01$ to 18 GHz <br> Maximum SWR: $\leqslant 1.5, .01$ to 18 GHz <br> Output Polarity: Negative <br> Connectors: <br> APC - 3.5 (SMR) (m) input, SMC (m) output | HP 33330C | P, A |
| Termination | Frequency Range: 10 MHz to 18 GHz Impedance: 5052 <br> Connector: Type N(m) | $\begin{aligned} & \text { HP 909A } \\ & \text { Option } 012^{7} \end{aligned}$ | P |
| Tuning Voltage Circuit | Refer to Figure 5-17 | None | A |
| Crystal Bypass Networks | Refer to Figure 5-6 | None | A |
| Special Extender Board | Refer to Figure 5-9 | None | A |
| Extender Cable | Extends Spectrum Analyzer Plug-In for Servicing Refer to Figure 1-3. | HP 5060-0303 | P, A, T |
| Cable | Frequency Range: 10 MHz to 21 GHz <br> Maximum SWR: $\leqslant 1.4$ at 21 GHz <br> Length: 61 cm (24 inches) <br> Connectors: SMA ( m ) both ends | HP 8120-1578 | P, A |
| Cable | BNC (m) to SMC (f), 36 inches long | HP 11592-60001 | P, A |
| Cable | 48 inch, $50 \Omega$ coaxial cable with BNC (m) connectors on both ends (3 required) | HP 10503A | P, A, T |
| Cable | RG-214/U with Type N connectors (2 required) | HP 11500A | P, A |
| Cable | BNC (m) to Banana Plug | HP 10111A | P, A, T |
| Test Cable | Connectors: BNC (m) to SMB (f) Length: $\geqslant 61 \mathrm{~cm}$ (24 inches) | HP 85680-60093 | A, T |
| * $\mathrm{P}=$ Performance Test; A = Adjustments; $\mathrm{T}=$ Troubleshooting <br> ${ }^{6}$ Option number specifies attenuation value. <br> ${ }^{7}$ Option 012 provides type N male connector. |  |  |  |

TABLE1-4. RECOMMENDEDTESTEQUIPMENT(4OF 4)

| Instrument | Critical Specifications | Recommended Model | Use* |
| :---: | :---: | :---: | :---: |
| Adapter | Type $\mathrm{N}(\mathrm{m})$ to BNC (f) (2 required) | HP 1250-0780 | P, A, T |
| Adapter | Type $\mathrm{N}(\mathrm{m})$ to SMA (f) (2 required) | HP 1250-1250 | P, A |
| Adapter | Type N (f) to SMA (f) (2 required) | HP 1250-1745 | P, A |
| Adapter | Type $\mathrm{N}(\mathrm{f})$ to Type N (f) (2 required) | HP 1250-1472 | P, A |
| Adapter | Type N(f) to BNC (m) | HP 1250-1477 | P |
| Adapter | BNC (f) to SMC (m) | HP 1250-0832 | A |
| Adapter | BNC (f) to BNC (f) | HP 1250-0080 | P |
| Adapter | BNC (f) to alligator clips (2 required) | HP 8120-1292 | A, T |
| Adapter | BNC (f) to SMB (f) | HP 1250-1236 | P |
| Adapter | SMB (m) to SMB (m) | HP 1250-0669 | A |
| Adapter | SMB (f) to SMB (f) | HP 1250-0672 | A |
| Adapter | SMC (m) to SMC (m) | HP 1250-0827 | A |
| Adapter | BNC Tee | HP 1250-0781 | P, A |
| Tuning Tool | Allen Driver inserted through drilled-out 5/16" nut driver | HP 08555-60107 | A |

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## SECTION II INSTALLATION AND OPERATION VERIFICATION

### 2.1. INTRODUCTION

2-2. This section includes information on initial inspection, preparation for use, and storage and shipping requirements for the HP 8559A.

## 2-3. INITIAL INSPECTION

2-4. Inspect the shipping container for damage. If the shipping container or cushioning material is damaged, it should be kept until the contents of the shipment have been checked for completeness and the instrument has been checked mechanically and electrically. The contents of the shipment should be as shown in Figure 1-1. The electrical performance is checked by the Operation Verification procedure in this section. If the contents are incomplete, or if the instrument does not pass Operation Verification tests, notify the nearest Hewlett-Packard office. If the shipping container is damaged, or the cushioning material shows signs of stress, notify the carrier as well as the Hewlett-Packard office. Keep the shipping materials for carrier's inspection. The HP office will arrange for repair or replacement without waiting for claim settlement.

## 2-5. PREPARATIONFOR USE

## 2-6. Installation

2-7. When properly installed, the spectrum analyzer obtains all necessary power from the display mainframe. The rear panel connector provides the interface.

## CAUTION

BEFORE SWITCHING ON THIS INSTRUMENT, make sure it is adapted to the voltage of the ac power source to be used and the proper fuse is installed. Failure to set the ac power input of the instrument for the correct voltage level could cause damage to the instrument when plugged in. Refer to the display mainframe Operation and Service Manual for line voltage and fuse selection.

2-8. To install the spectrum analyzer in the mainframe:
a. Set display mainframe LINE switch to OFF.
b. Pull out lock knob and slide plug-in toward rear of compartment until it is seated firmly in place.
c. Push in lock knob to secure spectrum analyzer in mainframe.

## 2-9. Side Stop Kits

2-10. Side stops unique to the installation of this instrument into the HP 853A Spectrum Analyzer Display are included with the HP 853A. Refer to the HP 853A Operation and Service Manual for further information.

2-11. Installation of a Side Stop Kit, HP Part Number 08558-60131, prevents the removal of the analyzer from the HP 180-series mainframe without the use of hand tools. This kit contains two side stops, mounting hardware, label, and installation instructions. (Refer to Table 2-1 for part numbers of individual items.)

TABLE 2-1. SIDE STOPKIT (08558-60131)

| Quantity | Description | HP Part <br> Number | C <br> D |
| :---: | :--- | :---: | :--- |
| 2 | SIDE STOP | $08558-00094$ | 7 |
| 4 | MACHINE SCREW, | $2200-0168$ | 9 |
| 1 | 4-40, .438 IN-LG |  |  |
| 1 | 82 DEG FLATHEAD |  |  |
| 1 | LABEL, FRONT-PANEL | $7120-8131$ | 7 |
| LABEL, INSTRUCTIONS | $7120-8215$ | 8 |  |

## 2-12. To install side stops:

## WARNING

Before removing covers from display mainframe, disconnect line power by removing ac power cord.

1. Remove side covers from bottom section of mainframe. (Remove only right side cover if mainframe is a rack-mounted model.)
2. Use flathead machine screws to install side stops as shown in Figure 2-1.
3. Reinstall side covers on mainframe.
4. Place label on front panel of spectrum analyzer (upper right-hand corner) to indicate that the plug-in is secured with side stops.

2-13. To remove side stops:
WARNING
Before removing covers from display mainframe, disconnect line power by removing ac power cord.

1. Remove side covers from bottom section of mainframe. (Remove only right side cover if mainframe is a rack-mounted model.)
2. Remove side stops. See Figure 2-1.
3. Reinstall side covers on display mainframe.


* ONLY ONE SIDE STOP AND TWO SCREWS ARE USED FOR RACKMOUNT MODELS


## 2-14. GraticuleOverlays

## 2-15. To install a graticule overlay:

1 Select proper overlay. HP Part Number 50208565 is for HP 180TR display mainframes, HP Part Number 5020-8566 is for HP 181T/TR display mainframes, and HP Part Number 5020-8567 is for HP 182 T display mainframes.
2. For HP 180TR and HP 181T/TR mainframes, remove CRT bezel and metallic-mesh contrast filter. Insert proper overlay and replace contrast filter and CRT bezel.
3. For HP 182T mainframes, grasp top portion of CRT bezel and pull straight up. Remove metal-lic-mesh contrast filter and insert proper overlay and contrast filter. (Either the metallic-mesh contrast filter or a light blue contrast filter may be used.)
4. Slide bezel back into place to retain overlay and filter.

2-16. When the HP 8559A is properly installed in the display mainframe, the interconnections are as listed in Table 2-2.

## 2-17. Operating Environment

2-18. Temperature. This instrument has been type tested for 95 percent relative humidity at $40^{\circ} \mathrm{C}$ for five days. The operating environment should be within the following limits:

Temperature ......................... 0 to $55^{\circ} \mathrm{C}$ Altitude . . ....... $<4572$ meters ( 15,000 feet)

## 2-19. Modifications

2-20. A Modification Kit, HP Part Number 0018069503, provides materials and information necessary to add Option 807 rear-panel connections to the standard HP 180-series display. Refer to Table 1-3 in Section I. Option 807 is factory-installed in HP 180TR, HP 181T, HP 181TR, and HP 182 T mainframes. The modification kit is required for use with other mainframes if all four rear-panel outputs are needed.

TABLE2-2. HP MODEL 8559A MAINFRAME INTERCONNECTIONS

| Pin on P1 | Signal or Voltage | Pin on P1 | Signal or Voltage |
| :---: | :---: | :---: | :---: |
| 1 | CRT HORIZ (adjusted horizontal signal) | $\begin{aligned} & 17 \\ & 18 \end{aligned}$ | BLANKING <br> NC |
| 2 | GROUND from mainframe (jumpered to pin 8) | 19 | GROUND from mainframe (jumpered to pin 24) |
| 3 | NC | 20 | AUTO SWP |
| 4 | L NORM | 21 | BEAM FINDER |
| 5 | Y NORM | 22 | NC |
| 6 | NC | 23 | NC |
| 7 | SING SWP | 24 | GROUND from mainframe |
| 8 | GROUND from mainframe (jumpered to pin 2) | 25 | (jumpered to pin 19) NC |
| 9 | MAN SWP | 26 | NC |
| 10 | NC | 27 | NC |
| 11 | AUX D Horizontal Output (to mainframe rear panel) | $\begin{aligned} & 28 \\ & 29 \end{aligned}$ | -12.6 VDC from mainframe <br> +15 VDC from mainframe |
| 12 | AUX C 21.4 MHz IF Output (to mainframe rear panel) | $30$ | +100 VDC from mainframe 30 V p-p from mainframe |
| 13 | AUX B Penlift/Blanking Output (to mainframe rear panel) | 32 | (for LINE TRIGGER) NC |
| 14 | AUX A Vertical Output (to mainframe rear panel) | $\begin{gathered} \text { W5 } \\ (2 \text { contacts }) \end{gathered}$ | +VERT (top contact, yellow wire) |
| $\begin{aligned} & 15 \\ & 16 \end{aligned}$ | $\begin{aligned} & \text { GROUND } \end{aligned}$ |  | - VERT (bottom contact, orange wire) |

## 2-21. STORAGE AND SHIPMENT

## 2-22. Environment

2-23. The instrument may be stored or shipped in environments within the following limits:

Temperature: $\quad-40^{\circ} \mathrm{C}$ to $+75^{\circ} \mathrm{C}$
Altitude: $<7620$ meters $(25,000$ feet $)$
The instrument should also be protected from temperature extremes which cause condensation within the instrument.

## 2-24. Packaging

2-25. Original Packaging. Containers and materials identical to those used in factory packaging are available through Hewlett-Packard offices. If the instrument is being returned to Hewlett-Packard for servicing, attach a tag indicating the type of service required, return address, model number, and full serial number. A supply of these tags is provided at the end of this section. Also mark the container FRAGILE to assure careful handling. In any correspondence, refer to the instrument by model number and full serial number.

2-26. Other Packaging. The following general instructions should be used for repackaging with commercially available materials:

1. Wrap the instrument in heavy paper or plastic. If shipping to a Hewlett-Packard office or service center, attach a tag indicating the type of service required, return address, model number, and full serial number. A supply of these tags is provided at the end of this section.
2. Use a strong shipping container. A double-wall carton made of 350 -pound test material is adequate.
3. Use enough shock-absorbing material (3-inch to 4-inch layer) around all sides of the instrument to provide firm cushion and prevent movement inside the container. Protect the control panel with cardboard.
4. Seal the shipping container securely.
5. Mark the shipping container FRAGILE to assure careful handling.

## 2-27. OPERATION VERIFICATION

2-28. The Operation Verification tests only the most critical specifications and operating features of the instrument. It requires much less time and equipment than the complete performance tests provided in Section IV, and is recommended for verification of overall instrument operation, either as part of incoming inspection or after repair. Operation Verification consists of the following performance tests:

- Paragraph 4-11, Frequency Span Accuracy
- Paragraph 4-17, Average Noise Level
- Paragraph 4-21, Bandwidth Switching (Amplitude Variation)
- Paragraph 4-22, Input Attenuator Accuracy
- Paragraph 4-25, Calibrator Accuracy
- Paragraph 4-26, Display Fidelity


FIGURE2.2. PACKAGINGFORSHIPMENTUSING FACTORYPACKAGINGMATERIALS

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## SECTION III OPERATION

## 3-1. INTRODUCTION

3-2. This section provides operating information for the HP 8559A Spectrum Analyzer plug-in. It also provides a brief description of display mainframe controls. For a detailed description of the display mainframe, refer to its manual.

3-3. The HP 8559A Spectrum Analyzer plug-in can be used with either the 180 -series display mainframes or the HP 853A Spectrum Analyzer Display mainframe.

## 3-4. DESCRIPTION

## 3-5. HP 8559A Spectrum Analyzer

3-6. The HP 8559A employs harmonic mixing to cover a measurement range of 10 MHz to 21 GHz in six frequency bands. It can display frequency spans as narrow as 100 kHz , and as wide as 9 GHz (the latter in full span mode). A five-digit LED readout indicates the spectrum analyzer center frequency with a resolution of 1 MHz . The HP 8559A can be used to measure signals over an amplitude range of -111 dBm to +30 dBm .

## 3-7. HP 853A Spectrum Analyzer Display

3-8. The HP 853A Spectrum Analyzer Display is a large-screen, digital storage display mainframe for use exclusively with the HP 8559A, 8558B, and 8557A Spectrum Analyzer plug-ins. Digital memory provides buffer storage for two independent traces, both of which can be displayed or blanked as desired. Digital processing also provides push-button features such as maximum signal hold, digital averaging, and trace normalization. A conventional ana$\log$ display mode can also be selected.

## 3-9. HP.IB

3-10. The HP 853A has limited HP-IB capabilities. CRT trace and graticule data is dumped directly to a listen-only HP-IB plotter by pressing two front-panel push buttons. Control settings on the spectrum analyzer plug-in cannot be monitored via the HP-IB;
however, all digital display functions are programmable via a controller, and two lines of annotation can be displayed on the CRT for labelling purposes or operator prompting. In addition, controller commands allow transfer of trace data for analysis or storage.

## 3-11. CONTROLS, INDICATORS, AND CONNECTORS

## 3-12. Control Grouping

3-13. The Spectrum Analyzer plug-in and Display mainframe front-panel controls fall into three general groups: those that deal with the display, those that deal with frequency, and those that deal with amplitude. These controls are shown in Figure 3-1 and accompanied by detailed explanations of their use.

3-14. Display. The display group consists of:
SWEEP TIME/DIV
SWEEP TRIGGER
VERT POSN

VERT GAIN
MANUALSWEEP
HORIZ GAIN (rear
panel of HP 8559A)

VIDEO FILTER
BASELINE CLIPPER HORIZONTAL POSITION INTENSITY FOCUS TRACE ALIGN

3-15. The display group enables the operator to calibrate the display and to select a variety of scan and display conditions. However, when the SWEEP TIME/DIV Control is placed in the AUTO position, sweep time is controlled by the RESOLUTION BW, FREQ SPAN/DIV, and VIDEO FILTER controls.

3-16. Frequency. The frequency group consists of:

TUNING
FREQUENCYBAND GHz
ALT IF
SIG IDENT
RESOLUTIONBW
FREQ SPAN/DIV

3-17. The frequency group enables the operator to control how the Spectrum Analyzer displays the frequency domain. The RESOLUTION BW and FREQ SPAN/DIV controls, when pushed in, are coupled together, and moving either control moves the other. When the SWEEP TIME/DIV control is in the AUTO position, varying the RESOLUTION BW or the FREQ SPAN/DIV (coupled or uncoupled) will change the sweep time to maintain calibration. With the two controls coupled together in the optimum position, RESOLUTION BW's of 3 MHz to 1 kHz will be automatically selected as the FREQ SPAN/ DIV is narrowed from F (Full) to 0 (Zero). TUNING controls coarse and fine (coarse is larger knob) set the center frequency of the displayed spectrum. RESOLUTION BW control determines the resolution of the signals on the CRT.

3-18. Amplitude. The amplitude group consists of:

## REFERENCE LEVEL dBm <br> INPUT ATTEN <br> REF LEVEL FINE <br> REF LEVEL CAL <br> $10 \mathrm{~dB} /$ DIV - $1 \mathrm{~dB} /$ DIV - LIN (Amplitude Scale)

3-19. The amplitude group enables the operator to measure signal amplitude in units of either voltage or dBm .

## 3-20. OPERATING PRECAUTIONS

## 3-21. Signal Input

3-22. The HP 8559A Spectrum Analyzer plug-in is a sensitive measuring instrument. Overloading the input with too much power, peak voltage, or dc voltage will permanertly damage the input circuits. Do not exceed the input levels specified below:

## Maximum Input (Damage) Levels

## HP 8559A

Total Power:
$+20 \mathrm{dBm}(0.1 \mathrm{~W}, 2.2 \mathrm{Vrms})$ with 0 dB input attenuation
$+30 \mathrm{dBm}(1 \mathrm{~W}, 7.1 \mathrm{Vrms})$ with $\geq 10 \mathrm{~dB}$ input attenuation
dc or ac ( $<100 \mathrm{~Hz}$ ): $\quad \pm 7.1 \mathrm{~V}$
Peak Pulse Power: $\quad+50 \mathrm{dBm}(100 \mathrm{~W},>10 \mu \mathrm{sec}$ pulse width, $0.01 \%$ duty cycle) with $\geq 30 \mathrm{~dB}$ input attenuation

## NOTE

When you are measuring input signals of unknown power levels, a preliminary instrument setting of $\geq 30$ dB INPUT ATTEN is recommended.

## CAUTION

Although the spectrum analyzer's reference level can be set for power levels up to +60 dBm , the total input power must not exceed the absolute maximum limits listed above.

## 3-23. Line Power On

3-24. Before connecting the line power cord, make sure the proper line voltage and line fuse have been selected for the display mainframe. Failure to set the ac power input selector on the display mainframe to correspond with the level of the ac source voltage could cause damage to the instrument when the power cord is plugged in.

## WARNING

> The spectrum analyzer and any device connected to it must be connected to power line ground. Failure to ensure proper grounding could result in a shock hazard to personnel or damage to the instrument.

3-25. LINE power is switched at the display mainframe front panel. A safety indicator lights when the ac power is on. NEVER remove a spectrum analyzer plug-in from the display mainframe without first switching the ac LINE power switch to OFF.

3-26. For optimum performance, you should allow the spectrum analyzer to warm up for at least 30 minutes before using it to make measurements.

## 3-27. FRONT-PANEL ADJUSTMENT PROCEDURE

3-28. The front-panel adjustment procedure adapts the HP 8559A Spectrum Analyzer plug-in to a particular display mainframe, and should be performed daily after instrument warm-up. The step-by-step adjustment is also an excellent way for new users to become acquainted with the various spectrum analyzer controls. Once the procedure is completed, the
spectrum analyzer is calibrated for absolute amplitude and frequency measurements. Set the controls as shown in Table 1 before you start the adjustment procedure.

TABLE 1. ADJUSTMENTSETTINGS

| Function | Setting |
| :---: | :---: |
| Spectrum Analyzer Plug-In <br> INPUT ATTEN (dB)* REFERENCE LEVEL Option 002 <br> REF LEVEL FINE <br> Amplitude Scale FREQ SPAN/DIV RESOLUTION BW SWEEP TIME/DIV SWEEP TRIGGER START-CENTER (8558B, 8557A) <br> FREQUENCY BAND GHz (8559A) <br> TUNING <br> BASELINE CLIPPER VIDEO FILTER <br> *On older plug-ins, set OPTIMUM INPUT to $-\mathbf{3 0} \mathrm{dBm}$. | 10 dB 0 dBm +50 dBmV 0 dBm LIN $\mathbf{1 0 ~ M H z}$ (uncoupled) 1 MHz (uncoupled) AUTO FREE RUN CENTER $.01-3$ $>\mathbf{8 0 ~ M H z}$ OFF OFF |
| HP 853A Spectrum Analyzer Display <br> TRACE A <br> TRACE B <br> DGTL AVG <br> INPUT-B $\rightarrow \mathrm{A}$ | WRITE STORE BLANK OFF OFF |
| HP 180-Series Display Mainframe <br> DISPLAY <br> MAGNIFIER <br> SCALE (180TR, 182T) <br> PERSISTENCE(181T/TR) <br> Display Mode (181T/TR) | $\begin{gathered} \text { INT } \\ \text { X1 } \\ \text { OFF } \\ \text { MIN } \\ \text { WRITE } \end{gathered}$ |

3-29. Display Adjustments-HP 853A Spectrum Analyzer Display

1. Switch LINE power OFF then ON while holding PLOT GRAT push button depressed to activate the digital test routines. The "\#0" that appears on the left side of the CRT means digital test routine \#0 is now activated.
2. Press and release the PLOT GRAT push button four times to step to digital test routine \#4, as indicated by the "\#4" displayed on the left side of the CRT.
3. With an adjustment tool, adjust the FOCUS control as necessary to make the characters on the CRT as clear as possible.
4. Adjust the X POSN and Y POSN controls the align the square trace pattern with the outermost CRT graticule lines.
5. Momentarily press the PLOT GRAT and PLOT TRACE push buttons simultaneously to exit the digital test routines.

## 3-30. Display Adjustments - HP 180-Series Display Mainframe

1. With an adjustment tool, adjust the VERTICAL POSN control to place the CRT trace on a horizontal graticule line near the CRT center.
2. Reduce the INTENSITY and set the SWEEP TIME/DIV control to MAN. Use the MAN SWEEP knob to center the CRT dot.

## CAUTION

Leaving a dot on the CRT for prolonged periods at high intensity can burn the phosphor.
3. Adjust FOCUS and ASTIG controls for the smallest round dot possible.
4. Reset the SWEEP TIME/DIV control to AUTO and increase the INTENSITY for an optimum CRT trace. Adjust the HORIZONTAL POSITION control to center the CRT trace. If the horizontal deflection is not exactly 10 divisions, adjust the HORIZ GAIN control located on the rear panel of the spectrum analyzer plug-in.

## NOTE

To adjust the HORIZ GAIN, you must switch the LINE power OFF, then remove the spectrum analyzer plug-in from the mainframe.
5. Adjust TRACE ALIGN so that the CRT trace is parallel to the horizontal graticule line.

## 3-31. Frequency and Amplitude Adjustments

1. Adjust VERTICAL POSN to align the CRT trace with the bottom graticule line.
2. Center the LO feedthrough (i.e., the "signal" at 0 MHz ) on the CRT with the TUNING control.
3. Narrow the FREQ SPAN/DIV to 200 kHz . Adjust the REF LEVEL FINE control as necessary to position the signal peak near the top CRT graticule line.
4. Center the LO feedthrough again, if necessary, and adjust the FREQ ZERO to calibrate the FREQUENCY MHz readout at 00.0 MHz .
5. Set the FREQ SPAN/DIV control to 1 MHz and the REF LEVEL FINE control to 0. Adjust the TUNING control for a FREQUENCY MHz readout of approximately 250 MHz .
6. Press the 10 dB /DIV Amplitude Scale push button, and set the REFERENCE LEVEL control to $-20 \mathrm{dBm}(+30 \mathrm{dBmV}$ for Option 002 instruments).
7. Connect the 250 MHz CAL OUTPUT to the spectrum analyzer input, and center the signal on the CRT with the TUNING control. The FREQUENCY MHz readout will indicate 250 $\mathrm{MHz} \pm 3 \mathrm{MHz}$.
8. Press the LIN Amplitude Scale push button. Adjust the REF LEVEL FINE control to place the signal peak at the top CRT graticule line.
9. Press the $10 \mathrm{~dB} /$ DIV Amplitude Scale push button. Adjust VERTICAL GAIN to place the signal peak at the top CRT graticule line.
10. Repeat steps 8 and 9 until the signal peak remains at the top CRT graticule line when the Amplitude Scale is alternated between $10 \mathrm{~dB} /$ DIV and LIN.
11. Set the REF LEVEL FINE control to 0, and the REFERENCE LEVEL control to -30 dBm ( +20 dBmV for Option 002 instruments).
12. Press the LIN Amplitude Scale push button, and adjust REF LEVEL CAL to place the signal peak at the top CRT graticule line.


## SECTIONIV PERFORMANCE TESTS

## 4-1. INTRODUCTION

4-2. The procedures in this section test the electrical performance of the instrument using the specifications in Section I as the performance standards. The performance tests included in this section are listed in Table 4-1. Most of the tests can be performed without access to the interior of the instrument. If a test measurement is marginal, perform the appropriate adjustment procedures in Section V.

TABLE 4-1. PERFORMANCETESTS

| Paragraph | Test |
| :---: | :--- |
| $4-11$ | Frequency Span Accuracy |
| $4-12$ | Tuning Accuracy |
| $4-13$ | Residual FM |
| $4-14$ | Noise Sidebands |
| $4-15$ | Resolution Bandwidth Accuracy |
| $4-16$ | Resolution Bandwidth Selectivity |
| $4-17$ | Average Noise Level |
| $4-18$ | Residual Responses |
| $4-19$ | Frequency Response |
| $4-20$ | Gain Compression |
| $4-21$ | Bandwidth Switching (Amplitude Variation) |
| $4-22$ | Input Attenuator Accuracy |
| $4-23$ | Reference Level Accuracy |
| $4-24$ | Sweep Time Accuracy |
| $4-25$ | Calibrator Output Accuracy |
| $4-26$ | Display Fidelity |

## 4-3. INSTRUMENTSTESTED

4-4. Since a compatible display mainframe is required for operation of the HP Model 8559A Spectrum Analyzer plug-in, the specifications listed in Table 1-1 apply when both instruments are functioning together. Consequently, the performance tests in this section verify the proper operation of both the HP 8559A and the display mainframe.

### 4.5. EQUIPMENT REQUIRED

4-6. The equipment required for the performance tests is listed under Recommended Test Equipment in Section I. Any equipment that satisfies the critical specifications given in the table may be substituted for the recommended model.

### 4.7. TEST RECORD

4-8. Results of the performance tests may be tabulated in the Performance Test Record at the end of this section. The test record lists test specifications and acceptable limits.

### 4.9. CALIBRATIONCYCLE

4-10. This instrument requires periodic calibration. Calibration should be verified every six months by means of the performance tests.

## PERFORMANCE TESTS

## NOTE

## Perform the Front Panel Adjustment Procedure in Section III before proceeding with performance tests. Allow at least 30 minutes warmup time.

## 4-11. FREQUENCY SPAN ACCURACY

## SPECIFICATION:

There are 14 calibrated spans ranging from 10 kHz per division to 200 MHz per division in a $1,2,5$ sequence. Frequency error between any two points on the display is within $\pm 5$ percent of the indicated frequency separation.

## DESCRIPTION:

Wide span widths are checked using the $100-10-$, and $1-\mathrm{MHz}$ outputs of a comb generator. Narrow span widths are checked using the output of a comb generator modulated by a function generator. Since the comb generator produces frequency components separated by a precisely determined frequency interval, the resultant spectral lines displayed on the CRT are evenly spaced when no span error exists in the instrument. Thus, span error is the cumulative variation of distance among the spectral line intervals displayed across the CRT. The amount of span error is determined by comparing the distance of the first nine graticule divisions with the displayed distance of the corresponding spectral line intervals.


FIGURE 4.1. FREQUENCY SPAN ACCURACY TEST SETUP

## EQUIPMENT:

Comb Generator ..... HP 8406A
Frequency Counter
Function Generator ..... HP 3310A
BNC Tee ..... HP 1250-0781
Adapter, Type N (m) to BNC (f) (2 required) ..... HP 1250-0780

## PERFORMANCE TESTS

## 4-11. FREQUENCY SPAN ACCURACY (Cont'd)

## PROCEDURE:

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz . .................................................................... . . . . . . 01 - 3
TUNING . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1.5 GHz
FREQ SPAN/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 200 MHz
RESOLUTION BW .......................................... . . . OPTIMUM, coupled (pushed in)
INPUTATTEN ..................................................................................... . . 0 dB
REFERENCELEVEL ......................................................................... -10 dB
REFLEVELFINE ..................................................................................... 0
AmplitudeScale ............................................................................. $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . AUTO
SWEEPTRIGGER .............................................................................. FREE RUN
ALTIF .......................................................................................... OFF

BLCLIP ................................................................................................... . . . OFF
VIDEOFILTER ......................................................................................... OFF

Comb Generator:
COMB FREQUENCY - MHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 100 MC
INTERPOLATION AMPLITUDE -1 MHz .................................................. OFF
OUTPUTAMPLITUDE . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 10 o'clock

Function Generator:
FUNCTION .................................................................................. SINE
RANGE . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 10K
Frequency ..................................................................................... 200 kHz
DCOFFSETLEVEL ...................................................................................... 0
2. Connect equipment as shown in Figure 4-1 but do not connect function generator to comb generator.

## PERFORMANCE TESTS

## 4-11. FREQUENCY SPAN ACCURACY (Cont'd)

3. Adjust spectrum analyzer TUNING control to position one spectral line (from comb generator) at first graticule line (left-hand edge of display). Measure the error between 17 th spectral line and 9 th graticule line as shown in Figure 4-2. Error should be no greater than $\pm 0.4$ division.


CENTERFREQUENCY
FIGURE 4-2. FREQUENCYSPAN ACCURACYMEASUREMENT FOR SEVENTEENTHSPECTRALLINE
4. Set FREQ SPAN/DIV to 100 MHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between ninth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
5. Set FREQ SPAN/DIV to 50 MHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between fifth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
6. Set comb generator COMB FREQUENCY - MHz for $10-\mathrm{MHz}$ comb. Set spectrum analyzer FREQ SPAN/DIV to 20 MHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between 17th spectral line and ninth graticule line as shown in Figure 4-3. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
7. Set FREQ SPAN/DIV to 10 MHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between ninth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div

## PERFORMANCE TESTS

4-11. FREQUENCY SPAN ACCURACY (Cont'd)


CENTERFREQUENCY
FIGURE 4-3. FREQUENCY SPAN ACCURACY MEASUREMENTFOR NINTH SPECTRALLINE
8. Set FREQ SPAN/DIV to 5 MHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between fifth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
9. Set comb generator COMB FREQUENCY - MHz for $1-\mathrm{MHz}$ comb and increase OUTPUT AMPLITUDE control to maximum setting. Set spectrum analyzer FREQ SPAN/DIV to 2 MHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between 17th spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
10. Set FREQ SPAN/DIV to I MHz. Adjust TUNING control to position one spectral line at first graticule line. Measure the error between ninth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
11. Set FREQ SPAN/DIV to 500 kHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between fifth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
12. Set comb generator COMB FREQUENCY - MHz for $10-\mathrm{MHz}$ comb. Adjust spectrum analyzer TUNING to position an in-band spectral line on the center graticule line (use SIG IDENT if necessary).

## PERFORMANCE TESTS

## 4-11. FREQUENCY SPAN ACCURACY (Cont'd)

13. Set function generator frequency to $200 \mathrm{kHz}( \pm 0.5)^{\circ}$ using frequency counter. Connect function generator output to comb generator MODULATION input. Set function generator OUTPUT LEVEL for a clean $200-\mathrm{kHzcomb}$ on the spectrum analyzer display.

## NOTE

To obtain a clean comb on the spectrum analyzer display, use either the LOW or HIGH output of the function generator and readjust the OUTPUT LEVEL control as necessary.
14. Set spectrum analyzer FREQ SPAN/DIV to 200 kHz . Adjust TUNING control to position one spectral line on the first graticule line. Measure the error between ninth spectral line and ninth graticule line. Error should be no greater than $\pm 0.4$ division.
$\qquad$ div
15. Using the procedure of NOTE in step 13, vary spectrum analyzer FREQ SPAN/DIV and function generator output frequency in accordance with Table 4-2. Adjust spectrum analyzer TUNING control to position one spectral line on the first graticule line. Measure the span error between ninth spectral line and ninth graticule line.

## NOTE

Disconnect function generator from comb generator when setting frequency with frequency counter. Increase spectrum analyzer REFERENCE LEVEL control setting as necessary for the lowest frequencies.

TABLE4-2. NARROW SPAN WIDTHERROR MEASUREMENT

| Spectrum Analyzer |  | Function Generator Output Frequency* | Span Width Error |  |
| :---: | :---: | :---: | :---: | :---: |
| FREO SPAN/DIV | RESOLUTION BW |  | Maximum | Actual |
| 100 kHz | OPTIMUM | 100 kHz | k0.4 div. | _ div. |
| 50 kHz | OPTIMUM | 50 kHz | $\pm 0.4$ div. | div. |
| 20 kHz | OPTIMUM | 20 kHz | $\pm 0.4$ div. | _div. |
| 10 kHz | OPTIMUM | 10 kHz | k0.4 div. | __div. |

[^2]
## PERFORMANCE TESTS

## 4-12. TUNING ACCURACY

## SPECIFICATION:

$0.1-3.0 \mathrm{GHz}: \quad \pm(1 \mathrm{MHz}+0.3 \%$ of center frequency)
$3.0-21.0 \mathrm{GHz}: \quad \pm(5 \mathrm{MHz}+0.2 \%$ of center frequency)

## DESCRIPTION:

An external RF source is used to provide a frequency-calibrated input signal to the spectrum analyzer for three points on each frequency band. The digital FREQUENCY GHz readout is compared with the known test frequency to find the amount of readout (or tuning) error. The 10 dB attenuator is necessary to reduce LO emission from the spectrum analyzer to the frequency counter when using the sweep oscillator.


NOTE
The HP 8350A Sweep Oscillator may be substituted for the HP 8620C in this procedure.

## EQUIPMENT

Comb Generator ..... HP 8406A
Sweep Oscillator ..... HP 8620C
RF Plug-In ..... HP 86290B, Opt. HO8
Frequency Counter ..... HP 5342A, Opt. 005
Power Splitter ..... HP 11667A-C16
10-dB Attenuator ..... HP 8491B, Opt. 010
Cable Assembly, RG-214/U, with Type N Connectors (2 required) ..... HP 11500A
Adapter, Type N(f) to N(f) ..... HP 1250-1472
Adapter, Type N(m) to BNC (f) (2 required) ..... HP 1250-0780

## PERFORMANCE TESTS

## 4-12. TUNING ACCURACY (Cont'd)

## PROCEDURE:

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... 0.035 GHz
FREQ SPAN/DIV ..... 200 kHz
RESOLUTIONBW OPTIMUM, coupled (pushed in)
INPUT ATTEN ..... 10 dB
REFERENCELEVEL ..... $-10 \mathrm{dBm}$
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF
2. Connect CAL OUTPUT signal of spectrum analyzer to INPUT 50R. Adjust TUNING control to position signal at center graticule line of display. Adjust FREQ CAL potentiometer for a FREQUENCY GHz display of 0.035 .
3. Connect comb generator to spectrum analyzer INPUT $50 \Omega$ as shown in Figure 4-4.
4. Set comb generator controls as follows:

> COMB GENERATOR - MHz 10 MC
> INTERPOLATION AMPLITUDE - 1 MHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . OFF
> OUTPUT AMPLITUDE . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . Full clockwise
5. Adjust spectrum analyzer TUNING control to center $10-\mathrm{MHz}$ comb tooth. FREQUENCY GHz readout should indicate:

| Min. | Actual | Max. |
| :--- | :--- | :--- |
| 0.09 |  | 0.011 |

6. Set comb generator COMB FREQUENCY - MHz for 100 MHz comb. Set spectrum analyzer FREQ SPAN/DIV to 1 MHz , and adjust TUNING control to position $1.5-\mathrm{GHz}$ comb tooth at center graticule line of display. FREQUENCY GHz readout should indicate:

| Min. | Actual | Max. |
| :--- | :--- | :--- |
| 1.94 |  | 1.506 |

7. Connect sweep oscillator to spectrum analyzer INPUT $50 \Omega$ as shown in Figure 4-4.

## PERFORMANCE TESTS

## 4-12. TUNING ACCURACY (Cont'd)

## NOTE

The 10 dB attenuator should be connected directly to the INPUT $50 \Omega$ of the spectrum analyzer and the 11667A power splitter (no cable assembly should be used between attenuator and analyzer or power splitter).
8. Adjust sweep oscillator for CW output at 3.000 GHz , as measured by frequency counter. Vary POWER LEVEL control as required for accurate measurement. Adjust spectrum analyzer TUNING control to center signal on display. FREQUENCY GHz readout should indicate:

| Min. | Actual | Max. |
| :--- | :--- | :--- |
| 2.90 |  | 3.010 |

9. Using procedure of step 8 , check spectrum analyzer tuning accuracy at remaining frequencies listed in Table 4-3. Indication on FREQUENCY GHz readout must fall within corresponding test limits at each frequency.

## NOTE

Use SIG IDENT to verify that spectrum analyzer is tuned to desired in-band signal response whenever tuning error appears excessive.

TABLE 4-3 TUNING ACCURACY MEASUREMENT

| Spectrum Analyzer | RF Source | FREQUENCY GHz READOUT |  |  |
| :---: | :---: | :---: | :---: | :---: |
| FREQUENCY BAND ( GHz )* | Frequency (GHz)"'" | Minimum (GHz) | Actual (GHz) | $\begin{aligned} & \text { Maximum } \\ & (\mathrm{GHz}) \end{aligned}$ |
| 0.01-3 | $\begin{gathered} 0.01 \\ 1.5 \\ 3.0 \end{gathered}$ | $\begin{aligned} & 0.009 \\ & 1.494 \\ & 2.990 \end{aligned}$ |  | $\begin{aligned} & 0.011 \\ & 1.506 \\ & 3.010 \end{aligned}$ |
| 6-9 | $\begin{aligned} & 6.1 \\ & 7.5 \\ & 9.0 \end{aligned}$ | $\begin{aligned} & 6.083 \\ & 7.480 \\ & 8.977 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & 6.117 \\ & 7.520 \\ & 9.023 \\ & \hline \end{aligned}$ |
| 3-9 | $\begin{aligned} & 3.1 \\ & 6.0 \\ & 9.0 \end{aligned}$ | $\begin{aligned} & 3.089 \\ & 5.983 \\ & 8.977 \end{aligned}$ |  | $\begin{aligned} & 3.110 \\ & 6.017 \\ & 9.023 \end{aligned}$ |
| 9-15 | $\begin{gathered} \hline 9.1 \\ 12.0 \\ 15.0 \end{gathered}$ | $\begin{gathered} \hline 9.077 \\ 11.971 \\ 14.965 \end{gathered}$ |  | $\begin{gathered} \hline 9.123 \\ 12.029 \\ 15.035 \end{gathered}$ |
| 6-15 | $\begin{gathered} \hline 6.1 \\ 10.5 \\ 15.0 \end{gathered}$ | $\begin{gathered} \hline 6.083 \\ 10.474 \\ 14.965 \end{gathered}$ |  | $\begin{gathered} \hline 6.117 \\ 10.526 \\ 15.035 \end{gathered}$ |
| 12.1-21 | $\begin{aligned} & \hline 12.1 \\ & 17.0 \\ & 21.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 12.071 \\ & 16.961 \\ & 20.953 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \hline 12.129 \\ & 17.039 \\ & 21.047 \\ & \hline \end{aligned}$ |

## PERFORMANCE TESTS

## 4-13. RESIDUAL FM

## SPECIFICATION:

Less than 2 kHz peak-to-peak for a time interval $\leq 0.1$ second; less than 2 kHz peak-to-peak in a 180 -series display mainframe with 220/240 line voltage.

## DESCRIPTION:

This test measures the inherent short-term instability (residual FM) of the LO system in the spectrum analyzer. A stable signal (supplied by a comb generator) is applied to the spectrum analyzer input and slope-detected with the linear portion of the $10-\mathrm{kHz}$ bandwidth filter in zero span (fixed-tuned receiver - see Figure 4-6). Variations of the spectrum analyzer's LO frequency (residual FM) can be measured as an amplitude shift on the CRT display ( $1 \mathrm{kHz} \approx 0.7$ major division with LIN Amplitude Scale).


## EQUIPMENT:

> Comb Generator . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $1250-0780$ Adapter, Type N (m) to BNC (f) (2 required) . . . . .

## PROCEDURE:

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $01-3$
TUNING . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 3.000 GHz
FREQUENCY SPAN/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 100 kHz
RESOLUTIONBW ............................................................................. . . . 10 kHz
INPUT ATTEN . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 30 dB
REFERENCELEVEL . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 20 dBm
REFLEVELFINE ........................................................................................... 0
Amplitude Scale . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .
SWEEP TIME/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . AUTO
SWEEPTRIGGER . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . FREE RUN
ALTIF ........................................................................................ OFF
SIGIDENT ................................................................................... OFF
BLCLIP . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . OFF
VIDEOFILTER ......................................................................................... . OFF

## PERFORMANCE TESTS

## 4-13. RESIDUAL FM (Cont'd)

Comb Generator:
COMB FREQUENCY - MHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 100 MC
INTERPOLATIONAMPLITUDE - 1 MHz ..................................................... OFF
OUTPUT AMPLITUDE .............................................................. Full clockwise
2. Connect OUTPUT of comb generator to spectrum analyzer INPUT $50 \Omega$ as shown in Figure 4-5.

## NOTE

The 8559 A is sensitive to vibration. Be sure spectrum analyzer is in a vibration-free environment.
3. Adjust spectrum analyzer TUNING control to display 3.0 GHz signal produced by comb generator. Adjust REFERENCE LEVEL and REF LEVEL FINE controls to position peak of signal at top graticule line.
4. Keep 3.0 GHz signal centered on CRT with TUNING control while reducing FREQ SPAN/DIV to zero.
5. Set RESOLUTIONBW to 10 kHz and SWEEP TIME/DIV to 0.1 sec .
6. Slightly readjust spectrum analyzer FINE TUNING control until trace appears between fourth and seventh graticule lines. Peak-to-peak variation of trace should not exceed 1.4 vertical division for each horizontal division (see Figure 4-7).
$\qquad$ div

## NOTE

For 2201240 line voltages, peak-to-peak variation of trace should not exceed 1.4 vertical divisions $(2 \mathrm{kHz})$ in a 180 -series display mainframe.


FIGURE46. RESIDUALFM TO AM CONVERSIONDISPLAY


FIGURE4-7. RESIDUALFM DISPLAY

## PERFORMANCE TESTS

## 4-14. NOISE SIDEBANDS

## SPECIFICATION:

Noise sidebands are at least 70 dB below a CW signal, 30 kHz or more away from the signal with a 1 kHz resolution bandwidth and full video filtering.

## DESCRIPTION:

A stable 1.8 GHz CW signal is applied at a -20 dBm level to the spectrum analyzer and displayed on the CRT. The amplitudes of noise-associated sidebands and unwanted responses near the signal are measured.


## EQUIPMENT:

> Comb Generator
> HP 8406A
> Adapter, Type N (m) to BNC (f) (2 required)
> HP 1250-0780

## PROCEDURE:

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... 1.8 GHz
FREQ SPAN/DIV ..... 1 MHz
RESOLUTION BW ..... 30 kHz , uncoupled
INPUT ATTEN0 dB
REFERENCELEVEL ..... $-20 \mathrm{dBm}$
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF

## PERFORMANCE TESTS

## 4-14. NOISE SIDEBANDS(Cont'd)

## Comb Generator:

> COMB FREQUENCY - MHz 100 MC
> INTERPOLATION AMPLITUDE $-1 \mathrm{MHz} . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . ~ O F F$
> OUTPUT AMPLITUDE
> Full clockwise
2. Connect equipment as shown in Figure 4-8.
3. Adjust TUNING control to locate $1.8-\mathrm{GHz}$ comb tooth on CRT.
4. Adjust REFERENCE LEVEL and REF LEVEL FINE controls to position peak of $1.8-\mathrm{GHz}$ signal at top graticule line.
5. Decrease FREQ SPAN/DIV to $\mathbf{2 0} \mathrm{kHz}$ and RESOLUTION BW to 1 kHz . Adjust TUNING as necessary to keep signal centered.
6. Position signal at center of display. Set VIDEO FILTER control fully clockwise (not in MAX detent position). Measure noise sidebands existing more than 1.5 divisions ( $\mathbf{3 0} \mathrm{kHz}$ ) from $1.8-\mathrm{GHz}$ signal. Noise sidebands should be more than 70 dB ( 7 divisions) down from top graticule line.
$\qquad$ div. down

## PERFORMANCE TESTS

## 4-15. RESOLUTION BANDWIDTH ACCURACY

## SPECIFICATION:

Individual resolution bandwidth $3-\mathrm{dB}$ points are calibrated to $\pm 15 \%$ ( $\pm 30 \%$ for 3 MHz bandwidth).

## DESCRIPTION:

Resolution bandwidth accuracy is measured in the linear mode to eliminate log amplifier errors. Since signal level at the $3-\mathrm{dB}$ points (half-power points) is related to peak signal level by a voltage ratio of 0.707:1.O, a peak level of 7.1 vertical divisions on the spectrum analyzer display gives a half-power level of 5 vertical divisions:

$$
\begin{aligned}
0.707(\text { voltage ratio }) & =X \operatorname{div} / 7.1 \operatorname{div} \\
X \operatorname{div} & =(7.1)(0.707) \\
& \approx 5 \operatorname{div}
\end{aligned}
$$

In the $30-, 10-, 3-$, and $1-\mathrm{kHz}$ bandwidths, a 21.4 MHz signal (final IF) is injected directly into Bandwidth Filter No. 1 Assembly A11 to provide the stability required for measurement of narrow resolution bandwidths.


FIGURE4-9. RESOLUTIONBANDWIDTHACCURACYTESTSETUP,3MHz TO 100 kHz

## EQUIPMENT:

Signal Generator ..... HP 8640B
Extender Cable Assembly
Adapter, Type $\mathrm{N}(\mathrm{m})$ to BNC (f) (2 required) ..... HP 1250-0780
Adapter, Type SMB (f) to BNC (f) ..... HP 1250-1236

## PERFORMANCE TESTS

## 4-15. RESOLUTIONBANDWIDTH ACCURACY (Cont'd)

## PROCEDURE:

## WARNING

> Part of this test must be performed with power supplied to the instrument and with protective covers removed. The test should be performed only by sewice-trainedpersonnelwho are aware of the hazards involved.

1. Set equipment controls as follows:

Spectrum Analyzer:FREQUENCY BAND GHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 01 - 3
TUNING ..... 0.035 GHz
FREQ SPAN/DIV ..... 0
RESOLUTIONBW ..... 3 MHz
INPUTATTEN ..... 10 dB
REFERENCELEVEL ..... 0 dBm
REFLEVELFINE ..... 0
AmplitudeScale ..... LIN
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF
Signal Generator:
COUNTERMODE ..... INT, EXPAND X10
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 35 MHz
RF ..... ON
OUTPUTLEVEL ..... 0 dBm
2. Connect equipment as shown in Figure 4-9.
3. Adjust spectrum analyzer TUNING control to locate peak of $35-\mathrm{MHz}$ signal on CRT. Reduce signal generator output if necessary.

## NOTE

If necessary, select $10 \mathbf{d B} / D I V$ to locate signal, then switch to LIN.
4. Adjust signal generator OUTPUT LEVEL to position trace at 7.1 divisions above graticule baseline.

## PERFORMANCE TESTS

## 4-15. RESOLUTION BANDWIDTH ACCURACY (Cont'd)

5. Tune signal generator frequency until trace drops to 5 divisions above graticule baseline. Record signal generator frequency
$\qquad$ MHz
6. Tune signal generator frequency in direction opposite to that of step 5 until trace peaks ( 7.1 divisions above graticule baseline) and then drops to 5 divisions above graticule baseline. Record signal generator frequency.

## NOTE

The bandwidths recorded in this performance test are required for calculations in 4-16 Resolution Bandwidth Selectivityperformancetest.
7. Calculate and record resolution bandwidth at $3-\mathrm{dB}$ points (difference between frequencies recorded in steps 5 and 6).

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| 2.0 |  | 3.90 MHz |

8. Select ALT IF (switch pushed in), leaving FREQ SPAN/DIV set to 0 . Set signal generator to 35 MHz and repeat steps 3 through 7 .

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| 2.0 |  | 3.90 MHz |

9. Return ALT IF switch to OFF position. Set RESOLUTION BW to 1 MHz , leaving FREQ SPAN/DIV set to 0 . Set signal generator to 35 MHz and repeat steps 3 through 7 .

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| 850 |  | 1150 kHz |

10. Set RESOLUTION BW to 300 kHz , leaving FREQ SPAN/DIV set to 0 . Set signal generator to 35 MHz and repeat steps 3 through 7 .

| Min. | Actual | Max. |
| :--- | :--- | ---: |
| 255 |  | 345 kHz |

11. Set RESOLUTION BW to 100 kHz , leaving FREQ SPAN/DIV set to 0 . Set signal generator to 35 MHz and repeat steps 3 through 7 .

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| 85 |  | 115 kHz |

## PERFORMANCE TESTS

## 4-15. RESOLUTION BANDWIDTH ACCURACY (Cont'd)



FIGURE4-10. RESOLUTIONBANDWIDTHACCURACY TESTSETUP, 30 kHz TO 1 kHz

## WARNING

In the following procedure, the plug-in must be removed from the display mainframe and connected through the extender cable assembly. Be very careful; the energy at some points in the instrument will, if contacted, cause personal injury. This test should be performed only by a skilled person who knows the hazard involved.
12. Set equipment controlsas follows:

## Spectrum Analyzer:

FREQUENCY BAND GHz ..... 01-3
TUNING ..... $>0.010 \mathrm{GHz}$
FREQ SPAN/DIV ..... 0 kHz
RESOLUTIONBW ..... 30 kHz
INPUT ATTEN ..... 10 dB
REFERENCELEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... LIN
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF

## PERFORMANCE TESTS

### 4.15. RESOLUTIONBANDWIDTH ACCURACY (Cont'd)

SignalGenerator:
COUNTERMODE INT, EXPAND X10
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 21.4 MHz
RF ..... ON
OUTPUTLEVEL ..... $\approx-3 \mathrm{dBm}$
13. Connect equipment as shown in Figure 4-10.

## NOTE

For early instruments that do not feature A16J3, a $21.4-\mathrm{MHz}$ signal can be injected directly into the 300-MHz output (A10J1) of Third Converter Assembly A10. Set the signal generator OUTPUT LEVEL to $\mathbf{0 ~ d B m}$ and use the spectrum analyzer REFERENCE LEVEL and REF LEVEL FINE controls in step $14(\approx-40 \mathbf{d B m})$ to position the trace at 7.1 divisions above the graticule baseline.
14. Adjust signal generator frequency until spectrum analyzer trace is at peak. Set signal generator OUTPUT LEVEL to position trace at 7.1 divisions above graticule baseline. Set COUNTER MODE to EXPAND X 100 (most significant digit will overflow).
15. Tune signal generator frequency until trace drops to 5 divisions above graticule baseline. Record signal generator frequency.
$\qquad$
16. Tune signal generator frequency in direction opposite to that of step 15 until trace peaks ( 7.1 divisions above graticule baseline) and then drops to 5 divisions above graticule baseline. Record signal generator frequency.
$\xrightarrow{-} \mathrm{MHz}$
17. Calculate and record resolution bandwidth at $3-\mathrm{dB}$ points (difference between frequencies recorded in steps 15 and 16).

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| 25.0 kHz |  | 34.50 kHz |

18. Set RESOLUTION BW to 10 kHz , leaving FREQ SPAN/DIV set to 0 . Repeat steps 14 through 17 .

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| 8.0 kHz |  | 11.50 kHz |

## PERFORMANCE TESTS

## 4-15. RESOLUTION BANDWIDTH ACCURACY (Cont'd)

19. Set RESOLUTION BW to $3 \mathbf{k H z}$, leaving FREQ SPAN/DIV set to $\mathbf{0}$. Repeat steps 14 through 17 .

| Min. | Actual | Max. |
| :--- | :--- | ---: |
| $2.5 \mathbf{~ k H z}$ |  | $3.45 \mathbf{~ k H z}$ |

20. Set RESOLUTION BW to $\mathbf{1} \mathbf{k H z}$, leaving FREQ SPAN/DIV set to $\mathbf{0}$. Repeat steps 14 through 17 .

| Min. | Actual | Max. |
| :--- | ---: | ---: |
| $0.5 \mathbf{k H z}$ |  |  |
|  |  | $1.15 \mathbf{k H z}$ |

21. Leave signal generator connected to A 16 J 3 if continuing on with next performance test.

## PERFORMANCE TESTS

## 4-16. RESOLUTIONBANDWIDTHSELECTIVITY

## SPECIFICATION:

$60-\mathrm{dB} / 3-\mathrm{dB}$ resolution bandwidth ratio: $<15: 1$

## DESCRIPTION:

The $60-\mathrm{dB}$ bandwidth is measured for all resolution bandwidths. The $60-$ to $3-\mathrm{dB}$ resolution bandwidth ratio (shape factor) is then computed for each bandwidth by dividing the $3-\mathrm{dB}$ value (from the Resolution Bandwidth Accuracy test) into the $60-\mathrm{dB}$ value.

In the $30-10-, 3-$, and $1-\mathrm{kHz}$ bandwidths, a $21.4-\mathrm{MHz}$ signal (final IF) is injected into Bandwidth Filter No. 1 Assembly A11 to provide the stability required for the measurement of narrow resolution bandwidths.


FIGURE 4-11. RESOLUTIONBANDWIDTH SELECTIVITYTESTSETUP, 1 kHz TO 30 kHz

## WARNING

In the following procedure, the plug-in must be removed from the display mainframe and connected through the extender cable assembly. Be very careful; the energy at some points in the instrument will, if contacted, cause personal injury. This test should be performed only by a skilled person who knows the hazard involved.

## EQUIPMENT:

Signal Generator
Extender Cable Assembly
Adapter, SMB (f) to BNC (f) ..... HP 1250-1236
Adapter, Type N (m) to BNC (f) (2 required) ..... HP 1250-0780

## PERFORMANCE TESTS

## 4-16. RESOLUTION BANDWIDTH SELECTIVITY (Cont'd)

## PROCEDURE:

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... $>0.010 \mathrm{GHz}$
FREQ SPAN/DIV ..... 0
RESOLUTIONBW ..... 1 kHz
INPUTATTEN ..... 10 dB
REFERENCELEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIGIDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... 12 o'clock
Signal Generator:
COUNTERMODE INT, EXPAND X10
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 21.4 MHz
RF ..... ON
OUTPUTLEVEL ..... $\approx-3 \mathrm{dBm}$
2. Connect equipment as shown in Figure 4-11.

## NOTE

For early instruments that do not feature A16J3, a $321.4 \mathrm{MHz},-25 \mathrm{dBm}$ signal can be injected directly into the input of Third Converter Assembly A10 at blue cable A10W1. Set signal generator COUNTER MODE to EXPAND X100(most significant digit will overflow).
3. Adjust signal generator frequency until spectrum analyzer trace is at peak. Put signal generator OUTPUT LEVEL to position trace at top graticule line.
4. Tune signal generator until trace drops to 2 divisions above graticule baseline. Record signal generator frequency.

## PERFORMANCE TESTS

## 4-16. RESOLUTION BANDWIDTH SELECTIVITY (Cont'd)

5. Tune signal generator in direction opposite to that of step 4 until trace peaks (top graticule line) and then drops to 2 divisions above graticule baseline. Record signal generator frequency.
$\qquad$
6. Calculate and record resolution bandwidth at $60-\mathrm{dB}$ points (difference between frequencies recorded in steps 4 and 5).
$\qquad$ kHz
7. Set RESOLUTION BW to 3 kHz , leaving FREQ SPAN/DIV set to 0 . Repeat steps 3 through 6 .
$\qquad$ kHz
8. Set RESOLUTIONBW to 10 kHz , leaving FREQ SPAN/DIV set to 0 . Repeat steps 3 through 6 .
$\qquad$ kHz
9. Set RESOLUTION BW to 30 kHz , leaving FREQ SPAN/DIV set to 0 . Repeat steps 3 through 6 .
10. Disconnect signal generator from A16J3. Set the display's LINE power to OFF and remove extender cable assembly. Install plug-in in mainframe and set LINE power to ON.
11. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... 0.035 GHz
FREQ SPAN/DIV ..... 0
RESOLUTION BW ..... 100 kHz
INPUT ATTEN ..... 10 dB
REFERENCELEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER 12 o'clock

## PERFORMANCE TESTS

### 4.16. RESOLUTION BANDWIDTHSELECTIVITY (Cont'd)

Signal Generator:

| COUNTERMODE | INT, EXPAND X10 |
| :---: | :---: |
| AM | OFF |
| FM | . OFF |
| FREQUENCYTUNE | 35 MHz |
| RF | ON |
| OUTPUTLEVEL | 0 dBm |

12. Connect equipment as shown in Figure 4-12.


FIGURE 4-12. RESOLUTIONBANDWIDTHSELECTIVITYTESTSETUP, 100 kHz TO3MHz
13. Adjust spectrum analyzer TUNING to locate peak of $35-\mathrm{MHz}$ signal on CRT. Reduce signal generator output if necessary.
14. Adjust signal generator OUTPUT LEVEL to position trace at top graticule line.
15. Tune signal generator frequency until trace drops to 2 divisions above graticule baseline. Record signal generator frequency.
$\qquad$ MHz
16. Tune signal generator frequency in direction opposite to that of step 16 until trace peaks (top graticule line) and then drops to $\mathbf{2}$ divisions above graticule baseline. Record signal generator frequency.
$\qquad$ MHz
17. Calculate and record resolution bandwidth at $60-\mathrm{dB}$ points (difference between frequencies recorded in steps 16 and 17).

## PERFORMANCE TESTS

## 4-16. RESOLUTION BANDWIDTHSELECTIVITY(Cont'd)

18. Set RESOLUTION BW to 300 kHz , leaving FREQ SPAN/DIV set to 0. Repeat steps 14 through 18 .
$\qquad$ kHz
19. Set RESOLUTION BW to 1 MHz , leaving FREQ SPAN/DIV set to 0 . Repeat steps 14 through 18 .
$\qquad$ MHz
20. Select ALT IF (switch pushed in). Set RESOLUTION BW to 3 MHz , leaving FREQ SPAN/DIV set to 0 . Repeat steps 14 through 18.
$\qquad$
21. Return ALT IF switch to OFF position. With RESOLUTION BW still in 3 MHz and FREQ SPAN/DIV set to 0 , repeat steps 14 through 18 .
$\qquad$ MHz
22. In Table 4-4, record 3-dB bandwidths computed in 4-15 Resolution Bandwidth Accuracy test.
23. In Table 4-4, record $60-\mathrm{dB}$ bandwidths recorded in this procedure.
24. For each resolution bandwidth, divide $60-\mathrm{dB}$ bandwidth by $3-\mathrm{dB}$ bandwidth to obtain Resolution Bandwidth Ratio. Each ratio should be less than 15: 1 .

TABLE4-4. RESOLUTIONBANDWIDTH SELECTIVITY

| RESOLUTION BW Setting | Actual 3 dB BW | Actual 60 dB BW | Resolution Bandwidth Ratio ( $60 \mathrm{~dB} / 3 \mathrm{~dB}$ BW) |
| :---: | :---: | :---: | :---: |
| $3 \mathbf{~ M H z}$ $\mathbf{3} \mathbf{~ M H z}$ (ALT IF) $1 \mathbf{~ M H z}$ $\mathbf{3 0 0} \mathbf{~ k H z}$ $\mathbf{1 0 0} \mathrm{kHz}$ 30 kHz 10 kHz 3 kHz 1 kHz |  |  |  |

## PERFORMANCE TESTS

## 4-17. AVERAGENOISE LEVEL

## SPECIFICATION:

The maximum average noise level for each frequency band, with 1 kHz resolution bandwidth and 0 dB attenuation, is given in Table 4-5.

## DESCRIPTION:

The average noise level of the spectrum analyzer is checked by observing the average noise power level displayed on the CRT when no input signal is applied to the instrument.


FIGURE 4-13. AVERAGE NOISELEVEL MEASUREMENT,. $01-3 \mathrm{GHz}$

## EQUIPMENT:



## NOTE

The HP 853A Spectrum Analyzer Display may be substituted for the HP 181T/TR in this procedure.

## NOTE

This test can be performed with no input termination if INPUT ATTEN is set to $\mathbf{2 0 ~ d B}$. Note that the input attenuation must then be taken into consideration in establishing the equivalent REFERENCE LEVEL control setting for the measurement. A REFERENCE LEVEL setting of -40 dBm with 20 dB INPUT ATTEN is equivalent to a REFERENCE LEVEL setting of $\mathbf{- 6 0} \mathbf{~ d B m}$ with $\mathbf{0 d B}$ INPUT ATTEN.

## PERFORMANCE TESTS

## 4-17. AVERAGE NOISE LEVEL (Cont'd)

## PROCEDURE:

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... 0.010 GHz
FREQ SPAN/DIV ..... F
RESOLUTIONBW ..... 3 MHz , uncoupled
INPUTATTEN ..... 0 dB
REFERENCE LEVEL ..... $-60 \mathrm{dBm}$
REF LEVEL FINE ..... 0
Amplitude Scale $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BL CLIP ..... OFF
VIDEOFILTER Full CW (not in detent)
2. With FREQ SPAN/DIV set to F, set VIDEO FILTER fully clockwise, but not in detent. Adjust TUNING to position marker at frequency where displayed average noise level is highest.

## NOTE <br> Do not tune marker beyond specified band edge.

3. Set VIDEO FILTER to detent and FREQ SPAN/DIV to 0.
4. Set RESOLUTIONBW to 1 kHz .
5. Measure average noise level displayed on CRT (see Figure 4-13) and record results in Table 4-5.
6. Set FREQUENCY BAND GHz to 6-9 and repeat steps 2 through 5 .
7. Set FREQUENCY BAND GHz to $3-9$ and repeat steps 2 through 5 .
8. Set FREQUENCY BAND GHz to 9-15 and repeat steps $\mathbf{2}$ through 5 .
9. Set FREQUENCY BAND GHz to 6-15 and repeat steps 2 through 5.
10. Set FREQUENCY BAND GHz to $12.1-21$ and repeat steps 2 through 5 for the frequency range of 12.1 - 18.0 GHz .

## PERFORMANCE TESTS

## 4-17. AVERAGE NOISELEVEL (Cont'd)

## NOTE

## Do not tune above 18.0 GHz for this step.

11. Repeat steps 2 through 5 for the frequency range of $18.0-21.0 \mathrm{GHz}$.
12. Repeat entire procedure with ALT IF on.

TABLE 4-5. AVERAGENOISELEVEL

| $\begin{gathered} \text { FREQUENCY } \\ \text { BAND GHz } \\ \text { Setting } \end{gathered}$ | Specified Frequency Range (GHz) |  | Average Noise Level |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Reg. IF | ALTIF | Maximum | Actual (Reg. IF) | Actual (ALT IF) |
| .01-3 | 0.010-3.060 | 0.025-3.060 | $-111 \mathrm{dBm}$ | - $\quad$ dBm | - $\quad$ dBm |
| 6-9 | 6.035-9.060 | 6.020-9.060 | $-108 \mathrm{dBm}$ | - | - |
| 3-9 | 3.033-9.120 | 3.048-9.120 | $-103 \mathrm{dBm}$ | - _ dBm | - _ dBm |
| 9-15 | 9.058-15.120 | 9.043-15.120 | $-98 \mathrm{dBm}$ | $-\quad$ _ dBm | - _ CBm |
| 6-15 | 6.055-15.180 | 6.070-15.180 | $-93 \mathrm{dBm}$ | - | - _ $\quad$ dBm |
| 12.1-21 | 12.080-18.000 | 12.065-18.000 | $-92 \mathrm{dBm}$ | - __dBm | - _ dBm |
| 12.1-21 | 18.000-21.000 | 18.000-21.000 | $-90 \mathrm{dBm}$ | - ___ dBm | - ___dBm |

## PERFORMANCE TESTS

## 4-18. RESIDUAL RESPONSES

## SPECIFICATION:

Residual responses are less than $-90 \mathrm{dBm}(0.01-3.06 \mathrm{GHz})$ with 0 dB input attenuation and no signal present at input. They are less than $-90 \mathrm{dBm}(0.025-3.06 \mathrm{GHz})$ with ALT IF selected.

## DESCRIPTION:

Signals present on the display without an input signal applied to the spectrum analyzer are residual responses. The $. \mathrm{Ol}-3 \mathrm{GHz}$ frequency band is checked for residual responses greater than -90 dBm .

## EQUIPMENT:

> Variable Persistence/Storage Display . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 909 AP , Opt. 012 $50 \Omega$ Termination, Type $(\mathrm{m})$. . .

NOTE
The HP 853A Spectrum Analyzer Display may be substituted for the HP 181T/TR in this procedure.

## NOTE

This test can be performed with no input termination if INPUT ATTEN is set to 20 dB . Note that the input attenuation must then be taken into consideration in establishing the equivalent REFERENCE LEVEL control setting for the measurement. A REFERENCE LEVEL setting of $-40 \mathbf{d B m}$ with 20 dB INPUT ATTEN is equivalent to a REFERENCE LEVEL setting of $-60 \mathbf{d B m}$ with $\mathbf{0 d B}$ INPUT ATTEN.

## PROCEDURE:

1. Set spectrum analyzer controls as follows:

| FREQUENCY BAND GHz | . $01-3$ |
| :---: | :---: |
| TUNING | 0.050 GHz |
| FREQ SPAN/DIV | 10 MHz |
| RESOLUTION BW | 1 MHz , uncoupled |
| INPUTATTEN | 0 dB |
| REFERENCELEVEL | $-60 \mathrm{dBm}$ |
| REFLEVELFINE | ......... 0 |
| AmplitudeScale | $10 \mathrm{~dB} / \mathrm{DIV}$ |
| SWEEP TIME/DIV | AUTO |
| SWEEPTRIGGER | FREE RUN |
| ALTIF | ...... OFF |
| SIGIDENT | . OFF |
| BLCLIP | OFF |
| VIDEOFILTER | .. 12 o'clock |

## PERFORMANCE TESTS

## 4-18. RESIDUAL RESPONSES(Cont'd)

2. Terminate INPUT $50 \Omega$ connector with 50 -ohm termination.
3. Adjust TUNING control to position LO feedthrough signal on leftmost vertical graticule line.
4. Set RESOLUTION BW control to 10 kHz , leaving FREQ SPAN/DIV set to 10 MHz . Adjust BL CLIP control clockwise until just the peaks of the noise are displayed. Set the SWEEP TRIGGER control to SINGLE and display PERSISTENCE control to MAX.
5. Set display to WRITE and momentarily press ERASE. Turn SWEEP TRIGGER control clockwise to trigger a single sweep, adjusting BL CLIP and display INTENSITY controls until just the peaks of the noise are displayed. Press ERASE and trigger another sweep.
6. Set display to VIEW and check for residual responses greater than -90 dBm . Record frequency and amplitude of residual response with the greatest amplitude.
$\qquad$
$\qquad$
dBm

## NOTE

Residual responses are often visible within 10 MHz of the HP 8559A LO feedthrough signal ( 25 MHz with ALT IF selected). These residual responses are not within the instrument's specified frequency range and should be excluded from consideration in this performance test.
7. Increase TUNING control setting in $100-\mathrm{MHz}$ increments and use procedure of steps $5-7$ to check for residual responses from 10 MHz to $3.060 \mathrm{GHz}(25 \mathrm{MHz}-3.060 \mathrm{GHz}$ with ALT IF selected).

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE

## SPECIFICATION:

Frequency response measured with 0 or 10 dB of input attenuation includes input attenuator flatness, mixer flatness, and band-to-band amplitude variation. Table 4-6 shows the frequency response specifications.

TABLE46. FREQUENCYRESPONSESPECIFICATIONS

| FREQUENCY BAND (GHz) | Frequency Response <br> ( $\pm \mathrm{dB}$ Maximum) |
| :---: | :---: |
| $.01-3$ | 1.0 |
| $6-9$ | 1.0 |
| $3-9$ | 1.5 |
| $9-15$ | 1.8 |
| $6-15$ | 2.1 |
| $12.1-18.0$ | 2.3 |
| $18.0-21.0$ | 3.0 |

## DESCRIPTION:

Frequency response is checked in each frequency band. With the spectrum analyzer set to full sweep, an RF input signal is very slowly swept across the entire frequency band. The resulting display is a series of narrow signals that vary in height across the CRT. Since the RF source is leveled and held flat across each frequency band, variations in amplitude on the display represent variations in the frequency response of the spectrum analyzer. Leveling within reasonable limits becomes difficult from 18 GHz to 21 GHz , so the RF output at the power splitter is characterized and compensated for when making the measurement of this frequency range.


FIGURE4-14. FREQUENCY RESPONSE TESTSETUP

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE(Cont'd)

## NOTE <br> The HP 853A Spectrum Analyzer Display is not recommended for use in this procedure. <br> The HP 8350A Sweep Oscillator may be substituted for the HP 8620C in this procedure, if necessary.

## EQUIPMENT:

| Variable Persistence/Storage Display | HP 181T/TR |
| :---: | :---: |
| Sweep Oscillator | HP 8620C |
| RF Plug-in | HP 86222A |
| RF Plug-in | HP 86290B-H08 |
| Power Meter | HP 435A/B |
| Power Sensor | HP 8485A |
| Power Splitter | HP 11667A, Opt. C16 |
| Attenuator, 20-dB | HP 8491B, Opt. 020 |
| Crystal Detector | HP 33330C |
| Adapter, Type N(m) to SMA (f) (2 requ | HP 1250-1250 |
| Adapter, Type N(f) to SMA(f) | HP 1250-1745 |
| Adapter, Type N(m) to N (m) | HP 1250-0778 |
| Test Cable, SMC (m) to BNC (m) | HP 11592-60001 |
| Cable Assembly, SMA (m) to SMA (m) | . HP 8120-1578 |

## PROCEDURE:

1. Set equipment controls as follows:

## Spectrum Analyzer:

FREQUENCY BAND GHz ..... 01-3
TUNING ..... 0.000 GHz
FREQ SPAN/DIV ..... 10 MHz
RESOLUTIONBW ..... 300 kHz , coupled
INPUT ATTEN ..... 0 dB
REFERENCELEVEL ..... $-20 \mathrm{dBm}$
REFLEVELFINE ..... - 4
Amplitude Scale ..... $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIGIDENT ..... OFF
BLCLIP ..... OFF
VIDEO FILTER Full CW (not in detent)

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE(Cont'd)

Sweep Oscillator:

2. Center LO feedthrough signal on CRT with spectrum analyzer TUNING control. Adjust FREQ CAL for a FREQUENCY GHz readout of $\mathbf{0 . 0 0 0}$.


FIGURE4-15. TYPICALFREQUENCY RESPONSE FOR . 01 TO 2.4 GHz
3. Using $0.01-2.4 \mathrm{GHz}$ sweep oscillator plug-in, connect equipment as shown in Figure 4-14. Connect output of power splitter, through $20-\mathrm{dB}$ attenuator, to spectrum analyzer input. Turn sweep oscillator RF power ON and adjust ALC GAIN control for leveled output indication.

## NOTE

## Use maximum possible ALC GAIN to avoid leveling errors during swept measurements.

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE(Cont'd)

4. Adjust spectrum analyzer TUNING control for a FREQUENCY GHz readout of 0.100 . Set sweep oscillator to CW with frequency of 100 MHz and use CW control to center signal on spectrum analyzer display.
5. Calibrate and zero power sensor and meter. Disconnect power splitter from 20-dB attenuator and connect to power sensor. Adjust sweep oscillator POWER LEVEL control for a power meter indication of -8 dBm .
6. Connect output of power splitter through $20-\mathrm{dB}$ attenuator directly (do not use cable) to spectrum analyzer input. Select Amplitude Scale setting of $1 \mathrm{~dB} /$ DIV, and adjust REF LEVEL FINE control as necessary to place peak of 100 MHz signal at center horizontal graticule line of spectrum analyzer display.
7. Adjust spectrum analyzer TUNING control for a FREQUENCY GHz readout of 0.060 . Adjust sweep oscillator CW control for 60 MHz signal, centered on spectrum analyzer display.
8. Set sweep oscillator AF control for 100 MHz sweep. Adjust spectrum analyzer display PERSISTENCE control fully clockwise. Adjust sweep oscillator SWEEP TIME vernier for slow sweep ( 30 seconds or longer) and trigger a sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line ( 10 MHz to 110 MHz ).
Maximum ___ divisions
Minimum___ divisions
9. Adjust spectrum analyzer TUNING control for a FREQUENCY GHz readout of 0.100 . Set sweep oscillator to CW with frequency of 100 MHz and use CW control to center signal on spectrum analyzer display.
10. Set spectrum analyzer FREQ SPAN/DIV control to F (full band) and RESOLUTION BW control to 3 MHz . Adjust TUNING control fully clockwise to position tuning marker at high end of selected frequency band. Adjust REF LEVEL FINE control as necessary to place peak of 100 MHz signal (near LO feedthrough signal) at center horizontal graticule line of spectrum analyzer display.
11. Set sweep oscillator for FULL BAND ( 10 MHz to 2.4 GHz ) and trigger a sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line ( 10 MHz to 2.4 GHz ). Record deviation of signal peak located at 8th vertical graticule line (approximately 2.1 GHz ).
Maximum__ divisions
Minimum $\quad$ divisions
8th graticule line__ divisions
12. Remove $0.01-2.4 \mathrm{GHz}$ RF Plug-in from sweep oscillator mainframe and replace with $\mathbf{2 - 2 2} \mathbf{~ G H z ~ R F}$ Plug-in. Select band $4(2.0-22 \mathrm{GHz})$ on HP 8620C sweep oscillator.
13. Set sweep oscillator to CW with frequency of 2.1 GHz and use CW control to position signal on 8th vertical graticule line of spectrum analyzer display. Adjust ALC GAIN control for leveled sweep oscillator output and adjust POWER LEVEL control to place signal peak at same amplitude measured in step 11.

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE(Cont'd)

NOTE
Use maximum possible ALC GAIN to avoid leveling errors during swept measurements.

Do not adjust spectrum analyzer REF LEVEL FINE control or sweep oscillator POWER LEVEL control during the remaining steps of this performance test.
14. Adjust spectrum analyzer TUNING control fully counterclockwise to position tuning marker at low end of selected frequency band. Set sweep oscillator CW control to 2.5 GHz and AF control for 1 GHz sweep. Trigger a sweep, and record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line ( 2 GHz to 3 GHz ).
Maximum___ divisions
Minimum___ divisions

## NOTE

It is normal for the HP 8559A to exhibit baseline lift with an input signal at approximately 3.0075 GHz (2.9925 with ALT IF selected). Adjust sweep oscillator sweep range as necessary to avoid baseline lift during frequency response measurements.

If frequency response appears out of specification near a band edge, use a frequency counter with sweep oscillator in CW to ensure the frequency in question is within the specified band.
15. Compare values recorded in steps 8,11 , and 14 , and record overall greatest positive and greatest negative deviation from center horizontal graticule line for entire $.01-3 \mathrm{GHz}$ frequency band. Frequency response (deviation from center horizontal graticule line) should not exceed $\pm 1.0 \mathrm{~dB}$ ( $\pm 1.0$ division).
Maximum ___ divisions $(.01-3 \mathrm{GHz})$
Minimum ___ divisions $(.01-3 \mathrm{GHz})$
16. Calculate mean deviation for $.01-3 \mathrm{GHz}$ frequency band using maximum and minimum values recorded in step 15. (For example, a maximum of +0.5 and a minimum of -0.7 results in a mean deviation of -0.1 )


## PERFORMANCE TESTS

### 4.19. FREQUENCY RESPONSE (Cont'd)

Frequency Response, 3-18 GHz

## NOTE

For the higher frequency bands, multiple responses may appear on spectrum analyzer display during frequency response measurement. Adjust INTENSITY control as necessary for optimum display of in-band signal peaks.
17. Select $6-9 \mathrm{GHz}$ frequency band on spectrum analyzer. Set sweep oscillator to $\mathbf{C W}$ and frequency to 7.5 GHz . Use CW control to center signal on spectrum analyzer display. Set AF control for 3 GHz and trigger a sweep. Adjust spectrum analyzer TUNING control clockwise several turns to reposition tuning marker. Trigger another sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line (neglect deviations caused by tuning marker).
Maximum___ divisions
Minimum__ divisions
18. To calculate frequency response for $6-9 \mathrm{GHz}$ frequency band, subtract mean deviation of step 16 from maximum and minimum values recorded in step 17. Frequency response should not exceed $\pm 1.0 \mathrm{~dB}$ ( $\pm 1.0$ division).
Maximum___ divisions $(6-9 \mathrm{GHz})$
Minimum__ divisions $(6-9 \mathrm{GHz})$
19. Select $3-9 \mathrm{GHz}$ frequency band on spectrum analyzer. Set sweep oscillator to $\mathbf{C W}$ and frequency to 6.0 GHz . Use $\mathbf{C W}$ control to center signal on spectrum analyzer display. Set AF control for 6 GHz and trigger a sweep. Adjust spectrum analyzer TUNING control to reposition tuning marker. Trigger another sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line (neglect deviations caused by tuning marker).
Maximum___ divisions
Minimum__ divisions
20. Subtract mean deviation of step 16 from maximum and minimum values recorded in step 19. Frequency response for $3-9 \mathrm{GHz}$ frequency band should not exceed $\pm 1.5 \mathrm{~dB}$ ( $\pm 1.5$ divisions).
Maximum __ divisions $(3-9 \mathrm{GHz})$
Minimum__ divisions $(3-9 \mathrm{GHz})$

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE (Cont'd)

21. Select $9-15 \mathrm{GHz}$ frequency band on spectrum analyzer. Set sweep oscillator to $\mathbf{C W}$ and frequency to 12.0 GHz . Use CW control to center signal on spectrum analyzer display. Trigger a 6 GHz sweep. Adjust spectrum analyzer TUNING control to reposition tuning marker. Trigger another sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line (neglect deviations caused by tuning marker).
Maximum ___ divisions
Minimum ___ divisions
22. Subtract mean deviation of step 16 from maximum and minimum values recorded in step 21. Frequency response for $9-15 \mathrm{GHz}$ frequency band should not exceed $\pm 1.8 \mathrm{~dB}$ ( $\pm 1.8$ divisions).
Maximum ___ divisions $(9-15 \mathrm{GHz})$
Minimum ___ divisions $(9-15 \mathrm{GHz})$
23. Select $6-15 \mathrm{GHz}$ frequency band on spectrum analyzer. Set sweep oscillator to $\mathbf{C W}$ and frequency to 10.5 GHz . Use $\mathbf{C W}$ control to center signal on spectrum analyzer display. Set AF control for 9 GHz and trigger a sweep. Adjust spectrum analyzer TUNING control several turns to reposition tuning marker. Trigger another sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line (neglect deviations caused by tuning marker).
Maximum ___ divisions
Minimum ___ divisions
24. Subtract mean deviation of step 16 from maximum and minimum values recorded in step 23. Frequency response for 6-15 GHz frequency band should not exceed $\pm 2.1 \mathrm{~dB}$ ( $\pm 2.1$ divisions).
Maximum___ $\quad$ divisions $(6-15 \mathrm{GHz})$
Minimum___ divisions $(6-15 \mathrm{GHz})$
25. Select $12.1-21 \mathrm{GHz}$ frequency band on spectrum analyzer and adjust TUNING control fully clockwise. Set sweep oscillator to $\mathbf{C W}$ and frequency to 15 GHz . Set AF control for 6 GHz and trigger a sweep. Record greatest positive and greatest negative deviation of signal peaks from center horizontal graticule line (12.1 GHz to 18 GHz ).
Maximum ___ divisions
Minimum___ divisions

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE (Cont'd)

26. Subtract mean deviation of step 16 from maximum and minimum values recorded in step 25. Frequency response for $12.1-18 \mathrm{GHz}$ portion of $12.1-21 \mathrm{GHz}$ frequency band should not exceed $\pm 2.3 \mathrm{~dB}( \pm 2.3$ divisions).
Maximum ___ divisions $(12.1-18 \mathrm{GHz})$
Minimum ___ divisions $(12.1-18 \mathrm{GHz})$

## Frequency Response, 18 - 21 GHz

27. Disconnect power splitter from $20-\mathrm{dB}$ attenuator and connect it to the power sensor. Set sweep oscillator to CW with frequency of 18.0 GHz and measure output at power splitter with power meter.
$\qquad$
28. Use CW control to slowly tune sweep oscillator from 18 GHz to 21 GHz . Note all peak deviations from reference power level (recorded in step 27) and the frequencies at which they occur. Record frequencies and power levels in Table 4-7.
29. Connect output of power splitter through $20-\mathrm{dB}$ attenuator to spectrum analyzer input. Adjust spectrum analyzer TUNING control counterclockwise several turns. Use CW control to tune sweep oscillator to frequencies recorded in step 28 and record deviation of signal peak from center horizontal graticule line.
30. Set sweep oscillator to $\mathbf{C W}$ with frequency of 19.5 GHz . Set AF control for 3 GHz and trigger a sweep. Note greatest positive and greatest negative deviation of signal peaks ( 18 GHz to 21 GHz ). Use sweep oscillator CW control to tune to points of greatest deviation. Record frequencies and deviations from center horizontal graticule line in Table 4-7.
31. Disconnect power splitter from $20-\mathrm{dB}$ attenuator and connect it to the power sensor. Use $\mathbf{C W}$ control to tune sweep oscillator to frequencies recorded in step 30 and record power levels in Table 4-7.
32. Algebraically subtract reference power level recorded in step 27 from each power meter indicated recorded in Table 4-7. Record results in Power Deviation column (see example). Add corresponding deviation from center horizontal graticule line to each power deviation and record results in Sum of Deviations column. Subtract mean deviation of step 16 from each value in Sum of Deviations column and record results in Deviation from Mean column. Frequency response for $18-21 \mathrm{GHz}$ portion of $12.1-21 \mathrm{GHz}$ frequency band should not exceed $\pm 3.0 \mathrm{~dB}$ ( $\pm 3$ divisions).

## PERFORMANCE TESTS

## 4-19. FREQUENCY RESPONSE (Cont'd)

TABLE 4.7. CORRECTINGFOR FREQUENCY RESPONSEOF SIGNALSOURCE

*deviation relative to power meter indication at 18.0 GHz , recorded in step 27.

EXAMPLE(MEAN DEVIATIONOF -0.1dB)

| Frequency <br> (GHz) | Power Meter <br> Indication <br> $\mathbf{( d B m})$ | Power <br> Deviation <br> (dB) | Deviation from <br> Center Graticule <br> Line (divisions <br> or dB) | Sum of <br> Deviations <br> (dB) | Deviation <br> from Mean <br> (dB) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 18.0 | -8.0 | $\mathbf{0}$ (Ref.) | -0.4 | -0.4 | -0.3 |
| 18.6 | -9.0 | -1.0 | -1.0 | -2.0 | -1.9 |
| 19.6 | -8.5 | -0.5 | -1.0 | -1.5 | -1.4 |
| 20.1 | -7.0 | +1.0 | 0.0 | +1.0 | +1.1 |
| 21.8 | -9.0 | -1.0 | -0.4 | -1.4 | -1.3 |
| 20.6 | -8.5 | -0.5 | -2.0 | -2.5 | -2.4 |
| 21.2 | -7.5 | +0.5 | +1.5 | +2.0 | +2.1 |

## PERFORMANCE TESTS

### 4.20. GAIN COMPRESSION

## SPECIFICATION:

Gain compression is less than 0.5 dB for a -10 dBm input level with 0 dB attenuation.

## DESCRIPTION:

Gain compression is measured by changing the power level at the spectrum analyzer input from -20 dBm to -10 dBm . The displayed signal level will change by less than 10 dB , indicating gain compression in the input mixer. Since a $10-\mathrm{dB}$ change in IF gain is used to keep the signal trace near the same point on the display when the input power is increased, the error due to this IF gain change is first measured, then subtracted from the displayed deviation to give the deviation due only to gain compression.


FIGURE4-16. GAINCOMPRESSIONTESTSETUP

EQUIPMENT:

| Signal Generator | HP 8640B |
| :---: | :---: |
| Power Meter . | HP 435A/B |
| Power Sensor | HP 8481A |
| Power Splitter | HP 11667A, Opt. C16 |
| 20-dB Attenuator | HP 8491B, Opt. 010 |
| Adapter, Type $\mathrm{N}(\mathrm{m})$ to BNC (f) (2 required). | HP 1250-0780 |
| Adapter, Type $\mathrm{N}(\mathrm{f})$ to $\mathrm{N}(\mathrm{f})$ | HP 1250-1472 |

## PERFORMANCE TESTS

## 4-20. GAIN COMPRESSION (Cont'd)

## PROCEDURE:

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... 0.050 GHz
FREQ SPAN/DIV ..... 100 kHz
RESOLUTION BW 300 kHz , uncoupled
INPUTATTEN ..... 10 dB
REFERENCE LEVEL ..... 10 dBm
REFLEVELFINE ..... $-10$
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALT IF ..... OFF
SIGIDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF
Signal Generator:
COUNTERMODE ..... INT
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 50 MHz
RF ..... ON
OUTPUTLEVEL ..... $-4 \mathrm{dBm}$
2. Connect equipment as shown in Figure $4-16$. Note that the $10-\mathrm{dB}$ attenuator is placed between the power splitter and spectrum analyzer INPUT $50 \Omega$ connector.
3. Adjust signal generator OUTPUT LEVEL control for a power meter reading of $-10 \mathrm{dBm}(-20 \mathrm{dBm}$ at spectrum analyzer INPUT $50 \Omega$ connector).
4. Adjust spectrum analyzer TUNING control to center 50 MHz signal on CRT. Set Amplitude Scale control to $1 \mathrm{~dB} / \mathrm{DIV}$ and adjust REF LEVEL FINE control to place peak of signal at a convenient horizontal graticule line other than top graticule line.
5. Adjust signal generator OUTPUT LEVEL control for a power meter reading of $0 \mathrm{dBm}(-10 \mathrm{dBm}$ at spectrum analyzer INPUT 50及 connector).
6. Set spectrum analyzer REFERENCE LEVEL control to 0 dBm , leaving REF LEVEL FINE control at setting established in step 4. Record deviation of signal peak from reference graticule line of step 4 (stepgain error). Values above reference line are positive ( + ); those below are negative ( - ).

## PERFORMANCE TESTS

## 4-20. GAIN COMPRESSION(Cont'd)

7. Adjust signal generator OUTPUT LEVEL control for a power meter reading of $-10 \mathrm{dBm}(-20 \mathrm{dBm}$ at spectrum analyzer 50Qconnector).
8. Set spectrum analyzer INPUT ATTEN control to 0 dBm , REFERENCE LEVEL control to -20 dBm , and REF LEVEL FINE control to 0 . Adjust REF LEVEL CAL control to place peak of signal at reference graticule line of step 4 .
9. Adjust signal generator OUTPUT LEVEL control for a power meter reading of $0 \mathrm{dBm}(-10 \mathrm{dBm}$ at spectrum analyzer 50Qconnector).
10. Set spectrum analyzer REFERENCE LEVEL control to - 10 dBm . Record deviation of signal peak from reference graticule line of step 4 .
11. Calculate gain compression by algebraically subtracting step-gain error (step 4) from deviation of signal peak (step 7). Gain compression should be less than 0.5 dB ,
$\qquad$ dB
12. Set spectrum analyzer INPUT ATTEN control to 10 dB and REFERENCE LEVEL control to -10 dBm . Connect CAL OUTPUT to INPUT $50 \Omega$ connector and recalibrate REF LEVEL CAL control setting.

## PERFORMANCE TESTS

## 4-21. BANDWIDTH SWITCHING (AMPLITUDE VARIATION)

## SPECIFICATION:

Bandwidths 3 MHz to $300 \mathrm{kHz}: \quad< \pm 0.5 \mathrm{~dB}$
Bandwidths 3 MHz to $1 \mathrm{kHz}: \quad< \pm 1.0 \mathrm{~dB}$

## DESCRIPTION:

The CAL OUTPUT signal is applied to INPUT $50 \Omega$ connector and displayed on CRT. The peak of displayed $35-\mathrm{MHz}$ signal is centered on CRT and adjusted for a vertical deflection of several divisions. The amplitude variation of the signal is measured for each RESOLUTION BW control setting. The overall variation between RESOLUTION BW settings of 3 MHz through 300 kHz should be less than 1.0 dB ( $\pm 0.5 \mathrm{~dB}$ ). The overall variation between RESOLUTION BW settings of 3 MHz through 1 kHz should be less than $2.0 \mathrm{~dB}( \pm 1.0 \mathrm{~dB})$.

## PROCEDURE:

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... 0.035 GHz
FREQ SPAN/DIV ..... 1 MHz
RESOLUTION BW ..... oupled
INPUT ATTEN ..... 10 dB
REFERENCE LEVEL ..... 0 dBm
REFLEVELFINE ..... $-10$
Amplitude Scale ..... $1 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF
2. Connect CAL OUTPUT signal to INPUT $50 \Omega$ connector.
3. Adjust TUNING control to center $35-\mathrm{MHz}$ signal on CRT.
4. Adjust REF LEVEL FINE control to position peak of signal seven divisions above graticule baseline.
5. Set RESOLUTION BW and FREQ SPAN/DIV controls to settings indicated in Table 4-8. Record deviation of signal peak from referencegraticule line for each RESOLUTION BW control setting. Values above reference line set in step 4 are positive $(+)$; values below reference line are negative $(-)$.
6. To find overall variation in Table 4-8, algebraically subtract greatest negative amplitude deviation from greatest positive amplitude deviation. If all changes in amplitude are of the same sign, overall variation is largest positive or largest negative change in amplitude. Overall variation between 3 MHz and 300 kHz RESOLUTION BW setting should be $<1.0 \mathrm{~dB}( \pm 0.5 \mathrm{~dB})$. Overall variation between 3 MHz and 1 kHz RESOLUTION BW settings should be $<2.0 \mathrm{~dB}( \pm 1.0 \mathrm{~dB})$.

## PERFORMANCE TESTS

## 4-21. BANDWIDTH SWITCHING (AMPLITUDE VARIATION)(Cont'd)

TABLE 4.8. BANDWIDTHSWITCHING (AMPLITUDE VARIATION)

| $\begin{gathered} \text { RESOLUTION } \\ \text { BW } \\ \text { Setting } \end{gathered}$ | FREQ SPAN/DIV Setting | Amplitude Deviation (dB) | Overall Variation Between 3 MHz and 300 kHz RESOLUTION BW Settings (dB) | Overall Variation Between 3 MHz and 1 kHz RESOLUTION BW Settings (dB) |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} 3 \mathrm{MHz} \\ 1 \mathrm{MHz} \\ 300 \mathrm{kHz} \end{array}$ | $\begin{array}{r} 1 \mathrm{MHz} \\ 500 \mathrm{kHz} \\ 100 \mathrm{kHz} \end{array}$ | $\qquad$ | $\qquad$ |  |
| 100 kHz 30 kHz 10 kHz $\mathbf{3 k H z}$ 1 kHz | 50 kHz <br> 10 kHz <br> 10 kHz <br> 10 kHz <br> 10 kHz |  |  |  |

## PERFORMANCE TESTS

## 4-22. INPUT ATTENUATOR ACCURACY

## SPECIFICATION

Step Accuracy ( 0 dB to 60 dB ): $\quad< \pm 1.0 \mathrm{~dB}$ per $10-\mathrm{dB}$ step, 0.01 to 18.0 GHz Maximum CumulativeStep Error ( 0 dB to 60 dB ): $\quad< \pm 2.4 \mathrm{~dB}, 0.01$ to 18.0 GHz

## DESCRIPTION

The input attenuator accuracy is tested over the range of 0 to 60 dB using an RF substitution method. A step attenuator that has been calibrated at 30 MHz by a Standards Laboratory is used for substitution. The known error of the calibrated attenuator is taken into account when computing the input attenuator accuracy.


FIGURE4-17. INPUT ATTENUATOR ACCURACY TESTSETUP

## EQUIPMENT:

| Signal Generator | HP 8640B |
| :---: | :---: |
| Step Attenuator ( $10 \mathrm{~dB} /$ step) | HP 355D, Opt. H82 |
| 10-dB Attenuator | HP 8491B, Opt. 010 |
| Adapter, Type N (m) to BNC (f) (2 required) | HP 1250-0780 |

## PERFORMANCE TESTS

## 4-22. INPUT ATTENUATOR ACCURACY (Cont'd)

## PROCEDURE:

1. Connect equipment as shown in Figure 4-17 and set controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $01-3$
TUNING . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 30 MHz
FREQ SPAN/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 2 MHz
RESOLUTIONBW .............................................................................. 1 MHz
INPUTATTEN . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 60 dB
REFERENCELEVEL . . . ............................................................................... 0 dBm
REFLEVELFINE ....................................................................................... . . . 0
Amplitude Scale . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 10 dB dDIV
SWEEP TIME/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . AUTO
SWEEPTRIGGER . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . FREE RUN
ALTIF .............................................................................................. OFF

BLCLIP . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . OFF
VIDEOFILTER . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 2 o'clock
Signal Generator:
COUNTER MODE INT EXPAND X10
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 30.0 MHz
RF .....  ON
OUTPUTLEVEL ..... 0 dBm
2. Set step attenuator to 0 dB and use spectrum analyzer TUNING control to center 30 MHz signal from signal generator on CRT display. Set FREQ SPAN/DIV to 20 kHz , RESOLUTION BW to 10 kHz , and Amplitude Scale to $1 \mathrm{~dB} / \mathrm{DIV}$.
3. Adjust signal generator OUTPUT LEVEL control to position peak of signal seven divisions above graticule baseline.
4. Set step attenuator and INPUT ATTEN control to settings indicated in Table 4-9. For each setting, record deviation of signal peak from reference graticule line set in step 3 .

## NOTE

The REFERENCE LEVEL control setting changes by 10 dB for every $10-\mathrm{dB}$ change in INPUT ATTEN. Do not change the REFERENCE LEVEL setting after changing the INPUT ATTEN setting.

## PERFORMANCE TESTS

### 4.22. INPUT ATTENUATOR ACCURACY (Cont'd)

TABLE 4-9. INPUT ATTENUATOR ACCURACY

| INPUT ATTEN Setting (dB) | Step Attenuator Setting (dB) | Amplitude Deviation (dB) | Step Attenuator Error (Calibration)" | Corrected Deviation (dB) |
| :---: | :---: | :---: | :---: | :---: |
| 60 | 0 | 0 (Ref) | (Ref) | 0 (Ref) |
| 50 | 10 |  | - |  |
| 40 | 20 |  |  |  |
| 30 | 30 |  |  | - |
| 20 | 40 |  |  |  |
| 10 | 50 |  |  |  |
| 0 | 60 |  |  |  |
| *Attenuations > dial settings are positive ( + ). Attenuations < dial settings are negative ( - ). For example, 9.99 dB calibration for a $\mathbf{1 0 ~ d B}$ attenuator setting represents an error of $\mathbf{- 0 . 0 1} \mathbf{d B}$. |  |  |  |  |

5. To compute corrected deviation for each setting, add step attenuator error to amplitude deviation. Corrected deviation should not exceed $\pm 1.0 \mathrm{~dB}$ between any two adjacent INPUT ATTEN setting.
$\qquad$ dB Maximum Error per 10-dB Step
6. Record maximum positive and maximum negative corrected deviation values. Difference between these two values (maximum cumulative step error) should not exceed 2.4 dB .
$\qquad$ dB Maximum PositiveCorrected Deviation
$\qquad$ dB Maximum Negative Corrected Deviation
$\qquad$ dB Maximum Cumulative Step Error

## PERFORMANCE TESTS

## 4-23. REFERENCE LEVEL ACCURACY

## SPECIFICATION:

Step Accuracy (steps referenced with 0 dB input attenuation):
-10 dBm to $-80 \mathrm{dBm}: \quad \pm 0.5 \mathrm{~dB}$
-10 dBm to $-100 \mathrm{dBm}: \pm 1.0 \mathrm{~dB}$
Vernier Accuracy: $\pm 0.5 \mathrm{~dB}$

## DESCRIPTION:

The reference level accuracy is tested over the range of -10 dBm to -100 dBm by checking the IF gain steps in $1 \mathrm{~dB} /$ DIV (Log) and in LIN. The resulting maximum deviation in each case must be less than $\pm 0.5 \mathrm{~dB}$ from -10 dBm to -80 dBm and less than $\pm 1.0 \mathrm{~dB}$ from -10 dBm to -100 dBm .


FIGURE4-18. REFERENCELEVELACCURACYTEST SETUP

## EQUIPMENT:

Signal Generator HP 8640B
10-dB Attenuator ..... HP 8491B, Opt. 010
Step Attenuator ( $1 \mathrm{~dB} /$ step)
Step Attenuator ( $10 \mathrm{~dB} /$ step) ..... HP 355D, Opt. H82
Adapter, Type $\mathrm{N}(\mathrm{m})$ to BNC (f) (2 required) ..... HP 1250-0780

## PERFORMANCE TESTS

## 4-23. REFERENCE LEVEL ACCURACY (Cont'd)

## PROCEDURE:

## Step Accuracy in Log Mode

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... 30 MHz
FREQ SPAN/DIV ..... 100 kHz
RESOLUTION BW ..... 30 kHz , uncoupled
INPUTATTEN ..... 0 dB
REFERENCE LEVEL ..... $-10 \mathrm{dBm}$
REFLEVELFINE ..... 0
Amplitude Scale ..... $1 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... 2 o'clock
Signal Generator:
COUNTERMODE INT, EXPAND X10
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 30 MHz
RF ..... ON
OUTPUTLEVEL ..... $-2 \mathrm{dBm}$
2. Connect equipment as shown in Figure $4-18$ using $10-\mathrm{dB}$ step attenuator. Set step attenuator to 0 dB and adjust spectrum analyzer TUNING control to center 30 MHz signal on CRT Set FREQ SPAN/DIV control to 10 kHz and RESOLUTION BW control to 3 kHz , adjusting TUNING control as necessary to keep signal centered on CRT
3. Adjust signal generator OUTPUT LEVEL control to position peak of signal 6 divisions above graticule baseline. Set step attenuator and spectrum analyzer REFERENCE LEVEL control to settings indicated in Table 4-10. Record deviation of signal peak from 6th division for each setting.
4. To calculate Corrected Deviation, add Step Attenuator Error (calibration data at 30 MHz ) to Deviation from 6th Division for each setting. Corrected Deviation should not exceed $\pm 0.5 \mathrm{~dB}$ from -10 dBm to -80 dBm , and should not exceed $\pm 1.0 \mathrm{~dB}$ from -10 dBm to -100 dBm . Record maximum values.


## PERFORMANCE TESTS

## 4-23. REFERENCE LEVEL ACCURACY (Cont'd)

TABLE4-10. IFGAIN ACCURACYIN LOG MODE

| REFERENCE LEVEL Setting (dBm) | Step Attenuator Setting (dB) | Deviation from 6th Division (dB) | Step Attenuator Error (Calibration)" (dB) | Corrected Deviation (dB) |
| :---: | :---: | :---: | :---: | :---: |
| -10 | 0 | 0 (Ref) | (Ref) | 0 (Ref) |
| -20 | 10 |  |  |  |
| -30 | 20 |  | - |  |
| -40 | 30 |  | - |  |
| -50 | 40 |  | - |  |
| -60 | 50 | - |  |  |
| -70 | 60 |  | - |  |
| -80 | 70 |  |  |  |
| -90 | 80 |  |  |  |
| -100 | 90 |  |  |  |

## Step Accuracy in Linear Mode

5. Set spectrum analyzer Amplitude Scale switch to LIN and REFERENCE LEVEL control to -10 dBm . Set step attenuator to 0 dB . Readjust signal generator OUTPUT LEVEL control to position peak of signal 6 divisions above graticule baseline.
6. Set step attenuator and spectrum analyzer REFERENCE LEVEL control to settings indicated in Table 4-11. Record deviation of signal peak from 6th division for each setting.
7. Using Table 4-12, convert Deviation from 6th Division in Linear Mode to Deviation in dB for each setting. Record dB values in Table 4-11.
8. To calculate Corrected Deviation, add Step Attenuator Error to Deviation from 6th Division in dB for each setting. Corrected Deviation should not exceed $\pm 0.5 \mathrm{~dB}$ from -10 dBm to -80 dBm and $\pm 1.0 \mathrm{~dB}$ from -10 dBm to -100 dBm . Record maximum values.

$$
\begin{aligned}
& \text { 工 } \\
& \mathrm{dB}(-10 \mathrm{dBm} \text { to }-80 \mathrm{dBm}) \\
& \mathrm{dB}(-10 \mathrm{dBm} \text { to }-100 \mathrm{dBm})
\end{aligned}
$$

## PERFORMANCE TESTS

4-23. REFERENCELEVEL ACCURACY (Cont'd)
TABLE4.11. IFGAIN ACCURACYIN LINEAR MODE

| REFERENCE LEVEL Setting (dBm) | Step Attenuator Setting (dB) | Deviation from 6th Division Linear Mode (div.) | Deviation from 6th Division in dB* | Step Attenuator Error (Calibration)**(dB) | Corrected Deviation (dB) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| -10 | 0 | 0 (Pef.) | 0 (Pef.) | Ref. | 0 (Pef.) |
| -20 | 10 | $\underline{-}$ |  | - |  |
| -30 | 20 |  |  |  |  |
| -40 | 30 |  |  |  |  |
| -50 | 40 |  |  |  |  |
| -60 | 50 | - | $\square$ | $\longrightarrow$ | - |
| -70 | 60 |  |  |  |  |
| -80 | 70 |  |  |  |  |
| -90 | 80 |  |  |  |  |
| -100 | 90 |  |  |  |  |

*Use Table 4-12 to convert deviation in linear mode to deviation in dB.
${ }^{* *}$ Attenuations $>$ dial settings are positive ( + ). Attenuations $<$ dial settings are negative ( - ).

TABLE 4-12. CONVERSIONTABLE, DEVIATION IN LINEAR MODE

| POSITIVE DEVIATIONS <br> (Above 6th division from graticule baseline) |  | NEGATIVE DEVIATIONS <br> (Below 6th division from graticule baseline) |  |
| :---: | :---: | :---: | :---: |
| Linear (Divisions) | dB | Linear (Divisions) | dB |
| 0 | 0 | 0 | 0 |
| +.1 | +0.14 | -.1 | -0.15 |
| +.2 | +0.28 | -.2 | -0.29 |
| +.3 | +0.42 | -.3 | -0.45 |
| +.4 | +0.56 | -.4 | -0.60 |
| +.5 | +0.70 | -.5 | -0.76 |
| +.6 | +0.82 | -.6 | -0.92 |
| +.7 | +0.96 | -.7 | -1.08 |
| +.8 | +1.09 | -.8 | -1.24 |
| +.9 | +1.21 | -.9 | -1.41 |
| +1.0 | +1.34 | -1.0 | -1.58 |
| +1.1 | +1.46 | -1.1 | -1.76 |
| +1.2 | +1.58 | -1.2 | -1.94 |
| +1.3 | +1.70 |  |  |
| +1.4 | +1.82 |  |  |
| +1.5 | +1.94 |  |  |

## PERFORMANCE TESTS

## 4-23. REFERENCE LEVEL ACCURACY (Cont'd)

## Vernier Accuracy

9. Replace $10-\mathrm{dB}$ step attenuator with $1-\mathrm{dB}$ step attenuator. Set spectrum analyzer controls as follows:

| FREQUENCY BAND GHz | . $01-3$ |
| :---: | :---: |
| TUNING | 0.030 GHz |
| FREQ SPAN/DIV | 50 kHz |
| RESOLUTIONBW | 300 kHz , uncoupled |
| INPUTATTEN | . 0 dB |
| REFERENCE LEVEL | $-10 \mathrm{dBm}$ |
| REFLEVELFINE | 0 |
| AmplitudeScale | $1 \mathrm{~dB} / \mathrm{DIV}$ |
| SWEEP TIME/DIV | ... AUTO |
| SWEEPTRIGGER | FREE RUN |
| ALT IF | . . OFF |
| SIGIDENT | . OFF |
| BLCLIP | OFF |
| VIDEOFILTER | 2 o'clock |

10. Set step attenuator to 0 dB . Center signal on CRT and adjust signal generator OUTPUT LEVEL control to position peak of signal 6 divisions above graticule baseline. Set step attenuator and spectrum analyzer REFERENCE LEVEL FINE control to settings indicated in Table 4-13. Record deviation of signal peak from 6th division for each setting.
11. To compute Corrected Deviation, add Step Attenuator Error to Deviation from 6th Division for each setting. Corrected Deviation should not exceed $\pm 0.5 \mathrm{~dB}$ for each setting. Record maximum value.

TABLE 4-13. VERNIER ACCURACY

| Step Attenuator Setting (dB) | REFERENCE LEVEL FINE Setting | Deviation from 6th Division (dB) | Step Attenuator Error (Calibration)* (dB) | Corrected Deviation (dB) |
| :---: | :---: | :---: | :---: | :---: |
| 0 | 0 | 0 (Ref) | (Ref) | 0 (Ref) |
| 1 | -1 |  |  |  |
| 2 | -2 |  |  |  |
| 3 | -3 |  |  |  |
| 4 | -4 |  |  |  |
| 5 | -5 |  |  |  |
| 6 | -6 |  |  |  |
| - 7 | -7 |  |  |  |
| 8 | -8 |  |  |  |
| 9 | -9 |  |  |  |
| 10 | -10 |  |  |  |
| 11 | -11 |  |  |  |
| 12 | -12 |  |  |  |

[^3]
## PERFORMANCE TESTS

## 4-24. SWEEP TIME ACCURACY

## SPECIFICATION:

There are 20 selectable and calibrated sweep times in a $1-2-5$ sequence from $2 \mu \mathrm{sec} / \mathrm{DIV}$ to $10 \mathrm{sec} / \mathrm{DIV}$ (excluding $2 \mathrm{sec} /$ DIV).

Sweep time accuracy: $\pm 10 \%$ ( $\pm 20 \%$ for 5 and $10 \mathrm{sec} /$ DIV)

## DESCRIPTION:

For SWEEP TIME/DIV control settings of 10 msec and less, the triangle-wave output of a function generator is used to modulate a $100-\mathrm{MHz}$ signal applied to the spectrum analyzer input. This signal is demodulated in zero span, displaying a triangular waveform on the CRT. The function genertor is tuned to align the waveform with the vertical CRT graticule lines. The period of the function generator output is then measured with a counter to determine the sweep time.
For SWEEP TIME/DIV control settings of 20 msec and greater, the display (AUX B) PENLIFT/BLANKING output is connected directly to the counter. The blanking signal is "low" during a spectrum analyzer sweep; the time interval between the falling and rising edges is measured to determine the sweep speed.


## EQUIPMENT:

| Signal G | HP 8640B |
| :---: | :---: |
| Function Generator | HP 3310A |
| 50 MHz Universal Counter | HP 5300B/5302A |
| BNC Tee | HP 1250-0781 |
| Cable Assembly RG-214/U | HP 11500A |

## PERFORMANCE TESTS

## 4-24. SWEEP TIME ACCURACY (Cont'd)

## PROCEDURE:

1. Set equipment controls as follows:
Spectrum Analyzer:
FREQUENCY BAND GHz ..... 01-3
TUNING ..... 0.100 GHz
FREQ SPAN/DIV ..... 10 MHz
RESOLUTIONBW 3 MHz , uncoupled
INPUTATTEN ..... 10 dB
REFERENCELEVEL ..... $-10 \mathrm{dBm}$
REFLEVELFINE ..... 0
AmplitudeScale ..... LIN
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIGIDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF
Signal Generator:
COUNTERMODE INT, EXPAND X10
AM ..... OFF
FM ..... 100 MHz
FREQUENCYTUNE ..... ON
OUTPUT LEVEL ..... $-10 \mathrm{dBm}$
Function Generator:
FUNCTION ..... TRI
RANGE ..... 10K
Frequency ..... 250 kHz
DCOFFSETLEVEL ..... 0
50 MHz Universal Counter:
FUNCTION ..... PERAVGB
SAMPLE RATE Full counterclockwiseTIME BASE
1 ms
SENSITIVITY (A) ..... 9 o'clock
A 50 MHz Input ..... (falling edge)SENSITIVITY (B)
B 10 MHz Input
$\square$ (rising edge)

## PERFORMANCE TESTS

## 4-24. SWEEP TIME ACCURACY (Cont'd)

2. Connect equipment as shown in Figure 4-19. Connect counter's B 10 MHz input to the function generator low output and the signal generator's AM input.
3. Adjust spectrum analyzer TUNING control to center $100-\mathrm{MHz}$ signal on CRT Set FREQ SPAN/DIV control to 0, leaving RESOLUTION BW control at 3 MHz setting. Set SWEEP TIME/DIV control to 2 $\mu \mathrm{sec}$.
4. Set AM switch of HP 8640B to AC position. Adjust function generator AMPLITUDE control and signal generator AM MODULATION control for 50 percent modulation as indicated on the signal generator meter.
5. Set spectrum analyzer SWEEP TRIGGER control to VIDEO. Adjust REFERENCE LEVEL and REF LEVEL FINE controls to center waveform on CRT
6. Adjust function generator Frequency vernier to display exactly five cycles of triangle wave modulation on CRT, as shown in Figure 4-20a. Counter should indicate an average period of $4.00 \pm 0.04 \mathrm{ps}$.


FIGURE 4-20. SWEEPTIME ACCURACY
7. Calculate actual sweep time per division by dividing average period from step 6 by 2 . Record value in Table 4-14.
8. For spectrum analyzer SWEEP TIME/DIV control settings of 5 psec through 10 msec , adjust function generator RANGE and frequency controls to display exactly 10 cycles of triangle wave modulation on CRT, as shown in Figure 4-20b. Average period readings displayed on counter correspond to actual sweep time per division. Record values in Table 4-14.

## PERFORMANCE TESTS

## 4-24. SWEEP TIME ACCURACY (Cont'd)

TABE 4-14. SWEEP TIME ACORACY, $2 \mu$ SEC THROUGH 10 MSEC

| SWEEP <br> TIME/DIV <br> Setting | Function <br> Generator <br> Frequency <br> (Approx.) | Sweep Time per Division |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Minimum | Actual | Maximum |
| 2 psec | 250 kHz | 1.80 psec | $\ldots$ - $\mu \mathrm{sec}$ | 2.20 psec |
| 5 psec | 200 kHz | 4.40 psec | $\ldots \mu \mathrm{sec}$ | 5.50 psec |
| 10 psec | 100 kHz | 9.00 psec | $\ldots \mathrm{sec}$ | 11.00 psec |
| 20 psec | 50 kHz | 18.00 psec | $\ldots$ - $\mu \mathrm{sec}$ | 22.00 psec |
| 50 psec | 20 kHz | 45.00 psec | $\ldots \mu \mathrm{sec}$ | 55.00 psec |
| . 1 msec | 10 kHz | 90.0 psec | - $\mu \mathrm{sec}$ | 110.0 psec |
| . 2 msec | 5 kHz | 180.0 psec | - $\mu \mathrm{sec}$ | 220.0 psec |
| . 5 msec | 2 kHz | 450.0 psec | _ $\mu \mathrm{sec}$ | 550.0 psec |
| 1 msec | 1 kHz | 900 psec | - $\mu \mathrm{sec}$ | 1100 psec |
| 2 msec | 500 Hz | 1800 psec | $\ldots \mu \mathrm{sec}$ | 2200 psec |
| 5 msec | 200 Hz | 4500 psec | $\ldots \mathrm{sec}$ | 5500 psec |
| 10 msec | 100 Hz | 9.00 msec | _ msec | 11.00 msec |

9. Connect display rear-panel AUX B PENLIFT/BLANKING output to BNC tee at counter's B 10 MHz input. Connect other side of tee to counter's A 50 MHz input.
10. Set counter controls as follows:

| FUNCTION | T.I. A to B |
| :---: | :---: |
| SAMPLE RATE | Full counterclockwise |
| TIME BASE | 0.1 ms |
| SENSITIVITY (A) | 9 o'clock |
| A 50 MHz Input | (falling edge) |
| SENSITIVITY (B) | 9 o'clock |
| B 10 MHz Input | L(rising edge) |

11. Set spectrum analyzer SWEEP TIME/DIV to 20 msec . Adjust counter's SENSITIVITY controls for a time interval reading of $0.2000 \pm 0.0200 \mathrm{sec}$. Record sweep time value in Table 4-15.
12. Verify remaining spectrum analyzer SWEEP TIME/DIV control settings of 50 msec through 10 sec , recording sweep time values in Table 4-15.

## PERFORMANCE TESTS

## 4-24. SWEEP TIME ACCURACY (Cont'd)

TABLE 4-15. SWEEPTIME ACCURACY,20 MSECTHROUGH10SEC

| WEEP TIME/DIV Setting | Sweep Time |  |  |
| :---: | :---: | :---: | :---: |
|  | Minimum | Actual | Maximum |
| 20 msec <br> 50 msec <br> .1 sec <br> .2 sec <br> .5 sec <br> 1 sec <br> 5 sec <br> 10 sec | $\begin{gathered} 0.180 \mathrm{sec} \\ 0.450 \mathrm{sec} \\ 0.90 \mathrm{sec} \\ 1.80 \mathrm{sec} \\ 4.50 \mathrm{sec} \\ 9.0 \mathrm{sec} \\ 40.0 \mathrm{sec} \\ 80.0 \mathrm{sec} \end{gathered}$ |  | $\begin{gathered} 0.220 \mathrm{sec} \\ 0.550 \mathrm{sec} \\ 1.10 \mathrm{sec} \\ 2.20 \mathrm{sec} \\ 5.50 \mathrm{sec} \\ 11.0 \mathrm{sec} \\ 60.0 \mathrm{sec} \\ 120.0 \mathrm{sec} \end{gathered}$ |

## PERFORMANCE TESTS

## 4-25. CALIBRATOR OUTPUT ACCURACY

## SPECIFICATION:

Amplitude: $\quad-10 \mathrm{dBm} \pm 0.3 \mathrm{~dB}$
Frequency: $35 \mathrm{MHz} \pm 400 \mathrm{kHz}$

## DESCRIPTION:

The frequency of the calibrator output signal is measured with a microwave counter. The calibrator output level is measured using a power meter.


FIGURE 4-21. CALIBRATOR ACCURACY TEST SETUP

## EQUIPMENT:

$$
\begin{aligned}
& \text { Frequency Counter .......................................................... HP 5342A, Opt. } 005 \\
& \text { Power Meter................................................................................. HP 435A/B } \\
& \text { Power Sensor . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . HP 8481A }
\end{aligned}
$$

## PROCEDURE:

1. Connect spectrum analyzer CAL OUTPUT to frequency counter's $10 \mathrm{~Hz}-500 \mathrm{MHz}(50 \Omega)$ input as shown in Figure 4-20. Measured output frequency should be $35 \mathrm{MHz} \pm 400 \mathrm{kHz}$.
2. Zero and calibrate power meter. Connect power sensor, through adapter, to spectrum analyzer's CAL OUTPUT and measure power level. Calibrator output level should be $-10 \mathrm{dBm} \pm 0.3 \mathrm{~dB}$.
$\qquad$

## PERFORMANCE TESTS

## 4-26. DISPLAY FIDELITY

## SPECIFICATION:

Log Incremental Accuracy: $\pm 0.1 \mathrm{~dB}$ per dB from Reference Level Log Maximum Cumulative Error: $< \pm 1.5 \mathrm{~dB}$ over entire $70-\mathrm{dB}$ range Linear Accuracy; $\pm 3 \%$ of Reference Level

## DESCRIPTION:

The amplitude of the log display amplifier is tested by connecting a DVM to the display (AUX A) VERTICAL OUTPUT connector. A wide resolution bandwidth setting is selected so the signal appears as a straight horizontal line on the CRT. The DVM is used to provide good resolution when checking for +1 dB per 10 dB step $(0.1$ $d B / d B)$.


## EQUIPMENT

Signal Generator
Digital Voltmeter
Step Attenuator ( $10 \mathrm{~dB} /$ step) ..... HP 355D, Opt. H82
Adapter, Type N(m) to BNC(f) (2 required) ..... HP 1250-0780
Cable, BNC to Banana Plug ..... HP 11001A

## PROCEDURE:

## Log Display Accuracy

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz .....  $01-3$
TUNING .............................................................................. 0.030 GHz

## PERFORMANCE TESTS

## 4-26. DISPLAY FIDELITY (Cont'd)

FREQ SPAN/DIV ..... 500 kHz
RESOLUTION BW ..... 300 kHz , uncoupled
INPUT ATTEN ..... 10 dB
REFERENCE LEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... LIN
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BL CLIP ..... OFF
VIDEO FILTER ..... OFF
Digital Voltmeter:
RANGE ..... 100
FUNCTION ..... V (DC)
AUTO CAL ..... AUTO
TRIGGER ..... INTERNAL
MATH ..... OFF
Signal Generator:
COUNTERMODE ..... INT
AM ..... OFF
FM ..... OFF
FREQUENCYTUNE ..... 30 MHz
RF ..... ON
OUTPUT LEVEL ..... 0 dBm
2. With no signal at spectrum analyzer's INPUT 5052, measure and record offset voltage at (AUX A) VERTICAL OUTPUT connector.
$\qquad$
mV
3. Connect equipment as shown in Figure 4-22. Set step attenuator to 0 dB .
4. Set spectrum analyzer's Amplitude Scale to $10 \mathrm{~dB} /$ DIV and adjust TUNING control to center signal on CRT display.
5. Set spectrum analyzer's FREQ SPAN/DIV control to zero (0), VIDEO FILTER full CW (not in detent), and RESOLUTION BW control to 1 MHz . Adjust TUNING control for maximum reading on DVM.
6. Set signal generator OUTPUT LEVEL control for DVM reading of $(+800 \mathrm{mV}+$ offset (step 2$) \pm 0.5$ mV ). Trace should be approximately at top CRT graticule line.
7. Record DVM readings for step attenuator settings, from 0 dB through 70 dB , in Table 4-16.

## PERFORMANCE TESTS

## 4-26. DISPLAY FIDELITY (Cont'd)

TABLE4-16. AMPLITUDELOG DISPLAY ACCURACY

| Attenuator Setting (dB) | DVM Reading (mV) | Corrected DVM Reading* (mV) | Theoretical Reading (mV) | Theoretical Reading Subtracted From Corrected DVM Reading (mV) | Difference <br> Between <br> Adjacent <br> Readings (mV) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  | +800 (Ref.) | +800 | 0 |  |
| 10 |  |  | +700 |  |  |
| 20 |  |  | +600 |  | - |
| 30 |  |  | +500 |  |  |
| 40 |  |  | +400 |  |  |
| 50 |  |  | +300 |  | - |
| 60 |  |  | +200 |  |  |
| 70 |  |  | +100 |  |  |

*DVM Reading minus offset recorded in step 2.

EXAMPLETABLEOF 4.16

| Attenuator <br> Setting <br> $\mathbf{( d B )}$ | DVM <br> Reading <br> $(\mathbf{m V})$ | Corrected <br> DVM <br> Reading <br> $(\mathbf{m V})$ | Theoretical <br> Reading <br> $(\mathbf{m V})$ | Theoretical <br> Reading Subtracted <br> From Corrected <br> DVM Reading <br> $(\mathbf{m V})$ | Difference <br> Between |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | +805 | +800 | +800 | 0 | Adjacent <br> Readings <br> $(\mathbf{m V})$ |
| 10 | +708 | +703 | +700 | +3 |  |
| 20 | +599 | +594 | +600 | -6 | -3 |
| 30 | +497 | +492 | +500 | -8 | +9 |
| 40 | +406 | +401 | +400 | +1 | +2 |

*DVM Reading minus offset recorded in step 2.
8. After recording DVM readings for step attenuator settings from 0 dB through 70 dB , calculate each Corrected DVM Reading by algebraically subtracting offset recorded in step 2. Record results in Table 4-16 (see sample computations).
9. Algebraically subtract corresponding Theoretical Reading from each Corrected DVM Reading, recording results in Table 4-16. Maximum value should not exceed $\pm 15 \mathrm{mV}$, corresponding to $\pm 1.5 \mathrm{~dB}$. Divide maximum value by 10 to calculate Log Maximum Cumulative Error (in dB).
$\qquad$ dB Log Maximum Cumulative Error

## PERFORMANCE TESTS

## 4-26. DISPLAY FIDELITY (Cont'd)

10. Algebraically subtract each converted reading (Theoretical Reading Subtracted from Corrected DVM Reading) from previous converted reading. Record results in Table 4-16 (see sample computations). Maximum difference between adjacent readings should not exceed +10 mV , corresponding to $\pm 1 \mathrm{~dB} / 10 \mathrm{~dB}$ or $\pm 0.1 \mathrm{~dB} / \mathrm{dB}$. Divide maximum value by 100 to calculate Log Incremental Error (in $\mathrm{dB} / \mathrm{dB}$ ).
$\qquad$ $\mathrm{dB} / \mathrm{dB}$ Log Incremental Error
11. Replace $10-\mathrm{dB}$ step attenuator with $1-\mathrm{dB}$ step attenuator. Set step attenuator to 0 dB .
12. Set spectrum analyzer Amplitude Scale to LIN and adjust TUNING control for maximum reading on DVM.
13. Adjust signal generator OUTPUT LEVEL for DVM reading of $800 \mathrm{mV}+$ offset (step 2 ) $\pm 0.5 \mathrm{mV}$. Trace should be approximately at top CRT graticule line.
14. Record DVM reading for step attenuator settings of 6 dB and 12 dB in Table 4-17.
15. Calculate each Corrected DVM Reading by algebraically subtracting offset recorded in step 2. Record results in Table 4-17.
16. Algebraically subtract corresponding Theoretical Reading from each Corrected DVM Reading, recording results in Table 4-17. Maximum value should not exceed $\pm 24 \mathrm{mV}$, corresponding to $\pm 3 \%$ of 800 mV Reference Level. Divide maximum value by 8 to calculate Percent Linear Error.
$\qquad$ \% of Reference Level Linear Error
TABLE4-17. AMPLITUDELINEARDISPLAY ACCURACY

| Attenuator <br> Setting <br> (dB) | DV M <br> Reading <br> $(\mathrm{mV})$ | Corrected <br> DVM <br> Reading <br> $(\mathbf{m V})$ | Theoretical <br> Reading <br> $(\mathbf{m V})$ | Theoretical <br> Reading Subtracted <br> From Corrected <br> DV M Reading <br> $(\mathrm{mV})$ |
| :---: | :---: | :---: | :---: | :---: |
| 0 | - | $+800($ Ref. $)$ | +800 <br> +401 <br> 6 <br> 6 <br> 12 | -201 |

*DVM Reading minus offset recorded in step 2.

TABLE4-18. PERFORMANCETESTRECORD (10F4)

Hewlett-Packard Company
Model 8559A
Spectrum Analyzer . $01-21 \mathrm{GHz}$

TABLE4-18. PERFORMANCETESTRECORD(2OF4)


TABLE 4-18. PERFORMANCE TESTRECORD(3OF 4)

| Para. No. | Test Description | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-18. | Residual Responses <br> 6. Residual Responses, Ol GHz to 3 GHz <br> 7. Residual Responses, Ol GHz to 3 GHz (ALT IF) |  |  |  |
|  |  |  |  | -90 dBm -90 dBm |
| 4-19. | Frequency Response <br> 15. Frequency Response, .01 to 3.0 GHz <br> 18. Frequency Response, 6.0 to 9.0 GHz <br> 20. Frequency Response, 3.0 to 9.0 GHz <br> 22. Frequency Response, 9.0 to 15.0 GHz <br> 24. Frequency Response, 6.0 to 15.0 GHz <br> 26. Frequency Response, 12.1 to 18.0 GHz <br> 32. Frequency Response, 18.0 to 21.0 GHz |  |  |  |
|  |  |  |  | $\pm 1.0 \mathrm{~dB}$ |
|  |  |  |  | $\pm 1.0 \mathrm{~dB}$ |
|  |  |  |  | $\pm 1.5 \mathrm{~dB}$ |
|  |  |  |  | $\pm 1.8 \mathrm{~dB}$ |
|  |  |  |  | $\pm 2.1 \mathrm{~dB}$ |
|  |  |  |  | $\pm 2.3 \mathrm{~dB}$ |
|  |  |  |  | $\pm 3.0 \mathrm{~dB}$ |
| 4-20. | Gain Compression |  |  |  |
|  | 11. Gain Compression |  |  | 0.5 dB |
| 4-21. | Bandwidth Switching (Amplitude Variation) |  |  |  |
|  | 6. 3 MHz to 300 kHz (overall variation) <br> 3 MHz to 1 kHz (overall variation) | $\begin{aligned} & -0.5 \mathrm{~dB} \\ & -1.0 \mathrm{~dB} \end{aligned}$ |  | $+0.5 \mathrm{~dB}$ |
|  |  |  |  | +1.0 dB |
| 4-22. | Input Attenuator Accuracy |  |  |  |
|  | 5. Maximum Error per $10-\mathrm{dB}$ step $(0 \mathrm{~dB}-60 \mathrm{~dB})$ <br> 6. Maximum Cumulative Step Error $(0 \mathrm{~dB}-60 \mathrm{~dB})$ | $-1.0 \mathrm{~dB}$ |  | +1.0 dB +2.4 dB |
| 4-23. | Reference Level Variation |  |  |  |
|  | 4. Reference Level Error in Log ( -10 dBm to -80 dBm ) | $-0.5 \mathrm{~dB}$ |  | $+0.5 \mathrm{~dB}$ |
|  | $(-10 \mathrm{dBm} \text { to }-100 \mathrm{dBm})$ <br> 8. Reference Level Error in LIN | $-1.0 \mathrm{~dB}$ |  | $+1.0 \mathrm{~dB}$ |
|  | ( -10 dBm to -80 dBm ) <br> Reference Level Error in LIN | $-0.5 \mathrm{~dB}$ |  | $+0.5 \mathrm{~dB}$ |
|  | ( -10 dBm to -100 dBm ) | $-1.0 \mathrm{~dB}$ |  | $+1.0 \mathrm{~dB}$ |
|  | 11. Vernier Error | $-0.5 \mathrm{~dB}$ |  | +0.5 dB |

TABLE4-18. PERFORMANCETESTRECORD (4OF4)


Bescelk

## SECTION V <br> ADJUSTMENTS

## 5-1. INTRODUCTION

5-2. This section describes the adjustments used to restore the HP 8559A to its peak operating condition after a repair or to compensate for changes resulting from component aging. Illustrations showing the appropriate test setups are included in the adjustment procedures. Table 5-1 lists all the adjustments by adjustment name, adjustment reference designator, and by the paragraph number of the adjustment procedure. Included in the table is a brief description of the purpose of the adjustment.

5-3. Data taken during an adjustment should be recorded in the spaces provided in the procedure. Comparison of initial data with data taken during later adjustments is useful for preventative maintenance and troubleshooting.

## WARNING

The adjustments in this section require the HP 8559A to be removed from the display mainframe and connected through an extender cable assembly. Be very careful; the energy at some points in the instrument will, if contacted, cause personal injury. The adjustments in this section should be performed only by a skilled person who knows the hazard involved.

## NOTE

Before performing any adjustments, allow 1 hour warmup time, unless otherwise noted.

## 5-4. EQUIPMENTREQUIRED

5-5. Test equipment and accessories required for the adjustment procedures are listed in Table 1-3. If the listed equipment is not available, substitute
equipment may be used provided it meets the minimum specifications given in the table.

## 5-6. Adjustment Tools

5-7. Required service accessories, with part numbers, are illustrated in Section I.

5-8. For adjustments that require a non-metallic tuning tool, use fiber tuning tool, HP Part Number 8710-0033 (check digit 4). When a non-metallic tuning tool is not required, you may use an ordinary small, flat-bladed screwdriver or other suitable tool. Regardless of the tool used, do not try to force any adjustment control. Slug-tuning inductors and variable capacitors, especially, are easily damaged by excessive force.

### 5.9. Extender Cable Installation

## WARNING

Disconnect display mainframe line power cord before installation of extender cable assembly.

5-10. Pull out the lock knob and slide the spectrum analyzer out of the display mainframe. If side stops are installed, refer to Section II for removal.

5-11. Carefully slide the extender cable assembly, HP Part Number 5060-0303, into the display mainframe, aligning the metal guide plate with the slotted side rails of the mainframe. Firmly seat the extender cable assembly to ensure good contact.
$5-12$. Connect the opposite end of the cable to the spectrum analyzer. The plug is keyed so it will go on correctly and will not make contact upside down. Remove the orange and the yellow leads from pins 3 and 4 on the A15 board at the rear of the spectrum analyzer. Connect the corresponding leads from the extender cable assembly to these pins by means of the insulated alligator clips.

## 5-13. RELATED ADJUSTMENTS

5-14. These adjustments should be performed when the troubleshooting information in Section VIII indicates that an adjustable circuit is not operating correctly. Perform the adjustments after repair or replacement of the circuit. The troubleshooting procedures and Table 5-2 specify the required adjustments.

## 5-15. FACTORY SELECTED COMPONENTS

$5-16$. Table 5-3 is a list of factory selected components used in the HP 8559A. The components are listed by reference designator, related adjustment paragraph, and by basis of selection. Factory selected components are identified by an asterisk (*) in the schematic diagrams in Section VIII and in the Replaceable Parts list in Section VIII. Part numbers for standard values of selected components are listed in Table 5-4.

TABLE 5-1. ADJUSTABLECOMPONENTS(10F3)

| Adjustment Name | Reference Designator | Adjustment Paragraph | Description |
| :---: | :---: | :---: | :---: |
| GAIN | A1A2R28 | 5-30 | Adjusts DPM high indication. |
| OFFSET | A1A2R29 | 5-30 | Adjusts DPM low indication. |
| 2nd MIXER MATCH | A5L2 | $5-26$ | Adjusts Second Converter output match. |
| Z1 | A5Z1 | 5-26 | Adjusts First IF Bandpass Filter Response. |
| Z2 | A5Z2 | 5-26 | Adjusts First IF Bandpass Filter Response. |
| Z3 | A5Z3 | 5-26 | Adjusts First IF Bandpass Filter Response. |
| 2nd LO FREQUENCY | A5Z4 | 5-26 | Adjusts Second LO Frequency. |
| 3 GHz | A7R8 | 5-25 | Adjusts YTO low-end frequency. |
| - lov | A7R29 | 5-17 | Adjusts -lOV Power Supply output. |
| +14.5V | A7R41 | 5-17 | Adjusts +14.5V Power Supply output. |
| 6 GHzC | A7R47 | 5-25 | Coarse adjusts YTO high-end frequency. |
| 6 GHz F | A7R75 | 5-25 | Fine adjusts YTO high-end frequency. |
| MO | A7R81 | 5-25 | Adjusted to optimize centering between wide and narrow frequency spans. |
| DC | A7R83 | 5-25 | Adusts delay compensation. |
| FM | A7R92 | 5-25 | Adjusts YTO linearity. |
| REG | A8R34 | 5-26 | Adjusts varactor bias voltage for proper Second LO Shift between Regular and Alternate IF. |
| OFF | A8R39 | 5-26 | Adjusts varactor bias voltage (offset) for Second LO frequency with Regular IF. |
| SIG ID | A8R40 | 5-26 | Adjusts Second LO shift for signal identifier 1 MHz below signal. |
| DPM ZERO | A8R61 | $5 \cdot 30$ | Adjusts DPM Driver output for OV with OV input (offset adjustment). |
| Vo | A8R62 | 5.17 | Adjusts varactor bias voltage (offset) with Alternate IF |
| $+10 \mathrm{~V}$ | A9R2 | 5-17 | Adjusts +10V Power Supply output. |
| 1 ms | A9R10 | 5-18 | Adjusts sweep ramp to calibrate $1 \mathrm{~ms} /$ DIV sweep time. |
| 5 ms | A9R13 | 5-18 | Adjusts sweep ramp to calibrate $5 \mathrm{~ms} / \mathrm{DIV}$ sweep time. |
| XTL | A9R72 | 5-21, 5-22 | Adjusts 3 kHz IF bandwidth. |
| LC | A9R85 | 5-21, 5-22 | Adjusts 1 MHz IF bandwidth. |
| C9 | A10C9 | 5-27 | Adjusts Second IF Bandpass Filter Response. |
| C10 | A10C10 | 5-27 | Adjusts Second IF Bandpass Filter Response. |
| C11 | A10C11 | 5-27 | Adjusts Second IF Bandpass Filter Response. |
| C12 | A10C12 | 5-27 | Adjusts Second IF Bandpass Filter Response. |
| CAL FREQ | A10C46 | 5-29 | Adjusts CAL OUTPUT frequency. |
| LO ADJ | A10L12 | 5-27 | Adjusts Third LO frequency. |
| CAL AMPL | A10R13 | $5 \cdot 29$ | Adjusts CAL OUTPUT amplitude. |
| SYM | A11C15 | 5-21 | Adjusts symmetry of first crystal bandwidth filter stage. |
| LC CTR | A11C23 | $5-21$ | Adjusts centering of first LC bandwidth filter stage. |
| CTR | A11C25 | 5-21 | Adjusts centering of first crystal bandwidth filter stage. |

TABLE5-1. ADJUSTABLECOMPONENTS(2OF3)

| Adjustment Name | Reference Designator | Adjustment Paragraph | Description |
| :---: | :---: | :---: | :---: |
| SYM | A11C38 | 5-21 | Adjusts symmetry of second crystal bandwidth filter stage. |
| LC CTR | A11C45 | 5-21 | Adjusts centering of second LC bandwidth filter stage. |
| CTR | A11C54 | 5-21 | Adjusts centering of second crystal bandwidth filter stage. |
| C73 (LC DIP) | A11C73 | 5-21 | Dip adjusts first LC bandwidth filter stage. |
| C74 (LC DIP) | A11C74 | 5-21 | Dip adjusts second LC bandwidth filter stage. |
| LC | AllR26 | 5-21 | Adjusts LC feedback of bandwidth filter. |
| XTL | A11R31 | $5-21$ | Adjusts crystal feedback of bandwidth filter. |
| RF GAIN | A12R5 | $5-23$ | Adjusts overall gain of step gain amplifiers. |
| 10D (10 dB) | A12R6 | 5-24 | Adjusts 10 dB step gain amplifier. |
| 20D (20 dB) | A12R21 | 5-24 | Adjusts first 20 dB step gain amplifier. |
| 40D (40 dB) | A12R29 | 5-24 | Adjusts second 20 dB step gain amplifier. |
| LC CTR | A13C23 | 5-21 | Adjusts centering of first LC bandwidth filter stage. |
| CTR | A13C25 | 5-21 | Adjusts centering of first crystal bandwidth filter stage. |
| SYM | A13C38 | 5-21 | Adjusts symmetry of second crystal bandwidth filter stage. |
| LC CTR | A13C45 | 5-21 | Adjusts centering of second LC bandwidth filter stage. |
| CTR | A13C54 | 5-21 | Adjusts centering of second crystal bandwidth filter stage. |
| C73 (LC DIP) | A13C73 | 5-21 | Dip adjusts first LC bandwidth filter stage. |
| C74 (LC DIP) | A13C74 | 5-21 | Dip adjusts second LC bandwidth filter stage. |
| LC | A13R26 | 5-21 | Adjusts LC feedback of bandwidth filter. |
| XTL | A13R31 | 5-21 | Adjusts crystal feedback of bandwidth filter. |
| OFFSET | A14R10 | 5-19 | Adjusts -8 V temperature compensated supply. |
| TC | A14R21 |  | Adjusts gain of +1 V supply to provide temperature compensation for log mode temperature controlled variable gain amplifier. (Factory adjustable only.) |
| SLOPE | A14R23 | 5-19 | Adjusts gain of log mode temperature controlled gain amplifier. |
| G6 | A14R27 | 5-19 | Adjusts combined gain of 2 nd and 3 rd stages in linear mode. |
| G5 | A14R30 | 5-19 | Adjusts gain of 4th stage in linear mode. |
| G4 | A14R33 | 5-19 | Adjusts gain of 5th stage in linear mode. |
| LIN | A14R34 | 5-19 | Adjusts combined gain of 6th and 7th stages in linear mode. |
| $-10 \mathrm{~dB}$ | A14R39 | 5-19 | Adjusts shape of log fidelity curve at -10 dB . |
| $-30 \mathrm{~dB}$ | A14R69 | 5-19 | Adjusts shape of log fidelity curve at -30 dB . |
| 1 VT | A14R88 |  | Adjusts voltage at A14TP1 for approximately +1 V . <br> (Factory adjustable only.) |

TABLE5-1. ADJUSTABLECOMPONENTS(3OF3)

| Adjustment Name | Reference Designator | Adjustment Paragraph | Description |
| :---: | :---: | :---: | :---: |
| LOG GAIN | A14R121 | 5-19 | Adjusts dc offset circuitry at output of Log Amplifier Assembly A14 for 10 dB steps in log mode. |
| 1 dB (offset) | A15R1 | 5-20 | Adjusts LOG $10 \mathrm{~dB} /$ DIV translation. |
| $\mathrm{OD}(0 \mathrm{~dB})$ | A12R35 | 5-24 | Adjusts variable gain amplifier for 0 dB with REF LEVEL FINE control set to 0 dB . |
| $-12 \mathrm{D}(-12 \mathrm{~dB})$ | A12R39 | $5-24$ | Adjusts variable gain amplifier for -12 dB with REF LEVEL FINE control set to -12dB. |
| 1B | A12R47 | 5-28 | Adjusts slope of Band 1 response. |
| 2B | A12R48 | 5-28 | Adjusts slope of Band 2 response. |
| 3B | A12R49 | 5-28 | Adjusts slope of Band 3 response. |
| 4B | A12R51 | 5-28 | Adjusts slope of Band 4 response. |
| 5B | A12R53 | 5-28 | Adjusts slope of Band 5 response. |
| 5 C | A12R54 | 5-28 | Adjusts highend breakpoint in slope of Band 5 response. |
| 6B | A12R55 | 5-28 | Adjusts slope of Band 6 response. |
| 6 C | A12R56 | 5-28 | Adjusts high-end breakpoint in slope of Band 6 response. |
| 1 A | A12R57 | 5-28 | Adjusts gain of Band 1. |
| 2 A | A12R58 | 5-28 | Adjusts gain of Band 2. |
| 3A | A12R59 | 5-28 | Adjusts gain of Band 3. |
| 4A | A12R60 | 5-28 | Adjusts gain of Band 4. |
| 5 A | A12R61 | 5-28 | Adjusts gain of Band 5. |
| 6A | A12R62 | 5-28 | Adjusts gain of Band 6 . |
| v3+ | A12R70 | 5-28 | Adjusts diode bias for Band 6. |
| v 3 - | A12R71 | 5-28 | Adjusts diode bias for Band 5. |
| V1 | A12R72 | 5-28 | Adjusts diode bias for Bands 1 and 2. |
| v 2 - | A12R83 | 5-28 | Adjusts diode bias for Band 3. |
| v2+ | A12R87 | 5-28 | Adjusts diode bias for Band 4. |
| SYM | A13C15 | 5-21 | Adjusts symmetry of first crystal bandwidth filter stage. |

TABLE5-2. RELATEDADJUSTMENTS

| Assembly Replaced or Repaired |  | Perform the Following Related Adjustments | Paragraph Number |
| :---: | :---: | :---: | :---: |
| A1A1 | DPM Display | Frequency Display Adjustments | 5-30 |
| A1A2 | DPM Driver | Frequency Display Adjustments | 5-30 |
| A2 | Front Panel Switch Assembly | First Converter Adjustments CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-25 \\ & 5-29 \end{aligned}$ |
| A3 | Input Attenuator | Frequency Response Adjustments | 5-28 |
| A4 | First Mixer | First Converter Adjustments Frequency Response Adjustments CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-25 \\ & 5-28 \\ & 5-29 \end{aligned}$ |
| A5 | Second Converter | Second Converter Adjustments CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-26 \\ & 5-29 \end{aligned}$ |
| A6 | YIG-Tuned Oscillator | First Converter Adjustments Frequency Response Adjustments CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-25 \\ & 5-28 \\ & 5-29 \end{aligned}$ |
| A7 | Frequency Control | Power Supply Checks and Adjustments First Converter Adjustments | $\begin{aligned} & 5-17 \\ & 5-25 \end{aligned}$ |
| A8 | Marker | First Converter Adjustments | 5-25 |
| A9 | Sweep Generator/ Bandwidth Control | Power Supply Checks and Adjustments Calibrated Sweep Time Adjustments 3-dB Bandwidth Adjustments | $\begin{aligned} & 5-17 \\ & 5-18 \\ & 5-22 \end{aligned}$ |
| A10 | Third Converter | Third Converter Adjustments CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-27 \\ & 5-29 \end{aligned}$ |
| $\begin{aligned} & \text { A11, } \\ & \text { A13* } \end{aligned}$ | Bandwidth Filters | Bandwidth Filter Adjustments 3-dB Bandwidth Adjustments | $\begin{aligned} & 5-21 \\ & 5-22 \end{aligned}$ |
| A12 | Step Gain | RF Gain Adjustments <br> Step Gain Adjustments <br> CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-23 \\ & 5-24 \\ & 5-29 \end{aligned}$ |
| A14 | Log Amplifier | Log Amplifier Log and Linear Adjustments 1-dB Offset Adjustment CAL OUTPUT and REF LEVEL CAL Adjustments | $\begin{aligned} & 5-19 \\ & 5-20 \\ & 5-29 \end{aligned}$ |
| A15 | Vertical Driver/ Blanking | I-dB Offset Adjustment | 5-20 |
| A16 | Motherboard | No related adjustments |  |

TABLE53. FACTORYSELECTEDCOMPONENTSIN ALPHA-NUMERICALORDER


| CAPACITORS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| RANGE: 1 to 24 pF TYPE: Tubular TOLERANCE: $\begin{aligned} & 1 \text { to } 9.1 \mathrm{pF}= \pm .25 \mathrm{pF} \\ & 10 \text { to } 24 \mathrm{pF}= \pm 5 \% \end{aligned}$ |  |  | RANGE: 27 to 680 pF TYPE: Dipped Mica TOLERANCE: $\pm 5 \%$ |  |  |
| Value (pF) | HP Part Number | C | Value $(\mathrm{pF})$ | HP Part Number | C |
| 1.01.21.51.82.0 | $0160-2236$ <br> $0160-2237$ <br> $0150-0091$ <br> $0160-2239$ <br> $0160-2240$ | 89814 | $\begin{aligned} & 27 \\ & 30 \\ & 33 \\ & 36 \\ & 39 \end{aligned}$ | 0160-2306 | 3 |
|  |  |  |  | 0160-2199 | 2 |
|  |  |  |  | 0160-2150 | 5 |
|  |  |  |  | 0160-2308 | 5 |
|  |  |  |  | 0140-0190 | 7 |
| 2.2 | 0160-2241 | 5 | 43 | $\begin{aligned} & 0160-2200 \\ & 0160-2307 \end{aligned}$ | 6 4 |
| 2.4 | 0160-2242 | 6 | 47 | $\begin{aligned} & 0160-2307 \\ & 0160-2201 \end{aligned}$ | 4 7 |
| $\begin{aligned} & 2.7 \\ & 3.0 \end{aligned}$ | 0160-2243 | 7 | 51 | 0140.0191 | 7 8 |
|  | 0160-2244 | 8 | 62 | 0140-0205 | 5 |
| 3.3 | 0150-0059 | 8 |  |  |  |
|  |  |  | 68 | 0140-0192 | 9 |
| 3.6 | 0160-2246 | 0 | 75 | 0160-2202 | 8 |
| 3.9 | 0160-2247 | 1 | 82 | 0140-0193 | 0 |
| 4.3 | 0160-2248 | 2 | 91 | 0160-2203 | 0 |
| 4.7 | 0160-2249 | 3 | 100 | 0160-2204 |  |
| 5.1 | 0160-2250 | 6 |  | 0140-0194 |  |
|  |  |  | 120 | 0160-2205 | 1 |
| 5.6 | 0160-2251 | 7 | 130 | 0140-0195 | 2 |
| 6.2 | $0160 \cdot 2252$ | 8 | 150 | 0140-0196 | 3 |
| 6.8 | 0160-2253 | 9 | 160 | 0160-2206 | 2 |
| 7.5 | 0160-2254 | 0 |  |  |  |
| 8.2 | 0160-2255 | 1 | 180 | 0140-0197 | 4 |
|  |  |  | 200 | 0140-0198 | 5 |
| 9.1 | 0100-2256 | 2 | 220 | 0160-0134 | 1 |
| 10.0 | 0160-2257 | 3 | 240 | 0140-0199 | 6 |
| 11.0 | 0160-2258 | 4 | 270 | 0140-0210 | 2 |
| 12.0 | 0160-2259 |  |  | 0160-2207 |  |
| 13.0 | 0160-2260 | 8 | 330 | 0160-2208 | 4 |
|  |  |  | 360 | 0160-2209 | 5 |
| 15.0 | 0160-2261 | 9 | 390 | 0140-0200 | 0 |
| 16.0 | 0160-2262 | 0 | 430 | 0160-0939 | 4 |
| 18.0 | 0160-2263 | 1 |  |  |  |
| 20.0 | 0160-2264 | 2 | 470 | 0160-3533 | 0 |
| 22.0 | 0160-2265 | 3 | 510 | 0160-3534 | 1 |
|  |  |  | 560 | 0160-3535 | 2 |
| 24.0 | 0160-2266 | 4 | $\begin{aligned} & 620 \\ & 680 \end{aligned}$ | $0160-3536$ $0160-3537$ | 3 4 |
|  |  |  |  | 0160-3537 |  |

TABLE 5-4. HPPART NUMBERSOFSTANDARDVALUE REPLACEMENTCOMPONENTS(2OF3)

| RESISTORS |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RANGE: 10 to 464K Ohms TYPE: Fixed-Film WATTAGE: .125 at $125^{\circ} \mathrm{C}$ TOLERANCE: $\pm 1.0 \%$ |  |  |  |  |  |  |  |  |
| Value ( $\Omega$ ) | HP Part Number | $\begin{aligned} & \mathbf{C} \\ & \mathbf{D} \end{aligned}$ | Value <br> ( $\Omega$ ) | HP Part Number | $\begin{aligned} & \text { C } \\ & \text { D } \end{aligned}$ | Value <br> $(\Omega)$ | HP Part Number | C |
| 10.0 | 0757.0346 | 2 | 464 | 0698-0082 | 7 | 21.5 K | 0757-0199 | 3 |
| 11.0 | 0757-0378 | 0 | 511 | 0757-0416 | 7 | 23.7 K | 0698-3158 | 4 |
| 12.1 | 0757-0379 | 1 | 562 | $0757-0417$ | 8 | 26.1K | 0698-3159 | 5 |
| 13.3 | 0698-3427 | 0 | 619 | 0757-0418 | 9 | 28.7 K | 0698-3449 | 6 |
| 14.7 | 0698-3428 | 1 | 681 | 0757-0419 | 0 | 31.6 K | 0698-3160 | 8 |
| 16.2 | 0757-0382 | 6 | 750 | 0757-0420 | 3 | 34.8 K | 0757-0123 | 3 |
| 17.8 | 0757-0294 | 9 | 825 | 0757-0421 | 4 | 38.3 K | 0698-3161 | 9 |
| 19.6 | 0698-3429 | 2 | 909 | 0757-0422 | 5 | 42.2 K | 0698-3450 | 9 |
| 21.5 | 0698-3430 | 5 | 1.0 K | 0757-0280 | 3 | 46.4 K | 0698-3162 | 0 |
| 23.7 | 0698-3431 | 6 | 1.1 K | 0757-0424 | 7 | 51.1 K | 0757-0458 | 7 |
| 26.1 | 0698-3432 | 7 | 1.21 K | 0757-0274 | 5 | 56.2K | 0757-0459 | 8 |
| 28.7 | 0698-3433 | 8 | 1.33 K | 0757-0317 | 7 | 61.9 K | 0757-0460 | 1 |
| 31.6 | 0757-0180 | 2 | 1.47 K | 0757-1094 | 9 | 68.1 K | 0757-0461 | 2 |
| 34.8 | 0698-3434 | 9 | 1.62 K | 0757-0428 | 1 | 75.OK | 0757.0462 | 3 |
| 38.3 | 0698-3435 | 0 | 1.78 K | 0757-0278 | 9 | 82.5 K | 0757-0463 | 4 |
| 42.2 | 0757-0316 | 6 | 1.96K | 0698-0083 | 8 | 90.9 K | 0757-0464 | 5 |
| 46.4 | 0698.4037 | 0 | 2.15 K | 0698-0084 | 9 | 100 K | 0757-0465 | 6 |
| 51.1 | 0757-0394 | 0 | 2.37 K | 0698-3150 | 6 | 110 K | 0757-0466 | 7 |
| 56.2 | 0757-0395 | 1 | 2.61 K | 0698-0085 | 0 | 121 K | 0757-0467 | 8 |
| 61.9 | 0757-0276 | 7 | 2.87 K | 0698-3151 | 7 | 133K | 0698-3451 | 0 |
| 68.1 | 0757-0397 | 3 | 3.16 K | 0757-0279 | 0 | 147K | 0698.3452 | 1 |
| 75.0 | 0757-0398 | 4 | 3.48 K | 0698-3152 | 8 | 162K | 0757-0470 | 3 |
| 82.5 | 0757-0399 | 5 | 3.83 K | 0698-3153 | 9 | 178K | 0698.3243 | 8 |
| 90.9 | 0757-0400 | 9 | 4.22 K | 0698-3154 | 0 | 196K | 0698-3453 | 2 |
| 100 | 0757-0401 | 0 | 4.64 K | 0698-3155 | 1 | 215 K | 0698-3454 | 3 |
| 110 | 0757-0402 | 1 | 5.11 K | 0757-0438 | 3 | 237K | 0698-3266 | 5 |
| 121 | 0757-0403 | 2 | 5.62 K | 0757-0200 | 7 | 261K | 0698-3455 | 4 |
| 133 | 0698-3437 | 2 | 6.19 K | 0757-0290 | 5 | 287K | 0698-3456 | 5 |
| 147 | 0698-3438 | 3 | 6.81 K | 0757-0439 | 4 | 316 K | 0698-3457 | 6 |
| 162 | 0757-0405 | 4 | 7.50 K | 0757-0440 | 7 | 348K | 0698-3458 | 7 |
| 178 | 0698-3439 | 4 | 8.25 K | 0757-0441 | 8 | 383K | 0698-3459 | 8 |
| 196 | 0698-3440 | 7 | 9.09 K | 0757-0288 | 1 | 422K | 0698.3460 | 1 |
| 215 | 0698-3441 | 8 | 10.0K | 0757-0442 | 9 | 464 K | 0698-3260 | 9 |
| 237 | 0698-3442 | 9 | 11.0K | 0757-0443 | 0 |  |  |  |
| 261 | 0698.3132 | 4 | 12.1 K | 0757-0444 | 1 |  |  |  |
| 287 | 0698-3443 | 0 | 13.3K | 0757-0289 | 2 |  |  |  |
| 316 | 0698-3444 | 1 | 14.7K | 0698.3156 | 2 |  |  |  |
| 348 | 0698-3445 | 2 | 16.2K | 0757-0447 | 4 |  |  |  |
| 383 | 0698-3446 | 3 | 17.8K | 0698-3136 | 8 |  |  |  |
| 422 | 0698-3447 | 4 | 19.6K | 0698.3157 | 3 |  |  |  |

TABLE5-4. HPPART NUMBERS OF STANDARDVALUEREPLACEMENTCOMPONENTS(3OF 3)

| RESISTORS |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RANSE: <br> TYPE: F WATTAG TOLERAN |  | $\begin{aligned} & 1.47 \mathrm{M} \\ & \mathrm{~m} \\ & \text { it } 125^{\circ} \mathrm{C} \\ & 1 \% \end{aligned}$ |  |  |  | 目N |  |  |  |  |
| Value <br> ( $\Omega$ ) | HP Part Number | $\begin{aligned} & \mathbf{C} \\ & \mathbf{D} \end{aligned}$ | Value ( $\Omega$ ) | HP Part Number | $\begin{aligned} & \mathbf{C} \\ & \mathbf{D} \end{aligned}$ | Value ( $\Omega$ ) | HP Part Number | $\begin{aligned} & \mathbf{C} \\ & \mathbf{D} \end{aligned}$ | Value <br> $(\Omega)$ | HP Part Number | $\begin{aligned} & \text { C } \\ & \text { D } \end{aligned}$ |
| 10.0 | 0757-0984 | 4 | 215 | 0698-3401 | 0 | 4.64 K | 0698-3348 | 4 | 110K | 0757-0859 | 2 |
| 11.0 | 0575-0985 | 5 | 237 | 0698-3102 | 8 | 5.11 K | 0757-0833 | 2 | 121 K | 0757-0860 | 5 |
| 12.1 | 0757.0986 | 6 | 261 | 0757-1090 | 5 | 5.62 K | 0757-0834 | 3 | 133K | 0757-0310 | 0 |
| 13.3 | 0757.0001 | 6 | 287 | 0757-1092 | 7 | 6.19 K | 0757-0196 | 0 | 147 K | 0698-3175 | 5 |
| 14.7 | 0698-3388 | 2 | 316 | 0698-3402 | 1 | 6.81 K | 0757-0835 | 4 | 162K | 0757-0130 | 2 |
| 16.2 | 0757-0989 | 9 | 348 | 0698-3403 | 2 | 7.50 K | 0757-0836 | 5 | 178K | 0757.0129 | 9 |
| 17.8 | 0698-3389 | 3 | 383 | 0698-3404 | 3 | 8.25 K | 0757.0837 | 6 | 196K | 0757-0063 | 0 |
| 19.6 | 0698-3390 | 6 | 422 | 0698-3405 | 4 | 9.09 K | 0757-0838 | 7 | 215K | 0757-0127 | 7 |
| 21.5 | 0698-3391 | 7 | 464 | 0698-0090 | 7 | 10.0 K | 0757-0839 | 8 | 237K | 0698-3424 | 7 |
| 23.7 | 0698-3392 | 8 | 511 | 0757-0814 | 9 | 12.1 K | 0757-0841 | 2 | 261 K | 0757-0064 | 1 |
| 26.1 | 0757-0003 | 8 | 562 | 0757-0815 | 0 | 13.3 K | 0698-3413 | 4 | 287 K | 0757-0154 | 0 |
| 28.7 | 0698-3393 | 9 | 619 | 0757-0158 | 4 | 14.7 K | 0698-3414 | 5 | 316 K | 0698-3425 | 8 |
| 31.6 | 0698-3394 | 0 | 681 | 0757.0816 | 1 | 16.2 K | 0757-0844 | 5 | 348K | 0757.0195 | 9 |
| 34.8 | 0698-3395 | 1 | 750 | 0757-0817 | 2 | 17.8 K | 0698-0025 | 8 | 383 K | 0757.0133 | 5 |
| 38.3 | 0698-3396 | 2 | 825 | 0757-0818 | 3 | 19.6K | 0698-3415 | 6 | 422 K | 0757-0134 | 6 |
| 42.2 | 0698-3397 | 3 | 909 | 0757.0819 | 4 | 21.5 K | 0698-3416 | 7 | 464 K | 0698-3426 | 9 |
| 46.4 | 0698-3398 | 4 | 1.00 K | 0757-0159 | 5 | 23.7 K | 0698.3417 | 8 | 511 K | 0757-0135 | 7 |
| 51.1 | 0757-1000 | 7 | 1.10 K | 0757-0820 | 7 | 26.1K | 0698-3418 | 9 | 562 K | 0757-0868 | 3 |
| 56.2 | 0757-1001 | 8 | 1.21 K | 0757-0821 | 8 | 28.7K | 0698-3103 | 9 | 619 K | 0757-0136 | 8 |
| 61.9 | 0757-1002 | 9 | 1.33 K | 0698-3406 | 5 | 31.6 K | 0698-3419 | 0 | 681 K | 0757-0869 | 4 |
| 68.1 | 0757-0794 | 4 | 1.47 K | 0757-1078 | 9 | 34.8 K | 0698-3420 | 3 | 750K | 0757.0137 | 9 |
| 75.0 | 0757-0795 | 5 | 1.62 K | 0757-0873 | 0 | 38.3 K | 0698-3421 | 4 | 825 K | 0757-0870 | 7 |
| 82.5 | 0757-0796 | 6 | 1.78 K | 0698-0089 | 4 | 42.2K | 0698-3422 | 5 | 909K | 0757-0138 | 0 |
| 90.0 | 0757.0797 | 7 | 1.96 K | 0698-3407 | 6 | 46.4 K | 0698-3423 | 6 | 1M | 0757-0059 | 4 |
| 100 | 0757-0198 | 2 | 2.15 K | 0698-3408 | 7 | 51.1 K | 0757-0853 | 6 | 1.1M | 0757.0139 | 1 |
| 110 | 0757-0798 | 8 | 2.37 K | 0698-3409 | 8 | 56.2 K | 0757-0854 | 7 | 1.21 M | 0757.0871 | 8 |
| 121 | 0757-0799 | 9 | 2.61 K | 0698-0024 | 7 | 61.9 K | 0757-0309 | 7 | 1.33 M | 0757-0194 | 8 |
| 133 | 0698-3399 | 5 | 2.87 K | 0698.3101 | 7 | 68.1 K | 0757-0855 | 8 | 1.47M | 0698-3464 | 5 |
| 147 | 0698-3400 | 9 | 3.16 K | 0698-3410 | 1 | 75.OK | 0757.0856 | 9 |  |  |  |
| 162 | 0757-0802 | 5 | 3.48 K | 0698-3411 | 2 | 82.5K | 0757-0857 | 0 |  |  |  |
| 178 | 0698-3334 | 8 | 3.83 K | 0698-3412 | 3 | 90.9 K | 0757.0858 | 1 |  |  |  |
| 196 | 0757-1060 | 9 | 4.22 K | 0698-3346 | 2 | 100K | 0757-0367 | 7 |  |  |  |

## ADJUSTMENTS

## 5-17. POWER SUPPLY CHECKS AND ADJUSTMENTS

## REFERENCE:

A7, A8, A9 Schematics

## DESCRIPTION:

The +14.5 V and -10 V regulated power supplies on Frequency Control Assembly A7 are adjusted. The (dependent) -12 V power supply is then checked for proper dc output (with less than $\pm 50 \mathrm{mV}$ variation) while the spectrum analyzer is tuned from 10 MHz to 3 GHz . The +10 V power supply on Sweep Generator/Bandwidth Control Assembly A9 and the VO (Varactor Offset) voltage on Marker Assembly A8 are then adjusted. Both the +10 V power supply voltage and the VO voltage are temperature-dependentand must be adjusted during the first five minutes after the spectrum analyzer is turned on (cold instrument).


FIGURE 5-1. POWERSUPPLYCHECKS AND ADJUSTMENTSTEST SETUP

## EQUIPMENT:

Digital Voltmeter ..... HP 3456A
Extender Cable ..... HP 5060-0303
Cable Assembly, BNC (m) to Banana Plug .Adapter, BNC (f) to Alligator ClipsHP 8120-1292

## ADJUSTMENTS

## 5-17. POWER SUPPLY CHECKS AND ADJUSTMENTS(Cont'd)

## PROCEDURE:

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... 0.010 GHz
FREQ SPAN/DIV ..... F (full)
RESOLUTION BW ..... coupled
INPUT ATTEN ..... 10 dB
REFERENCE LEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV ..... MAN
SWEEPTRIGGER ..... FREE RUN
ALTIF ..... OFF
SIGIDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF

## NOTE

## In all following adjustments, connect negative terminal of digital voltmeter to spectrum analyzer chassis unless otherwise instructed.

2. Connect equipment as shown in Figure 5-1. Install Frequency Control Assembly A7 on extender board and connect digital voltmeter to +14.5 V test points A7TP3.
3. Adjust +14.5 V potentiometer A7R41 for a voltmeter indication of $+14.500 \pm 0.002 \mathrm{Vdc}$.
4. Connect digital voltmeter to -10 V test point A 7 TP 2 and adjust -10 V potentiometer A 7 R 29 for a voltmeter indication of $-10.000 \pm 0.005 \mathrm{Vdc}$.
5. Use digital voltmeter to check for $-12.0 \pm 0$. I Vdc at collector (case) of transistor A7Q7, located near center of Frequency Control Assembly A7. Vary MAN SWEEP control over entire range and verify that voltage indication varies no more than $\pm 0.05 \mathrm{Vdc}$.
6. Remove extender board and reinstall Frequency Control Assembly A7.

## ADJUSTMENTS

## 5-17. POWER SUPPLY CHECKS AND ADJUSTMENTS(Cont'd)


#### Abstract

NOTE The two following voltage adjustments, +10 V and VO (Varactor Offset), must be performed while the spectrum analyzer is still cold (during first five minutes after turn-on). If the instrument has been operating longer than five minutes, turn off the display mainframe, remove A8 and A9 assemblies, and let them cool on bench for 15 minutes. Replace the two assemblies and proceed with adjustment of A9R2 and A8R62 during the first five minutes after turn-on.


7. Connect digital voltmeter to +10 V test point A9TP7 and adjust +10 V potentiometer A 9 R 2 for a voltmeter indication of $+10.000 \pm 0.100 \mathrm{Vdc}$.
8. Connect digital voltmeter to VO test point A8TP2. Set spectrum analyzer SWEEP TIME/DIV control to 10 ms and SWEEP TRIGGER control to SINGLE. Turn ALT IF and SIG IDENT on (pushbuttons depressed).
9. Voltage at A8TP2 will alternate between two values each time a sweep is triggered. Trigger sweep a few times until voltmeter indicates least negative VO voltage. Adjust VO potentiometer A8R62 for a voltmeter indication of $-2.00 \pm 0.10 \mathrm{Vdc}$.

## ADJUSTMENTS

## 5-18. CALIBRATED SWEEP TIME ADJUSTMENT

REFERENCE:
A9 Schematic

## DESCRIPTION:

A counter is used to adjust the time interval of the 1 millisecond per division and 5 milliseconds per division sweep times. Calibrated sweep times from 0.1 milliseconds through 50 milliseconds are then checked using the counter time-interval (T.I.) function.


FIGURE 5.2. CALIBRATED SWEEP TIME ADJUSTMENT TEST SETUP

## EQUIPMENT:

50 MHz Universal Counter
HP 5300B/5302A
Extender Cable Assembly
HP 5060-0303
BNC Tee
HP 1250-0781

PROCEDURE:

Since the calibrated sweep time adjustments are dependent on the +14.5 V and -10 V power supplies, the Power Supply Checks and Adjustments (paragraph 5-17) should be performed before starting this procedure.

## ADJUSTMENTS

## 5-18. CALIBRATEDSWEEP TIME ADJUSTMENT(Cont'd)

1. Set equipment controls as follows:

## NOTE

## If an HP 853A Spectrum Analyzer Display mainframe is used, and a sweep time faster than 10 msec is selected, an error message will appear on the analyzer's CRT and the analyzer will go into mixed mode.

Spectrum Analyzer:
FREQUENCY BAND GHz ..... $.01-3$
TUNING ..... $>0.010 \mathrm{GHz}$
FREQ SPAN/DIV ..... F (full)
RESOLUTION BW Optimum, coupled10 dB
REFERENCE LEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV 1 msec
SWEEP TRIGGER ..... FREE RUN
ALTIF ..... OFF
SIGIDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF
50 MHz Universal Counter:
FUNCTION ..... TI. A to B
SAMPLE RATE Full counterclockwise
TIME BASE ..... $10 \mu \mathrm{~S}$
SENSITIVITY (A) ..... 9 o'clock
A 50 MHz INPUT
(falling edge)SENSITIVITY (B)9 o'clock
B 10 MHz INPUT(rising edge)
2. Connect equipment as shown in Figure 5-2.
3. Adjust counter SENSITIVITY controls (both channels) as necessary until counter triggers and indicates a time interval of approximately 10.00 ms .
4. Adjust 1 ms potentiometer A9R 10 for a time interval indication of $10.00 \pm 0.80 \mathrm{~ms}$

## ADJUSTMENTS

## 5-18. CALIBRATEDSWEEP TIME ADJUSTMENT(Cont'd)

## NOTE

In early instruments, A9R13 is labeled " 2 ms." The adjustment of A9R13, however, should be performed with SWEEP TIME/DIV set at 5 ms .
5. Set spectrum analyzer SWEEP TIME/DIV control to 5 msec . Readjust counter SENSITIVITY controls as necessary and adjust 5 ms potentiometer A9R13 for a time interval indication of $50.00 \pm 4.00 \mathrm{~ms}$.
6. Check time interval for each SWEEP TIME/DIV control setting listed in Table 5-5. Readjust 1 ms potentiometer A9R10 and 5 ms potentiometer A9R13 as necessary if test limits are exceeded.

TABLE 5-5. CALIBRATED SWEEP TIME TESTLIMITS

| SWEEP TIME/DIV Setting | Sweep Time (ms) |
| :---: | :---: |
| .1 m s | $1.00 \pm 0.10$ |
| .2 ms | $2.00 \pm 0.20$ |
| .5 ms | $5.00 \pm 0.40$ |
| 1 ms | $10.00 \pm 0.80$ |
| 2 ms | $20.00 \pm 1.50$ |
| 5 ms | $50.00 \pm 4.00$ |
| 10 ms | $100.00 \pm 8.00$ |
| 20 ms | $200.00 \pm 16.00$ |
| 50 ms | $500.00 \pm 40.00$ |

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS

## REFERENCE:

A14 and A15 Schematics

## DESCRIPTION:

Step attenuators are used to change the level of the input signal to the spectrum analyzer in calibrated steps. The output of Vertical Driver and Blanking Assembly A15 is monitored, and adjustments are performed to calibrate Log Amplifier Assembly A14.


FIGURE53. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTSTEST SETUP

## EQUIPMENT:

Signal Generator HP 8640B
Digital Voltmeter ..... HP 3456A
Step Attenuator ( $10-\mathrm{dB} /$ step) ..... HP 355D, Opt. H82
Step Attenuator (1-dB/step) ..... HP 355C, Opt. H80
Cable Assembly, Banana Plug to BNC (m) ..... HP 11001A
Adapter, Type N(m) to BNC (f) ..... HP 1250-0780
Adapter, SMC (m) to BNC (f) ..... HP 1250-0832
Extender Cable Assembly ..... HP 5060-0303

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS(Cont'd)

## PROCEDURE:

1. Set equipment controls as follows:

Spectrum Analyzer:
FREQUENCY BAND GHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 01 - 3
TUNING . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $>0.010 \mathrm{GHz}$
FREQ SPAN/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 0
RESOLUTION BW . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 300 kHz , uncoupled
INPUTATTEN . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 10 dB
REFERENCELEVEL . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 50 dBm
REFLEVELFINE 0
Amplitude Scale . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .
SWEEP TIME/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . AUTO
SWEEPTRIGGER . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . FREE RUN
ALTIF ............................................................................................... . . OFF
SIG IDENT . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . OFF
BLCLIP............................................................................................... . OFF
VIDEOFILTER ...................................................................................... . OFF
Signal Generator:
COUNTERMODE .................................................................................. . INT
AM ................................................................................................... . . . . OFF
FM ................................................................................................... . . . . OFF
FREQUENCY TUNE ...................................................................... . . . 321.4 MHz
RF................................................................................................. ON
OUTPUTLEVEL .................................................................. approx. -28 dBm
2. Set $1-\mathrm{dB}$ step attenuator to 10 dB and $10-\mathrm{dB}$ step attenuator to 0 dB . Remove AlOWl (blue cable) from A5J2 and connect equipment as shown in Figure 5-3, using adapter to connect step attenuator to A10W1.

## NOTE

## The HP 355C 10 dB attenuation is included to compensate for 10 dB of gain on Step Gain Assembly A12 with the TEST-NORM switch in TEST.

3. Set TEST-NORM switch on Step Gain Assembly A12 to TEST position. Adjust signal generator FREQUENCY TUNE control for maximum signal amplitude on display with $10-\mathrm{dB}$ step attenuator set to 0 dB (reduce signal generator OUTPUT LEVEL control setting as necessary to bring signal on-screen).

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS (Cont'd)

4. Disconnect signal generator output from step attenuator. Adjust spectrum analyzer VERTICAL POSN control to position signal trace at bottom CRT graticule line. Measure dc offset voltage at A15TP1 and record.
$\qquad$
mV
5. Connect signal generator to step attenuator and adjust signal generator FINE TUNE control to peak signal on CRT display.
6. Adjust signal generator OUTPUT LEVEL for digital voltmeter (DVM) reading ( $\pm 1 \mathrm{mV}$ ) of 800 mV plus offset recorded in step 4, as measured at A15TP1. Adjust spectrum analyzer VERTICAL GAIN control to position signal trace at top graticule line.
7. Set spectrum analyzer Amplitude Scale control to $10 \mathrm{~dB} /$ DIV.
8. Set $10-\mathrm{dB}$ step attenuator to 0 dB and adjust SLOPE potentiometer A14R23 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 800 mV plus offset recorded in step 4, as measured at A15TP1.
9. Set $10-\mathrm{dB}$ step attenuator to 60 dB and adjust OFFSET potentiometer A14R 10 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 200 mV plus offset recorded in step 4, as measured at A15TP1.
10. Repeat steps 8 and 9 until no further adjustment is necessary.
11. Set $10-\mathrm{dB}$ step attenuator to 30 dB and adjust SLOPE potentiometer A14R23 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 500 mV plus offset recorded in step 4, as measured at A15TP1.
12. Set $10-\mathrm{dB}$ step attenuator to 60 dB and adjust OFFSET potentiometer A14R 10 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 200 mV plus offset recorded in step 4.
13. Repeat steps 11 and 12 until no further adjustment is necessary.
14. Set $10-\mathrm{dB}$ step attenuator to 10 dB and adjust -30 dB potentiometer A14R69 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 700 mV plus offset recorded in step 4 .
15. Set $10-\mathrm{dB}$ step attenuator to 0 dB and adjust -10 dB potentiometer A14R 39 for DVM reading $( \pm 1 \mathrm{mV})$ of 800 mV plus offset recorded in step 4.
16. Set $10-\mathrm{dB}$ step attenuator to 60 dB and adjust OFFSET potentiometer A14R 10 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 200 mV plus offset recorded in step 4.
17. Set $10-\mathrm{dB}$ step attenuator to 0 dB and adjust SLOPE potentiometer A14R23 for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 800 mV plus offset recorded in step 4 .
18. Repeat steps 16 and 17 until no further adjustment is necessary.
19. Check log fidelity per Table 5-6. If test limits are not met, repeat steps 8 through 18 .

## ADJUSTMENTS

5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS(Cont'd)

TABLE5-6: LOG FIDELITYCHECK

| Step <br> Attenuator Setting (dB) | DVM Readipg | Corrected DVM Reading* (mV) | Test Limits (mV) | Theoretical Reading (mV) | Theoretical Reading Subtracted from Corrected DVM Reading (mV) | Difference Between Adjacent Readings*" (mV) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  |  | $800 \pm 1$ | 800 |  |  |
| 10 |  |  | $700 \pm 3$ | 700 |  |  |
| 20 |  |  | $600 \pm 4$ | 600 |  |  |
| 30 |  |  | $500 \pm 4$ | 500 |  |  |
| 40 |  |  | $400 \pm 5$ | 400 |  |  |
| 50 |  |  | $300 \pm 6$ | 300 |  |  |
| 60 |  |  | $200 \pm 7$ | 200 |  |  |
| 70 |  |  | $100 \pm 8$ | 100 |  |  |
| DVM readin <br> All values i | nus offset Difference | ed in step 4 een Adjace | dings col | must be less | $r$ equal to $\pm 10 \mathrm{mV}$. |  |

## Example ( +5 mV offset):

TABLE5-7. SAMPLECOMPUTATIONSOF AMPLITUDELOG DISPLAY ACCURACY

| Step <br> Attenuator <br> Setting <br> $(\mathbf{d B})$ | DVM <br> Reading <br> $(\mathbf{m V})$ | Corrected <br> DVM <br> Reading* <br> $(\mathbf{m V})$ | Theoretical <br> Reading <br> $(\mathbf{m V})$ | Theoretical <br> Reading Subtracted <br> from Corrected <br> DVM Reading <br> $(\mathbf{m V})$ | Difference <br> Between <br> Adjacent <br> Readings*" <br> $(\mathbf{m V})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | +805 | +800 | +800 | 0 |  |
| 10 | +708 | +703 | +700 | $-\mathbf{+ 3}$ | $-\mathbf{- 3}$ |
| 20 | +599 | +594 | +600 | $-\mathbf{- 6}$ | $-\mathbf{+ 9}$ |
| 30 | +497 | +492 | +500 | $-\mathbf{- 8}$ | $-\mathbf{+ 2}$ |
| 40 | +406 | +401 | +400 | $-\mathbf{+ 1}$ | $-\mathbf{- 9}$ |

[^4]
## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS(Cont'd)

## Linear Output and Linear Step Gain

20. Disconnect A10W1 from step attenuator and reconnect to A5J2.

## CAUTION

## When reconnecting A10W1 to A5J2, do not tighten to over 6 inch pounds of torque; A5J2 can be damaged if the connector is overtightened.

Set spectrum analyzer controls as follows:

```
INPUT ATTEN . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 10 dB
REFERENCE LEVEL . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . ........... . . - - 50 dBm
FREQ SPAN/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 0
```



Set signal generator controls as follows:

```
OUTPUT LEVEL approx. -5 dBm
FREQUENCY ................................................................................ 30 MHz
```

Set $10-\mathrm{dB}$ step attenuator to 0 dB .
21. Remove adapter from step attenuator and connect step attenuator to spectrum analyzer input. Adjust the signal generator OUTPUT LEVEL for a DVM reading ( $\pm 1 \mathrm{mV}$ ) of 800 mV plus offset recorded in step 4 (measured at A15TPI).
22. Set spectrum analyzer amplitude scale for Linear display (LIN) and adjust LIN control A14R34 for DVM reading $( \pm 1 \mathrm{mV})$ of 800 mV plus offset recorded in step 4 .
23. Make adjustments indicated in Table 5-8, then recheck that all steps meet the DVM test limits. Between adjustments, recheck tuning of spectrum analyzer to be certain signal remains peaked.

TABLE 5.8. LINEAR GAIN ADJUSTMENTS

| Adjustment | Step Attenuator | Reference Level (dBm) | DVM Reading" |
| :---: | :---: | :---: | :---: |
| A14R34 | 0 | -50 | Ref: $800 \pm 1 \mathrm{mV}$ |
| A14R33 | 10 | -60 | $800 \pm 5 \mathrm{mV}$ |
| A14R30 | 20 | -70 | $800 \pm 5 \mathrm{mV}$ |
| A14R27 | 30 | -80 | $800 \pm 5 \mathrm{mV}$ |
| No adjustment | 40 | -90 | $800 \pm 20 \mathrm{mV}$ |
| *After subtracting offset. |  |  |  |$.$|  |
| :--- |

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS(Cont'd)

## Log Gain

24. Set spectrum analyzer controls as follows:

> REFERENCE LEVEL . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 50 dBm
> Amplitude Scale. . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 db /DIV
25. Set $10-\mathrm{dB}$ step attenuator to 0 dB . Retune spectrum analyzer to peak signal. Adjust signal generator OUTPUT LEVEL for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 800 mV plus offset recorded in step 4 , as measured at A15TP1.
26. Set $10-\mathrm{dB}$ step attenuator to 40 dB . Set REFERENCE LEVEL to -90 dBm and adjust LOG GAIN control A14R121 for DVM reading of 800 mV plus offset recorded in step 4, as measured at A15TP1.
27. Check log gain steps according to Table 5-9. If limits are not met, repeat steps 25 through $\mathbf{2 7}$. If limits still are not met, return to step 1 .

TABLE 59. LOGGAIN ADJUSTMENTLIMITS

| Step Attenuator | Reference Level (dBm) | DVM Reading* $^{*}$ |
| :---: | :---: | :---: |
| 0 | -50 | Ref: $800 \pm 1 \mathrm{mV}$ |
| 10 | -60 | $800+30 \mathrm{mV}$ |
| 20 | -70 | $800+30 \mathrm{mV}$ |
| 30 | -80 | $800+30 \mathrm{mV}$ |
| 40 | -90 | $800+30 \mathrm{mV}$ |
| *After subtracting offset. |  |  |

28. Set spectrum analyzer controls as follows:

29. Set both step attenuators to 0 dB . Reduce signal generator OUTPUT LEVEL until signal appears at top of display. Adjust spectrum analyzer FINE TUNE to peak trace on display and adjust signal generator OUTPUT LEVEL for DVM reading ( $\pm 1 \mathrm{mV}$ ) of 800 mV plus offset recorded in step 4 , as measured at A15TP1. Increase attenuation in 1-dB steps as shown in Table 5-10 and take DVM readings to check log amplifier output.
30. Return TEST-NORM switch A12S1 to NORM.

## ADJUSTMENTS

5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTS(Cont'd)

TABLE5-10. LOG AMPLIFIER OUTPUT LIMITS

| Step Attenuator Setting (dB) | D V M Reading (mV) | Corrected DVM Reading* (mV) | Test Limits (mV) | Theoretical Reading (mV) | Theoretical Reading Subtracted from Corrected D V M Reading (mV) | Difference Between Adjacent Readings** (mV) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  |  | $800 \pm 1$ | +800 | 0 |  |
| 1 |  |  | $700 \pm 10$ | +700 |  |  |
| 2 |  |  | $600 \pm 20$ | +600 |  |  |
| 3 |  |  | $500 \pm 30$ | +500 |  |  |
| 4 |  |  | $400 \pm 30$ | +400 |  |  |
| 5 |  |  | $300 \pm 30$ | +300 |  |  |
| 6 |  |  | $200 \pm 30$ | +200 |  |  |
| 7 |  |  | $100 \pm 30$ | +100 |  |  |

* DVM Reading minus offset.
**All values in the Difference Between Adjacent Readings column must be less than or equal to $\pm 10 \mathrm{mV}$


## ADJUSTMENTS

## 5-20. 1-dB OFFSET ADJUSTMENT

## REFERENCE:

A15 Schematic

## DESCRIPTION:

Reference is set in 10 dB /DIV amplitude scale and 1 dB offset is adjusted in 1 dB /DIV for the same full display reference.


FIGURE 5-4. 1-dB OFFSET ADJUSTMENTTEST SETUP

## EQUIPMENT:

> Adapter, Type N (m) to BNC (f) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . HP 1250-0780
> Extender Cable Assembly HP 5060-0303
> BNC Cable, 9-Inch HP 10502A

## PROCEDURE:

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... $>60 \mathrm{MHz}$
FREQ SPAN/DIV ..... 1 MHz
RESOLUTION BW 1 MHz , uncoupled
INPUTATTEN ..... 10 dB
REFERENCE LEVEL ..... 0 dBm
REFLEVELFINE ..... 0
Amplitude Scale ..... LIN
SWEEP TIME/DIV ..... AUTO
SWEEP TRIGGER ..... FREE RUN
ALTIF ..... OFF
SIG IDENT ..... OFF
BLCLIP ..... OFF
VIDEOFILTER ..... OFF

## ADJUSTMENTS

## 5-20. $\quad 1$-dB OFFSET ADJUSTMENT (Cont'd)

2. Connect equipment as shown in Figure 5-4.
3. Adjust vertical position to align trace on bottom graticule.
4. Set tuning to 35 MHz . Set TUNING control to center the trace on the display. Set REF LEVEL FINE for a full-screen trace (signal at top graticule line).
5. Set AmplitudeScale to 10 dB /DIV. Adjust VERT GAIN if necessary for full screen trace.
6. Repeat steps 3 and 4 until the trace is full screen in both LIN and 10 dB /DIV.

## NOTE

1 dBIDIV will read approximately 0.5 dB ( 0.5 division) low when using extender cable assembly. Adjusting A15R1 1 dB OFFSET for a trace 0.5 division down from top graticule line should place signal at top graticule line when HP 8559A is properly installed in display mainframe.
7. Set Amplitude Scale to $1 \mathrm{~dB} /$ DIV. Adjust A15R1 1 dB OFFSET for a trace 0.5 division down from top graticule line.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS

## REFERENCE:

A9, A11, and A13 Schematics

## DESCRIPTION:

The crystal and LC bandwidth filter circuits are adjusted for symmetry, center, and peak. The 3-dB bandwidths are adjusted with Sweep Generator/Bandwidth Control Assembly A9 (paragraph 5-22).


FIGURE5-5. CRYSTALANDLC BANDWIDTHFILTER ADJUSTMENTSTESTSETUP

## EQUIPMENT:

```
Adapter, Type N(m) to BNC (f)
HP 1250-0780
Crystal Short (3 required)
See Figure 5-6
Extender Cable Assembly
HP 5060-0303
```


## NOTE

A crystal short consists of a $.01 \mu \mathrm{~F}$ capacitor (HP Part Number 0160-0161) and a 90.9 ohm resistor (HP Part Number 0757-0400) connected in series. Two square terminal connectors (HP Part Number 0362-0265) are used to connect the crystal short across the test points.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(Cont'd)



FIGURE5-6. CRYSTALSHORTCONFIGURATION

## PROCEDURE:

NOTE
Allow 30 minutes warmup time before performing adjustments.

1. Set spectrum analyzer controls as follows:
FREQUENCYBAND ..... $.01-3 \mathrm{GHz}$
TUNING ..... 35 MHz
FREQ SPAN/DIV ..... 200 kHz
RESOLUTIONBW ..... MHz
INPUTATTEN ..... 10 dB
REFERENCELEVEL ..... 0 dBm
Amplitude Scale ..... LIN
SWEEP TIME/DIV ..... 10 msec
SWEEPTRIGGER ..... FREE RUN
Crystal Alignment
2. Connect equipment as shown in Figure 5-5.

NOTE
If Sweep Generator A9 has been replaced or adjusted, perform steps 3 through 8. If not, proceed to step 9.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(Cont'd)

3. Center the signal with TUNING control. Using REF LEVEL FINE control, place signal peak at 7.1 divisions ( 0.9 division from top graticule line).
4. Adjust A9R85 LC until signal is five divisions wide at the fifth graticule line ( $\mathbf{1} \mathrm{MHz}$ wide at $3-\mathrm{dB}$ points).
5. Set FREQ SPAN/DIV to 10 kHz and RESOLUTION BW to 10 kHz .
6. Center the signal with FINE TUNING control.
7. Using REF LEVEL FINE control, place signal peak at 7.1 divisions.
8. Adjust A9R72 XTL until signal is one division wide at the fifth graticule line ( $\mathbf{1 0} \mathrm{kHz}$ wide at $3-\mathrm{dB}$ points).
9. Set FREQ SPAN/DIV to 20 kHz and RESOLUTION BW to 30 kHz .
10. Center signal with TUNING control.
11. Adjust REF LEVEL FINE control to place signal at sixth graticule line.
12. Remove top guide rail. Connect crystal shorts (through cover access holes) across the following pairs of test points: A13TP1/TP2, A11TP1/TP2, and A11TP4/TP5.

## NOTE

Keep crystal spike centered during adjustments. The SYM and CTR adjustments for each crystal interact(the signal also drifts in this narrow span).
13. Adjust front-panel TUNING control to center bandpass spike (Figure 5-7) on the CRT display.

## NOTE

A non-metallic tuning tool is required for adjustments on the AII and A13 bandwidth filter assemblies.
14. Adjust A13C54 CTR for minimum signal amplitude. Then adjust A13C38 SYM and A13C54 CTR for a centered and symmetrical bandpass as shown in Figure 5-7.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(Cont'd)



FIGURE5-7. ADJUSTINGCRYSTALSYMMETRY AND CRYSTALCENTERING
15. Removecrystal short from A13TP1/TP2 and connect it across A13TP4/TP5.
16. Adjust A13C25 CTR for minimum signal amplitude. Then adjust A13C15 SYM and A13C25 CTR for a centered and symmetrical bandpass.
17. Removecrystal short from A11TP4/TP5 and connect it across A13TP1/TP2.
18. Adjust A11C54 CTR for minimum signal amplitude. Then adjust A11C38 SYM and A11C54 CTR for a centered and symmetrical bandpass.
19. Remove crystal short from A11TP1/TP2 and connect it across A11TP4/TP5.
20. Adjust A11C25 CTR for minimum signal amplitude. Then adjust A11C15 SYM and A11C25 CTR for a centered and symmetrical bandpass.
21. Remove the crystal shorts.
22. Set FREQ SPAN/DIV to 10 kHz and RESOLUTION BW to 30 kHz . Center signal on CRT with TUNING control.
23. Switch RESOLUTION BW from 30 kHz to 10 kHz and back several times. Verify that signal shift does not exceed 3 kHz ( 0.3 divisions). If signal shift is out of tolerance, return to step 11.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS (Cont'd)

LC Alignment

## CAUTION

Accidentally shorting the case of A9Q1 (directly below A9TP6) to ANY test point will cause catastrophic failure to Sweep Generator Assembly A9.
24. Set RESOLUTION BW control to 100 kHz . Jumper A9TP6 to A9TP8. This forces the BW7 line to + 15V. Set FREQ SPAN/DIV to 100 kHz .

NOTE
When Bandwidth Filter Assemblies A11 and A13 are installed with covers in place, midget copper alligator clips (HP Part Number 1400-0483)can be used to short test points to the cover.
25. Perform preliminary LC filter adjustments as follows:

NOTE
It might be necessary to adjust the REF LEVEL FINE control to obtain an onscreendisplay during the following adjustments.
a. Remove $\mathrm{A}!3$ cover and install A13 on extender board.
b. Short to ground the following test points: A13TP6, A11TP3, and A11TP6. (This widens all but one LC pole).
c. Center signal on CRT with TUNING control. Adjust A13C73 for minimum signal amplitude.
d. Disconnect short from A13TP6 and short to ground A13TP3.
e. Adjust A13C74 for minimum signal amplitude. Remove shorts from A13TP3, A11TP3, and AllTP6.
f. Reinstall A13 and cover. Short A13TP3 and A13TP6 to ground. Remove A11 cover and install All on extender board.
g. Short Al1TP6 to ground.
h. Adjust A11C73 for minimum signal amplitude.
i. Disconnect short from A11TP6 and short to ground A11TP3.
j. Adjust A11C74 for minimum signal amplitude.
k. Disconnect shorts from test points and reinstall A11 and cover. Leave jumper from A9TP6 to A9TP8 in place.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(Cont'd)

26. Short to ground A11TP3, A11TP6, and A13TP3. Set RESOLUTION BW to 100 kHz and set FREQ SPAN/DIV to 20 kHz .
27. Center signal on CRT with TUNING control. Adjust A13C45 LC CTR for symmetrical bandpass display on CRT. Use FINE TUNING control to keep crystal spike centered.

## NOTE

The crystal spike represents the center frequency of the crystal poles. In this procedure we are aligning the LC poles with the crystal poles. On some instruments, the crystal spike may not be very pronounced, in which case the center frequency of the 100 kHz RBW will have to be compared to the center frequency of the 30 kHz RBW.
28. Move short from A13TP3 to A13TP6. Leave other shorts in place. Center signal on CRT with TUNING control. Adjust A13C23 LC CTR for symmetrical bandpass display on CRT, keeping crystal spike centered.
29. Move short from A11TP6 to A13TP3. Leave other shorts in place. Center signal on CRT with TUNING control. Adjust A1lC45 LC CTR for symmetrical bandpass display on CRT, keeping crystal spike centered.
30. Move short from A11TP3 to A11TP6. Leave other shorts in place. Center signal on CRT with TUNING control. Adjust A11C23 LC CTR for symmetrical bandpass display on CRT, keeping crystal spike centered.
31. Disconnect shorts from A11TP6, A13TP3, A13TP6, and from ground. Remove jumper from A9TP6 and A9TP8.
32. Set FREQ SPAN/DIV to 10 kHz and RESOLUTION BW to 30 kHz . Center signal on CRT with TUNING control. Set RESOLUTION BW to 100 kHz and note where signal crosses center vertical graticule line.
33. Adjust A11C23, A11C45, A13C23, and A13C45 in succession so that amplitude of signal is peaked where it crosses center vertical CRT graticule line, repeating step 32 between adjustments as necessary.
34. Repeat steps 32 and 33 until 30 kHz and 100 kHz bandwidths are centered with each other. If signal shift between 30 kHz and 100 kHz bandwidths is greater than 10 kHz ( 1 division), repeat steps 24 through 33.

## Bandwidth Amplitude

35. Set AmplitudeScale switch to $1 \mathrm{~dB} /$ DIV and jumper A9TP6 to A9TP8.
36. Short A11TP3, A11TP6, A13TP3, and A13TP6 to ground.
37. Set RESOLUTION BW to 100 kHz and FREQ SPAN/DIV to 200 kHz .

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(Cont'd)

38. Adjust FINE TUNING and REF LEVEL FINE controls for a centered signal at 7 divisions from bottom graticule line.
39. Remove shorts from A13TP3 and A13TP6 and center signal with FINE TUNING control. Adjust A13R26 LC for a signal amplitude of 7 divisions. Replace shorts on A13TP3 and A13TP6.
40. Remove shorts from A11TP3 and A11TP6. Adjust A11R26 LC for a signal amplitude of 7 divisions.
41. Repeat steps 36 through 40 until no further adjustment is necessary. Remove shorts from A11TP3, A11TP6, A13TP3, and A13TP6.
42. Adjust A11R31 XTL and A13R31 XTL fully counterclockwise.
43. Set RESOLUTION BW to 1 kHz and FREQ SPAN/DIV to 10 kHz . Center signal with FINE TUNING control. Adjust A11R31 XTL and A13R31 XTL equally for a signal amplitude of 7 divisions. Each potentiometer should be adjusted to accomplish half the necessary increase in signal amplitude.
44. Remove jumper from A9TP6 and A9TP8.
45. Set FREQ SPAN/DIV to 500 kHz and RESOLUTION BW to 3 MHz .
46. Center signal with TUNING control. Adjust REF LEVEL FINE control for a signal amplitude of 7 divisions.
47. Step down RESOLUTION BW from 3 MHz tp 300 kHz . Variation in signal amplitude should be less than $\pm 0.4 \mathrm{~dB}$.
48. Set FREQ SPAN/DIV to 10 kHz , TIME/DIV to AUTO, and step down RESOLUTION BW from 100 kHz to 1 kHz . Variation of signal amplitude should be less than $\pm 0.7 \mathrm{~dB}$ from the 7 th division reference.
49. Repeat steps 35 through 46 until variation in signal amplitude is within limits.

## NOTE

If amplitude variation between crystal and LC poles exceeds specification, A11R7*IA13R7* can be replaced to bring the crystal poles to the amplitude of the LC poles.

## ADJUSTMENTS

## 5-22. 3-dB BANDWIDTH ADJUSTMENTS

## REFERENCE:

A9 Schematic

## DESCRIPTION:

The $3-\mathrm{dB}$ bandwidths for the 3 MHz through the 30 kHz RESOLUTION BW settings are adjusted using the CAL OUTPUT as the signal source. The 3-dB bandwidths for the $10 \mathrm{kHz}, 3 \mathrm{kHz}$, and 1 kHz RESOLUTION BW settings are adjusted by injecting a stable 321.4 MHz signal into the Third Converter (A10) of the spectrum analyzer.


FIGURE5-8. 3-dBBANDWIDTH ADJUSTMENTTESTSETUP

EQUIPMENT:
Signal Generator ..... HP 8640BFrequency Counter5342A
Step Attenuator ..... HP 355D
Adapter, Type N (m) to BNC (f) (2 required) ..... HP 1250-0780
Extender Cable Assembly ..... HP 5060-0303
Test Cable, BNC to SMB ..... HP 85680-60093
BNC Tee ..... HP 1250-0781

## ADJUSTMENTS

## 5-22. 3-dB BANDWIDTH ADJUSTMENTS (Cont'd)

## PROCEDURE:

1. Set spectrum analyzer controls as follows:

| FREQUENCYBAND | $0.01-3 \mathrm{GHz}$ |
| :---: | :---: |
| TUNING | 35 MHz |
| FREQ SPAN/DIV | 200 kHz |
| RESOLUTIONBW | 1 MHz |
| INPUTATTEN | 10 dB |
| REFERENCELEVEL | 0 dBm |
| Amplitude Scale | LIN |
| SWEEP TIME/DIV | 2 msec |
| SWEEPTRIGGER | FREE RUN |
| VIDEOFILTER | OFF |
| BASELINECLIPPER | ... OFF |
| 853A (if used) | G DISPLAY) |

2. Connect CAL OUTPUT to spectrum analyzer INPUT
3. Set a 7.1 division signal level on display with REF LEVEL FINE control. Signal will be 0.9 division from top graticule line.
4. Adjust A9R85 LC control for a 5 division wide signal at fifth graticule line.
5. Set RESOLUTION BW to 3 MHz and FREQ SPAN/DIV to 500 kHz . If necessary, reset signal level to 7.1 divisions with REF LEVEL FINE control. The bandwidth at the fifth graticule line should be between 5.4 and 6.6 divisions.

## NOTE

A9R85 LC may be further adjusted to bring the 3 MHz and 300 kHz bandwidths within limits; however, the final measurement of the 1 MHz bandwidth must be between 4.5 and 5.5 division at the fifth graticule line. (If the 3 MHz bandwidth cannot be brought within limits by adjustment of A9R85 LC, change the value of factory-selected resistor A9R120*. If the 300 kHz bandwidth cannot be brought within limits by adjustment of A9R85 LC, change the value of A9R116*.)
6. Set RESOLUTIONBW to 300 kHz and FREQ SPAN/DIV to 50 kHz . If necessary, reset signal level to 7.1 divisions with REF LEVEL FINE control. The bandwidth should be between 5.4 and 6.6 divisions at the fifth graticule line.
7. Set RESOLUTION BW to 100 kHz and FREQ SPAN/DIV to 20 kHz . If necessary, reset signal level to 7.1 divisions with REF LEVEL FINE control. The bandwidth should be between 4.3 and 5.7 divisions at the fifth graticule line.

## ADJUSTMENTS

## 5-22. 3-dB BANDWIDTH ADJUSTMENTS(Cont'd)

## NOTE

If the 100 kHz bandwidth is not within the specified limits, change the values of factory-selected resistors A11R19*, A11R43*, A13R19*, and A13R43*. If the bandwidth is too wide, increase the value of the resistors; if the bandwidth is too narrow, decrease the value of the resistors. The fac-tory-selected resistors need not be of equal value, but each must be within one standard value of the others.
8. Set RESOLUTION BW to 30 kHz and FREQ SPAN/DIV to 10 kHz . If necessary, reset signal level with REF LEVEL FINE control. The bandwidth should be between 2.6 and 3.4 divisions at the fifth graticule line.

## NOTE

If the 30 kHz bandwidth is not within the specified limits, change the values of factory-selectedresistors A11R23*, A11R48*, A13R23*, and A13R48*. If the bandwidth is too wide, decrease the value of the factory-selectedresistors; if the bandwidth is too narrow, increase the value of the resistors. The factory-selectedresistors must be within three standard values of the nominal value.
9. Connect signal generator as shown in Figure 5-8. Tune signal generator to approximately 21.4 MHz . Set the signal generator to approximately 0 dBm and the step attenuator to 10 dB . Set COUNTER MODE to EXPAND X 100.
10. Place spectrum analyzer on right side and connect test cable to Third Converter 21.4 MHz output connector A16J3. If connector is not present (some early instruments were not so supplied), remove AlOWl from A5J2 and connect AlOWl through a 10 dB step attenuator set to 30 dB and the signal generator set for a -10 dBm output level. The 10 dB step attenuator between BNC tee and frequency counter can be eliminated.
11. Set HP 8559A RESOLUTION BW to 1 MHz . Tune signal generator to peak signal on CRT display (near 21.4 MHz ) ( 321.4 MHz if injecting into A10W1). Adjust the output level of signal generator to place the signal at 7.1 divisions.
12. Set RESOLUTION BW to 3 kHz . Tune signal generator to peak signal on CRT display.
13. Adjust REF LEVEL FINE to place signal at 7.1 divisions.
14. Note the counter frequency and tune the signal generator 1500 Hz below the center frequency noted. Record the new counter frequency.

## ADJUSTMENTS

## 5-22. 3-dB BANDWIDTH ADJUSTMENTS(Cont'd)

15. Adjust A9R72 XTL to bring signal level to the fifth graticule line (three divisions from the top graticule line).
16. Increase signal generator frequency until signal on CRT display peaks and then decreases to the fifth graticule line. Record counter frequency.
17. Compare new frequency with frequency recorded in step 14. The difference between the two frequencies should be 2800 to 3200 Hz . If the bandwidth is not within limits, repeat steps 12 through 17, slightly readjusting A9R72 XTL, until the specified limits are achieved.
18. Set RESOLUTION BW to 10 kHz . Tune signal generator to peak signal on CRT display.
19. Adjust REF LEVEL FINE to place signal at 7.1 divisions.
20. Decrease signal generator frequency until the signal on the CRT display is at the fifth graticule line. Record this frequency.
21. Increase the signal generator frequency until the signal on the CRT display peaks and then decreases to the fifth graticule line. Record this frequency.
22. Compare new frequency with frequency recorded in step 20. The difference between the two frequencies should be 9.000 kHz to 11.000 kHz .

## NOTE

> A9R72 XTL may be further adjusted to bring the 10 kHz and 1 kHz bandwidths within limits; however, the final measurement of the 3 kHz bandwidth must be between 2700 Hz and 3300 Hz . (If the 10 kHz bandwidth cannot be brought within limits by adjusting A9R72 XTL, change the value of factoryselected resistor A9R111*. If the 1 kHz bandwidth cannot be brought within limits by adjusting A9R72 XTL, change the value of A9R109*.)
23. Set RESOLUTION BW to 1 kHz . Tune signal generator to peak signal on CRT display.
24. Adjust REF LEVEL FINE to place signal at 7.1 divisions.
25. Record the counter frequency.

## ADJUSTMENTS

## 5-22. 3-dB BANDWIDTH ADJUSTMENTS(Cont'd)

26. Increase signal generator frequency until signal on CRT display decreases to the fifth graticule line. Record the counter frequency.
27. Compare new frequency with frequency originally noted in step 25 . The difference between the two frequencies should be 450 Hz to 550 Hz .

## ADJUSTMENTS

## 5-23. RF GAIN ADJUSTMENT

## REFERENCE:

A12 Schematic

## DESCRIPTION

The RF gain (sensitivity) of Step Gain Assembly A12 is adjusted by injecting a 21.4 MHz signal at XA10P1. Third Converter Assembly A10 is removed and replaced with a special extender board for applying the 21.4 MHz signal from the signal generator.


FIGURE 5-9. RF GAIN ADJUSTMENT TEST SETUP

## EQUIPMENT:

Signal Generator ..... HP 8640B
Digital Voltmeter ..... HP 3456A
Power Meter ..... HP 435A/B
Power Sensor ..... HP 8481A
Special Extender Boardwith 51.1 ohm resistor
Test Cable, BNC (m) to Banana Plug ..... HP 10111A
Extender Cable Assembly ..... HP 5060-0303
Adapter, BNC (f) to Alligator Clips (2 required) ..... HP 8120-1292

## ADJUSTMENTS

## 5-23. RF GAIN ADJUSTMENT (Cont'd)

NOTE
To make special extender board, solder 51.1 ohm resistor from pin 18 to pin 22 of standard 24 pin extender board, HP Part No. 5060-0258. Leave resistor leads long for easy connection of clip leads.

## PROCEDURE:

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz .....  $01-3$
FREQ SPAN/DIV ..... 1 MHz
RESOLUTIONBW ..... 1 MHz
INPUTATTEN ..... 0 dB
REF LEVEL dBm ..... $-10$
REFLEVELFINE ..... 0
Amplitude Scale ..... LIN
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... FREE RUN
VIDEOFILTER ..... MIN
2. Connect equipment as shown in Figure 5-9. Resistor on extender board should be toward rear of HP 8559A.
3. Set signal generator frequency to 21.4 MHz . Set output level for approximately -5 dBm .

## NOTE

To remove Third Converter Assembly A10, it will be necessary to disconnect A10W1 from A5J2 and temporarily remove Marker Assembly A8 and Sweep Generator/Res BW Assembly A9.
4. Connect output of signal generator across 51.1 ohm resistor on special board using BNC to clip-lead adapter. The red lead (center conductor) should be connected to pin 18 of extender board.
5. Set signal generator frequency for peak amplitude on CRT display. Connect output of signal generator to power meter through a power sensor and set output level to $\mathbf{- 3} \mathrm{dBm}$. Reconnect signal generator output to clip-lead adapter.
6. Adjust A12R5 GAIN adjustment for signal one division from top graticule line. DVM should indicate $+700 \mathrm{mV} \pm 30 \mathrm{mV}$. Remove special extender board and replace Third Converter Assembly A10.

NOTE
If step gain adjustments will be performed next, do not reconnect A10W1 to A5J2.

## ADJUSTMENTS

5-23. RF GAIN ADJUSTMENT (Cont'd)

## CAUTION

When reconnecting A10W1 to A5J2, exercise caution; the connector should not be torqued more than 6 inch-pounds, otherwise damage to A5J2 will result.


#### Abstract

NOTE Front panel VERTICAL GAIN and POSN control settings can affect the voltage measured at A15TP1. Vertical calibration should be checked after adjusting A12R5 for $700 \mathbf{m V}$ (Refer to Section III).


## ADJUSTMENTS

## 5-24. STEP GAIN ADJUSTMENTS

## REFERENCE:

A12 Schematic

## DESCRIPTION:

REF LEVEL FINE, 0 dB , and -12 dB adjustments are properly set and step gains of $10 \mathrm{~dB}, 20 \mathrm{~dB}$, and 40 dB are adjusted.


FIGURE5-10. STEPGAIN ADJUSTMENTSTEST SETUP

## EQUIPMENT:

Signal Generator ..... HP 8640B
Step Attenuator ( $1 \mathrm{~dB} /$ Step) ..... HP 355C, Option H80
Step Attenuator ( $10 \mathrm{~dB} /$ Step) ..... HP 355D, Option H82
Digital Voltmeter ..... HP 3456A
Adapter, Type N(m) to BNC (f) ..... HP 1250-0780
Adapter, BNC (m) to SMC (m) ..... HP 1250-0831
Cable, BNC (m) to Banana Plug HP 10111A
Extender Cable Assembly ..... HP 5060-0303
Adapter, BNC (f) to Alligator Clips ..... HP 8120-1292

## ADJUSTMENTS

## 5-24. STEP GAIN ADJUSTMENTS (Cont'd)

## PROCEDURE:

1. Set spectrum analyzer controls as follows:

| FREQ SPAN/DIV | 1 MHz |
| :---: | :---: |
| RESOLUTIONBW | . 1 MHz |
| INPUTATTEN | 10 dB |
| REF LEVEL dBm |  |
| Amplitude Scale | $1 \mathrm{~dB} / \mathrm{DIV}$ |
| SWEEP TIME/DIV | AUTO |
| SWEEPTRIGGER | FREE RUN |
| VIDEO FILTER | MIN |

2. Connect equipment as shown in Figure $5-10$. Connect signal generator tuned to 321.4 MHz with approximately -30 dBm output to one side of a $1 \mathrm{~dB} /$ step attenuator. Connect step attenuator output to A10W1 through adapter. Tune signal generator frequency for peak amplitude on display.
3. Set step attenuator to 12 dB and REF LEVEL FINE to -12 . Set signal generator level for a signal one division down from top graticule line.
4. Adjust A12R39-12 D until signal stops rising on display, then adjust A12R39 counterclockwise until signal drops approximately one third to one half of a division.
5. Set signal generator level so signal is one division down from top graticule line on display.
6. Set step attenuator to $\mathbf{0} \mathrm{dB}$ and REF LEVEL FINE to $\mathbf{0}$.
7. Adjust A12R350 D adjustment for a signal level one division from top graticule line.
8. Set step attenuator to 12 dB and REF LEVEL FINE to -12 . DVM indication should be $700 \pm 30 \mathrm{mV}$ (offset). If offset is greater than $\pm 30 \mathrm{mV}$, repeat steps 3 through 8 until DVM indication is within limits.
9. Replace $1 \mathrm{~dB} /$ step attenuator with $10 \mathrm{~dB} /$ step attenuator set to 0 dB . Set REF LEVEL FINE control to 0 .
10. Tune signal generator frequency for peak amplitude on the display (near 321.4 MHz ).
11. Set signal generator level for a signal one division down from top graticule line. Set step attenuator to 10 dB and REF LEVEL dBm to -10 .
12. Adjust A12R6 10 D adjustment for signal level one division from top graticule line.
13. Set step attenuator to 20 dB and REF LEVEL dBm to $\mathbf{- 2 0}$.
14. Adjust A12R21 20 D adjustment for signal level one division from top graticule line.
15. Set attenuator to 40 dB and REF LEVEL dBm to -40 .

## ADJUSTMENTS

5-24. STEP GAIN ADJUSTMENTS(Cont'd)

## NOTE

Some video filtering might help reduce noise. Set VIDEO FILTER control so noise is reduced, but the signal amplituderemains unchanged.
16. Adjust A12R2940 D adjustment for signal level one division from top graticule line.
17. Check REF LEVEL dBm control from 0 to -50 as shown in Table 5-11.

| TABLE5-11. REFLEVELCONTROLCHECK |  |  |
| :---: | :---: | :--- |
| Reference Level <br> $(\mathbf{d B m})$ Attenuator <br> (dB)Deviation From <br> Reference $(700+20 \mathrm{mV}$ ) |  |  |
| 0 | 0 | Reference mV |
| -10 | 10 | Reference +40 mV |
| 20 | 20 | Reference 240 mV |
| -30 | 30 | Reference +40 mV |
| -40 | 40 | Reference +40 mV |
| -50 | 50 | Reference $\pm 40 \mathrm{mV}$ |

18. Reconnect A10W1 to A5J2.

## CAUTION

When reconnecting A10W1 to A5J2, exercise caution. The connector should not be torqued to more than 6 inch-pounds; otherwise, damage to A5J2 will result.

## ADJUSTMENTS

## 5-25. FIRSTCONVERTER ADJUSTMENTS

## REFERENCE:

A3, A4, AS, A6, and A7 Schematics

## DESCRIPTION:

The First LO (A6 YTO) is adjusted by monitoring the YTO output at the RF input connector (LO emission) and the tuning voltage (TUNE) output of the A7 Frequency Control board, and adjusting the YTO low-end frequency for 3 GHz at OV tuning voltage and 6 GHz at -10 V tuning voltage.


FIGURE5-11. FIRST CONVERTER ADJUSTMENTSTEST SETUP

## EQUIPMENT:

Frequency Counter ..... HP 5342A
Digital Voltmeter ..... HP 3456A
Comb Generator ..... HP 8406A
Cable, BNC (m) to Banana Plug ..... HP 10111A
Extender Cable Assembly ..... HP 5060-0303
Adapter, BNC (f) to Alligator Clips ..... HP 8120-1292
Cable Assembly, RG-214/U, Type N Connectors ..... HP 11500A

## PROCEDURE

1. Allow one-half hour warmup time of equipment with spectrum analyzer connected to mainframe with extender cable.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(Cont'd)

## First LO Adjustments

2. Connect DVM to A7TP6TUNE.
3. Set spectrum analyzer controls as follows:
INPUT ATTEN ..... 0 dB
FREQ SPAN/DIV ..... 0
ALTIF ..... OFF
4. Connect frequency counter to spectrum analyzer RF Input.
5. Jumper A16TP1 DIODE BIAS to ground. A16TP1 is located on the motherboard through a hole in the analyzer left side gusset.
6. Adjust front-panel TUNING control for DVM indication of 0.000 Vdc (fully counterclockwise).
7. Adjust A7R8 ( $3 \mathbf{~ G H z}$ ) for frequency counter indication of $\mathbf{3 . 0 0 0} \mathbf{G H z} \pm 1 \mathrm{MHz}$. (If this adjustment cannot be achieved, factory select resistor A7R3* can be added - if it is not installed - or decreased to provide the proper range. Select a value of 147 K ohms for A7R3*, initially, and decrease this value to no less than 56.2 K ohms.)
8. Adjust front-panelTUNING control for DVM indication of $\mathbf{- 1 0 . 0 0 0} \mathrm{Vdc}$.
9. Set A7R75 6 GHzF (fine) to approximately mid-range( $\mathbf{R} 75$ is a 20 -turn potentiometer).
10. Adjust A 7 R 476 GHzC (coarse) for a frequency counter indication of $6.000 \mathrm{GHz} \pm 2 \mathrm{MHz}$.
11. Retune front-panel TUNING control for $\mathbf{0 . 0 0 0}$ Vdc DVM indication and readjust A7R8 $3 \mathbf{G H z}$ if necessary for frequency counter indication of $3.000 \mathrm{GHz} \pm 1 \mathrm{MHz}$.
12. Tune front-panelTUNING control for $-\mathbf{1 0 . 0 0 0} \mathrm{Vdc} \mathrm{DVM}$ indication.
13. Lightly tap the top edge of the A7 Frequency Control board with the handle of a small screwdriver to seat controls.
14. Adjust A7R756 GHzF (fine) for frequency counter indication of $6.000 \mathrm{GHz} \pm 1 \mathrm{MHz}$.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(Cont'd)

## Alternate IF First LO Shift Check

15. Press front-panel ALT IF pushbutton IN to activate alternate IF.
16. Verify YTO frequency shift according to Table 5-12.

TABLE5-12. FIRSTLO SHIFT CHECK

| FREQUENCY BAND GHz | ALT IF | FREQUENCY COUNTER INDICATION |
| :---: | :---: | :--- |
| $1(.01-3)$ | OFF | Reference $(\mathbf{6 . 0 0 0} \mathbf{~ G H z})$ |
| $1(.01-3)$ | ON | Reference $-15 \mathbf{~ M H z} \pm 800 \mathbf{~ k H z}$ |
| $2(6-9)$ | ON | Reference $+15 \mathbf{~ M H \mathbf { 5 8 0 0 } \mathbf { ~ k H z }}$ |
| $3(3-9)$ | ON | Reference $-7.5 \mathbf{M H} \mathbf{5 4 0 0} \mathbf{~ k H z}$ |
| $4(9-15)$ | ON | Reference $+7.5 \mathbf{M H} \pm 400 \mathbf{~ k H z}$ |
| $5(6-15)$ | ON | Reference $-5 \mathbf{M H z} \pm 300 \mathbf{~ k H z}$ |
| $6(12.1-21)$ | ON | Reference $+5 \mathbf{~ M H z ~ 5 3 0 0 ~ \mathbf { k H z }}$ |

17. Remove jumper from A19TP1 DIODE BIAS to ground.

FM Driver Sensitivity and Delay Compensation Adjustment
18. Disconnect frequency counter from spectrum analyzer RF Input and connect comb generator to RF Input.
19. Set comb generator for 1 MHz comb teeth.
20. Set spectrum analyzer controls as follows:

21. Tune front-panel TUNING control for approximately 1.5 GHz indication on front-panel FREQUENCY GHz display.
22. Adjust A7R83 DC (Delay Compensation) until the comb teeth on the left half of the mainframe CRT display have the same approximate spacing as those on the right half.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(Cont'd)

23. Adjust front-panel TUNING FINE control to place a comb tooth on the first vertical graticule line of the CRT display.
24. Adjust A7R92 FM to place a comb tooth on the ninth vertical graticule line of the CRT display.
25. Switch to 10 kHz RES BW and adjust A7R83 DC for even spacing of the comb teeth on the first two graticule lines.
26. Readjust TUNING FINE control to place a comb tooth on the first vertical graticule line. Adjust A7R92 FM to place a comb tooth on each of the graticule lines while keeping the first comb tooth aligned using the TUNING FINE control.
27. Repeat steps 25 and 26 to achieve the best span linearity.

## NOTE

## Trim potentiometer A7R83 (DC) controls the amount of delay compensation; A7R96* controls the time constant of the compensation. If the adjustment of A7R83 does not result in even comb tooth spacing, R96* will have to be re-selected for even spacing.

28. Switch to 30 kHz RES BW. The comb tooth spacing should not change. If there is a shift of the comb teeth, repeat steps 22 through 27 for best compromise in span linearity.
29. Tune to approximately 100 MHz and verify that a comb tooth placed on the first vertical graticule line, using the TUNING FINE control, will align the ninth comb tooth with the ninth vertical graticule line $\pm 1$ minor division.
30. Select the 10 kHz RES BW and verify that a comb tooth on the first vertical graticule line will align the ninth comb tooth with the ninth graticule line $\pm 1$ minor division.
31. Select the 30 kHz RES $\mathbf{B W}$ and repeat step 29 for a frequency of approximately 2.5 GHz .
32. Repeat step 30 for a frequency of approximately 2.5 GHz .
33. If necessary, A7R83 (DC) and A7R92 (FM) may be compromise adjusted for best span linearity at the three frequenciesindicated.
34. Set comb generator for $100-\mathrm{MHz}$ comb teeth.
35. Adjust front-panel TUNING control for 0.10 GHz indication on FREQUENCY display.
36. Set FREQ SPAN/DIV to 2 MHz .
37. Adjust TUNING to place 100-MHz comb tooth on center graticule line.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(Cont'd)

38. Set FREQ SPAN/DIV to 1 MHz . Note position of comb tooth.
39. Adjust A7R81 (MO) to place comb tooth midway between position noted in step 38 and center graticule line.
40. Set FREQ SPAN/DIV to 2 MHz .
41. Adjust TUNING to place comb tooth in center graticule line.
42. Set FREQ SPAN/DIV to 1 MHz . Note displacement of comb tooth from center graticule line.
43. Repeat steps 36 through 42 until displacement of comb tooth is less than 0.2 major division when FREQ SPAN/DIV is switched from 2 MHz to 1 MHz .

## ADJUSTMENTS

## 5-26. SECOND CONVERTER ADJUSTMENTS

## REFERENCE:

A3, A4, A5, A6, and A8 Schematics

## DESCRIPTION:

First, the Second LO is adjusted for proper frequency using a frequency counter. Next, the signal identifier (SIG ID) and alternate IF (ALT IF) signals are adjusted so that the displayed signal appears in the same location in both regular and alternate IF and the signal identifier is always 1 MHz away from this signal in either regular or alternate IF. Last, the first IF bandpass filter is aligned for a bandpass wide enough to allow for the first LO shift and amplitude characteristicssuch that there will be a minimal shift in displayed signal amplitude when the analyzer is switched from regular to alternate IF.


FIGURE5-12. SECONDCONVERTERADJUSTMENTSTEST SETUP

## EQUIPMENT:

Frequency Counter ..... HP 5342A
FunctionGenerator ..... HP 3310A
Test Cable, BNC (m) to SMB (f) ..... HP 85680-60093
Adapter, BNC (f) to Alligator Clips ..... HP 8120-1292
Adapter, SMB (m) to SMB (m) ..... HP 1250-0669
Adapter, SMB (f) to SMB (f) ..... HP 1250-0672
Adapter, Type N (m) to BNC (f) (2 required) ..... HP 1250780
Special Tuning Tool, Allen driver inserted through drilled-out 5/16 inch nut driver ..... HP 08555-60107
Oscilloscope ..... HP 1740A
Extender Cable Assembly ..... HP 5060-0303

## ADJUSTMENTS

## 5-26. SECOND CONVERTER ADJUSTMENTS(Cont'd)

## PROCEDURE:

## Second LO Preliminary Adjustment

1. Allow one-half hour warm-up time of equipment with analyzer connected to mainframe with extender cable.
2. Connect frequency counter input to A5J3 2nd LO output using the test cable and two SMB adapters.
3. Select Band $1(.01-3)$ and Alternate IF on spectrum analyzer front-panel by depressing these pushbuttons.
4. Using the special Allen driver/nut driver tuning tool, adjust A5Z4 2nd LO FREQUENCY for a frequency counter indication of $2671.1 \mathrm{MHz} \pm 0.5 \mathrm{MHz}$.
5. Connect spectrum analyzer CAL OUTPUT to RF INPUT and adjust front-panel TUNING controls to center the calibrator signal on the CRT display.
6. Set spectrum analyzer controls as follows:
```
FREQ SPAN/DIV . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 1 MHz
```




```
FREQUENCY BAND GHz ...........................................................................
SIG IDENT .................................................................................... OFF
```



```
853A ............................. . . TRACE A & B STORE BLANK (ANALOGDISPLAY)
```

7. Depress front-panel SIG IDENT and ALT IF pushbuttons.
8. Turn SIG IDENT off and on while monitoring the display. The signal traces which appear when SIG IDENT is switched on are the signal identifier signals. The others are the alternate IF signals.
9. Adjust TUNING to place one of the signal identifier signals on a graticule line. This will be the reference graticule line.
10. Turn ALT IF off. Adjust A8R34 REG to center the signal identifier signal on the reference graticule line.
11. Turn ALT IF on. Verify that the signal identifier signal appears on reference graticule line. If not, repeat step 10.
12. Adjust A8R40 SIG ID to place the alternate IF signal 1 MHz (1 division) higher than the signal identifier signal.
13. Turn ALT IF off. Adjust A8R39 OFF to center the signal on the same graticule line as the alternate IF signal ( 1 MHz higher than reference graticule line).

## ADJUSTMENTS

## 5-26. SECOND CONVERTER ADJUSTMENTS(Cont'd)

14. Turn ALT IFon and verify that the two signals do not appear to move.
15. Change spectrum analyzer FREQ SPAN/DIV to 500 kHz .
16. Repeat steps 7 through 14 if necessary to align both signal identifier signals and both alternate IF signals and spaced 1 MHz (2 divisions) apart on the CRT display.
17. Depress front-panel ALT IF pushbutton. Turn SIG IDENT off.
18. Note Second LO frequency on frequency counter.
19. Adjust A5Z4 2nd LO FREQUENCY if necessary for a frequency counter indication of $2671.1 \mathrm{MHz} \pm 0.5$ MHz.
20. If second LO frequency is readjusted, recheck second LO shift adjustments, steps 5 through 16.
21. Set spectrum analyzer controls as follows:

22. Adjust front-panel REF LEVEL dBm and REF LEVEL FINE controls to place signal peak in upper half of CRT display for convenient viewing.
23. Adjust front-panelTUNING control to place signal peak 3.75 divisions to the left of center screen on the CRT.
24. Connect the HIGH output of the function generator to an oscilloscope and adjust function generator output for a OV to +20 V ramp and frequency to 500 Hz .
25. Disconnect the function generator from the oscilloscope and connect it to A5A2TP1 VARACTOR by using the 8120-1292 adapter.
26. The following adjustments refer to aligning the Second Converter after internal repair of the converter. If the entire converter has been replaced, it will probably not be necessary to perform all of the adjustments.
27. Adjustments A5Z1, A5Z2, A5Z3, and A5L2 are used to align the bandpass filter and output match of the Second Converter. Z1 and L2 are used to adjust amplitude and Z2 and Z3 are used to center the response about the center frequency.

## ADJUSTMENTS

## 5-26. SECOND CONVERTER ADJUSTMENTS(Cont'd)

28. The requirements for the converter response are illustrated in Figure 5-13a and are as follows: Bandpass should be at least $17 \mathrm{MHz}, 1 \mathrm{~dB}$ down. Amplitude of response at 3.75 divisions to the left and 3.75 divisions to the right of center screen should be as near the same as possible. These are the positions of the IF signals for regular and alternate IE This is illustrated in composite photo Figure 5-13b. These positions should be the same distance from the roll-off point at each end of the response curve.
29. Distance from roll-off points can be checked by centering signal with function generator disconnected then reconnecting function generator and switching ALT IF on and off. This is illustrated in Figure 5-13c and 513d.
30. Adjust $\mathbf{A} 5 \mathrm{Z} 1, \mathrm{Z} 2, \mathrm{Z} 3$ and L 2 to satisfy the requirements of the converter response. If entire converter has been replaced, try adjusting A5Z1 and L2 first. Do not adjust A2 and A3 unless it is necessary to meet requirements. Do not sacrifice amplitude to achieve flatness.
31. When adjustment is complete, disconnect function generator from A5A2TP1, center signal on display, and turn ALT IF on and off while monitoring signal.
32. Amplitude difference between regular and alternate IF should be no more than 0.4 dB .

## ADJUSTMENTS

## 5-26. SECOND CONVERTER ADJUSTMENTS(Cont'd)

THESE POINTS SHOULD BE AT SAME AMPLITUDE WITH BANDPASS
$>17 \mathrm{MHz}$ WIDE 1 dB DOWN AS SHOWN

a TYPICAL BANDPASS RESPONSE

THESE POINTS SHOULD BE AT SAME AMPLITUDE LEVEL $\pm 0.4 \mathrm{~dB}$

ALTERNATE

b. COMPOSITE PHOTO SHOWING LOCATION OF IF SIGNALS
$>17 \mathrm{MHz}$ BETWEEN THESE

TWO POINTS IF SIGNAL

LOCATION OF ALTERNATE IF SIGNAL
c. ROLL-OFF AT HIGH-END OF RESPONSE
d. ROLL-OFF AT LOW-END OF RESPONSE
$\Delta \mathbf{F}_{1}$ AND $\Delta \mathbf{F}_{2}$ MUST $\mathrm{BE} \geqslant 1 \mathrm{MHz}$ BUT $\leqslant 4 \mathrm{MHz}$
$\Delta F_{1}$ MUST EQUAL $\Delta F_{2} \pm 0.2 \mathrm{MHz}$

FIGURE5-13. FIRST IF BANDPASS FILTER RESPONSE

## ADJUSTMENTS

## 5-27. THIRD CONVERTER ADJUSTMENTS

## REFERENCE:

A10 Schematic

## DESCRIPTION:

First, the Third LO is adjusted for proper frequency using a frequency counter. Next, the second IF bandpass filter is aligned by injecting a frequency modulated 321.4 MHz signal at the necessary level and monitoring the 21.4 MHz output signal with another spectrum analyzer. The filter is aligned for a bandpass wide enough to accommodate any frequency drift occurring in the RF section of the analyzer and the amplitude necessary to provide the overall gain characteristics required by the analyzer.


FIGURE5-14. THIRDCONVERTER ADJUSTMENTSTESTSETUP

## EQUIPMENT

Frequency Counter .HP 5342ASweep Oscillator . ..... HP 8620C/86222A
Spectrum Analyzer ..... HP 8569B
Function Generator ..... HP 3310A
Test Cable, BNC (m) to SMB (f) (2 required) ..... HP85680-60093
Adapter, SMC (m) to SMC (m) ..... HP 1250-0827
Adapter, Type N (m) to BNC (f) (3 required) ..... HP 1250-0780
20 dB Attenuator ..... HP 8491B, Option 020
10 dB Attenuator ..... HP 8491B, Option 010
Test Cable, BNC (m) to SMC (f) ..... HP 11592-60001
Extender Cable Assembly ..... HP 5060-0303

## ADJUSTMENTS

## 5-27. THIRD CONVERTER ADJUSTMENTS(Cont'd)

## PROCEDURE:

1. Allow one-half hour warmup time of equipment with analyzer connected to mainframe with extender cable.

## Third LO Adjustment

2. Connect frequency counter to A10J1 300 MHz output using the BNC to SMB test cable.
3. Adjust A10L12 LO ADJ for frequency counter indication of $300.00 \mathrm{MHz} \pm 0.1 \mathrm{MHz}$.

## Second IF Bandpass Filter Alignment

4. Disconnect blue cable A10W1 at second converter output connector A5J2.
5. Set sweep oscillator controls for an output of 321.4 MHz at 0 dBm (measured directly at output of sweep oscillator). Use the frequency counter and spectrum analyzer to set the output frequency and amplitude.
6. Connect output through 10 and 20 dB attenuators to cable disconnected in step 4 , using the BNC to SMB test cable and SMB male to SMB male adapter.
7. Place analyzer on right side and connect test cable to Third Converter 21.4 MHz output connector. If connector is not present (some early instruments were not so supplied), it is necessary to solder a coaxial cable to XA10P1 pin 18 and ground (center conductor of coaxial cable to XA10P1 and shield to ground).
8. Connect test cable or soldered cable to 8569 B spectrum analyzer input.
9. Set 8569 B spectrum analyzer controls as follows:

| TUNING | 21.4 MHz |
| :---: | :---: |
| RESBW | 300 kHz |
| FREQ SPAN/DIV | $1 \mathrm{MHz} / \mathrm{DIV}$ |
| INPUTATTEN | . 10 dB |
| REF LEVEL dBm. | $-10 \mathrm{dBm}$ |
| Amplitude Scale | 10 dB LOG |
| TIME/DIV | $1 \mathrm{mSEC} / \mathrm{DIV}$ |

10. Set H P 8559A RES BW to 1 kHz and TRIGGER to FREE RUN.
11. Center the 21.4 MHz signal on the 8569 B spectrum analyzer, adjust reference level to place signal within top division on CRT, then change scale to $1 \mathrm{~dB} /$ DIV. Adjust REF LEVEL FINE to place signal peak in upper half of display.
12. Set function generator controls for a 200 Hz triangle wave output and connect to sweep oscillator RF PlugIn rear-panel FM input. Set FM/NORM/PL switch to FM.

## ADJUSTMENTS

## 5-27. THIRD CONVERTER ADJUSTMENTS(Cont'd)

13. Adjust function generator amplitude and frequency for at least 10 MHz deviation ( $\pm 5 \mathrm{MHz}$ ) and an easy-to-view display on the 8569 B spectrum analyzer. Refer to Figure 5-15. Increasing the frequency of the function generator will increase the swept frequency range of the sweep oscillator.
14. Adjust second IF bandpass filter adjustments A 10 C 9 through A 10 C 12 for the flattest bandpass response possible at the greatest amplitude possible centered at 21.4 MHz and at least 6 MHz ( 6 divisions) wide at 1 dB down from the highest point on the response curve. Do not sacrifice large amounts of amplitude for flatness. Some early instruments may display ripple on the response. This ripple should be $\leq 1 \mathrm{~dB}$ peak-topeak. Peak of adjusted response should be at $-10 \mathrm{dBm} \pm 2 \mathrm{~dB}$.

## NOTE

The output level of the third converter is actually 0 dBm . Due to the mismatch error ( $\approx 9.5 \mathrm{~dB}$ ) encountered in this measurement, the level measured will be approximately $\mathbf{- 1 0 ~ d B m}$.
15. Refer to Figure 5-15 for example of properly adjusted bandpass response and requirements for response.


FIGURE 5.15. SECONDIF BANDPASS FILTERRESPONSE

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS

## REFERENCE:

A3, A4, A5, A6, and A12 Schematics

## NOTE

Perform CAL OUTPUT and REF LEVEL CAL adjustments (5-29) before proceeding with frequency response adjustments.

## DESCRIPTION:

Frequency Response (flatness) is adjusted in six parts corresponding to the six harmonic bands of the analyzer. In each band, the analyzer is swept-tuned with a tracking signal source comprising a sweep oscillator and synchronizer. The sweep oscillator is tuned with an external sweep ramp generated by scaling the analyzer sweep output (AUX D) with a special tuning voltage circuit. This provides synchronization of the sweeps of the two instruments (sweep oscillator and analyzer), thus providing phase-lock of the two instruments. Each of the bands is adjusted for optimum flatness and all bands are adjusted for equal amplitudes.


FIGURE5-16. FREQUENCYRESPONSEADJUSTMENTSTESTSETUP

## ADJUSTMENTS

5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)


FIGURE5-17. TUNING VOLTAGECIRCUIT

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)

## EQUIPMENT:

| Sweep Oscillator | HP 8620C |
| :---: | :---: |
| RF Plug-In (. $01-2.4 \mathrm{GHz}$ ) | HP 8622A/B |
| RF Plug-In (2-22 GHz) | HP 86290B-H08 |
| Synchronizer | HP 8709A-H10 |
| Power Meter | HP 435A/B |
| Power Sensor ( $.01-18 \mathrm{GHz}$ ) | HP 8481A |
| Power Sensor (.05-26.5 GHz) | HP 8485A |
| Crystal Detector ( $.01-26.5 \mathrm{GHz}$ ) | HP 33330C |
| 20 dB Attenuator | HP 8491B, Option 020 |
| Tuning Voltage Circuit | Refer to Figure 5-17 |
| Cable, SMA (m) to SMA (m) | HP8120-1578 |
| Cable, BNC (m) to SMC (f) | HP 11592-60001 |
| Adapter, Type N (m) to SMA (f) (2 required) | HP 1250-1250 |
| Adapter, Type N(f) to SMA (f) (2 required) | HP 1250-1745 |
| Adapter, Type N (f) to Type N(f) | HP 1250-1472 |
| Extender Cable Assembly | HP 5060-0303 |
| Power Splitter | 11667A-C16 |

## PROCEDURE:

1. Allow one-half hour warmup time of equipment with analyzer connected to mainframe with extender cable.
2. Connect equipment as shown in Figure 5-16 with power meter/power sensor connected to 20 dB attenuator and HP 86222A/B (. $01-2.4 \mathrm{GHz}$ plug-in) installed in sweep oscillator mainframe.
3. Set sweep oscillator controls as follows:

## Mainframe:

SWEEP MODE ..... EXT
MARKERS ..... OFF
All rear panel switches ..... OFF
Plug-in
RF OFF/ON ..... OFF
ALC ..... EXT
POWER LEVEL ..... Fully CCW
FM/NORM/PL (rear-panel) ..... PL
4. Set synchronizer controls as follows:
POLARITY
$6 \mathrm{MHz} / \mathrm{VOLT}$

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)

5. Set spectrum analyzer controls as follows:
REF LEVEL FINE ..... 0 dBm
REF LEVEL dBm ..... $-20$
INPUTATTEN ..... 10 dB
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
FREQ SPAN/DIV ..... F (full)
RESOLUTIONBW ..... 3 MHz
FREQUENCY BAND GHz .....  $01-3$
TIME/DIV ..... 20 msec
TRIGGER ..... FREE RUN
BLCLIP ..... OFF
VIDEOFILTER ..... MIN
ALTIF ..... OFF
SIGIDENT ..... OFF
TUNING ..... 2.5 GHz

## $.01-3$ GHz Adjustment

6. Place sweep oscillator plug-in RF OFF/ON switch to ON.
7. Adjust sweep oscillator controls for a CW output of 2 GHz at -7 dBm .
8. Disconnect power meter/power sensor and connect 20 dB attenuator directly to analyzer RF INPUT as shown in Figure 5-16.
9. Adjust sweep oscillator controls for full sweep.
10. Adjust Tuning Voltage Circuit GAIN control fully clockwise then adjust OFFSET control to center phaselocked signal on CRT. Refer to Figure 5-18a.


FIGURE 5-18. ILLUSTRATION OF PHASE-LOCKING PROCEDURE

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)

11. Adjust Tuning Voltage Circuit GAIN control to expand the phase-locked display over $81 / 2$ divisions on CRT (.01-2.4 GHz). Refer to Figure 5-18b. It may be necessary to readjust OFFSET slightly to achieve phase-lock over entire range.
12. Optimum phase-lock is indicated by a smooth trace over full swept frequency range on CRT and minimum needle movement on synchronizer phase error meter.
13. Place CRT trace in top division of display using analyzer REF LEVEL FINE control.
14. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} /$ DIV and adjust REF LEVEL FINE control to place trace in upper half of display.
15. Remove CAUTION label (PC Board) from cover of A12 Step Gain by removing two pozi-drive screws.
16. Adjust A12R72 V1 (bias) for maximum amplitude of trace on CRT.
17. Adjust A12R47 1B (tilt) for best overall flatness of trace on CRT.

## NOTE

Remember, you are viewing only a portion $(.01-2.4 \mathrm{GHz})$ of Band 1. The
remainder of Band 1 may have an effect on this adjustment.
18. Note highest and lowest points on CRT trace for reference. Also note level of trace at 2.1 GHz position on CRT (8th vertical graticule line).

Highest $\qquad$ Lowest $\qquad$ 2.1 GHz $\qquad$
19. Place sweep oscillator LINE switch OFF.
20. Disconnect cables from HP $86222 \mathrm{~A} / \mathrm{B}(.01-2.4 \mathrm{GHz}$ plug-in) and remove plug-in from sweep oscillator mainframe.
21. Install HP 86290B ( $2-18.6 \mathrm{GHz}$ plug-in) or HP 86290B-H08 (2-22 GHz plug-in), if available, in sweep oscillator mainframe and reconnect cables as shown in Figure 5-16 with 20 dB attenuator connected to analyzer RF INPUT.
22. Set RF plug-in controls the same as for the plug-in removed (refer to step 3) and select Band 4 (2-18.6 or $2-22 \mathrm{GHz}$ ) on sweep oscillator mainframe.
23. Place RF plug-in RF OFF/ON switch ON. Change analyzer AmplitudeScale to $10 \mathrm{~dB} / \mathrm{DIV}$.
24. Adjust sweep oscillator for swept output from 2 to 3 GHz .
25. Adjust spectrum analyzer TUNING controls for FREQUENCY GHz indication of 2.500 and change FREQ SPAN/DIV to 100 MHz . Make sure RES BW remains at 3 MHz .

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)

26. Adjust Tuning Voltage Circuit GAIN and OFFSET controls to phase-lock swept signal from 2 to 3 GHz .
27. Adjust RF plug-in POWER LEVEL control to place trace at approximately -27 dBm on CRT.
28. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} /$ DIV.
29. Adjust RF plug-in POWER LEVEL control to place 2.1 GHz position of CRT trace to same level as that noted in step 18.
30. Note flatness of trace from 2 to 3 GHz . Total deviation of trace from Ol to 3 GHz should not exceed 2.0 dB.
31. Center trace about the sixth horizontal graticule line on the CRT using analyzer REF LEVEL FINE control. Do not change this setting for remainder of procedure. This will be used as amplitude reference for remaining frequency bands.

## NOTE

Be careful during the adjustment of the remaining frequency bands. It is possible to achieve a phase-locked display of a frequency range other than the one selected on the spectrum analyzer. For example, it is possible to achieve a phase-locked display for $6-9 \mathrm{GHz}$ when $3-9 \mathrm{GHz}$ has been selected. This can be avoided by paying close attention to synchronizer polarity and RF plug-in band switch points. Figure 5-19 illustrates the typical appearance of each of the bands. Use it for reference.

## 6 to 9 GHz Adjustment

32. Change synchronizer POLARITY to + .
33. Change spectrum analyzer FREQ SPAN/DIV to F (full), Amplitude Scale to $10 \mathrm{~dB} / \mathrm{DIV}$, and FREQUENCY BAND GHz to $6-9$. Set TUNING to above 9 GHz .
34. Adjust sweep oscillator for swept output from 6 to 9 GHz .
35. Adjust Tuning Voltage Circuit GAIN and OFFSET controls to phase-lock swept signal from 6 to 9 GHz . Refer to Figure 5-19b.
36. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} /$ DIV.
37. Adjust A12R58 2A (offset) and A12R48 2B (tilt) for best overall flatness of trace from 6 to 9 GHz with trace approximately centered about the sixth horizontal graticule line on the CRT.
38. Total deviation of CRT trace from 6 to 9 GHz should not exceed 2.0 dB .

## ADJUSTMENTS

5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)


FIGURE5-19. TYPICAL PHASE-LOCKEDRESPONSEOF EACH FREQUENCYBAND

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)

## 3 to 9 GHz Adjustment

39. Change synchronizer POLARITY to - .
40. Change spectrum analyzer Amplitude Scale to $10 \mathrm{~dB} /$ DIV and FREQUENCY BAND GHz to $3-9$.
41. Adjust sweep oscillator for swept output from 3 to 9 GHz .
42. Adjust Tuning Voltage Circuit GAIN and OFFSET controls to phase-lock swept signal from 3 to 9 GHz . Refer to Figure 5-19c.
43. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} / \mathrm{DIV}$.
44. Adjust A12R83 V2 - (bias), A12R59 3A (offset), and A12R49 3B (tilt) for best overall flatness of trace from 3 to 9 GHz with trace approximately centered about the sixth horizontal graticule line on the CRT.
45. Total deviation of trace from 3 to 9 GHz should not exceed 3.0 dB .

## 9 to 15 GHz Adjustment

46. Change synchronizer POLARITY to + .
47. Change spectrum analyzer Amplitude Scale to 10 dB /DIV and FREQUENCY BAND GHz to $9-15$.
48. Adjust sweep oscillator for swept output from 9 to 15 GHz .
49. Adjust Tuning Voltage Circuit GAIN and OFFSET controls to phase-lock swept signal from 9 to 15 GHz . Refer to Figure 5-19d.
50. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} / \mathrm{DIV}$.
51. Adjust A12R87 V2 + (bias), A12R60 4A (offset), and A12R51 4B (tilt) for best overall flatness of trace from 9 to 15 GHz with trace approximately centered about the sixth horizontal graticule line on the CRT.
52. Total deviation of trace from 9 to 15 GHz should not exceed 3.6 dB .

## 6 to 16 GHz Adjustment

53. Change synchronizer POLARITY to - .
54. Change spectrum analyzer Amplitude Scale to $10 \mathrm{~dB} /$ DIV and FREQUENCY BAND GHz to 6-15.
55. Adjust sweep oscillator for swept output from 6 to 15 GHz .
56. Adjust Tuning Voltage Circuit GAIN and OFFSET controls to phase-lock swept signal from 6 to 15 GHz . Refer to Figure 5-19e.

## ADJUSTMENTS

## 5-28. FREQUENCY RESPONSE ADJUSTMENTS(Cont'd)

57. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} /$ DIV.
58. Adjust A12R71 V3 - (bias), A12R61 5A (offset), A12R53 5B (tilt), and A12R54 5C (breakpoint) for best overall flatness of trace from 6 to 15 GHz with trace approximately centered about the sixth horizontal graticule line on the CRT.
59. Total deviation of trace from 6 to 15 GHz should not exceed 4.2 dB .

## 12.1 to 21 GHz Adjustment

## NOTE

## If an HP 86290B-H08 (2-22 GHz plug-in) is not available, a standard HP 86290B ( 2 - 18.6 GHz plug-in) may be used to adjust the spectrum analyzer flatness from 12.1 to 18.6 GHz using this procedure.

60. Change synchronizer POLARITY to + .
61. Change spectrum analyzer Amplitude Scale to $10 \mathrm{~dB} /$ DIV and FREQUENCY SPAN GHz to 12.1 - 21 .
62. Adjust sweep oscillator for swept output from 12 to 18.6 GHz or 12 to 21 GHz , depending on which RF plug-in is used.
63. Adjust Tuning Voltage Circuit GAIN and OFFSET controls to phase-lock swept signal from 12 to 18.6 GHz or 12 to 21 GHz . Refer to Figure 5-19f.
64. Change spectrum analyzer Amplitude Scale to $1 \mathrm{~dB} / \mathrm{DIV}$.
65. Adjust A12R70 V3+ (bias), A12R62 6A (offset), A12R55 6B (tilt), and A12R566C (breakpoint) for best overall flatness of trace from 12.1 to 18.6 GHz or 12.1 to 21 GHz with trace approximately centered about the sixth horizontal graticule line on the CRT.
66. Total deviation of trace from 12.1 to 18 GHz should not exceed 4.6 dB and from 18 to 21 GHz should not exceed 6.0 dB .
67. If unable to achieve flatness specifications, it may be necessary to plot a characterization curve of the sweep oscillator output from 12 to 21 GHz . This can be done by measuring the power output of the sweep oscillator (at the 20 dB attenuator) every 500 MHz from 12 to 21 GHz using a power meter. The values obtained can then be plotted on the CRT and flatness adjusted to this corrected curve. Total deviation then becomes the difference between the largest positive and largest negative deviation from the plotted curve.

This characterization will require the use of an $18-21 \mathrm{GHz}$ thermistor mount and K-Band waveguide adapter in addition to equipment previously used. Recommended equipment is listed under EQUIPMENT in this procedure along with previously used equipment.

## ADJUSTMENTS

## 5-29. CAL OUTPUT AND REF LEVEL CAL ADJUSTMENTS

## NOTE

These adjustments should be followed by frequency response adjustments, since adjustment of A12R57 1A (offset) will shift the freapuency response of Band 1 (. $01-3 \mathrm{GHz}$ ).

## REFERENCE:

A10 and A12 Schematics

## DESCRIPTION:

The 35 MHz CAL OUTPUT signal is adjusted for proper amplitude and frequency using a power meter and frequency counter. Adjustment range of the front-panel REF LEVEL CAL control is set using the CAL OUTPUT signal as a reference.


## EQUIPMENT:

| Frequency Counter | HP 5342A |
| :---: | :---: |
| Power Meter | HP 432A/435A/B |
| Power Sensor | H P 8481A |
| Adapter, Type N (m) to BNC (f) | H P 1250-0780 |
| Extender Cable Assembly | H P 5060-0303 |

## ADJUSTMENTS

## 5-29. CAL OUTPUT AND REF LEVEL CAL ADJUSTMENTS(Cont'd)

## PROCEDURE:

## CAL OUTPUT Adjustment

1. Allow one-half hour warmup time of equipment with spectrum analyzer connected to mainframe with extender cable.
2. Connect power meter/power sensor to front-panel CAL OUTPUT connector as shown in Figure 5-20.
3. Place spectrum analyzer on its right side. Adjust A10R13 CAL AMPL for power meter indication of $-10.0 \mathrm{dBm} \pm 0.1 \mathrm{~dB}$. A10R13 is accessed through motherboard.
4. Disconnect power meter/power sensor and connect frequency counter to CAL OUTPUT connector.
5. Adjust A10C46 CAL FREQ for frequency counter indication of $35.00 \mathrm{MHz} \pm 0.01 \mathrm{MHz}$. A10C46 is accessed through motherboard.
6. Repeat steps 2 through 5 until CAL OUTPUT signal is properly adjusted for both amplitude and frequency.
7. Connect CAL OUTPUT to analyzer INPUT.
8. If not already removed, removeCAUTION label (PC Board) from A12 Step Gain.
9. Set spectrum analyzer controls as follows:

| Amplitude Scale | $10 \mathrm{~dB} / \mathrm{DIV}$ |
| :---: | :---: |
| REF LEVEL dBm |  |
| INPUT ATTEN | 10 dB |
| FREQ SPAN/DIV | 1 MHz |
| RESOLUTIONBW | 1 MHz |
| TIME/DIV | AUTO |
| TRIGGER | FREE RUN |
| FREQUENCY BAN | . 01 - |

10. Center 35 MHz calibration signal on CRT using TUNING controls.
11. Adjust front-panel REF LEVELCAL fully counterclockwise.
12. Change Amplitude Scale to 1 dB /DIV and adjust REF LEVEL FINE if necessary to place signal peak on first horizontal graticule line above bottom reference line of CRT.
13. Adjust front-panel REF LEVEL CAL to raise signal peak three divisions ( $\mathbf{3} \mathrm{dB}$ ) on CRT (to fourth graticule line above bottom referenceline on CRT).
14. Change Amplitude Scale to $10 \mathrm{~dB} /$ DIV, REF LEVEL dBm to -10 , and set REF LEVEL FINE to 0 dBm .

## ADJUSTMENTS

## 5-29. CAL OUTPUT AND REF LEVEL CAL ADJUSTMENTS(Cont'd)

15. Signal peak should now be approximately at top graticule line (Reference Level) on CRT.
16. Switch between 10 dB /DIV and LIN while adjusting A12R57 1A (offset) to place signal peak at same level in both $10 \mathrm{~dB} /$ DIV and LIN.
17. Level at which signal peaks are coincident should be at top graticule line (Reference Level). If not, adjust front-panel VERTICAL GAIN to place signal peak at Reference Level line. Be sure VERTICAL POSN is properly adjusted for baseline on bottom graticule line.
18. Replace CAUTION label (PC Board) on A12 Step Gain.

## ADJUSTMENTS

## 5-30. FREQUENCY DISPLAY ADJUSTMENTS

## REFERENCE:

A1 and A8 Schematics

## DESCRIPTION:

The Digital Panel Meter (DPM) OFFSET and GAIN controls are adjusted for proper FREQUENCY display indication at corresponding tuning voltage (DPMA) levels.


FIGURE 5-21. FREQUENCY DISPLAY ADJUSTMENTS TEST SETUP

EQUIPMENT:Digital VoltmeterHP 3456A
Cable, BNC (m) to Banana Plugs
Extender Cable Assembly
Adapter, BNC (f) to Alligator Clips ..... HP 8120-1292

## ADJUSTMENTS

## 5-30. FREQUENCY DISPLAY ADJUSTMENTS(Cont'd)

## PROCEDURE:

1. Allow one-half hour warmup time of equipment with analyzer connected to mainframe with extender cable.
2. Jumper A8TP5 DPM to ground.
3. Set front-panelFREQUENCY BAND GHz to Band $1(.01-3)$.
4. Connect DVM to A1A2TP1 DPMA. A1A2TP1 is located below the board and is accessible through cutout in left side gusset.
5. Adjust A8R61 DPM ZERO for DVM indicationof 0.000 Vdc .
6. Adjust A1A2R29 OFFSET for front-panel FREQUENCY GHz indication of $\mathbf{0 . 0 0 0}$.
7. Remove jumper from A8TP5 to ground.
8. Select Band $6(12.1-21)$ on analyzer.
9. Adjust front-panel TUNING control for DVM indication of -4.000 Vdc .
10. Adjust A1A2R28 GAIN for front-panelFREQUENCY indication of 20.000.

## SECTION VI REPLACEABLE PARTS

### 6.1. INTRODUCTION

6-2. The replaceable parts list breakdown for each major assembly is located in Section VIII, following the circuit description for the assembly. This section contains information for ordering the replacement parts not listed in Section VIII. Table 6-1 includes a list of reference designations and a list of abbreviations used in the parts list. Table 6-2 lists names and addresses that correspond to the manufacturer code numbers in the parts list. Table 6-3 lists the replaceable parts in alpha-numerical order by reference designation.

### 6.3. REPLACEABLEPARTS LIST

6-4. Table 6-3, the list of replaceable parts, is organized as follows:

1. Major assemblies and their part numbers.
2. Accessories supplied and their part numbers.
3. Miscellaneous chassis parts and their part numbers.
4. Mechanical chassis parts and their part numbers.

6-5. The following information is listed for each part:

1. The Hewlett-Packard part number.
2. The part number check digit (CD).
 ance of the part in the list.
3. The description of the part.
4. A five-digit code indicating a typical manufac-
turer of the part.
5. The manufacturer's part number.

## 6-6. ORDERING INFORMATION

6-7. To order a part listed in the replaceable parts table, quote the Hewlett-Packard part number (with check digit), indicate the quantity required, and address the order to the nearest Hewlett-Packard office. The check digit will ensure accurate and timely processing of your order.

6-8. To order a part that is not listed in the replaceable parts table, include the instrument model number, instrument serial number, the description and function of the part, and the number of parts required. Address the order to the nearest HewlettPackard office.

## TABLE6.1. REFERENCEDESIGNATIONSAND ABBREVIATIONS(10F3)

| A | Assembly |
| :---: | :---: |
| AT | Attenuator, Isolator, Limiter, Termination |
| B | Fan, Motor |
| BT | Battery |
| C | Capacitor |
| CP | Coupler |
| CR | Diode, Diode Thyristor, |
|  | Step Recovery Diode, Varactor |
| DC | Directional Coupler |
| DL | . Delay Line |
| DS | Annunciator, Lamp, Light |
|  | Emitting Diode (LED), |
|  | Signaling Device (Visible) |
| E | MiscellaneousElectrical Part |

## REFERENCE DESIGNATIONS

| F .............................. . Fuse | RT | Thermistor |
| :---: | :---: | :---: |
| FL . . . . . . . . . . . . . . . . . . . . . . . . . . Filter | S | Switch |
| HY .............. . . . . . . . . Circulator | T | Transformer |
| J . . . . . . . . . . . . . . ElectricalConnector | TB | Terminal Board |
| (Stationary Portion), Jack | TC | . Thermocouple |
| K . . . . . . . . . . . . . . . . . . . . . . . . . Relay | TP | Test Point |
| L . . . . . . . . . . . . . . . . . . . Coil, Inductor | U | egrated Circuit, Microcircuit |
| M . . . . . . . . . . . . . . . . . . . . . . . . Meter | V | Electron Tube |
| MP . . . . . Miscellaneous MechanicalPart | VR | Breakdown Diode (Zener), |
| P ................. ElectricalConnector |  | Voltage Regulator |
| (MovablePortion), Plug | W | . Cable, Wire, Jumper |
| Q . . . . . . . . Silicon Controlled Rectifier | X | . . . . . . So. Socket |
| (SCR), Transistor, | Y | Crystal Unit (Piezoelectric, |
| Triode Thyristor |  | Quartz) |
| R . . . . . . . . . . . . . . . . . . . . . . . Resistor |  | Tuned Cavity, Tuned Circuit |

## ABBREVIATIONS

| CPRSN ................. Compression | FDTHRU . . . . . . . . . . . . . Feed Through |
| :---: | :---: |
| CUP-PT .................. . Cup Point | FEM......................... . . Female |
| CW ..................... Clockwise, | FIL-HD . . . . . . . . . . . . . . . Fillister Head |
| Continuous Wave | FL . . . . . . . . . . . . . . . Flash, Flat, Fluid |
|  | FLAT-PT .................. Flat Point |
| D | FR . . . . . . . . . . . . . . . . . . . . . . . Front |
|  | FREQ . . . . . . . . . . . . . . . . . . . Frequency |
| D . . . . . . . . . . Deep, Depletion, Depth, | FT . . . . . . . . . Current Gain Bandwidth |
| Diameter, Direct Current | Product (TransitionFrequency), |
| DA . . . . . . . . . . . . . . . . . . Darlington | Feet, Foot |
| DAP-GL . . . . . . Diallyl Phthalate Glass | FXD ......................... ${ }^{\text {. }}$. Fixed |
| DBL......................... Double |  |
| DCDR ...................... . Decoder |  |
| DEG . . . . . . . . . . . . . . . . . . . . . . Degree | G |
| D-HOLE . . . . . . . . . . . . D-Shaped Hole |  |
| DIA . . . . . . . . . . . . . . . . . . Diameter | GEN . . . . . . . . . . . General, Generator |
| DIP . . . . . . . . . . D Dual In-Line Package | GND . . . . . . . . . . . . . . . . . . Graund |
| DIP-SLDR . . . . . . . . . . . . . . . Dip Solder | GP . . . . . . . . . . General Purpose, Group |
| D-MODE . . . . . . . . . . . . Depletion Mode |  |
| DO . . . . . . . . Package Type Designation | H |
| DP ............ Deep, Depth, Diametric |  |
| Pitch, Dip | H . . . . . . . . . . . . . . . . . . . Henry, High |
| DP3T ............. Double Pole Three | HDW .................... Hardware |
| Throw | HEX . ........ Hexadecimal, Hexagon, |
| DPDT ........... Double Pole Double | Hexagonal |
| Throw | HLCL ...................... Helical |
| DWL ......................... . . Dowel | HP ........ Hewlett-Packard Company, |
|  | High Pass |
| E |  |
| E-R . . . . . . . . . . . . . . . . . . . . . E E-Ring | I |
| EXT ............... $\begin{array}{r}\text { Extended, Extension, } \\ \text { External, Extinguish }\end{array}$ | IC .................... $\begin{gathered}\text { Collector Current, } \\ \text { Integrated Circuit }\end{gathered}$ |
| F | ID . . . . . . . . . . . . . . Identification, Inside |
| F . . . . . . . . F Fahrenheit, Farad, Female, | IF . . . . . . . . . . . . . . . . Forward Current, |
| Film (Resistor), Fixed, | Intermediate Frequency |
| Flange, Frequency | IN . . . . . . . . . . . . . . . . . . . . . . . . . Inch |
| FC . . . . . . . Carbon Film/Composition, | INCL . . . . . . . . . . . . . . . . . . Including |
| Edge of Cutoff Frequency, Face | INT ........ Integral, Intensity, Internal |

## TABLE6-1. REFERENCEDESIGNATIONS AND ABBREVIATIONS(2OF3)



TABLE6-1. REFERENCEDESIGNATIONSAND ABBREVIATIONS(3OF 3 )

| MULTIPLIERS |  |  |  |  |  |
| :---: | :---: | :--- | :---: | :---: | :---: |
| Abbreviation | Prefix | Multiple | Abbreviation | Prefix | Multiple |
| T | tera | $10^{12}$ | m | milli | $10^{-3}$ |
| G | giga | $10^{9}$ | $\mu$ | micro | $10^{-6}$ |
| M | mega | $10^{6}$ | n | nano | $10^{-9}$ |
| k | kilo | $10^{3}$ | P | pico | $10^{-12}$ |
| da | deka | 10 | f | femto | $10^{-15}$ |
| d | deci | $10^{-1}$ | a | atto | $10^{-18}$ |
| c | centi | $10^{-2}$ |  |  |  |

TABLEG-2. MANUFACTURERSCODELIST

| Mfr. No. | Manufacturer Name | Address | Zip Code |
| :--- | :--- | :--- | :---: |
| 01121 | ALLEN-BRADLEY CO | MILWAUKEE, WI | 53204 |
| 01295 | TEXAS INSTR INC SEMICOND CMPNT DIV | DALLAS, TX | 75222 |
| 02111 | SPECTROL ELECTRONICS CORP | CITY OF IND, CA | 91745 |
| 02660 | BUNKER RAMO CORP AMPHENOL CONN DIV | BROADVILLE, IL | 60153 |
| 02768 | ILLINOIS TOOL WORKS INC FASTEX DIV | DES PLAINES, IL | 60016 |
| 03888 | K D I PYROFILM CORP | WHIPPANY, NJ | 07981 |
| 04713 | MOTOROLA SEMICONDUCTOR PRODUCTS | PHOENIX, AZ | 85008 |
| 06383 | PANDUIT CORP | TINLEYPARK, IL | 60477 |
| 06665 | PRECISION MONOLITHICS INC | SANTA CLARA, CA | 95050 |
| 07088 | KELVIN ELECTRIC CO | VAN NW S, CA | 91401 |
| 07263 | FAIRCHILD SEMICONDUCTOR DIV | MOUNTAIN VIEW, CA | 94042 |
| 11236 | CTS OF BERNE INC | BERNE, IN | 46711 |
| 17856 | SILICONIX INC | SANTA CLARA, CA | 95054 |
| 19701 | MEPCO/ELECTRA CORP | MINERAL WELLS, TX | 76067 |
| 20940 | MICRO-OHM CORP | EL MONTE, CA | 91731 |
| 24046 | TRANSITRON ELECTRONIC CORP | WAKEFIELD, MA | 01880 |
| 24546 | CORNING GLASS WORKS (BRADFORD) | BRADFORD, PA | 16701 |
| 27014 | NATIONAL SEMICONDUCTOR CORP | SANTA CLARA, CA | 95051 |
| 28480 | HEWLETT-PACKARD CO CORPORATE HQ | PALO ALTO, CA | 94304 |
| $3 L 585$ | RCA CORP SOLID STATE DIV | SOMERVILLE,NJ |  |
| 30161 | AAVID ENGINEERING INC | LACONIA, NH | 03246 |
| 30983 | MEPCO/ELECTRA CORP | SANDIEGO, CA | 92121 |
| 32997 | BOURNS INC TRIMPOT PROD DIV | RIVERSIDE, CA | 92507 |
| 33095 | SPECTRUM CONTROL INC | FAIRVIEW, PA | 16415 |
| 37942 | MALLORY P R AND CO INC | INDIANAPOLIS, IN | 46206 |
| 52063 | EXAR INTEGRATED SYSTEMS INC | SUNNYVALE, CA | 94086 |
| 52763 | STETTNER ELECTRONICS INC | CHATTANOOGA, TN | 13035 |
| 56289 | SPRAGUE ELECTRIC CO | NORTH ADAMS, MA | 01247 |
| 71041 | BOSTON GEAR WKS DIV OF NA ROCKWELL | QUNCY, MA | 02171 |
| 72136 | ELECTRO MOTIVE CORP | FLORENCE, SC | 06226 |
| 72982 | ERIE TECHNOLOGICAL PRODUCTS INC | ERIE, PA | 16512 |
| 73138 | BECKMAN INSTRUMENTS INC HELIPOT DIV | FULLERTON, CA | 92634 |
| 74970 | JOHNSON E F CO | WASECA, MN | 56093 |
| 78707 | TEK BEARING CO INC | NEW YORK,NY | 10013 |

TABLE6-3. REPLACEABLEPARTS


TABLE6.3. REPLACEABLEPARTS


TABLE 6.3. REPLACEABLE PARTS


| Reference <br> Designator | HP Part <br> Number | C | Qty | Description | Mfr. Code | Mfr. Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 08559-00030 | 2 | 1 | PANEL, FRONT | 28480 | 08559-00030 |
| 2 | 08559-00038 | 0 | 1 | GUSSET, LEFTSIDE | 28480 | 08559-00038 |
| 3 | 08559-00037 | 9 | 1 | GUSSET, RIGHt SIDE | 28480 | 08559-00037 |
| 4 | 08559-00003 | 9 | 1 | PANEL, REAR | 28480 | 08559-00003 |
| 5 | 5061-5426 | 9 | 1 | RAIL. GUIDE TOP | 28480 | 5061-5426 |
| 6 | 08559-20017 | 7 | 1 | EXTRUSION, CIRCUIT ENCLOSURE, TAPPED | 28480 | 08559-20017 |
| 7 | 08559-20015 | 5 | 1 | EXTRUSION. ENDPLATE ENCLOSURE: | 28480 | 08559-20015 |
| 8 | 08559-20014 | 4 | 1 | EXTRUSION, CIRCUIT ENCLOSURE, TAPPED | 28480 | 08559-20014 |
| 9 | 08559-20016 | 6 | 2 | EXtrusion, CIRCUIT ENCLOSURE | 28480 | 08559-20016 |
| 10 | 08559-20001 | 9 | 1 | WINDOW, FREQ. DISPLAY | 28480 | 08559-20001 |
| 11 | 5021-3254 | 3 | 1 | RAIL, GUIDE BOTTOM | 28480 | 5021-3254 |
| 12 | 08557-60045 | 3 | 1 | CABLEASSY (W5) VERTICAL OUTPUT | 28480 | 08557-60045 |
| 13 | 2200-0165 | 6 | 2 | SCREW. MACH 4-40.25 INLG 82 DEG | 28480 | 2200-0165 |
| 14 | 2360.0194 | 9 | 4 | SCREW, MACH 6-32.312 INLG |  |  |
|  |  |  |  | FL-HD-POZI | 2848C | 2360-0194 |
| 15 | 2360-0192 | 7 | 4 | SCREW, MACH 6-32.25 INLG |  |  |
|  |  |  |  | FL-HD-POZI | 2848G | 2360-0192 |
| 16 | 2360-0201 | 9 | 2 | SCREW. MACH 6-32.5INLG PAN-HD-POZI | 2848G | 2360-0201 |
| 17 | 0624-0099 | 1 | 80 | SCREW. TPG 4-40.375 IN LG |  |  |
|  |  |  |  | PAN-HD-POZI | 28480 | 0624-0099 |
| 18 | $2200 \cdot 0103$ | 2 | 14 | SCREW, MACH 4-40.25 INLG |  |  |
|  |  |  |  | PAN-HD-POZI | 28480 | 2200-0103 |
| 19 | 2200-017a | 3 | 1 | SCREW. MACH 4-40.625 INLG 82 DEG | 28480 | 2200-0170 |
| 20 | 0380-0005 | 1 | 1 | SPACER, RND. 312 INLG.18-IN-ID | 28480 | 0380-0005 |
| 21 | 2260-0003 | 7 | 1 | NUT. HEX PLSTC LKG 4-40 THD. 141 |  |  |
| 22 | 2200-0164 | 5 | 2 | INTHK <br> SCREW. MACH 4-40. 188 INLGUNCT | 28480 | 2260-0003 |
| 22 | 2200-0164 | 5 | 2 | SCREW. MACH 4-40. 188 IN LG UNCT <br> 82 DEG | 28480 | 2200-0164 |
| 23 | 2200-0769 | 6 | 3 | SCREW, MACH 4-40.438 INLG PAN-HD-POZI | 28480 | 2200.0769 |
| 24 | 08559-00006 | 2 | 1 | COVER. THIRDCONVERTER | 28480 | $2200-0769$ $08559-00006$ |
| 25 | 08559-00007 | 3 | 1 | COVER. BANDWIDTHFILTER NO. 1 | 28480 | 08559.00007 |
| 26 | 08559-00008 | 4 | 1 | COVER, STEPGAIN | 28480 | 08559-00008 |
| 27 | 08559-00009 | 5 | 1 | COVER, BANDWIDTH FILTER NO. 2 | 28480 | 08559-00009 |
| 28 | 08559-00C27 | 7 | 1 | COVER, LOG AMP | 28480 | 08559-00027 |
| 29 | 3050-0105 | 6 | 4 | WASHER. FL-MTLC NO. 4.125 IN ID | 28480 | 3050.0105 |
| 30 | 2420-0001 | 5 | 2 | NUT. HEX-W/LKWR 6-32 THD. 109 |  |  |
|  |  |  |  | INTHK | 28480 | 2420-0001 |
| 31 | 3050.0082 | 8 | 6 | WASHER. FIBER | 28480 | 3050.0082 |
| 32 | 2190-0104 | 0 | 1 | WASHER. LKINTL 7/16 IN. 439 INID | 28480 | 2190.0104 |
| 33 | 2950-0132 | 6 | 1 | NUT. HEX DBL-CHAM 7/16-28 THD .125 IN THK | 28480 | 2950-0132 |
| 34 | 0370-0606 | 7 | 11 | BEZEL, PB, 330 IN SQ: JADE GRAY | 28480 | 0370.0606 |
| 36 | 5040-8819 | 6 | 1 | PUSHBUTTON, SQUARE: WILLOW |  |  |
|  |  |  |  | GREEN | 28480 | 5040-8819 |
| 37 | 08565-40011 | 1 | 1 | POINTER, INPUT ATTENUATOR | 28480 | 08565-40011 |
| 38 | 1460-0532 | 0 | 1 | SPRING. CONICAL | 28480 | 1460-0532 |
| 39 | 08558-60167 | 1 | 1 | kNob ASSy, referencelevel | 28480 | 08558-60167 |
| 40 | 08565-00043 | 5 | 1 | INDEX DISK, REFERENCELEVEL | 28480 | 08565-00043 |
| 41 | 0510.0089 | 8 | 1 | ```RETAINER,RINGEXT.188IN DIA, BECU``` | 28480 | 0510-0089 |
| 42 | 08565-60047 | 5 | 1 | KNOB ASSY, REFLEVELFINE | 28480 | 08565-60047 |
| 43 | 08559-20052 | 0 | 1 | KNOB ASSV, RESOLUTION BW | 28480 | 08559-20052 |
| 44 | 08559-20053 | 1 | 1 | KNOB ASSY. FREQ SPAN/DIV | 28480 | 08559-20053 |
| 45 | 0370-3060 | 3 | 1 | KNOB, LOCK | 28480 | 0370-3060 |
| 46 | 08559-60002 | 4 | 1 | RFINPUTASSY | 28480 | 08559-60002 |
| 47 | 08559-20045 | 1 | 1 | CAbLE. RFINPUT | 28480 | 08559-20045 |

FIGURE6-1. MECHANICALCHASSIS PARTS(10F2)

| Reference Designater | Hp Part Number | c | aty | Description | Mfr. Code | Mfr. Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{48}$ | ${ }^{0370.3021}$ |  |  | knos Assr, Manval sweep | ${ }^{28480}$ | 0370.3021 |
| ${ }_{50}^{49}$ | (0859.20051 | ? | 1 | KNoo AsYV, Smeep Timeliv |  | (oas59,20051 |
| ${ }_{51}^{51}$ | 03370.3006 | ? |  | KNoo ASSS, FINE TUNE | ${ }^{28480}$ | 0337.3006 |
| ${ }_{53}^{52}$ | O.037.3004 | 5 | 1 |  | ${ }_{\substack{20480 \\ 28480}}$ |  |
| ${ }_{54}$ |  | 6 |  |  | 28480 | 2190.330 |
| 55 | 2950.0001 | - | 1 |  |  |  |
|  | ${ }_{2} 29000016$ | 3 |  |  |  |  |
| ${ }_{57}$ | ${ }_{\text {O855.00006 }}$ | 1 | 1 | INSULATOR, REAR HELU WTTH |  |  |
| ${ }^{58}$ | 88701.40001 | , | 2 | ExTRACTOR PC B Boano | ${ }_{288880}^{28890}$ | (oss50.0006 |
| ¢90 |  |  |  |  | ${ }_{\substack{20480 \\ 28480}}^{290}$ |  |
| ${ }_{62}^{61}$ | ${ }_{\text {3050.017 }}^{\text {3050.0162 }}$ | 4 |  | WSHR.FL 260 in 10 | 28880 <br> 28480 | ${ }_{\substack{3055.0017 \\ \text { 3050.0162 }}}^{\text {a }}$ |
| ${ }_{63}$ | 0590.1251 | 6 | 1 | NUT.SPCLY 15/32.32 THD .1 I 1 THK |  |  |
|  |  |  |  | - 5682 WO | ${ }^{22480}$ |  |
| ¢65 | 6350.0036 | $\bigcirc$ | 1 |  | ${ }_{26480}^{26850}$ | ${ }^{\text {O380.0.034 }}$ |
|  |  |  |  | PaN:HDPOzI | 29880 | 2200.0101 |
| (67 | ${ }_{\substack{2200.061 \\ 2510.0278}}^{2}$ | $\stackrel{1}{9}$ | ${ }_{2}^{20}$ |  | $\substack{28880 \\ 28480}$ |  |
| 69 | ${ }^{2360.0113}$ | 2 | 1 | SCREW. Mach 6.32 .3121 NLL |  |  |
| 70 | ${ }^{3050.029}$ | 2 | 1 |  | 28880 | 00.013 |
|  |  |  |  | . 562 IN 000 | 28480 | 3050.0929 |
|  |  |  |  |  | 28880 | 0360.0269 |
| 72 | 2200.0141 | - | $=$ |  | ${ }^{28480}$ | $2200 \cdot 0141$ |
| ${ }^{72}$ | 80.0009 | 3 | $=$ | NUT-HExW/KKwR 4.40 THD |  |  |
| 74 | ${ }^{0360.1669}$ | 3 | 1 |  | 28880 | 2260.0099 |
|  |  |  |  |  | ${ }^{28480}$ |  |
| ${ }_{76}$ | $\underbrace{10.0}_{\substack{14000.0031 \\ 2200045}}$ | ${ }_{2}$ | 1 | Comer |  |  |
| 7 | 2260.000 | 5 | 1 |  | 28880 | 2200.0 |
|  |  |  |  |  | 年28880 |  |
| ${ }_{79}^{79}$ | 3050.006 | ${ }_{5}$ | 1 |  | coize 28880 | $\underbrace{\text { 200, }}_{\substack{3050.066 \\ \text { 21900018 }}}$ |



## SECTION VII MANUAL BACKDATING CHANGES

### 7.1. INTRODUCTION

7-2. This section contains information for adapting this manual to earlier 8559A Spectrum Analyzers. If the serial number prefix of your spectrum analyzer appears on the title page of this manual, the contents of the manual are directly applicable to your instrument. If, however, your spectrum analyzer has a lower serial number prefix than what is shown on the title page, you must adapt this manual to your instrument by changing it as indicated in this section.

7-3. If your instrument has a higher serial number prefix that what is shown on the title page of this manual, it will be documented in a yellow MANUAL UPDATING CHANGES supplement. For additional important information about serial number coverage, refer to INSTRUMENTS COVERED BY MANUAL in Section I.

### 7.4. HOW TO USE THIS BACKDATING INFORMATION

7-5. Change and correction information in this supplement is itemized on separate pages corresponding to the original manual pages. The pages in this supplement are organized in numerical order by manual page number. These pages are intended to be inserted into the manual to either supplement or replace the original manual pages.
7-6. To adapt this manual to your instrument:

- Insert the change pages in this section into this manual adjacent to the original manual pages.
- Insert any complete replacement pages provided into this manual in the proper location. The original manual pages may be-discarded or the original manual may be left intact to document all instrument configurations.


## Page 1-3:

Table 1-1. HP 8559A Specifications (1 of 4)
2236A \& Below

2320A \& Below
Change "Residual FM" specification to read as follows: less than $1 \mathrm{kHz} \mathrm{p}-\mathrm{p}$ for a time interval less than or equal to .O1 sec, $100 / 120$ line voltages; less than $2 \mathrm{kHz} \mathrm{p}-\mathrm{p}, \mathbf{2 2 0 / 2 4 0}$ line voltages.
Delete the following under 'Maximum Input (without damage)
Levels":
Peak Pulse Power
+50 dBm ( $100 \mathrm{~W}, 10$ microsecond pulse width, $0.01 \%$ duty cycle) with input attenuation $>=30 \mathrm{~dB}$.
Change "Gain Compression" specification to read as follows: Gain compression is less than 0.5 dB for a 0 dBm input level with 0 dB input attenuation.
Under "Display Fidelity", change the Linear specification to read as follows:
<+-0.1 division over full 8 division deflection.
Change "Humidity Range (Operating)" to read as follows:
く95\% R.H. 0 -degrees C to +40-degrees C.
Change "EMI" to read as follows:
Conducted and radiated interference is within the requirements of methods CE03 and RE02 of MIL STD 461A, VDE 0871 and CISPR Publications 1, 2, and 4.

Change "Residual $\mathrm{FM}^{\prime \prime}$ specification to read as follows:
less than $1 \mathrm{kHz} \mathrm{p}-\mathrm{p}$ in 0.1 second.

Pages 4-10 and 4-11:

## Paragraph 4-13. Residual FM

2320A \& Below
Change SPECIFICATION to read as follows:
Less than 1 kHz peak-to-peak for a time interval 0.1 second; 100/120 line voltages; less than 2 kHz peak-to-peak in a 180series display mainframe with $220 / 240$ line voltage.
Replace the note in step 6 with the following:
NOTE
A $1 \mathbf{k H z}$ shift in Frequency produces a 0.7 division shift in amplitude.
In step 6, change the last sentence to read:
Peak-to-peak variation of trace should not exceed 0.7 division vertical for each horizontal division.

## Page 4-63:

Table 4-18. Performance Test Record (2 of 4)
2320A \& Below Under Para. No. 4-13. Residual FM, change the maximum Peak-toPeak Variation of Trace in test 6 to 0.7 div ( $1 \mathrm{kHz} / 0.1 \mathrm{sec}$ ).

## Pages 5-11 through 5-13:

Paragraph 5-17. Power Supply Checks and Adjustments
2236A \& Below Replace Paragraph 5-17 with new Paragraph 5-17 (SERIAL PREFIX 2236A) included in this Manual Backdating supplement.

## ADJUSTMENTS

## 5-17. POWER SUPPLY CHECKS AND ADJUSTMENTS(SERIAL PREFIX 2236A)

## REFERENCE:

A7, A8, A9 Schematics

## DESCRIPTION:

The +14.5 V and -10 V supplies on Frequency Control Assembly A7 are adjusted. The $-\mathbf{1 2 . 0 V}$ supply on A7 is checked for proper dc output with less than $\pm 50 \mathrm{mV}$ variation when tuning the HP 8559A from 0 to 3 GHz . The $\mathbf{+ 1 0 . 0 V}$ supply on Sweep Generator/Bandwidth Control Assembly A9 is adjusted and the VO (Varactor Offset) voltage on Marker Assembly A8 is adjusted. The +10.0 V supply and VO voltage must be adjusted during the first five minutes after the spectrum analyzer is turned on (cold instrument). However, the +14.5 V and $\mathbf{- 1 0 . 0 V}$ supplies must be adjusted first.


FIGURE5-1. POWER SUPPLYCHECKS AND ADJUSTMENTSTESTSETUP

## EQUIPMENT:

Digital Voltmeter
HP 3490A

## PROCEDURE:

1. Connect equipment as shown in Figure 5-1. Install Frequency Control Assembly A7 on extender board and connect digital voltmeter to $\mathbf{A 7 T P} 3+14.5 \mathrm{~V}$.
2. Adjust A7R52 $+\mathbf{1 4 . 5 V}$ adjustment for a voltmeter indication of $\mathbf{+ 1 4 . 5 0 0} \pm \mathbf{0 . 0 0 2}$ volts.
3. Connect digital voltmeter to A7TP2 and adjust A7R55 - 10V adjustment for a voltmeter indication of $-10.000 \pm 0.005$ volts.
4. Check for $-12.0 \pm \mathbf{0 . 1 V}$ at collector (base) of A 7 Q 1 .
5. Select FREQUENCY BAND GHz . $01-3$ and tune from 0 to 3 while monitoring the -12 V at collector of A7Q1. The -12 V supply should not vary more than $\pm 50 \mathrm{mV}$.

## ADJUSTMENTS

## 5-17. POWER SUPPLY CHECKS AND ADJUSTMENTS(SERIALPREFIX 2236A)(Cont'd)

6. Remove extender board and reinstall Frequency Control Assembly A7.

NOTE
The two following voltage adjustments, $\mathbf{+ 1 0 \mathrm { V }}$ and VO (Varactor Offset), must be adjusted while analyzer is still cold (during first five minutes after turn-on). If instrument has been operating longer than five minutes, turn off mainframe and remove assemblies A8 and A9. Let assemblies A8 and A9 cool on bench for 15 minutes. Replace the two assemblies and proceed with adjustment of A9R2 and A8R62 during the first five minutes after turn-on.
7. Connect digital voltmeter to A9TP6 +10 V and adjust A9R2 +10 V adjustment for a voltmeter indication of $+10.000 \pm 0.100 \mathrm{~V}$.
8. Connect digital voltmeter to A8TP2 VO. Set HP 8559A controls as follows:
FREQUENCY BAND GHz . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . .
9. The voltage at A8TP2 will change (between two values) each time a sweep is triggered. Trigger the sweep a few times and select the sweep that yields the least negative VO voltage. Adjust A8R62 VO adjustment for a voltmeter indication of $-2.00 \pm 0.10 \mathrm{~V}$.

## Pages 5-17 through 5-23:

## Paragraph 5-19, Log Amplifier and Linear Adjustments

2208A \& Below
Replace Paragraph 5-19 with new Paragraph 5-19 (SERIAL PREFIX
2208A) included in this Manual Backdating supplement.

## ADJUSTMENTS

### 5.19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENT (SERIAL PREFIX 2208A)

## REFERENCE:

A14 and A15 Schematics

## DESCRIPTION

$10 \mathrm{~dB} /$ DIV and LIN are adjusted for correct steps and full-screen display translations.


FIGURE53. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENTTESTSETUP

## EQUIPMENT:

> Signal Generator
> HP 8640B
> Digital Voltmeter HP 3490A
> Step Attenuator ( $10 \mathrm{~dB} /$ step )
> Adapter, Type N Male on one end, BNC female on other end HP 1250-0780
> Adapter, BNC Male on one end, SMA Male on other end HP 1250-0831

## PROCEDURE:

1. Set spectrum analyzer controls as follows:

| FREQUENCY BAND GHz | . $01-3$ |
| :---: | :---: |
| FREQ SPAN/DIV | 1 MHz |
| RESOLUTIONBW | 300 kHz |
| INPUT ATTEN | 10 dB |
| REF LEVEL dBm | -50 |
| AmplitudeScale . | LIN |
| SWEEP TIME/DIV | AUTO |
| SWEEP TRIGGER | EE RUN |

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENT (SERIAL PREFIX 2208A) (Cont'd)

2. Connect equipment as shown in Figure 5-3. Set signal generator frequency to $321.4 \mathbf{M H z}$ and output level to -40 dBm . Remove A10W1 from A5J2 2nd CONV OUT. Connect signal generator output through step attenuator and adapters to A10W1.
3. Set the TEST-NORM switch A12S1 to the TEST position. Tune signal generator frequency for maximum signal amplitude on oscilloscope display with step attenuator set at $\mathbf{0} \mathrm{dB}$.
4. Set output level of signal generator for a digital voltmeter reading of 700 mV , with step attenuator set at $\mathbf{0}$ dB and REF LEVEL dBm set to -50 .
5. Set HP 8559A REF LEVEL dBm to -80 and set step attenuator to 30 dB . Observe digital voltmeter reading.
6. Adjust A14R3 GAIN LIN for a digital voltmeter reading of 700 mV .
7. Repeat steps 4,5 , and 6 until the DVM reading in step 5 is $700 \pm 2 \mathrm{mV}$.
8. Set HP 8559A REF LEVEL dBm to - 50 and set step attenuator to 0 dB . Change REF LEVEL dBm and step attenuator settings as shown in Table 5-6. If Deviation from Reference is not within the given limits, readjust A14R3.

TABLE56. LINEAR GAIN ADJUSTMENTLIMITS

| Reference Level <br> $(\mathrm{dBm})$ | Step Attenuator <br> Setting (dB) | Deviation From <br> Reference |
| :---: | :---: | :---: |
| -50 | 0 | Reference $(700 \mathrm{mV})$ |
| -60 | 10 | $\pm 10 \mathrm{mV}$ |
| -70 | 20 | $\pm 20 \mathrm{mV}$ |
| -80 | 30 | $\pm 20 \mathrm{mV}$ |
| -90 | 40 | $\pm 30 \mathrm{mV}$ |

9. Set HP 8559A REF LEVEL dBm to 0 and disconnect signal generator from step attenuator. Record offset reading (DVM). The offset should be less than $\pm 30 \mathrm{mV}$.

Offset $\qquad$ mV
10. Reconnect signal generator as shown in Figure 5-3. Set Amplitude Scale to 10 dB/DIV and set step attenuator to 40 dB .
11. Set output level of signal generator for a digital voltmeter reading of 400 mV plus offset recorded in step 9 (algebraic sum). (Example: if offset if -23 mV , set output level of signal generator for a DVM reading of 377 mV .)

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENT(SERIAL PREFIX 2208A)(Cont'd)

12. Set step attenuator to 0 dB . Digital voltmeter should indicate 800 mV , plus offset (algebraic sum) $\pm 1 \mathrm{mV}$. If DVM reading is not within limits, adjust A14R2 LOG LIN adjustment for a digital voltmeter reading of 800 mV , plus offset minus 50 percent of overshoot. (Example: if DVM indicates 767 mV and should be indicating 777 mV ( -10 mV overshoot), adjust A14R2 for a DVM reading of 777 mV minus -5 mV , or 782 mV .)
13. Repeat steps 10,11 , and 12 until the digital voltmeter indicates 800 mV plus offset $\pm 1 \mathbf{m V}$ with no further adjustment of A14R2 in step 12.
14. Set the step attenuator to the positions shown in Table 5-7 and record DVM reading for each setting. Correct the DVM readings by algebraically adding the offset (recorded in step 9).

TABLE5-7. LOG FIDELTTY CHECK

| Step Attenuator Setting (dB) | $\begin{aligned} & \text { DVM Reading } \\ & (\mathrm{mV}) \end{aligned}$ | DVM Reading Corrected for Offset |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. (mV) | Actual (mV) | Max. (mV) |
| 0 |  | 799 | - | 801 |
| 10 |  | 697 | - | 703 |
| 20 |  | 596 | - | 604 |
| 30 |  | 496 | - | 504 |
| 40 |  | 395 |  | 405 |
| 50 |  | 294 | - | 306 |
| 60 |  | 193 | - | 207 |
| 70 |  | 92 | - | 108 |

15. Readjust A14R2 if necessary to meet the limits in Table 5-7.
16. Set step attenuator to 0 dB and set output level of signal generator for a digital voltmeter reading of 800 $\mathbf{m V}$ plus offset (recorded in step 9 ) $\pm 1 \mathrm{mV}$.
17. Set Amplitude Scale to LIN. The digital voltmeter should indicate the reading set in step $16 \pm \mathbf{2 5} \mathbf{m V}$. If it does, go to step 19. If it does not, or if log fidelity is not within limits, go to step 18 and select A14R16*.
18. Select A14R16* to obtain an output in step 17 within $\pm \mathbf{2 5} \mathbf{~ m V}$ of the reading set in step 16. Decreasing A14R16* 10 percent will increase the DVM reading approximately 30 mV in step 17.

## NOTE

Log fidelity must be considered when selecting A14R16*. That is, if the DVM READING CORRECTED FOR OFFSET in Table 5.7 is greater than 100 mV for a STEP ATTENUATOR SETTING of 70 dB , A14R16* should be selected for a DVM reading greater than the reading set in step 16. If the READING CORRECTED FOR OFFSET is less than 100 mV, A14R16* should be selected for DVM reading less than the reading set in step 16.

## ADJUSTMENTS

## 5-19. LOG AMPLIFIER LOG AND LINEAR ADJUSTMENT(SERIAL PREFIX 2208A)(Cont'd)

19. Set output level of signal generator for a digital voltmeter reading of 800 mV plus offset (algebraic sum) $\pm 1 \mathrm{mV}$.
20. Set Amplitude Scale to 10 dB /DIV and adjust A14R2 LOG LIN adjustment for a digital voltmeter reading of 800 mV plus offset.
21. Repeat step 14 to recheck the $\log$ fidelity.
22. Set the REF LEVEL dBm control to - 50. Set Amplitude Scale to $1 \mathrm{~dB} / \mathrm{DIV}$.
23. Set the step attenuator to $\mathbf{0 d B}$ and set output level of signal generator for a digital voltmeter reading of $\mathbf{7 0 0}$ mV (do not include offset).
24. Set the REF LEVEL dBm control to -90 and the step attenuator to 40 dB . Adjust A14R1 LOG GAIN adjustment for a digital voltmeter reading of 700 mV .
25. Change REFERENCE LEVEL and step attenuator settings as shown in Table 5-8. Deviation from Reference should not exceed the given limits.

TABLE 5-8. LOG GAIN ADJUSTMENTLIMITS

| Reference Level <br> $(\mathbf{d B m})$ | Step Attenuator <br> Setting (dB) | Deviation From <br> Reference |
| :---: | :---: | :---: |
| -50 | 0 | Reference $(700 \mathrm{mV})$ |
| -60 | 10 | $\pm 30 \mathrm{mV}$ |
| -70 | 20 | +30 mV |
| -80 | 30 | +30 mV |
| -90 | 40 | $\pm 30 \mathrm{mV}$ |

26. Return the TEST-NORM switch on assembly A12 to the NORM position.

Pages 5-26 through 5-32:
Paragraph 5-21. Bandwidth Filter Adjustments
1909A \& Below Replace Paragraph 5-21 with new Paragraph 5-21 (SERIAL PREFIX 1909A) included in this Manual Backdating supplement.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(SERIAL PREFIX 1909A)

## REFERENCE:

A9, A11, and A13 Schematics

## DESCRIPTION:

The crystal and LC bandwidth filter circuits are adjusted for symmetry, center, and peak. Three-dB bandwidths are adjusted in Sweep Generator/Bandwidth Control Assembly A9 (paragraph 5-22).


EQUIPMENT:
Adapter, Type N Male to BNC Female . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . HP 1250-0780
BNC Cable, 6-Inch
HP 10502A
Crystal Short (3 required)
See Figure 5-6

## NOTE

A crystal short consists of a.01 $\mu$ F capacitor (HP Part Number 0160-0161) and a 90.9 ohm resistor (HP Part Number 0757-0400) connected in series. Two square terminal connectors (HP Part Number 0362-0265) are used to connect the crystal short across the test points.


TERMINAL CONNECTORS
FIGURE $5-6$. CRYSTALSHORTCONFIGURATION

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

PROCEDURE:
NOTE
Allow 30 minutes warmup time before performing adjustments.

1. Set spectrum analyzer controls as follows:

| FREQUENCY BAND GHz | . $01-3$ |
| :---: | :---: |
| TUNING. | 35 MHz |
| FREQ SPAN/DIV | 10 kHz |
| RESOLUTIONBW | 1 kHz |
| INPUTATTEN | 30dB |
| REF LEVEL dBm | 0 |
| Amplitude Scale | LIN |
| SWEEP TIME/DIV | AUTO |
| SWEEPTRIGGER | E RUN |

Crystal Alignment
2. Connectequipment as shown in Figure 5-5.

NOTE
If Sweep Generator/Bandwidth Control Assembly A9 has been replaced or adjusted, perform steps 3 through 9 . If not, proceed to step 10.
3. Set FREQ SPAN/DIV to 500 kHz and RESOLUTIONBW to 1 MHz .
4. Center the signal with TUNING control. Using REF LEVEL FINE control, place signal at 7.1 divisions ( 0.9 division from top graticule line).
5. Adjust A9R85 LC until signal is two divisions wide at the fifth graticule line ( 1 MHz wide at $3-\mathrm{dB}$ points).
6. Set FREQ SPAN/DIV to 10 kHz and RESOLUTIONBW to 10 kHz .
7. Using REF LEVEL FINE control, place signal at 7.1 divisions.
8. Adjust A9R72 XTL until signal is one division wide at the fifth graticule line ( 10 kHz wide at 3 dB points).
9. Set FREQ SPAN/DIV to 10 kHz and RESOLUTION BW to 1 kHz .
10. Center signal with TUNING control. (It might be necessary to increase FREQ SPAN/DIV temporarily to find the signal.) Set REF LEVEL FINE control to place signal at sixth graticule line.

## NOTE

Do not readjust REF LEVEL FINE control until all crystal and LC bandwidth filter adjustments have been performed.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

11. Set FREQ SPAN/DIV to 20 kHz , RESOLUTIONBW to 30 kHz , and SWEEP TIME/DIV to 10 mSEC .

## NOTE

A non-metallic tuning tool is required for adjustments on Bandwidth Filter Assemblies A11 and A13.
12. Connect crystal shorts (through cover access holes) across A13TP1/TP2, A11TP1/TP2, and A11TP4/ TP5.

## NOTE

Keep crystal spike centered during adjustments. The SYM and CTR adjustments for each crystal are interacting.
13. Adjust front-panel TUNING control to center bandpass spike (Figure 5-7) on the CRT display.


FIGURE5-7. ADJUSTING CRYSTALSYMMETRY ANDCRYSTALCENTERING
14. Adjust A13C38 SYM and A13C54 CTR for a centered and symmetrical bandpass as shown in Figure 5-7. Adjust A13C54 CTR for minimum signal amplitude.
15. Remove crystal short from A13TP1/TP2.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

16. Adjust A13C15 SYM and A13C25 CTR for a centered and symmetrical bandpass. Adjust A13C25 CTR for minimum signal amplitude,
17. Remove crystal short from A11TP4/TP5.
18. Adjust A11C38 SYM and A11C54 CTR for a centered and symmetrical bandpass. Adjust A11C54 for minimum signal amplitude.
19. Remove crystal short from A11TP1/TP2.
20. Adjust A11C15 SYM and A11C25 CTR for a centered and symmetrical bandpass. Adjust A11C25 for minimum signal amplitude.
21. Remove the crystal shorts.

## LC Alignment

22. Perform preliminary LC filter adjustments as follows:

## NOTE

When Bandwidth Filter Assemblies A11 and A13 are installed with covers in place, midget copper alligator clips (HP Part Number 1400-0483) can be used to short test points to the cover.
a. Install A13 on extender board.
b. Short to ground the following test points: A13TP6, A11TP3, and A11TP6. Jumper A9TP1 to A9TP2.
c. Adjust A13C73 ior minimum signal amplitude.
d. Disconnect short from A13TP6 and short to ground A13TP3.
e. Adjust A13C74 for minimum signal amplitude.
f. Reinstall A13 and install A11 on extender board.
g. Disconnect short from A13TP3 and short to ground A11TP6.
h. Adjust A11C73 for minimum signal amplitude.
i. Disconnect short from A11TP6 and short to ground A11TP3.
j. Adjust A11C74 for minimum signal amplitude.
k. Disconnect shorts from test points and reinstall A11. Replace covers on A11 and A13 assemblies. Remove jumper from A9TP1/A9TP2.

## ADJUSTMENTS

## 5-21. BANDWIDTHFILTER ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

23. Carefully center signal on CRT in 30 kHz RESOLUTION BW; then switch RESOLUTION BW to 100 $\mathbf{k H z}$. Note where signal intersects the center vertical graticule line.
24. Adjust A13C45 LC CTR for maximum signal amplitude where the signal intersects the center vertical graticule line.
25. Switch RESOLUTION BW to $30 \mathbf{k H z}$ and center signal; then switch to $100 \mathbf{k H z}$. Note where signal intersects the center vertical graticule line.
26. Adjust A13C23 LC CTR for maximum signal amplitude where the signal intersects the center vertical graticule line.
27. Switch RESOLUTION BW to $30 \mathbf{k H z}$ and center signal; then switch to $100 \mathbf{k H z}$. Note where signal intersects the center vertical graticule line.
28. Adjust A11C45 LC CTR for maximum signal where the signal intersects the center vertical graticule line.
29. Switch RESOLUTION BW to $30 \mathbf{~ k H z}$ and center signal; then switch to $100 \mathbf{~ k H z}$. Note where signal intersects the center vertical graticule line.
30. Adjust A11C23 LC CTR for maximum signal amplitude where the signal intersects the center vertical graticule line.
31. Switch RESOLUTION BW between $100 \mathbf{k H z}$ and $30 \mathbf{k H z}$ to be sure the signal is centered at both bandwidth settings.

## Bandwidth Amplitude

32. Set Amplitude Scale to 1 dB/DIV and SWEEP TIME/DIV to AUTO.
33. Set RESOLUTIONBW to $3 \mathbf{M H z}$ and FREQ SPAN/DIV to 50 kHz .
34. Adjust fine TUNING and REF LEVEL FINE for a centered signal at 7 divisions.
35. Set RESOLUTION BW to 100 kHz and center signal with fine TUNING control. Adjust A13R26 LC and A11R26 LC equally to obtain a signal amplitude of 7 divisions.
36. Set RESOLUTION BW to $1 \mathbf{k H z}$ and FREQ SPAN/DIV to $10 \mathbf{k H z}$. Center signal with fine TUNING control. Adjust A11R31 XTL and A13R31 XTL equally for a signal amplitude of 7 divisions.

NOTE
Each potentiometer should be adjusted to accomplish half the necessary increase in signal amplitude.

## ADJUSTMENTS

## 5-21. BANDWIDTH FILTER ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

37. Set FREQ SPAN/DIV to $10 \mathbf{k H z}$ and RESOLUTION BW to $1 \mathbf{k H z}$ with arrows aligned (OPTIMUM). Push in to couple the two controls.
38. Adjust REF LEVEL FINE for a signal amplitude of 7 divisions.
39. With controls coupled, step RESOLUTION BW from $1 \mathbf{k H z}$ to $3 \mathbf{M H z}$. Variation in signal amplitude should be less than $\pm 0.4 \mathrm{~dB}$.
40. If variation in signal amplitude is not within limits, repeat steps 32 through 39.

## Pages 5-33 through 5-37:

Paragraph 5-22. 3 dB Bandwidth Adjustment
1909A \& Below Replace Paragraph 5-22 with new Paragraph 5-22 (SERIAL PREFIX 1909A) included in this Manual Backdating supplement.

## ADJUSTMENTS

## 5-22. 3 dB BANDWIDTH ADJUSTMENTS(SERIALPREFIX 1909A)

## REFERENCE:

A9 Schematic

## DESCRIPTION:

The 3-dB bandwidths for the $3 \mathrm{MHz}, 1 \mathrm{MHz}$ and 300 kHz RESOLUTION BW settings are adjusted using the CAL OUTPUT as the signal source. The $3-\mathrm{dB}$ bandwidths for the $10 \mathrm{kHz}, 3 \mathrm{kHz}$, and 1 kHz RESOLUTION BW settings are adjusted by injecting a stable 321.4 MHz signal into the third converter of the spectrum analyzer.


## PROCEDURE

1. Set spectrum analyzer controls as follows:
FREQUENCY BAND GHz ..... 01-3
TUNING ..... 35 MHz
FREQ SPAN/DIV ..... 200 kHz
RESOLUTIONBW ..... 1 MHz
INPUT ATTEN ..... 20dB
REF LEVEL dBm .....  0
Amplitude Scale ..... LIN
SWEEP TIME/DIV ..... 1 msec
SWEEPTRIGGER ..... FREE RUN
VIDEOFILTER ..... MIN
2. Connect equipment as shown in Figure 5-8 except for signal input to A10W1. Connect CAL OUTPUT to spectrum analyzer INPUT $50 \Omega$.

## ADJUSTMENTS

## 5-22. $3 \mathbf{d B}$ BANDWIDTHADJUSTMENTS(SERIAL PREFIX 1909A) (Cont'd)

3. Set signal level of 7.1 divisions on display with REF LEVEL FINE control. (Signal should be 0.9 division from top graticule line.)
4. Set RESOLUTION BW to $1 \mathbf{M H z}$ and FREQ SPAN/DIV to 200 kHz . Adjust A9R85 LC to set bandwidth of 5 divisions at the fifth graticule line.
5. Set RESOLUTION BW to $3 \mathbf{M H z}$ and FREQ SPAN/DIV to 500 kHz . The bandwidth at the fifth graticule line should be between 5.4 and 6.6 divisions.

## NOTE


#### Abstract

A9R85 LC may be further adjusted to bring the 3 MHz and 300 kHz bandwidths within limits; however, the final measurement of the 1 MHz bandwidth must be between 4.5 and 5.5 divisions at the fifth graticule line. (If the 3 MHz bandwidth cannot be brought within limits by adjustment of A9R85 LC, change the value of factory-selected resistor A9R95*.)


6. Set RESOLUTION BW to $300 \mathbf{k H z}$ and FREQ SPAN/DIV to 50 kHz . The bandwidth should be between 5.4 and 6.6 divisions at the fifth graticule line. (If the bandwidth cannot be adjusted within the specified limits, change the value of factory-selectedresistor A9R89*.)
7. Set RESOLUTION BW to $100 \mathbf{k H z}$ and FREQ SPAN/DIV to 20 kHz . The bandwidth should be between 4.3 and 5.7 divisions at the fifth graticule line.

## NOTE

> If the $\mathbf{1 0 0} \mathrm{kHz}$ bandwidth is not within the specified limits, change the values of factory-selected resistors A13R19*, A13R43*, and A11R43*. If the bandwidth is too wide, increase the value of the resistors; if the bandwidth is too narrow, decrease the value of the resistors. The three factory-selected resistors need not be of equal value, but each must be within one standard value of the others.
8. Set RESOLUTION BW to $30 \mathbf{k H z}$ and FREQ SPAN/DIV to $10 \mathbf{k H z}$. The bandwidth should be between 2.6 and 3.4 divisions at the fifth graticule line.

> NOTE
> If the 30 kHz bandwidth is not within the specified limits, change the values of factory-selected resistors A11R23*, A11R48*, A13R23*, and A13R48*. If the bandwidth is too wide, decrease the value of the factory-selected resistors; if the bandwidth is too narrow, increase the value of the resistors. The four factory-selected resistors need not be of equal value, but each must be within one standard value of the others.
9. Connect signal generator through the BNC Tee connector to the step attenuator and to the frequency counter as shown in Figure 5-8. Set the signal generator to approximately 0 dBm and the step attenuator to 30 dB .

## ADJUSTMENTS

## 5-22. 3 dB BANDWIDTH ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

10. Remove A10W1 from A5J2 2nd CONV OUT Connect step attenuator through adapter to A10W1.
11. Set HP 8559A RESOLUTION BW to 1 MHz . Adjust the output level of signal generator to place the signal near center graticule line. Tune signal generator frequency to peak signal on oscilloscope display (near 321.4 MHz ).
12. Set RESOLUTION BW to 3 kHz . Tune signal generator to peak signal on oscilloscope display.
13. Adjust output level of signal generator to place signal at 7.1 divisions.
14. Note the counter frequency and tune the signal generator 1500 Hz below the center frequency noted. Record the new counter frequency.
$\qquad$ MHz
15. Adjust A9R72 XTL to bring signal level to the fifth graticule line (three divisions from the top graticule line).
16. Increase signal generator frequency until signal on oscilloscope display peaks and then decreases to the fifth graticule line. Record counter frequency.
$\xrightarrow{-} \mathbf{M H z}$
17. Compare new frequency with frequency recorded in step 14. The difference between the two frequencies should be 2800 to 3200 Hz . If the bandwidth is not within limits, repeat steps 12 through 17, slightly readjusting A9R72 XTL, until the specified limits are achieved.
18. Set RESOLUTION BW to 10 kHz . Tune signal generator to peak signal on oscilloscope display.
19. Adjust REF LEVEL FINE to place signal at 7.1 divisions.
20. Decrease the signal generator frequency until the signal on the oscilloscope display drops to the fifth graticule line. Record counter frequency.
_ MHz
21. Increase the signal generator frequency until the signal on the oscilloscope display peaks and then decreases to the fifth graticule line. Record counter frequency.
$\qquad$ MHz

## ADJUSTMENTS

## 5-22. 3 dB BANDWIDTH ADJUSTMENTS(SERIAL PREFIX 1909A)(Cont'd)

22. Compare new frequency with frequency recorded in step 20. The difference between the two frequencies should be 9.000 kHz to 11.000 kHz .


#### Abstract

NOTE A9R72 XTL may be further adjusted to bring the 10 kHz and 1 kHz bandwidths within limits; however, the final measurement of the 3 kHz bandwidth must be between 2700 Hz and 3300 Hz (If the 10 kHz bandwidth cannot be brought within limits by adjustment of A9R72 XTL, change the value of fac-tory-selectedresistor A9R78*.)


23. Set RESOLUTION BW to $1 \mathbf{k H z}$. Tune signal generator to peak signal on oscilloscope display.
24. Adjust REF LEVEL FINE to place signal at 7.1 divisions. Record counter frequency.
$\qquad$
25. Increase signal generator frequency until signal on oscilloscope display drops to the fifth graticule line. Record new counter frequency.
$\qquad$
26. The difference between the two frequencies recorded in steps 24 and 25 should be $\mathbf{4 5 0 ~ H z}$ to 550 Hz .
27. Reconnect A10W1 to A5J2.

Pages 5-44 through 5-48:
Paragraph 5-25. First Converter Adjustments
2236A \& Below Replace Paragraph 5-25 with new Paragraph 5-25 (SERIAL PREFIX 2236A) included in this Manual Backdating supplement.

2004A \& Below Delete steps 28 through 37.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(SERIAL PREFIX 2236A)

## REFERENCE:

A3, A4, A5, A6, and A7 Schematics

## DESCRIPTION:

The First LO (A6 YTO) is adjusted by monitoring the YTO output at the RF input connector (LO feedthrough) and the tuning voltage (TUNE) output of the A7 Frequency Control board and adjusting the YTO low-end frequency for 3 GHz at OV tuning voltage and 6 GHz at -10 V tuning voltage.

The FM Driver is adjusted by inputting comb signals to the analyzer and adjusting for proper spacing (span linearity) of displayed signals on the CRT display.


FIGURE5-11. FIRSTCONVERTER ADJUSTMENTS TEST SETUP

## EQUIPMENT:

```
Frequency Counter
Digital Voltmeter(DVM) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . HP 3490A
Comb Generator . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . HP 8406A
```

PROCEDURE:

1. Allow one-half hour warmup time of equipment with analyzer connected to mainframe with extender cable.

## First LO Adjustments

2. Connect DVM to A7TP4 TUNE.
3. Set analyzer controls as follows:
INPUT ATTEN ..... 0 dB
FREQ SPAN/DIV ..... 0 (zero)
ALTIF OFF (out)

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(SERIAL PREFIX 2236A)(Cont'd)

4. Connect frequency counter to analyzer RF Input.
5. Jumper A16TP1 DIODE BIAS to Ground. A16TP1 is located on the Motherboard through a hole in the analyzer side frame.
6. Adjust front-panel TUNING control for DVM indication of $\mathbf{0 . 0 0 0} \mathrm{Vdc}$ (fully counterclockwise).
7. Adjust A7R74 3 GHz for frequency counter indication of $3.000 \mathrm{GHz} \pm 1 \mathrm{MHz}$. If this adjustment cannot be achieved, selectable resistor A7R94* can be changed to provide the proper range necessary.
8. Adjust front-panel TUNING control for DVM indication of $\mathbf{- 1 0 . 0 0 0}$ Vdc.
9. Set A7R956 GHz F (fine) to approximately midrange ( R 95 is a 20 -turn potentiometer).
10. Adjust A8R28 6 GHzC (coarse) for a frequency counter indication of $6.000 \mathrm{GHz} \pm 2 \mathrm{MHz}$.
11. Retune front-panel TUNING control for $\mathbf{0 . 0 0 0} \mathrm{Vdc}$ DVM indication and readjust A7R 743 GHz if necessary for frequency counter indication of $3.000 \mathrm{GHz} \pm 1 \mathrm{MHz}$.
12. Tune front-panel TUNING control for $\mathbf{- 1 0 . 0 0 0}$ Vdc DVM indication.
13. Lightly tap the top edge of the A7 Frequency Control board with the handle of a small screwdriver to seat controls.
14. Adjust A7R95 6 GHzF (fine) for frequency counter indication of $6.000 \mathrm{GHz} \pm 1 \mathrm{MHz}$.

## Alternate IF First LO Shift Check

15. Press front-panel ALT IF pushbutton IN to activate alternate IE
16. Verify YTO frequency shift according to the following table.

| TABLE $5-10$. FRST LOSHIFTCHECK |
| :--- |
| FREQUENCY BAND GHz ALT IF FREQUENCYCOUNTER INDICATION <br> $1(.01-3)$ OFF Reference $(6.000 \mathrm{GHz})$ <br> $1(.01-3)$ ON Reference $-15 \mathrm{MHz} \pm 800 \mathrm{kHz}$ <br> $2(6-9)$ ON Reference $+15 \mathrm{MHz} \pm 800 \mathrm{kHz}$ <br> $3(3-9)$ ON Reference $-7.5 \mathrm{MHz} \pm 400 \mathrm{kHz}$ <br> $4(9-15)$ ON Reference $+7.5 \mathrm{MHz} \pm 400 \mathrm{kHz}$ <br> $5(6-15)$ ON Reference $-5 \mathrm{MHz} \pm 300 \mathrm{kHz}$ <br> $6(12.1-21)$ ON Reference $+5 \mathrm{MHz} \pm 300 \mathrm{kHz}$ |

17. Remove jumper from A16TP1 DIODE BIAS to Ground.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(SERIAL PREFIX 2236A)(Cont'd)

## FM Driver Adjustment

18. Disconnect frequency counter from analyzer RF Input and connect comb generator to RF Input,
19. Set comb generator for 1 MHz comb teeth.
20. Set analyzer controls as follows:
FREQ SPAN/DIV 1 MHz
RES BW . ..... 30 kHz
TIME/DIV ..... AUTO
FREQUENCY BAND GHz ..... Band 1 (.01-3)
REF LEVEL dBm ..... $-20$
INPUT ATTEN ..... 0 dB
ALTIF ..... OFF (out)
SIG IDENT ..... OFF (out)
AmplitudeScale ..... $10 \mathrm{~dB} /$ DIV
21. Tune front-panelTUNING control for approximately 1500 MHz indication on front-panel FREQUENCY display.
22. Adjust front-panel TUNING FINE control to place a comb tooth on the first graticule line on the mainframe CRT display.
23. Adjust A7R38 FM to place a comb tooth on the ninth graticule line.
24. Readjust TUNING FINE control to place a comb tooth on the first graticule line and adjust A7R38 FM to place a comb tooth on each of the graticule lines while keeping the first comb tooth aligned using the TUNING FINE control.
25. Tune to approximately 100 MHz and verify that when a comb tooth is placed on the first graticule line using the TUNING FINE control that the ninth comb tooth is aligned with the ninth graticule line $\pm 1$ minor division.
26. Repeat step 25 for frequency of approximately 2500 MHz .
27. If necessary, A7R38 FM may be compromise adjusted for best span linearity at the three frequencies indicated.
28. Set comb generator for $100-\mathrm{MHzcomb}$ teeth.
29. Adjust front-panel TUNING control for 100 MHz indication on FREQUENCY display
30. Set FREQ SPAN/DIV to 2 MHz .
31. Adjust TUNING to place $100-\mathrm{MHz}$ comb tooth on center graticule line.

## ADJUSTMENTS

## 5-25. FIRST CONVERTER ADJUSTMENTS(SERIAL PREFIX 2236A)(Cont'd)

32. Set FREQ SPAN/DIV to 1 MHz . Note position of comb tooth.
33. Adjust A7R99 MO to place comb tooth midway between position noted in step $\mathbf{3 2}$ and center graticule line.
34. Set FREQ SPAN/DIV to 2 MHz .
35. Adjust TUNING to place comb tooth on center graticule line.
36. Set FREQ SPAN/DIV to $1 \mathbf{M H z}$. Note displacement of comb tooth from center graticule line.
37. Repeat steps $\mathbf{3 0}$ through $\mathbf{3 6}$ until displacement of comb tooth is less than $\mathbf{0 . 2}$ major division when FREQ SPAN/DIV is switched from 2 MHz to 1 MHz .

Page 6-7:
Table 6-3. Replaceable Parts
2236A \& Below Change WB to HP Part Number 1250-1159, Check Digit 4, CABLE ASSEMBLY, YIO TO FIRST MIXER.

1951A,1945A Change W4 to HP Part Number 08559-60001, Check Digit 3,
\& Below CABLE ASSEMBLY, CAL OUTPUT.

## Page 6-8:

## Figure 6-1. Mechanical Chassis Parts

2236A \& Below Change item (2), GUSSET, LEFT, to PP Part Number 08559-60032, Check. Digit 4
Change item (3), GUSSET, RIGHT, to HP Part Number 08559-60031, Check Digit 3.

2208A \& Below Change item (1), PANEL FRONT, to P Part Number 08559-00001, Check Digit 7.
Change item (2), GUSSET, LEFT, to HP Part Number 08559-00005, Check Digit 1.
Change item (3), GUSSET, RIGHT, to H Part Number 08559-00004, Check Digit 0 .
Change item (11), GUIDE RAIL, BOTTOM, to $\mathbf{H}$ Part Number 08559_ 20013, Check Digit 3.

2019A00441
\& Below

Change HP Part Number 08559-00028 to HP Part Number 08558-00081, Check Digit 2, ATIENUATOR BRACKET.
Add H Part Number 08559-00023, Check Digit 3, BRACKET, ATIENUATOR DR SUPPORT.

Pages 8-17 through 8-23/8-24: DIGITAL PANEL METER ASSENBLY A1
Table 8-1. Digital Panel Meter Assembly A1, Replaceable Parts
2218A \& Below Replace Table 8-1 with new Table 8-1 (SERIAL PREFIX 2218A) included in this Manual Backdating supplement.

2208A \& Below Change A1A1 to HP Part Number 08559-60032, Check Digit 0. Add A1A1MP1, H Part Number 0380-1047, Check Digit 3, SPACER-RVTON .25-IN-LG . 15-IN-ID.

1945A00241,249, Change A1A2C4 and A1A2C5 to HP Part Number 0160-3914, Check 258,262,265,277 ; Digit 1, CAPACITOR-FXD .01UF +-10\% 100VDC CER.
1951A00283,286, Change A1A2L1 to HP Part Number 08559-80002, Check Digit 6, 288-290,292, COIL, 110 UH.
295-300; 2003A
\& Below
Figure 8-5. Digital Panel Meter Assembly Al, Component Locations
2218A \& Below Replace Figure 8-5 with new Figure 8-5 (SERIAL PREFIX 2218A) included in this Manual Backdating supplement.

Figure 8-6. Digital Panel Heter Assembly A1, Schematic Diagram

2218A \& Below

1945A00241,249,
258,262,265,277;
1951A00283,286,
288-290,292,
295-300; 2003A
\& Below

Replace Figure 8-6 with new Figure 8-6 (SERIAL PREFIX 2218A) included in this Manual Backdating supplement.

Make the following changes in function block (C): Change C4 and C5 to . O1UF. Change L1 to 110 UH .

TABLE8-1. DIGITALPANELMETER ASSEMBLYA1, REPLACEABLEPARTS(SERIALPREFIX2218A)

| Reference Designation | HP Part <br> Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 |  |  |  | FREQUENCY DISPLAY ASSEMBI Y |  |  |
| A1A1 | 08559-60072 | 8 | 1 | DPM DISPLAY | 28480 | 08559-60072 |
| A1A1DS1 A1A1DS | 1990-0693 $1990-0693$ | 7 | 5 | DISPLAY NUM SCG I-CHAR .3 H | 26480 $? 8480$ | $\begin{aligned} & \text { 1DS1-3533 } \\ & 1 \mathrm{DS} 1-3533 \end{aligned}$ |
| A1 A1DS3 | 1990-0693 | 7 |  | DISPLAY-NUH-SEG 1 -CHAR . 3 H | 28480 | $1 \mathrm{DE} 1-3533$ |
| A1A1DS 4 | 1790-0693 | 7 |  | DISPLAY-NUM SEG 1 CHAR 3 : 1 | 28480 | 1DS1-3533 |
| A1 A1DS5 | 1990-0693 | 7 |  | DISPLAY-NUM -SEG 1-CHAR 63 H | 2¢,480 | 1DS1-3533 |
| A1A1XDS1 | 1200-0834 | 5 | 5 | SOCKET-TC 10-CONT DIP DIP SLDR | 28480 | 1200-0834 |
| A1A1xDS2 | 1200-0834 | 5 |  | SOCKET-IC 10-CONT DIP DIP SIDR | 28480 | 12000-0834 |
| A1A1XDS3 | 1200-0834 | 5 |  | SOCKET-IC 10 CONT DIP DIP SLDR SOCKFT-IC 10-CONT DIP | 28480 28480 | $1200-0834$ 1200.0834 |
| A1A1XDS 4 A1A1 | $1200-0834$ $1200-0834$ | 5 5 |  | SOCKFT-IC 10-CONT DIP DIP SIP SOCKET IC 10 | 28480 38480 | 120000834 $1200-0834$ |
| A1 A2 | 08559-60033 | 1 | 1 | DPM DRIVER | 211480 | 08557-60033 |
| A1A2C1 | 0160-2220 | 0 | , | CAPACITOR FXD $120 \mathrm{OPF}+5 \%$ 300UDC MICA | 284880 | 0150-2220 |
| A1 A2C2 | 0160-3402 | 2 | 1 | CAPACITOR-FXD 10 O + $+5 \%$ 50UDC. HCT-POL Y | 29480 | $0160-3402$ DM15F391J030 OLU 1 CR |
| A1 A2C3 A1 A2C | $0140-0200$ $0160-3751$ | 0 4 | 1 | CAPACITOR FXD $3709 \mathrm{~F}+5 \% 300 \mathrm{DDC}$ HICA | 72136 28480 | DM15F391J030 OWU 1 CR $0160-3751$ |
| A1A2CS | 0160-3751 | 4 |  | CAPACITOR FXD 22009F + 5\% 50UDC CER | 28480 | 01s0-3751 |
| A1A2C6 | 0160-3661 | 5 | 1 | CAPACITOR-FXD . $1 \mathrm{UF}+-5 \%$ SOUDC MET POL.YC | 29480 | $0160-3661$ $150 \mathrm{D} 25 \times 920{ }^{\text {a }}$ ( |
| A1A2C7 A1 A2CB | $0180-0197$ $0180-1746$ | 8 5 | 1 2 | CAPACITOR-FXD $2.2 \mathrm{SUF}+-10 \%$ TOVDC TA CAPAC ITOR-FXD $\mathbf{1 5 U F}+-10 \% ~ 20 U D C ~ T A ~$ | 56287 58.289 | $150 \mathrm{D225} \mathrm{\times 9020A2}$ $150 \mathrm{D156} \mathrm{\times 902082}$ |
| A1 A2C9 | 0180-2208 | 6 | 1 | CAPACITOR FXD 220UF+ 10\% 10UDC TA | 56289 | $1500227 \times 901052$ |
| A1 A2C10 | 0180-1746 | 5 |  | CAPACITOR-FXD 15UIT-10x 20UDC TA | 58.289 | 150D156×902082 |
| A1A2Cl1 | 0160-3877 | 7 | $?$ | CAPAC ITOR - FXD - $011 \mathrm{JF}+\cdots 20 \%$ 100UDC CER | 28470 | $0160 \quad 3879$ |
| A1A2C12 A1A2C13 | $0160-0127$ $0160-3879$ | 2 7 | 1 | CAPACITOR-FXD 1UF +-20\% 2SUDC CER CAPACITOR -FXD .01UF + $-20 \% 1000 D C$ CEX | 28480 28480 | $\begin{aligned} & 016.0-0127 \\ & 01 \leqslant 0-3879 \end{aligned}$ |
| A1AECR 1 | 1901-0050 | 3 | 1 | DIODF SWITCHING gov 200MA TNR DO-35 | 28480 | 1901-0050 |
| A1A2J1 | 1251-4797 | 4 | 1 | CONNECTOR 10 PIN M POST TYPE | 28480 | 1251-4797 |
| A1 A2L 1 | $08559-80010$ $7140 \cdots 129$ | 6 | 1 | COIL, 540 UH INDISCTOR RF-CH MLD 220UH $5 \times, 166 D X, 3 B 5 I G$ | 28480 28480 | 08559.80010 $9140-0129$ |
| A1 A2L 3 | 9100-1641 | 0 | 1 | INDUCTOR RF-CH MLD $240 \mathrm{UH} 5 \%$, 166DX, 385LG | 28480 | $9100-1641$ |
| A1A2Q1 A1 A2Q2 | $1854-0404$ $1853-0281$ | 0 | 1 | TRANSISTOR NPN ST TO-18 PD=360MW TRANSISTOR PNP ${ }^{\text {SNO.907A SI TO } 18 \mathrm{PD}=400 \mathrm{KL}} \mathrm{l}$ | 28480 04713 | $1854-0404$ 3N2907A |
| A1A2Q2 A1A2Q3 | $1853-0281$ $1855-0420$ | 9 2 | 1 | TRANSISTOR PNP 2N2907A S TO 18 PD=40014 | 04713 01295 | 2N2907A 2N4:391 |
| A1 A294 | 1854-0071 | 7 | 1 | TRANSISTOR NPN SI PD=300MW FT $=200 \mathrm{MHz}$ | 28480 | 1854-0071 |
| A1A2R1 | 0811-0696 | 1 | 1 | RESISTOR 91K 1\% . 125 W PWW TC=0* 5 | 28480 | 0311-0696 |
| A1 A2R2 | 0811-0640 | 5 | 3 | RFSISTOR 100K . $01 \%$. 125 W PUU TC $=0+10$ | 28480 | 0811-0640 |
| A1A2R3 | 0757-0460 | 1 | 1 | RESISTOR 61.7K 1\% . 125 L K TC $=0+\cdots 100$ | 74546 | C4-1/8-T0-6192-F |
| A1 A2R 4 | 0698-3162 | 0 | 1 | RESISTOR 46.4K $1 \%$, 125w F TC=0t 100 | 24546 | C4 1/8-T0-46,42-F |
| A1ARRS | 0678-3155 | 1 | 1 | RESISTOR 4.64K $1 \%$. 125 W F TC $=0$ 0--100 | 74546 | C4 1/8- $\mathrm{TO-4641}^{\text {F }}$ |
| A1 A2R6 | 2100-1738 | 9 | 1 | RESIGTOR-TRMR 10K $10 \%$ C TOP-ADJ I -TRN PECIETOR-TRMP 100K $10 \%$ C TOP-ADJ 1 TRN | 73138 73138 | Q2PR10k |
| A1A2R A1 A2RE | -2100-2655 | 9 | 1 2 | RESISTOR -TRMR $100 \mathrm{~K} 10 \chi$ C TOP-ADJ 1 TRN RFSISTOR $10 \mathrm{~K} 1 \chi .125 \mathrm{~F}$ F TC=0+-100 | 73138 24546 | 82PR100K $\mathrm{C4}-1 / 8-\mathrm{TO-1002-F}$ |
| A1A2R9 | 0757-0442 | 9 |  | RCSISTOR $10 \mathrm{~K} 1 \boldsymbol{\chi}$. 125 W F Tr $=0+100$ | 24546 | C4-1/8-70-1002-F |
| A1 AZR 10 | 0757-0274 | 5 | 1 | RESISTOR 1.21\% $1 \%$. 125 W F TC=0 $+\cdots 100$ | 24546 | C4-1/8-T0-1211-F |
| A1ARR11 | 0757-0280 | 3 | , | RESISTOR $1 \mathrm{~K} 1 \boldsymbol{1 x} .12 \mathrm{EW}$ F TC=01-100 | 24546 | C4 1/8-T0-1001-F |
| A1 A2R12 | 0757-0438 | 3 | 2 | RESISTOR 5.11K 1\% , 125W F TC=04 100 | 74546 | C4- 1/8-T0-5111-F |
| A1A2R 13 A1 A2R 14 | 0698-3136 | 8 | 1 | RESISTOR 17.8K $1 \%$. 125W F TC=0 + 100 | 24546 | C4-1/8-T0-1782-F |
| A1ARR 15 | 0698-3442 | 9 | 1 |  | 24546 |  |
| $\begin{aligned} & \text { A1 A2R } 16 \\ & \text { A1ARR17 } \end{aligned}$ | $\begin{aligned} & 0757-0438 \\ & 0698-3438 \end{aligned}$ | 3 3 |  | RESISTOR S.11K 1\% .125W F TC=0+-100 RES ISTOR $1471 \%, 125 W$ F TC $=0+\cdots 100$ | $\begin{aligned} & 24546 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \mathrm{C4-1/8-TO-5111-F} \\ & \mathrm{C} 4 \sim 1 / \mathrm{B}-\mathrm{TO}-147 R-F \end{aligned}$ |
| A1 A2R 18 | 0757-0279 | 3 0 0 | 1 | RESISTOR 3.16K $1 \dot{\chi}$. 125 W F TC=0 $+\cdots 100$ | 24546 24546 | C4-1/8-T0-147R-F CA -1/8-T0-3161-F |
| A1ARR19 | 0698-0085 | 0 | 1 | RESKSTOR 2.61K $1 \%$. 1254 F TC $=0 \mathrm{D}+100$ | 24546 | C.4-1/8-T0-2611-F |
| A1 A2R20 | 0698-3438 | 3 |  | RESISTOR $147 \mathbf{1 \%}$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-147R-F |
| A1A2R21 | 0811-064i | 5 |  | RESKSTOR 100K . $01 \%$. 12 EWW PWU TC=0+-10 | 28480 | 0811-0640 |
| A1 AZR22 | 0811-0640 | 5 |  | RESISTOR 100K .01X . 125W PUU TC=0t-10 | 28480 | 0811-0640 |
| A1A2TP1 | 1251-0600 | 0 | 1 | CONNECTOR-SCL CONT PIN 1.14-MM-BSE--52 SQ | 28480 | 1251-0600 |
| A1 A2U1 A1AZU2 | $\begin{aligned} & 1826-1058 \\ & 1826-0588 \end{aligned}$ | 3 2 | 1 | IC OP AMP CP 8-TO-99 PKG IC CONV $16-$ DIP-P PKG | 28480 17856 | $\begin{aligned} & 1826-1058 \\ & \text { LD120CJ } \end{aligned}$ |
| A1 AzU3 | 1826-0587 | 1 | 1 | IC CONV 18-DIP-P PKG | 17856 | L.D121CJ |
| $\mathrm{Al}^{\text {A }}$ A2U4 | 1820-1903 | 5 | 1 | IC DRVR TTL DSPL DRVR | 07263 | 9368 PC |
| A1 A2U5 | 1810-0347 | 8 | 2 | NETUORK-RES O--SIP2. 2 KK OHM X 4 | 01121 | 2088222 |
| AIAZU6 | 1810-0347 | 8 |  | NETWORK-RES B-SIP2.2K OHM $\times 4$ | 01121 | 2088222 |
| A1AZVR 1 AIAZUR2 | $\begin{aligned} & 1912-0625 \\ & 1902-3149 \end{aligned}$ | 0 | 1 | DIODE-ZNR 1N829 6.2U 5\% DO-7 PD=.25W DIODE-ZNR 9.07U 5X DO-35 PDE.4W | $\begin{array}{r} 04713 \\ 28480 \end{array}$ | $\begin{aligned} & 1 \mathrm{~N} 829 \\ & 1902-3149 \end{aligned}$ |
| A1 AZUR3 | 1902-3024 | 9 | 1 | DIODE-ZNR 2.87 U 5\%DO-7 PDx. 4 W TCm. . $07 \%$ | 28480 | 1902-3024 |
| A1AEVR 4 | 1902-1286 | 1 | 1 | DIODE-ZNR 1N5342B 6, BU 5X PD=54 TC= +200\% | 04713 | 1 N5342B |
| A1 A2XA1 | 1251-3403 | 7 | 1 | CONNECTOR-PC EDGE 10-CONT/RDW 2-ROWS | 28480 | 1251-3403 |

See introduction to this section for ordering information
*Indicates factory selected value

A1A2
DPM DRIVER


A1A1
DPM DISPLAY



## Pages 8-25 through 8-49/8-50: FRONT WITCH ASSENBLY A2

Figure 8-10. Front Switch Assembly A2, Exploded View
2208A \& Below Delete Figure 8-10.
2109 A00441 Add HP Part Number 08558-00021, Check Digit 0, PLATE LEVEL, \& Below POT (S1).

Table 8-2. Front Switch Board Assembly A2A1, Replaceable Parts
2208A \& Below Replace Table 8-2 with new Table 8-2 (SERIAL PREFIX 2208A) included in this Manual Backdating supplement.

TABLE 8-2. FRONT SWITCH BOARD ASSEMBLY A2, REPLACEABLE PARTS (1 OF 2) (SERIAL PREFIX 2208A)

| Reference Designation | HP Part Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A2 | 03559-60043 | 3 | 1 | FRONT PANEL SWITCH ASSEMBLY | 28480 | 08559-60043 |
| A2CR1 | 1901-0033 | 2 | 1 | DIODE-GEN PRP $180 \cup 200 \mathrm{MA}$ DO 77 D ${ }^{\text {d }}$ | 28.480 28480 | $1901-0033$ $1901-0050$ |
| AECR2 | 1901-0050 | 3 | 4 | DIODE-SWITCHING $80 \cup$ 200MA 2NS DO-35 DIODE-SWITCHING BOU 200MA 2NS DO-35 | 28480 28480 | 1901-0050 |
| A2CR3 A2CR | $1901-0050$ $1901-0050$ | 3 3 |  | DIODE-SWITCHING DIODE-SWITCIING B0U 200 MA 200MA 2NS 2NS DO-35 | 28480 28480 | 1901-0050 |
| A2CR4 | 1901-0050 | 3 |  | DIODE-SWITCHING 80U 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A2J1 |  |  |  | PART OF W1 |  |  |
| A2J2 A2J |  | 0 | 1 | PART OF W2 SOCKET-IC 14 -CONT DIP SLDR | 28480 | 1200-0508 |
| A2J3 | 1200-0508 | 0 | 1 |  |  |  |
| A2R1 | $0757-0447$ $2100-3633$ | 4 | 1 |  | 24546 28480 | $\begin{aligned} & \text { C4-1/8-T0-1622-F } \\ & 2100-3633 \end{aligned}$ |
| A2R2 A2R3 | $2100-3633$ $2100-3744$ | 7 <br> 1 | 1 2 | RESISTOR-UAR CONTROL CP | 01121 | WP 4G024S103UZ |
| A224 | $2100 \cdot 3332$ | 3 | 1 | RESISTOR-TRMR 10 K 20\% CC TOP-ADJ 1 -TRN | 28480 24546 | 2100-3332 C4-1/8-T0-1212-F |
| A2R5 | 0757-0444 | 1 | 1 | RESISTOR 12.1 K 1 K . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-1212-F |
| A2R6 | 2100-3785 | 0 | 1 | RESISTOR-UAR CONTROL CCP 50010 Z LIN | 01121 01121 | WP 460245501UZ <br> WP4G024S103RZ |
| A2R7 A2R | $2100-3786$ $0757-0280$ | $\frac{1}{3}$ | 1 |  | 01121 2.4546 | WP4G024S103RZ <br> C.4-1/8-T0-1001-F |
| ARR8 A2R9 | 0757-0280 | 3 7 | 1 | NOT ASSIGNED <br> RESISTOR $1.33 \mathrm{~K} 1 \mathrm{x}, 125 \mathrm{~K}$ F TC=0 $=100$ |  | C4-1/8--T0-1331-F |
| A2R 10 A2R11 | $0757-0317$ $2100-3744$ | 7 1 | 1 | RESISTOR $1.33 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{FF}$ TC=0\%-100 RESISTOR-UAR CONTROL CCP 10 K 10 K LIN | 24546 01121 | WP 4G024S103U2 |
| A2S1 A2S2 A2S3 | 3101-2213 | 0 | 1 | REFERENCE LEVEL SWITCH (SEE AZ SWITCH PARTS) AMPLITUDE SCALE SWITCH SWEEP TIME SWITCH (SEE AZ SWITCH PARTS) | 28480 | 3101-2213 |
| A2S4 A2S5 A2S6 |  |  |  | SWEEP TRIGGER SWITCH (SEE AZ SWITCH PARTS) RESOLUTION BW SWITCH (SEE AZ SWITCH PARTS) FREQ SPAN/DIU SWITCH (SEE AZ SWITCH PARTS) |  |  |
| $\begin{aligned} & \text { A2S7 } \\ & \text { A2S8 } \\ & \text { A259 } \end{aligned}$ | $3101-2376$ $3101-2124$ $3101-2124$ | 6 <br> 2 <br> 2 | 1 2 | SWITCH-PB 6-STATION 10 MM C-C SPACING SWITCH-PB DPDT ALTNG ,2SA 115 SVAC SWITCH-PB DPDT ALTNG . 25A 115 VAC | 28480 28480 28480 | $\begin{aligned} & 3101-2376 \\ & 31011-2124 \\ & 3101-2124 \end{aligned}$ |
| A2UR1 | 1902-3172 | 8 | 1 |  | 28480 | 1902-3172 |
| A2W1 A2W2 | $\begin{aligned} & 08559-60004 \\ & 08559-60003 \end{aligned}$ | 6 5 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | RIBBON CABLE, DPM/REAR SHITCH RIBRON CABLE, FRONT SWITCH | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{array}{r} 08559-60004 \\ 08559-60003 \end{array}$ |
| $\begin{aligned} & \text { A2XD1 } \\ & \text { A2×D2 } \end{aligned}$ | $1200-0010$ $1200-0010$ | $9$ | 2 | SOCKET-TUBE 2-CONT SOCKET-TUBE 2-CONT | 28480 28480 | $\begin{aligned} & 1200-0010 \\ & 1200-0010 \end{aligned}$ |
|  |  |  |  | A2 SWITCH PARTS |  |  |
|  | $\begin{aligned} & 1410-0006 \\ & 08565-20049 \\ & 08558-20089 \\ & 1490-0841 \\ & 08558-00022 \end{aligned}$ | $\begin{aligned} & 8 \\ & 3 \\ & 2 \\ & 7 \\ & 1 \end{aligned}$ | 8 4 1 1 1 | ```BALL-BRG TYPE . 1875-DIA GRADE-50 SET BUSHING (51,53,54,55,56) BUSHING, SLOTTED (S6) COUPLER, (S1) CRANK, SLOTTED (S1)``` | 78707 28480 28480 28480 28480 | $\begin{aligned} & \text { GRADE. } 50 \\ & \text { OB565-20049 } \\ & 08558-20089 \\ & 1470-0841 \\ & 08558-00022 \end{aligned}$ |
|  | $\begin{aligned} & 00559-00012 \\ & 08558-00020 \\ & 08565-00006 \\ & 08558-00005 \\ & 08558-00024 \end{aligned}$ | $\begin{aligned} & 0 \\ & 9 \\ & 0 \\ & 4 \\ & 3 \end{aligned}$ | 1 1 1 1 1 | DETENT, ATTENUATOR (S1) <br> DETENT PLATE (S1) <br> DETENT, SWEEP TIME (S3) <br> DETENT, RESOLUTION BW (S5) <br> DETENT, SWEEP TIME ( 83 ) | $\begin{aligned} & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 08559-00012 \\ & 08558-00020 \\ & 08565-00006 \\ & 085588-00025 \\ & 08558-00024 \end{aligned}$ |
|  | $\begin{aligned} & 09558-00026 \\ & 08558-20088 \\ & 1430-0036 \\ & 08558-20058 \\ & 08559-60060 \end{aligned}$ | $\begin{aligned} & 5 \\ & 1 \\ & 6 \\ & 5 \\ & 4 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 4 \end{aligned}$ | ```DETENT, SWEEP TRIGGER (S4) GEAR, 20T (S1) GEAR, METER, 16T 32DP (S1) HUB, COUPLING (55, S6) HUB, DRIVE (S1, S3, S4)``` | $\begin{aligned} & 28480 \\ & 28480 \\ & 71041 \\ & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 08558-00026 \\ & 08558-20088 \\ & 6462 Y(40 D) \\ & 08558-20058 \\ & 08559-60060 \end{aligned}$ |
|  | $\begin{aligned} & 08558-20057 \\ & 08558-200062 \\ & 08558-20061 \\ & 29500-00006 \\ & 08559-20007 \end{aligned}$ | 6 1 0 3 5 | 2 1 1 1 4 | HUB, DRIVE (S5, S6) <br> LOCKOUT, FIXED (S1) <br> LOCKOUT, ROTATING (S1) <br> NUT, HEX 1/4-32 (S1) <br> NUT -HEX, SPACER ( $31,33,54,56$ ) | $\begin{aligned} & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 08558-20059 \\ & 08558-20062 \\ & 08558-20061 \\ & 0850-0008 \\ & 08559-20007 \end{aligned}$ |
|  | $\begin{aligned} & 1480-0367 \\ & 1480-0059 \\ & 08558-00021 \\ & 08558-20043 \\ & 08558-40005 \end{aligned}$ | 1 <br> 1 <br> 8 <br> 0 <br> 8 | $\begin{array}{r} 10 \\ 1 \\ 1 \\ 1 \\ 3 \end{array}$ | PIN, DOWEL, .062DIA (S1, S4, S5, S6) <br> PIN, ROLL O62DIA (Si) <br> PLATE LEVEL, POT (S1) <br> ROTOR ASSY, ATTENUATOR (S1) <br> ROTOR, DOUBLE CONTACT (S1, S4, S6) | 28480 <br> 28480 <br> 28480 <br> 28480 <br> 28480 | $\begin{aligned} & 1480-0367 \\ & 1488-0059 \\ & 08558-00021 \\ & 08558-20043 \\ & 08558-40005 \end{aligned}$ |
|  | $\begin{aligned} & 08558-20066 \\ & 08558-20108 \\ & 0510-0015 \\ & 0510-0053 \\ & 1410-1860 \end{aligned}$ | 5 5 6 0 6 4 | $\begin{aligned} & 1 \\ & 1 \\ & 3 \\ & 2 \\ & 5 \end{aligned}$ | ```ROTOR, FREQ SPAN (S6) ROTOR, SWEEP TIME RTNR-R . 125 OD (S3, S5) RTNR-R .18B OD (S1) SPR CPR , 180LG (S1, 53, S4, S5, S6)``` | $\begin{aligned} & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \\ & 2880 \end{aligned}$ | $\begin{aligned} & 08558-20066 \\ & 08558-20108 \\ & 0510-0015 \\ & 0510-0053 \\ & 1410-1860 \end{aligned}$ |

See introduction to this section for ordering information
*Indicates factory selected value

TABLE8-2. FRONTSWITCHBOARD ASSEMBLY A2, REPLACEABLEPARTS(2OF 2) (SERIALPREFIX 2218A)

| Reference Designation | HP Part Number |  | Oty | Description | $\mathrm{Mfr}$ Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | SHART, DRIUE, ATTENUATOR (SU)SHAFT, FREG SPAN (SG) SHAFT, FIXED, aFF IEUEL (S1)SHAFT, MAN SWIF (S4)SIAAT, SHAFT, MAN SUECP (S4)SHAFT, RET LEVEL ( $\mathrm{S1}$ ) SHAFT, REF LEUEL FINE (S1)SHAFT, RESDLUTION BW (SS)SHAFT, SWEEP TIME (S3) <br> SHAFT, SWF:P TRIGGR (S4) <br> SPACER <br> 1.2501 <br>  <br>  <br>  <br> ac misclllaneous parts <br>  SCRFU-SET 4-40. 125-IN-LC SMALL CUP-PT SCREU-SET 4-40, $094-$ IN-LC SMALL CUP PT SCREU SET $6-32,125$ IN-LG FLAT PT AI Y <br>  UASHER-FL MTLC NO. 8 , 18 ND UACHFR-FL MTLC NO UASHER-FL MTLC NO. 5 , 125 -IN-ID MYLAR CABLE SHIELD M |  |  |

[^5]*Indicates factory selected value

| Pages 8-51 through 8-65/8-66: YIG-TUIED OSCILLATOR ASSENBLY A6 |  |
| :---: | :---: |
| Table 8-3. RF Section, Replaceable Parts |  |
| 2240A \& Below | Add A5MP3, H Part Number 08559-20041, Check Digit 7, COVER, $2 \mathbb{N D}$ L.O. |
|  | Under Miscellaneous Parts: <br> Change the quantity of $\mathbf{H}$ Part Number 2200-0119 from 7 to 9 . Delete HP Part Number 2200-0156. |
| 2236A \& Below | Change A5 to HP Part Number 08559-60005, Check Digit 7. <br> Change A5MP2 to HP Part Number 08559-20002, Check Digit O, CAVITY BLOCK. |
|  | Change A6 to HP Part Number 5086-7301, Check Digit 5. <br> Add HP Part Number 08559-00033. YTO SHIELD. |
| 1951A00285 | NOTE |
| \& Below | The following components have preferred replacements; A5C4 and A5L2. If the instrument does not contain the preferred replacement values, as shown in this Replaceable Parts list and Schematic in the Manual, then both components should be changed at the same time. |
| $\begin{aligned} & \text { 1951A, 1945A } \\ & \& \text { Below } \end{aligned}$ | Change A5CR2 and A5CR3 to $\mathbf{P}$ Part Number 0122-0078, Check Digit 2, DIODE-VVC BVR=30V Q=225-MIN. |
| 1909A \& Below | Change A5L3 to HP Part Number 08559-00020, Check Digit 0 , COUPLING LOOP INPUT. |
| Figure 8-21. 2nd Converter, Component Locations |  |
| 2236A \& Below | Delete Front YIG Mounting Bracket, H Part Number 08559-00035. Delete Rear YIG Mounting Bracket, HP Part Number 08559-00036. |
|  | NOTE |
|  | Prior to 2236A serial prefix, the YIG-Tuned Oscillator Assembly A6 was mounted to the side gusset. |
| Figure 8-22. YIC-Tuned Oscillator Assembly A6 and Shielded Components |  |
| 2236A \& Below | Delete Figure 8-22. |
| Figure 8-25. RF Section, Schematic Diagram |  |
| 2236A \& Below | Replace appropriate sections of Figure $8-25$ with new P/O Figure 8-25 (SERIAL PREFIX 2236A) included in this Manual Backdating supplement. |



P/O FIGURE\&-25. RFSECTION,SCHEMATICDIAGRAM(SERIALPREFIX2236A)

## Pages 8-67 through 8-81/8-82: FREQUEMCY COMTROL ASSERBLY A7

Table 8-4. Frequency Control Assembly A7, Replaceable Parts

| 2236A \& Below | Replace Table 8-4 with new Table 8-4 (SERIAL PREFIX 2236A) included in this Manual Backdating supplement. |
| :---: | :---: |
| 2208A \& Below | Make the following changes to new Table 8-4 (SERIAL PREFIX 2236A) : |
|  | Change A7 to HP Part Number 08559-60021, Check Digit 7. |
|  | Add A7C1 and A7C2, HP Part Number 0180-2208, Check Digit 6, CAPACITOR-FXD 220UF +-10\% 10VDC TA. |
|  | Add A7C11, H Part Number 0160-2055, Check Digit 9, CAPACITORFXD . 01UF +80-20\% 100VDC CER. |
|  | Delete the following: <br> A7C 13, A7C14, A7CR8, A7CR9, A7Q19, and A7Q20. |
|  | Change A7R30 to HP Part Number 0698-3428, Check Digit 1, RESISTOR $14.7 \quad 1 \%$. 125W F TC=0+-100. |
|  | Change A7R31 to HP Part Number 0757-0199, Check Digit 3, RESISTOR $21.5 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$. |
|  | Add A7R98, $\mathbf{P}$ Part Number 0757-0465, Check Digit 6, RESISTOR 100K $1 \%$. 125W F TC=0+-100. |
|  | Delete the following: |
|  | A7R100, A7R101, A7R102, A7U12, and A7VR1. |
|  | Add ATW1, H Part Number 8159-0005, Check Digit 0, WIRE 22AWG W PVC 1X22 80C. |
| 2004A \& Below | Delete A7R99. |

Figure 8-28. Frequency Control Assembly A7, Component Locations

| 2236A \& Below | Replace Figure 8-28 with new Figure 8-28 (SERIAL PREFIX 2236A) <br> included in this Manual Backdating supplement. |
| :--- | :--- |
| 2208A \& Below | Replace Figure 8-28 with new Figure 8-28 (SERIAL PREFIX 2208A) <br> included in this Manual Backdating supplement. <br> Add the following to Figure 8-28 (SERIAL PREFIX 2208A): |
|  | Add C12 between TP2 and the negative (-) side of C8. <br> Add R99 to the 1 eft of TP7. |
| 2004A \& Below | Delete A7R99. |

Figure 8-29. Frequency Control Assembly A7. Schematic Diagram (1 of 2)
2236A \& Below Replace Figure 8-29 (1 of 2) with new Figure 8-29 (1 of 2) (SERIAL PREFIX 2236A) included in this Manual Backdating supplement.

2208A \& Below Make the following changes to Figure 8-29 (1 of 2) (SERIAL PREFIX 2236A):

Change A7 to $\mathbf{H}$ Part Number 08559-60021.
In function block (A), add R98, 100K, as follows: Open the FM/MAIN lice at the left side of R33. Connect one side of R98 to the left side of R33. Connect the other side of R98 to the FM/MAIN line.

Figure 8-29. Frequency Control Assembly A7, Schematic Diagram (1 of 2) (COG~'~)
2004A \& Below Make the following changes in function block (A): Delete R99. Connect pin 7 of U 10 B to pin 10 of U10C.

Figure 8-29. Frequency Control Assembly A7, Schematic Diagram (2 of 2)
2236A \& Below Replace Figure 8-29 (2 of 2) with new Figure 8-29 (2 of 2) (SERIAL PREFIX 2236A) included in this Manual Backdating supplement.

2208A \& Below Make the following changes to Figure 8-29 (2 of 2) (SERIAL PREFIX 2236A):

Change A7 to HP Part Number 08559-60021.
Replace function block (E) with P/O Figure 8-29 (SERIAL PREFIX 2208A) included in this Manual Backdating supplement.
In function block (G), delete C14 and R102.

TABLE 8-4. FREQUENCY CONTROL ASSEMBLY A7, REPLACEABLE PARTS (10F3) (SERIAL PREFIX 2236A)


See introduction to this section for ordering information
*Indicates factory selected value

TABLE8-4. FREQUENCYCONTROLASSEMBLYA7, REPLACEABLEPARTS(2OF3)(SERIALPREFIX2236A)


See introduction to this section for ordering information
*Indicates factory selected value

TABLE8-4. FREQUENCYCONTROLASSEMBLY A7, REPLACEABLEPARTS(3OF3) (SERIALPREFIX 2236A)


A7
FREQUENCYCONTROL


FIGURE828. FREQUENCYCONTROLASSEMBLY A7, COMPONENTLOCATIONS(SERIAi PREFIX2236A)


FIGURE 828. FREQUENCYCONTROL ASSEMBLY A7, COMPONENTLOCATIONS(SERIALPREFIX2208A)


P/O FIGURE829. FREQUENCY CONTROLASSEMBLY A7,SCHEMATICDIAGRAM(SERIALPREFIX 2208A)


Table 8-5. Marker Assembly A8, Replaceable Parts

| 2309A \& Below | Change A8 to HP Part Number 08559-60022, Check Digit 8. <br> Delete A8C2. <br> Change A8R13 to HP Part Number 0757-0438, Check Digit 3, RESISTOR <br> 5.11 K 1\% . 125 W F TC=0+-100. <br> Change A8R36 to HP Part Number 0757-0466, Check Digit 7, RESISTOR <br> $110 \mathrm{~K} 1 \%$. 125 W F $\mathrm{TC}=0+-100$. <br> Add A8R82, H Part Number 0757-0438, Check Digit 3, RESISTOR <br> $5.11 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+-100$. <br> Change A8R108 to H Part Number 0698-7277, Check Digit 6, <br> RESISTOR 51.1K $1 \% .125 \mathrm{~W}$ F $\mathrm{TC}=0+-100$. <br> Delete A8R 110. <br> Delete ARR111. <br> Change A8U4 to HP Part Number 1826-1058, Check Digit 8, IC CP AMP GP 8-T0-99 PKG. |
| :---: | :---: |
| 2152A \& Below | Delete A8CR21. <br> Change A8R33, A8R87 and A8R88 to HP Part Number 0757-0123, Check <br> Digit 3, RESISTOR $34.8 \mathrm{~K} 1 \%$. 125 W F TC=0+-100. <br> Delete A8R 108. <br> Delete A8R109. |
| 1945A00241,249, | Change A8R34 and A8R62 to HP Part Number 2100-0670, Check |
| 258,262,265,277: | Digit 6, RESISTOR-TRMR 10K 10\%C SIDE-ADJ 17-TRN. |
| $\begin{aligned} & 1951 \mathrm{~A} 0028 \mathrm{~S}, 286, \\ & 288-290,292, \end{aligned}$ | Change A8R 39 to HP Part Number 2100-3754, Check Digit 3, RESISTOR-TRMR 1M 10\% C SIDE-ADJ 17-TRN. |
| 295-300; 2003A | Change A8R 40 to HP Part Number 2100-3752, Check Digit 1, RESISTOR-TRMR 500K $10 \%$ C SIDE-ADJ 17-TRN |
|  | Change A8R61 to HP Part Number 2100-3750, Check Digit 9, RESISTOR-TRMR 20K 10\% C SIDE-ADJ 17-TRN. <br> Change A8R94 to A8R94*. <br> Change A8R94* to H Part Number 0757-0460, Check Digit 1, RESISTOR 61.9K $1 \%$.125W F TC=0+-100. |

Figure 8-32, Marker Assembly A8, Component Locations
2309A \& Below Replace Figure 8-32 with new Figure 8-32 (SERIAL PREFIX 2309A) included in this Manual Backdating supplement.

2152A \& Below Make the following changes to new Figure 8-32 (SERIAL PREFIX 2309A) : Delete A8CR21, A8R108, and A8R 109.

Figure 8-33. Narker Assembly A8, Schematic Diagram (1 of 2)

2309A \& Below | Change A8 to H Part Number 08559-60022. |
| :--- |
| Replace function block (I) of Figure 8-33 with new P/O Figure 8- |
|  |
|  |
|  |
|  |
|  |
| Backdating supplement. |

Figure 8-33. Marker Assembly A8, Schematic Diagram (2 of 2)

| 2309A \& Below | Change A8 to HP Part Number 08559-60022. <br> Replace right half of function block (E) of Figure 8-33 with new P/O Figure 8-33 (2 of 2) (SERIAL PREFIX 2309A) included in this Manual Backdating supplement. |
| :---: | :---: |
| 2017 A \& Below | In function block ( D ), change -1 OV to $\mathbf{- 1 2 . 6 V}$ at the wiper of R 61 and at pin 4 of U15. |
| 1945A00241,249, | Make the following changes in function block (E): |
| 258,262,265,277; | Change R34 to 10K. |
| 1951A00283.286. | Change R62 to 10K. |
| 288-290,292, | Change R94* to 61.9K. |

MARKER


FIGURE8-32. MARKER ASSEMBLYA8, COMPONENTLOCATIONS(SERIALPREFIX2309A)


P/OFIGURE8-33. MARKER ASSEMBLYA8,SCHEMATICDIAGRAM(1 OF 2)(SERIALPREFIX 2309A)


P/O FIGURE8-33. MARKER ASSEMBLYA8, SCHEMATIC DIAGRAM(20F2)(SERIALPREFIX 2309A)

Pages 8-97 through 8-115/8-116: SNEEP GENERATOR/BANDNIDTH CONTROL ASSENBLY A9
Table 8-6. Sweep Generator/Bandwidth Control Assembly A9, Replaceable Parts
2236A \& Below Change A9 to HP Part Number 08559-60074, Check Digit 0.
Change A9C24 to HP Part Number 0160-2055, Check Digit 9, CAPACITOR-FXD .01UF +80-20\% 100VDC CER.
Change A9C26 to $\mathbf{P}$ Part Number 0160-0153, Check Digit 4, CAPACTIOR-FXD 1000PF +-10\% 200VDC POLYE.
Change A9R70, A9R73, and A9R81 to HP Part Number 0698-7794, Check Digit 2, RESISTOR 10K . $25 \%$. 12 W .
Change A9R83 to HP Part Number 0698-8322, Check Digit 4, RESISTOR 111 OHM . 25\% . 12 W .
Change A9R 120* to H Part Number 0698-3153. Check Digit 9, RESISTOR 3.83K $1 \%$. 12 W .
Under Miscellaneous Parts, delete H Part Number 1200-0173.
2203A \& Below Change A9 to HP Part Number 08559-60071, Check Digit 7.
Delete AgCR29, A9Q56, A9R 106, A9R123, and A9R 124.
Change A9Q29 to HP Part Number 1855-0062, Check Digit 8, TRANSISTOR J-FET N-CHAN D-MODE SI.
Change A9R88 and A9R89 to HP Part Number 0757-0465, Check Digit 6, RESISTOR 100K $1 \%$. 125W F TC $=0+-100$.
Change A9R95 to HP Part Number 0757-0470, Check Digit 3, RESISTOR $162 \mathrm{~K} 1 \%$. 125 W F TC=0+-100.
Change A9R96 to HP Part Number 0757-0467, Check Digit 8, RESISTOR 121K $1 \%$. 125W F TC=0+-100.

2107A01633
Replace Table 8-6 with new Table 8-6 (SERIAL PREFIX
\& Below 2107A01633) included in this Manual Backdating supplement.

Figure 8-39. Sweep Generator/Bandwidth Control Assembly A9, Component Locations
2203A \& Below Replace Figure 8-39 with new Figure 8-39 (SERIAL PREFIX 2203A) included in this Manual Backdating supplement.

2107A01633 Replace Figure 8-39 with new Figure 8-39 (SERIAL PREFIX
\& Below 2107A01633) included in this Manual Backdating supplement.

Figure 8-40. Sweep Generator/Bandwidth Control Assembly A9, Schematic Diagram (1 of 2)

2236A \& Below Change A9 to HP Part Number 08559-60074.
2203A \& Below Change A9 to HP Part Number 08559-60071.
In function block ( 0 ), change R88 and R89 to 100K.
Replace function blocks (L). (M), and (N) with P/O Figure 8-40 (2 of 2) (SERIAL PREFIX 2203A) included in this Manual Backdating supplement.

2107A01633
\& Below
Replace Figure 8-40 (1 of 2) with new Figure 8-40 (1 of 2) (SERIAL PREFIX 2107A01633) included in this Manual Backdating supplement.
In function block (F), add a numeral 1 next to the ground symbol at the collector of Q5.

## Figure 8-40. Sweep Generator/Bandwidth Control Assembly A9, Schematic Diagran (2 of

 2)| 2236A \& Below | Change A9 to HP Part Number 08559-60074. <br> Change the following in function block (A): <br> C26 to .001UF. |
| :--- | :--- |
| R120* to 3830. |  |
| Change the following in function block (O): |  |
| R83 to 111. |  |
| Add a "1" next to the ground symbol at the source of Q23, 425, |  |
| Q29, and at the emitter of 448. |  |

TABLE86. SWEEPGENERATOR/BANDWIDTHCONTROLASSEMBLY A9, REPLACEABLE PARTS(10F4) (SERIALPREFIX 2107A01633)


TABLE 86. SWEEP GENERATORJBANDWIDTH CONTROLASSEMBLY A9, REPLACEABLE PARTS (2 OF 4) (SERIALPREFIX 2107A01633)

| Reference Designation | HP Part Number | ${ }_{0}^{\text {c }}$ | Oty | Description | $\begin{array}{\|l\|} \hline \text { Mfr } \\ \text { Code } \end{array}$ | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | ( |  |  |  |  |

See introduction to this section for ordering information
Indicates factory selected value

TABLE 8.-6. SWEEP GENERATOR/BANDWIDTH CONTROLASSEMBLY A9, REPLACEABLE PARTS (3 OF 4) (SERIAL PREFIX 2107A01633)

| Reference Designation | HP Part Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A9R36 | 0698-4037 | 0 |  | RESISTOR 46, 4 1x, 125W F TCa0 + 100 | 24546 | C4-1/8-T0-46R4-F |
| A9R37 | 0683-6845 | 1 | 1 | RESISTOR 680k $5 x$, 25W FC TC $=800 /+900$ | 01121 | CB6845 |
| A9R38 | 0698-3457 | 6 |  | RESISTOR $316 \mathrm{~K} 1 \mathrm{x}, 125 \mathrm{~W}$ F TC $=0+-100$ | 28480 | 0698-3457 |
| A9R39 | 0757-0439 | 4 | 3 | RESISTOR $6.81 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-6811-F |
| A9R40 | 0698-3451 | 0 | 2 | RESISTOR $133 \mathrm{~K} 1 \mathrm{x}, 125 \mathrm{~F}$ F $\mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-1333-F |
| A9R41 | 0757-0459 | 8 |  | RESISTOR 56.2 K 1 X , 1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-5622-F |
| A9R42 | 0698-7421 | 2 | 3 | RESISTOR 40K , 25\% , 1254 F TC $=0+-100$ | 19701 | MFAC:1/8-T0-4002-C |
| A9R43 | 0698-3194 | B | 3 | RESISTOR 20K , 25\% , 125W F TC $=0+-50$ | 33888 | PME5S-1/8-T2-2002-C |
| A9R44 | 0698-7794 | 2 |  | RESISTOR $10 \mathrm{~K}, .25 \mathrm{X}, 125 \mathrm{~W}$ F $\mathrm{TC}=0+-100$ | 19701 | MFAC1/8-T0-1602-C |
| A9R4S | 0757-0289 | 2 | 2 | RESISTIOR 13.3K $1 \mathrm{~K}, 125 \mathrm{~W}$ F TC=0+-100 | 19731 | MFAC1/B-T0-1332-F |
| A9R46 A9R47 | 0757-0199 $0757-0346$ | 3 2 | 19 2 | RESISTOR 21.5K $1 \%$. 125 M F TC=0+-100 RESISTOR $101 z, 1254 \quad F \quad T C=0+-100$ | 24546 24546 |  |
| A9R47 A9R48 | 0757-0346 $0757-0465$ | 2 | 2 |  | 24546 24546 | $\begin{aligned} & \text { C4-1/8-T0-10R0-F } \\ & \text { C4-1/8-T0-1003-F } \end{aligned}$ |
| A9R49 | 0757-0464 | 5 | 1 | RESISTOR 90.9K $1 \times$, 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-9092-F |
| A9R50 | 0757-0442 | 9 |  | RESISTOR 10 K 12.125 WF TC $=0+-100$ | 24546 | C4-1/8-70-1002-F |
| A9R51 | 0757-0279 | 0 |  | RESISTOR 3.16K 1x . 1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-3161-F |
| A9R52 | 0757-0439 | 4 |  | RESISTOR 6.81K $1 \%$, 1254 F TC=0+-100 | 24546 | C4-1/8-T0-6811-F |
| APR53 | 0757-0460 | 1 | ? | RESISTIR $61,9 \mathrm{~K} 1 \mathrm{1z}$, 125M F TC $=0+100$ | 24546 | C4-1/8-70-6192-F |
| A9R54 | 0757-0442 | 9 |  | RESISTOR $10 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| A9R55 | 0757-0442 | 9 |  | RESTSTOR 10 K 1 X . 1254 F TC=0+-100 | 24546 | C4-1/8-T0-1032-F |
| A9R56 | 0757-0465 | 6 |  | RESISTOR 100K 1 X , 125 W F TC=0+-100 | 24546 | C4-1/8-T0-1003-F |
| A9R57 | 0757-0439 | 4 |  | RESISTOR 6. $61 \mathrm{~K} \quad 1 \mathrm{X}, 125 \mathrm{~W}$ F $\mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-6811-F |
| A9R58 | 0757-0465 | 6 |  | RESISTOR 100 K 1 z , 125 W F $\mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-1603-F |
| ASR59 | 0757-0279 | 0 |  | RESISTOR $3.16 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-3161-F |
| A9R60 | 6698-3160 | 8 |  | RESISTOR 31.6K 1\% , 1254 F TC=0+-100 | 24546 | C4-1/8-T0-3162-F |
| A9R61 | 0757-0465 | 6 |  | RESISTOR 100 K 1 x , 125W F TC=0+-100 | 24546 | C4-1/8-T0-1003-F |
| A9R62 | 0757-0465 | 6 |  | RESISTOR 100 K 12.125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A9R63 | 0757-0346 | 2 |  | RESISTOR $101 \mathrm{~K}, 125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-10R3-F |
| A9R64 | 0757-0199 | 3 |  |  | 24546 | C4-1/8-T0-2152-F |
| A9R65 | 0757-0199 | 3 |  | RESISTOR 21.5K 12, 125W F TC=0+-100 | 24546 | C4-1/8-T0-2152-F |
| A9R66 | 0757-0199 | 3 |  | RESISTOR 21.5 K 1X , 125以 F TC $=0+100$ | 24546 | C4-1/8-T0-2152-F |
| A9R67 | 0757-0199 | 3 |  | RESISTOR 21.5K 1z , 125W F TC $=0+0+100$ | 24546 | C4-1/8-T0-2152-F |
| A9R68 | 0698-7412 | 1 |  | RESISTOR $13.3 \mathrm{~K}, 25 \mathrm{z}$, 125M F TC $=0+-100$ | 19701 | MF4C1/8-T0-1332-C |
| A9R69 | 0757-1094 |  | 1 | RESISTOR $1,47 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1471-F |
| A9R70 | 0757-0199 | 3 |  | RESISTOR 21.5K 1 x , 1254 F TC=0 0 - 100 | 24546 | C4-1/B-T0-2152-F |
|  |  |  |  | RESISTOR 21.5K 1Z . 125W F TC=0+-100 | $24546$ | $\mathrm{C} 4-1 / 8-\mathrm{TO} 0-2152-F$ |
| A9R72 | $2100-2850$ | 8 | 2 | RESISTOR-TRMR 10 K 10X UW SIDE-ADJ 20-TRN | $02660$ | $3010 p-103$ |
| A9R73 | 0757-0199 | 3 |  | RESISTOR 21.5 K 1X 12 , 254 F $\mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-2152-F |
| A9R74 A9R75 | $\begin{aligned} & 0698-3151 \\ & 0757-0199 \end{aligned}$ | 7 3 | 1 |  | 24546 24546 | $\begin{aligned} & \mathrm{C} 4-1 / 8-\mathrm{TO}-2871-F \\ & \mathrm{C} 4-1 / 8-\mathrm{TO} 0-2152-F \end{aligned}$ |
| A9R76 A9R77 | $\begin{aligned} & 0757-0442 \\ & 0757-0199 \end{aligned}$ |  |  | RESISTOR 10K 1 X . 125 F F TC $=0+-100$ RESISTOR 21.5K 1X . 125K F TC=0+-100 |  | $\begin{aligned} & \mathrm{C}_{4}-1 / 8-\mathrm{TO}-1002-F \\ & \mathrm{C}_{4}-1 / 8-\mathrm{T} 0-2152-F \end{aligned}$ |
| A9R77 A9R78 | $\begin{aligned} & 0757-0199 \\ & 0757-0458 \end{aligned}$ | 3 7 |  |  | $\begin{aligned} & 24546 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \mathrm{C}_{4}-1 / 8-\mathrm{T} 0-2152-F \\ & \mathrm{C}_{4}-1 / 8-\mathrm{T0}-5112-F \end{aligned}$ |
| A9879 | 0757-0199 | 3 |  | RESISTOR 21.5K 1x , 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-2152-F |
| A9R80 | 0757-0199 | 3 |  | RESISTOR 21.5K 1\% , 125W F TC=0+-100 | 24546 | C4-1/8-T0-2152-F |
| $\begin{aligned} & \text { A9RE1 } \\ & \text { A9RER2 } \end{aligned}$ | $\begin{aligned} & 0757-0199 \\ & 0698-0085 \end{aligned}$ | 3 0 | 1 |  | $\begin{aligned} & 24546 \\ & 24546 \end{aligned}$ | C4-1/8-T0-2152-F <br> $\mathrm{CA}-1 / 8-\mathrm{TO}$ |
| A9RE3 | $0698-0895$ $0698-3260$ | 9 | 1 |  | 24546 28480 | C4-1/8-T0-2611-F $0698-3260$ |
| A9R84 | 0757-0444 | 1 |  | RESISTOR 12, 1 K 1\% 12.125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1212-F |
| A9RES | 2100-2850 | 8 |  | RESISTOR-TRMR 10 K 10X WW SIDE-ADJ 20-TRN | 02660 | 3810P-103 |
| $\begin{aligned} & \text { A9R86 } \\ & \text { A9RE7 } \end{aligned}$ | $\begin{aligned} & 0698-7794 \\ & 0757-0199 \end{aligned}$ | 2 |  | RESISTOR 10 K . 25 X , 125W F TC=0 $0-100$ RESISTOR 21.5K $1 X$, 125 H F TC $=0+-100$ | $\begin{aligned} & 19701 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \text { MF 4C1/8-T0-1002-C } \\ & \mathrm{C} 4-1 / 8-\mathrm{TO} 0-2152-\mathrm{F} \end{aligned}$ |
| A9R88 | 0757-0199 | 3 |  | RESISTOR 21.5 K 1z , 125w F TC $=0+-100$ | 24546 | C4-1/8-T0-2152-F |
| A9R89 | 0757-0460 | 1 |  | RESISTOR 61.9K 1x , 125M F TC=0+-100 | 24546 | C4-1/8-T0-6192-F |
| A9R90 | 0698-7421 | 2 |  | RESISTOR 40K , 25\% , 125W F TC $=0+-100$ | 19701 | HF4C1/8-T0-4002-C |
| $\begin{aligned} & \text { A9R91 } \\ & \text { A9R92 } \end{aligned}$ | $\begin{aligned} & 0757-0199 \\ & 0757-0289 \end{aligned}$ | 3 |  | RESISTOR 21.5K 12 , 125W F TC=0+-100 RESISTOR 13.3K 12 . 125W F TC=0+-100 | $\begin{aligned} & 24546 \\ & 19781 \end{aligned}$ | $\begin{aligned} & \text { C4-1/8-T0-2152-F } \\ & \text { MF4C1/8-T0-1332-F } \end{aligned}$ |
| A9R92 <br> A9R93 | 0757-0269 $0698-3194$ | 2 8 8 |  | RESISTOR RESTSTOR 13, RKK R | 19761 03888 | MFAC1/8-T0-1332-F PHES5-1/8-T2-2002-C |
| A9R94 | 0757-0199 | 3 |  | RESISTOR 21,5K 1x , 125W F TC $=0+100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T} 0-2152-\mathrm{F}$ |
| A9R95 | 0698-3153 | 9 | 1 | RESISTOR 3.83K 1 X , 125M F TC $=0+-100$ | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T0} 0-3831-\mathrm{F}$ |
| A9R96 A9R97 | $\begin{aligned} & 0698-7412 \\ & 0757-0199 \end{aligned}$ | $\frac{1}{3}$ |  | RESISTOR 13.3K ,25x , 125W F TC=0+-100 RESISTOR 21.5K $1 x$. 125 W F TC=0+-100 | $\begin{aligned} & 19701 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \text { MF AC1/8-T0-1332-C } \\ & \text { C4-1/8-T0-2152-F } \end{aligned}$ |
| A9R98 | 0757-0442 | 9 |  | RESISTOR 10 K 1x, 125 W F TC=0 +-100 | 24546 | C4-1/8-T0-1002-F |
| A9R99 A9R110 | 0757-0199 | 3 |  | RESISTOR $21.5 \mathrm{~K} \quad 1 \mathrm{x}, 125 \mathrm{~F}$ F TC=0+-100 NOT ASSICNED | 24546 | C4-1/8-T0-2152-F |
| A9R101 A9R102 A9R103 A9R184 A9R105 | 0698-7794 | 2 |  | RESISTOR 10 K , $25 \%$, 125 W F TC=0+-100 NOT ABSIGNED <br> NOT ABSIGNED <br> NOT ASSICNED <br> NOT ASSIGNED | 19701 | HFAC1/8-T0-1002-C |
| A9R 116 <br> A9R107 <br> A9R108 <br> A9R109 <br> A9R110 | $\begin{aligned} & 0757-0442 \\ & 0757-0442 \\ & 0757-0442 \\ & 0698-3451 \end{aligned}$ | 9 |  | not assicned <br> RESISTOR 10 K 12 , 125W F TC=0+-100 <br> RESISTOR 10K 12,1254 F TC=0+-100 <br> RESISTOR $10 \mathrm{~K} \quad 1 \mathrm{x}, 125 \mathrm{~F}$ F $\mathrm{TC}=0+-100$ <br> RESISTOR 133K 1 X . 125 W F TC=0+-10 | $\begin{aligned} & 24546 \\ & 24546 \\ & 24546 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \text { C4-1/8-T0-1002-F } \\ & \text { C4-1/8-T0-1002-F } \\ & \text { C4-1/8-T0-1002-F } \\ & \text { C4-1/8-T0-1333-F } \end{aligned}$ |

See introduction to this section for ordering information *Indicates factory selected value

TABLE8-6. SWEEP GENERATOR/BANDWIDTH CONTROLASSEMBLYA9, REPLACEABLEPARTS (4OF4)(SERIALPREFIX 2107A01633)


See introduction to this section for ordering information
*Indicates factory selected value

SWEEP GENERATOR/BANDWIDTH CONTROL




PIO FIGURE8-40. A9 SWEEP GENERATOR/BANDWIDTH CONTROL,SCHEMATICDIAGRAM(2OF2)(SERIALPREFIX 2203A)



## Pages 8-117 through 8-127/8-128: THIRD CONVERTER ASSEMBLY A10

Table 8-7. Third Converter Assembly A10, Replaceable Parts

| 2218A \& Below | Delete the following: <br> A10C57, A10C58, A10C59, A10R52, A10R53, and A10U2. <br> Chacge A10R6 to HP Part Number 0757-0280, Check Digit 3, RESISTOR $1 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC=0+-100. <br> Change A10R8 to HP Part Number 0757-0420, Check Digit 3, RESISTOR $7501 \%$. 125W F TC $=0+100$. <br> Change A10R11 to HP Part Number 0757-0405, Check Digit 4, RESISTOR 162 1\% . 125W F TC $=0+-100$. |
| :---: | :---: |
| $\begin{aligned} & 2019 \text { A00721 } \\ & \& \text { Below } \end{aligned}$ | Change A10MP5 to HP Part Number 0363-0040, Check Digit 8, CONTACT-FINGER .58-WD .219-FREE-HGT. <br> Add A10MP6 and A10MP7, H Part Number 0363-0040. Check Digit 8, CONTACT-FINGER .58-WD .219-FREE-HGT. |
| $\begin{aligned} & 1945 A 00261,263, \\ & 269,271,280 \\ & \& \text { Below } \end{aligned}$ | Delete A10MP5,A10MP6, and A10MP7. |
| 1942A \& Below | NOTE <br> The following components have preferred replacements: A10C22, A10C50, A10C54, A10C55, A10CR1, A10CR4, and A10L15. If the instrument does not contain the preferred replacement values, as shown in the Replaceable Parts list and Schematic in the Manual, then these components should all be replaced at the same time. |

Figure 8-13. Third Converter Assembly A10, Component Locations
2218A \& Below
Replace Figure 8-43 with new Figure 8-43 (SERIAL PREFIX 2218A) included in this Manual Backdating supplement.

Figure 8-44. Third Converter Assembly A10, Schematic Diagram

| 2218A \& Below | Replace funcbion block ( $J$ ) of Figure 8-44 with new P/O Figure 844 (SERIAL PREFIX 2218A) included in this Manual Backdating supplement. <br> Make the following changes in function block (D). <br> Change R6 to 1000. <br> Change R8 to 750. <br> Change R11 to 162. <br> Change -10.6 VF to -12.6 VF in two places. |
| :---: | :---: |



FIGURE843. THIRDCONVERTERASSEMBLY A10, COMPONENTLOCATONS(SERIALPRERX 218A)


FIGURE8-44. THIRDCONVERTER ASSEMBLY A10, SCHEMATICDIAGRAM(SERIALPREFIX2218A)

## Pages 8-129 through 8-141/8-142: BANDNIDTH FILTER MO. 1 ASSEMBLY A11

Table 8-8: Bandwidth Filter No. 1 Assembly All, Replaceable Parts
1909A \& Below Change A11 to H Part Number 08559-60057, Check Digit 9, BANDWIDTH FILTER NO. 1.
Add A11C3, HP Part Number 0160-2236, Check Digit 8, CAPACTIOR-FXD 1PF +-.25PF 500VDC CER
Change A11C16*, A11C20*, A11C43*, and A11C64* to HP Part Number 0160-0134, Check Digit 1, CAPACITOR-FXD 220PF +-5\% 300VDC MICA.
Change A11C14 and A11C37 to HP Part Number 0160-2250, Check Digit 6, CAPACITOR-FXD 5.1PF +-.25PF 500VDC CER.
Change A11C21 and A11C44 to HP Part Number 0160-3431, Check Digit 7, CAPACTIOR-FXD 6.8PF +-. 5PF 500VDC CER
Change A11R23* and A11R48* to HP Part Number 0757-0441, Check Digit 8, RESISTOR 8.25K $1 \%$. 125W F TC=0+-100.
Delete A11R24 and A11R25.
Change A11R18 and A11R41 to HP Part Number 0757-0279, Check Digit 0 , RESISTOR 3.16K $1 \% .125 \mathrm{~W}$ F TC=0+-100.
Change A11R28 and A11R52 to HP Part Number 0757-0290, Check Digit 5, RESISTOR 6.19K $1 \%$.125W F TC=0+-100.

Figure 8-55. Bandwidth Filter No. 1 Assembly All, Component Locations

| 1909A \& Below | Delete R25. |
| :--- | :--- |
|  | Change R24 t o W1. |
|  | Add C3 below R5. |

Figure 836 . Bandwidth Filter No. 1 Assembly All, Schematic Diagram

1909A \& Below | Change All to HP Part Number 08559-60057. |
| :--- |
| In function block (B), add a capacitor, C3, 1.0 PF, in parallel |
| with R5. |
| Replace function block (C) with P/O Figure 8-56 (SERIAL PREFIX |
| 1909A) included in this Manual Backdating supplement. |
| Make the following changes in function block (D): |
| Change C14 to 5.1 PF. |
| Change R23* to 14.7 K . |
| Change R18 to 3160 . |
| Make the following changes in function block (F): |
| Change C43* to 220 PF. |
| Change C44 to 6.8 PF . |
| Change C64* to 220 PF. |
| Change R52 to 6190 . |
| Make the following changes in function block (G): |
| Change C37 to 5.1 PF. |
| Change R48 to 14.7 K . |
| Change R41 to 3160 . |



PIO FIGURE8-56. BANDWIDTHFLTER NO. 1 ASSEMBLY AII, SCHEMATICDIAGRAM(SERIAL PREFIX 1909A)

## Pages 8-143 through 8-155/8-156: SIEP GAIM ASSEMBLY A12

Table 8-10. Step Gain Assembly A12, Replaceable Parts
2107A \& Below Delete A12C40, A12C41, and A12C42.
Figure 8-60. Step Gain Assembly A12, Schematic Diagram
2107A \& Below In function block (E), delete C40.
In function block (F), delete C41.
In function block (G), delete C42.

Table 8-11: Bandwidth Filter No. 2 Assembly A13. Replaceable Parts


Figure 8-62. Bandwidth Filter No. 2 Assembly A13. Component Locations

| 1909 A \& Below $\quad$ | Delete R25. |
| :--- | :--- |
|  | Change R24 t o W1. |
|  | Add C3 below R5. |

Figure 8-63: Bandwidth Filter No. 2 Assembly A13, Schematic Diagram

```
1909A & Below Change A13 to HP Part Number 08559-60057.
    In function block (B), add a capacitor, C3, 1.0 PF, in parallel
        with R5.
    Replace function block (C) with P/O Figure 8-63 (SERIAL PREFIX
        1909A) included in this Manual Backdating supplement.
Make the following changes in function block (D):
    Change C14 to 5.1 PF.
    Change R23* to 14.7K.
    Change R18 to 3160.
Make the following changes in function block (F):
    Change C43* to 220 PF
    Change C44 to 6.8 PF.
    Change C64* to 220 PF
    Change R52 to 6190.
Make the following changes in function block (G):
    Change C37 to 5.1 PF.
    Change R48* to 14.7K.
    Change R41 to 3160.
```



PIO FIGURE 863. BANDWIDTHFLTER NO. 2 ASSEMBLY A13, SCHEMATICDIAGRAM(SERIALPREFIX 1909A)

Pages 8-167 through 8-179/8-180: LOG AMPLIFIER ASSEMBLY A14
Table 8-12. Log Amplifier Assembly A14, Replaceable Parts
2208A \& Below Replace Table 8-12 with new Table 8-12 (SERIAL PREFIX 2208A) included in this Manual Backdating supplement.

Figure 8-68. Log Amplifier Assembly A14, Component Locations
2208A \& Below Replace Figure 8-68 with new Figure 8-68 (SERIAL PREFIX 2208A) included in this Manual Backdating supplement.

Figure 8-69. Log Amplifier Assembly A14, Schematic Diagram, (1 of 2)
2208A \& Below Replace Figure 8-69 (1 of 2) with new Figure 8-69 (1 of 2) (SERIAL PREFIX 2208A) included in this Manual Backdating supplement.

Figure 8-69. Log Amplifier Assembly A14, Schematic Diagram (2 of 2)
2208A \& Below
Replace Figure 8-69 (2 of 2) with new Figure 8-69 (2 of 2) (SERIAL PREFIX 2208A) included in this Manual Backdating supplement.
Make the following corrections to Figure 8-69 (2 of 2) (SERIAL PREFIX 2208A):

Connect one side of R131 to the collector of Q25.
Connect the other side of R131 to the negative side of C79. Connect the positive side of C79 to ground.

TABLE 812. LOG AMPLIFIER ASSEMBLY A14, REPLACEABLEPARTS(1 OF 4) (SERIAL PREFIX 2208A)


See introductionto this section for ordering information 'Indicates factory selected value

TABLE 8-12. LOG AMPLIFIER ASSEMBLY A14, REPLACEABLE PARTS (2OF 4) (SERIAL PREFIX 2208A)


See introduction to this section for ordering information
${ }^{\text {-I }}$ Indicates factory selected value

TABLE812. LOG AMPLIFIERASSEMBLY A14, REPLACEABLEPARTS(3OF4)(SERIALPREFIX 2208A)

| Reference Designation | HP Part Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A14921 | 1854-0404 | 0 | 1 | TRANSISTOR NPN SI TO-18 PD=360MW | 28480 | 1854-0404 |
| A14922 | 1853-0020 | 4 |  | TRANSISTOR PNP SI PD=300MW FT=150MHZ | 28480 | 1853-0020 |
| A14923 | 1854-0071 | 7 |  | TRANSISTOR NPN SI PD 300 mH FT $=200 \mathrm{MHZ}$ | 28480 | 1854-0071 |
| A14824 | 1854-0071 | 7 |  | TRANSISTOR NPN SI PD $=300 \mathrm{MH}$ FT $=200 \mathrm{MHZ}$ | 28480 | $\begin{aligned} & \text { 1854-0071 } \\ & 2 N 219 A \end{aligned}$ |
| A14825 | 1854-0637 | 1 | 1 | TRANSISTOR NPN 2N2219A SI TO-5 PD=80DMW | 01295 | 2N2219A |
| A14R1 | 2100-3109 | 2 | 2 | RESISTOR-TRHR 2K 10x C SIDF-ADJ 17-TRN | 02111 | $43 P 202$ |
| A14R2 | 2100-3161 | 6 | 1 | RESISTOR-TRHR 20K $10 \%$ C SIDE-ADJ 17-TRN | 02111 | $43 P 203$ |
| A14R3 | 2100-31109 | 2 |  | RESISTOR-TRHR $2 \mathrm{~K} 10 \times \mathrm{C}$ C SIDE-ADJ 17-TRN | 02111 | 43P202 |
| A14R4 A1 AR5 | -0757-0442 | 9 0 | 6 | RESISTOR $10 \mathrm{~K} 1 \%$, 125W F TC=0+-100 RESISTOR 3.16K $1 \boldsymbol{\chi}$. 125 W F $\mathrm{TC}=0+-10$ | 24546 24546 | C4-1/8-T0-1002-F C4-1/8-T0-3161-F |
| A14R6* | 0757-0346 | 2 | 19 | RESISTOR $101 \pm, 125 \mathrm{w}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-10R 0-F |
| A1 4R7 | 0757-0442 | 9 |  | RESISTOR 10K 1 X . 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| A1 4R8* | 0757-0280 | 3 | 6 | RESISTOR 1 K 1 x , 125 H F TC=0 +-100 | 24546 | C4-1/8-T0-1901-F |
| A1 4R9 | 0757-0439 | 4 | 9 | RESISTOR 6, 81 K 1\% $125 \mathrm{HF} \mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-6811-F |
| A14R10 | 0757-0465 | 6 | 2 | RESTSTOR $100 \mathrm{~K} 1 \% .125 W F T C=0+\cdots 100$ | 24546 | C4-1/8-70-103-F |
| A1 4R11 | 0757-0440 | 7 | 2 | RESISTOR 7.5K $1 \%$, 125W F TC= $=0+-100$ | 24546 | C4-1/8-T0-7501-F |
| A14R12 | 0698-3157 | 3 | 2 |  | 24546 24546 | C4-1/8-T0-1962-F |
| A14R13 A14R14 | $0698-3444$ $0757-0420$ | $\frac{1}{3}$ | 8 1 |  | 24546 24546 | C4-1/8-TG-316R-F $\mathrm{C} 4-1 / 8-\mathrm{TO}-751 \mathrm{~F}$ |
| A14R15 | 0698-3136 | B | 1 | RESISTOR 17.8* 1 \% , 125 F TC=0+-100 | 24546 | C4-1/8-T0-1782-F |
| A14R16" | 0698-3443 | 0 | 1 |  | 24546 | C4 1/8-T0-287R-F |
| A1 4R17 <br> A14R18 | 0698-3156 | 2 | 1 | RESISTOR 14.7K 1\% . 125W F TC=0+-100 NOT ASSIGNED | 24546 | C4-1/8-T0-1472-F |
| A14R19 | 0698-0085 | 0 | 2 | RESISTOR 2.61 K 1 X , 1254 F TC=0+-100 | 24546 | C4-1/8-T0-2611-F |
| A14R20 | 0757-0279 | 0 |  | RESISTOR 3.16K $1 \%$. 125 W F TC=0+-100 | 24546 | C4-1/8-T0-3161-F |
| A14R21 A14R22 | $\begin{aligned} & 0757-0289 \\ & 0757-0346 \end{aligned}$ | $\left\|\begin{array}{l} 2 \\ 2 \end{array}\right\|$ | 12 | RESISTOR 13.3 K 1\% . 125W F TC=0 $\mathrm{i}-100$ <br> RESISTOR 10 1\%, 1254 F TC=0t-100 | $\begin{aligned} & 19701 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \text { MF 4C1/8-T0-1332-F } \\ & \text { C4-1/8-T0-10R0-F } \end{aligned}$ |
| A14R23 | 0698-3444 | 1 |  | RESISTOR 3161 X , . 2 2SW F TC=0+-100 | 24546 | C4-1/8-T0-316R-F |
| A1 AR24 | 0757-0279 | 0 |  | RESISTOR 3.16K $1 \%$, 125 F F TC=0 +-100 | 24546 | C4-1/8-T0-3161-F |
| A1 4R25 | 0698-3444 | 1 |  | RESISTOR 3161 x . 125 W F TC=0*-100 | 24546 | C4-1/8-T0-316R-F |
| A14R26 | 0757-0290 | 5 |  | RESISTOR 6, 19K 1\% , 1254 F TC=0 $0+-100$ | 19701 | MF AC1/8-T0-6191-F |
| A1 4R27 | 0757-0346 | 2 |  | RESISTOR 10 1\% 125 F F TCm $0+-100$ | 24546 | C4-1/8-T6-10R0-F |
| A1 4R28 A1 4R29 | 0698-3449 | 6 3 | 1 | RESISTOR 29.7 K RESISTOR 21.5K R | 24546 24546 | C4-1/8-T0-2872-F $\mathrm{C} 4-1 / 8-\mathrm{TO}$ - $2152-F$ |
| A14R30 | 0698-3152 | a | 2 | RESISTOR 3.48K 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-3481-F |
| A14R31 | 0757-0279 | 0 |  | RESISTOR 3.16K 1\% , 125 F ${ }^{\text {F }}$ TC=0+-100 | 24546 | C4-1/8-T0-3161-F |
| A14R32 | 0757-0289 | 2 |  | RESISTOR 13.3K 1\% . 125 F F TC=0 +-100 | 19701 | WFAC1/8-T0-1332-F |
| A14R33 | 6757-0289 | 2 |  | RESISTOR 13.3 K 1\% , 125H F TC=0+-100 | 19701 | MF4C1/8-T0-1332-F |
| A1 4R34 | 0698-3444 | 1 |  | RESISTOR $3161 \% .125 W$ F TC=0+-100 | 24546 | C4 1/8-T0-316R-F |
| A14235m | 0757-0346 | 2 |  | RESISTOR 10 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-10R0-F |
|  |  |  | 2 |  | $24546$ | C4-1/B-T0-147R-F |
| A1 4837 | 0757-0439 | 4 |  | RESISTOR 6.81K $1 \%$, 125 F F TC=0 +-100 | $24546$ | C4-1/8-T0-6811-F |
| A1 4R38 A1 4R39 | 8757-0279 $0698-3154$ | 0 | 1 | RESISTOR 3.16K RESISTOR 4.22 L R | 24546 24546 | C4-1/8-T0-3161-F $\mathrm{C4}-1 / 8-\mathrm{TO}-4221-\mathrm{F}$ |
| A14R40 | 0757-0280 | 3 |  | RESISTOR 1K 1\% . 125 H F TC=0 +-100 | 24546 | C4-1/8-70-1601-F |
| A14R41 | 0737-0346 | 2 |  | RESISTOR 1012.1254 F TC=0t-100 | 24546 | CA-1/8-T0-10R0-F |
| A14R42 | 0757-0346 $0757-0289$ | 2 |  |  | 24546 19701 | $\text { C } 4-1 / 8-70-10 R 0-F$ |
| A1 4R43 A14R44 | 0757-0289 | 2 |  | RESISTOR 13.3 K 1\% . 125 F F TC=0+-100 NOT ASSIGNED | 19701 | WFAC1/8-T0-1332-F |
| A1 4R45 | 0757-0439 | 4 |  |  | 24546 | C4-1/8-T0-6811-F |
| A14R46" | 0698-0083 | 8 | 2 | RESISTOR 1.96K 1\%.1254 F TC=0+-100 | 24546 | C4-1/8-T0-1961-F |
| A1 4R47 | 0757-0279 | 0 |  | RESISTOR 3,16K 1\% , 1254 F TC=0+-100 | 24546 | C4-1/8-T8-3161-F |
| A14R48 | 0757-0289 | 2 |  | RESISTOR 13.3k $1 \%$, 125W F TC=0+-100 | 19701 | MFAC1/8-T0-1332-F |
| A1 4R49 A1 4R50 | $0757-0416$ $0698-3444$ | 7 | 2 |  | 24546 24546 | $\begin{aligned} & \mathrm{CA}-1 / 8-\mathrm{TO}-511 \mathrm{R}-\mathrm{F} \\ & \mathrm{C} 4-1 / 8-\mathrm{TO}-316 \mathrm{R}-F \end{aligned}$ |
| A1AR51* | 0737-0346 |  |  | RESISTOR 10 12.1254 F TC=0t-100 |  | C4-1/8-T0-10R0-F |
| A14R52 | 0757-0465 | 6 |  | RESISTOR 100 K , $\%$, 125M F TC=0 0 - 100 | 24546 | C4-1/8-70-1003-F |
| A14R53 | 0698-0083 | B |  | RESISTOR 1,96K $1 \%$, 125M F TC=0+-100 | 24546 | C4-1/8-70-1961-F |
| A1 4R54 A1 4R55 | 3757-0288 $0698-3151$ | 3 |  |  | $\begin{aligned} & 24546 \\ & 24546 \end{aligned}$ | $\begin{aligned} & \mathrm{C} 4-1 / 8-\mathrm{TO}-1001-F \\ & \mathrm{C} 4-1 / 8-\mathrm{TO}-2071-F \end{aligned}$ |
| A14R56 A1 $4 \pi 57$ <br> A14R58 <br> A14 489 <br> A14R60 | $\begin{aligned} & 0757-0458 \\ & 0757-0346 \\ & 0757-0299 \\ & 0757-0442 \\ & 0698-3157 \end{aligned}$ | 7 2 2 3 3 | 1 |  | $\begin{aligned} & 24546 \\ & 24546 \\ & 19701 \\ & 24546 \\ & 24546 \end{aligned}$ | $\begin{aligned} & C 4-1 / 8-T 0-5112-F \\ & \text { C4-1/8-TT-1 } 18 R-F \\ & \text { WF4C1/8-T0-1 } 232-F \\ & \text { C4-1/8-T0-1 } 812-F \\ & C 4-1 / 8-T 0-1962-F \end{aligned}$ |
| A14R31 <br> A14in62 <br> A14R63 <br> A14R64* <br> A1 4265 | $\begin{aligned} & 0757-0442 \\ & 0698-3152 \\ & 0690-3159 \\ & 0757-6279 \\ & 0757-0290 \end{aligned}$ | ? 8 5 0 5 | $1{ }^{1}$ | RESIBTOR $10 \mathrm{~K} 12,1254 \mathrm{~F}$ TC=0+-100 <br> RESISTOR 3.48K $1 \%$, 1234 F TC=0 +-100 <br> RESISTOR 26.1K 1\% .1254 F TC= + + -100 <br> RESIETOR 3.16K $1 \%$, 125H F TC=0+-100 <br> RESISTOR b.19K 1\% . 125W F TC=0 +-100 | $\begin{aligned} & 24546 \\ & 24546 \\ & 24546 \\ & 24546 \\ & 19701 \end{aligned}$ | $\begin{aligned} & C 4-1 / 8-T 0-1002-F \\ & C 4-1 / 8-T 0-3411-F \\ & C 4-1 / 8-T 8-2612-F \\ & C 4-1 / 8-T 0-3161-F \\ & W F 4 C 1 / 8-T 0-6191-F \end{aligned}$ |
| A14R66 A1 4867 A14R68 A1 4269 A14R70 | $\begin{aligned} & 0757-1439 \\ & 0757-6379 \\ & 0757-8289 \\ & 0777-8449 \\ & 0757-6463 \end{aligned}$ | 4 1 2 7 4 | 1 1 | RESIETOR 6.01K 1\% , 125H F TC=0 + - 101 <br> RESISTOR $12.1 \quad 1 \%$. 125 F F TCm0t-1 10 <br> RESISTOR 13.3K $1 \%$, 1254 F TC=0+m101 <br> RES18TOR 7.5K $1 \%$. 1254 F TC=0+-10! <br> REEIGTOR 02.5K 1\% . 125W F TC=0t-101 | $\begin{aligned} & 24546 \\ & 19781 \\ & 19791 \\ & 24546 \\ & 24544 \end{aligned}$ | $\begin{aligned} & C 4-1 / 8-T 0-6811-F \\ & \text { WF4C1/日-T0-1211-F} \\ & \text { W } 4 C 1 / 8-T 0-1332-F \\ & C 4-1 / 8-T 8-7311-F \\ & C 4-1 / 1 /-T 0-252-F \end{aligned}$ |

See introduction to this section for ordering information -Indicates factory selected value

TABLE812. LOG AMPLIFIERASSEMBLY A14, REPLACEABLEPARTS (4OF4)(SERIALPREFIX2208A)

| Reference Designation | HP Part Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A14R71 | 0678-3444 | 1 |  | RESISTOR 316 1\% . 12SW F TC=04-100 | 24546 | C4 1/8-70-3162-F |
| A1 4R72 | 0757-0290 | 5 |  | RESISTOR 6.191 $1 \%$. 125 W F TC=0+-100 | 19701 | MF 4C1/8-T0-6191-F |
| A14R73* | 0698-3151 | 7 | 2 | NOT ASSIGNED RESISTOR 2, 7 \% $1 \% .125 \mathrm{~W}$ F TC=00+-100 |  |  |
| A14R75 | -0698-3151 | 9 | 2 |  | 24546 24546 | $\begin{aligned} & \text { C4-1/8-T0-2871-F } \\ & C 4-1 / 8-T 0-1002-F \end{aligned}$ |
| A1 4R76 A14R77 | $\begin{aligned} & 0757-0289 \\ & 0757-0280 \end{aligned}$ | 2 |  | RESISTOR 13.3K 1\% . 125W F TC=0 0 +100 <br>  | $\begin{aligned} & 19701 \\ & 24546 \end{aligned}$ | MF4C1/8-T0-1332-F C4-1/8-T0-1001-F |
| A1 4R78 | 0757-0346 | 2 |  | RESISTOR 10 1\% . 125 W F TC=0t-100 | 24546 | C4-1/8-T0-1001-F |
| A14R79 | 0757-0346 | 2 |  | RESISTOR 10 1\% . 125 W F TC=0 +100 | 24546 | C4-1/8-T0-10R0-F |
| A14R80 | 0757-0439 | 4 |  | RESISTOR 6. B1K 1\% . 125 W F TC=0t-100 | 24546 | C4-1/8-T0-6811-F |
| A14R81 | 0757-0403 | 2 | 1 | RESISTOR 121 1\% . 125 W F TC=0+- 100 | 24546 | C4 1/8-T0-121R-F |
| A1 4R82" | 0757-0290 | 5 | 8 | RESISTOR 6.19K 1\% , 125W F TC=0+-100 | 19701 | MF4C1/8-T0-6191-F |
| A14R83 | 0757-0418 | 9 | 1 | RESISTOR 619 1\% , 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-619R-F |
| A14R84 A14RE5 | $\begin{aligned} & 0757-0402 \\ & 0757-0279 \end{aligned}$ | 1 | 1 |  | 24546 24546 | C4-1/8-T0-111-F $\mathrm{C} 4-1 / \mathrm{B}-\mathrm{T} 0-3161-\mathrm{F}$ |
|  |  |  |  |  |  |  |
| A14R86 |  |  |  | NOT ASSIGNED |  |  |
| A1 4R87 | 0757-0289 | 2 |  | RESISTOR 13.3K $1 \%$, 125W F TC=0+-100 | 19701 | MFAC1/8-T0-1332-F |
| A1 4R88 | 0757-0416 | 7 |  |  | 24546 | C4-1/8-T0-511R-F |
| A14R89 A1 4R90 | $0757-0346$ $0698-3444$ | 2 |  |  | 24546 24546 | C4 $1 / 8-\mathrm{T} 0-10 \mathrm{C} 0-\mathrm{F}$ $\mathrm{CA}-1 / 8-\mathrm{T} 0-316 \mathrm{~F}-\mathrm{F}$ |
| A14R91 | 0757-0439 | 4 |  | RESISTOR 6.811 1\% . 125 w F TC=0+-100 |  |  |
| A14R92 | 0757-0346 | 2 |  | RESISTOR $101 \mathrm{X}, 125 \mathrm{~W}$ F TC=0 +-100 | 24546 | C4-1/8-T0-6811-F C4-1/8-T0-10RO-F |
| A14R93 | 0757-0438 | 3 | 1 | RESISTOR 5.11k $1 \%$, 125W F TC=0+-100 | 24546 | C4-1/8-T0-10R0-F |
| A14R94 | 0757-0346 |  |  | RESISTOR $101 \%$, 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-10R0-F |
| A14R95 | 0757-0289 | 2 |  | RESISTOR 13.3 K iz. 125 WF TC $=0+100$ | 19701 | MF 4 C1/8-T0-1332-F |
| A14R96 A14R97 | 0757-0280 $0757-0346$ | 3 |  | RESISTOR RESISTOR 10 10 RES | 24546 | C4-1/8-T0-1001-F |
| A14R98 | 0757-0346 | 2 |  | RESISTOR 10 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-10RO-F |
| A14R99 | 0757-0346 | 2 |  | RESISTOR 10 1\% , 125w F TC=0 +-100 | 24546 | C4-1/8-70-10R C-F |
| A14R100 | 0757-0346 | 2 |  | RESISTOR 10 1\% , 125世 F TC=04-100 | 24546 | C4-1/8-TC-1 ORO-F |
| A14R101 | 0757-0439 | 4 |  | RESISTOR 6. B1K 1\% . 125W F TC=0t-100 | 24546 | C4-1/8-T0-6811-F |
| A14R102" | 0757-0290 | 5 |  | RESISTOR 6.19K 1\% , 125W F TC=0+-100 RESISTOR $1621 \%$ 1254 F TC $=0$ 0 10100 | 17701 | MF4C1/8-T0-6191-F |
| A14R103 A14R104 | -0757-0405 | 4 | 1 |  | 24546 24546 | C4 1/8-T0-162R-F |
| A14R105 | 0757-0280 | 3 |  | RESISTOR $1 \mathrm{~K} 1 \% .125 \mathrm{WF}$ TC= $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A14R106 | 0757-0289 | 2 |  | RESISTOR 13.3X 17 , 1254 F TC=0+-100 | 19701 | MF 4C1/8-T0-1332-F |
| A14R108 | 0699-3444 | 1 | 1 |  | 19701 24546 | MF4C1/8-T0-9091-F C4-1/8-T0-316R-F |
| A14R109 | 0757-0439 | 4 |  |  | 24546 | C4-1/8-T0-6811-F |
| A14R110 | 0757-0346 | 2 |  | RESISTOR 10 1x . 1254 F TC=0+-100 | 24546 | C4-1/8-T0-10R0-F |
| A14R111 | 0698-3158 | 4 | 1 | RESISTOR 23.7K 1\% .125N F TC=0+-100 | 24546 | C4-1/日-T0-2372-F |
| A14R112 | 0698-3160 | 8 | 3 | RESISTOR 31.6K $1 \%$. 1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-3162-F |
| A14R115 | 0757-0346 | 2 |  | RESISTOR $10.1 \%$. 12 SW F TC=0+-100 | 24546 | C4-1/8-T0-3162-F $C 4-1 / 8-\mathrm{TO-10R0-F}$ |
| A1 4R116 | 0757-0289 | 2 |  | RESISTOR 13.3X 1\% . 125 F F TC=0 +-100 | 19701 | MFAC1/8-T0-1332-F |
| A14R117 | 0698-0085 | 0 |  | RESISTOR $2.61 \mathrm{~K} 1 \% \cdot 125 \mathrm{H}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-2611-F |
| A1 4R118 | 0757-0439 | , |  | RESISTOR 6. $61 \times 1 \chi$, 1254 F TC=0+-100 | 24546 | C4-1/8-T0-6811-F |
| A14R119* | 0757-0290 | 5 |  | RESISTOR 6.19K 1\% . 125 L F TC=0+-100 | 19701 | MFAC1/8-T0-6191-F |
| A14R120 | 0757-0279 | 0 |  | RESISTOR 3.16\% 1\% . 125 W F TC=04-100 | 24546 | C4-1/8-T0-3161-F |
| A14R121 <br> A14R122 | $\begin{aligned} & 0698-3438 \\ & 0757-0447 \end{aligned}$ | 3 | 2 |  | 24546 | C4-1/8-T0-147R-F |
| A14R123 | 0757-0447 | 4 |  | RESISTOR 16.2K $1 \%$, 125 F F TC=0+-100 | 24546 | C4-1/8-T0-1622-F |
| A1 4R124 | 0757-0441 | , | 1 | RESISTOR 8.25K 1\% . 125 W F TC=0+-100 | 24546 | C4-1/8-T0-8251-F |
| A14R125 | 0698-3260 | , | 1 |  | 28480 | 0698-3260 |
| A1 4R126 A14R127 | $\begin{aligned} & 0757-0442 \\ & 0757-0421 \end{aligned}$ | $\stackrel{9}{ }$ | 1 |  | 24546 24546 | $\begin{aligned} & C 4-1 / 8-T 0-1002-F \\ & C 4-1 / 8-T 0-825 R-F \end{aligned}$ |
| A14R128 | 0757-0290 | 5 | 1 | RESIETOR 6.19K $1 \%$. 125 H F TC=0+-100 | 19701 | HFAC1/8-T8-6191-F |
| A14R129 | 0757-0290 | 5 |  | RESISTOR 6.19K $1 \% .1254$ F TC=0 +-100 | 19701 | MF4C1/8-70-6191-F |
| A14R130\% | 0757-0467 | 8 | 1 | RESISTOR 121K 1X , 125W F TC=0+-100 | 24546 | C4-1/8-T0-1213-F |
| A14R131 | 0698-3429 | 2 | 1 | RESISTOR 19.6 1\%.125W F TC=0t-100 | 03888 | PHESS-1/8-T0-19R6-F |
| A14U1 | 1826-0092 | 3 | 1 | IC OP AMP GP DUAL TO-99 PKC | 28488 | 1826-8492 |
| A14UR1 A14V12 A14VR3 | $\begin{aligned} & 1902-0041 \\ & 1912-0048 \\ & 1902-0579 \end{aligned}$ | 1 1 3 | 1 1 1 | DIODE-ZNR 5.11U 5\% DO-35 PD=, 4 DIODE-ZNR 6.81V 5\% DO-35 PD=,4W DIODE-ZNR 5.1U 5\% PD=14 1R=1 OUA | 28480 <br> 28488 <br> 28480 | $\begin{aligned} & 1902-0041 \\ & 1902-81448 \\ & 1902-0579 \end{aligned}$ |
|  |  |  |  | h 14 HISCELLANEOUS PARTs |  |  |
|  | 08559-00310 | 0 | 1 | COVER, LOC AMPLIFIER | 28488 | 18559-00010 |
| See introduction to this section for ordering information *Indicates factory selected value |  |  |  |  |  |  |

## A14

LOG AMPLIFIER


FIGURE868. LOG AMPLIFIER ASSEMBLY A14,COMPONENTLOCATIONS(SERIAL PREFIX 2208A)


Pages 8-191 and 8-199/8-200: MOTHERBARD ASSEMBLY A16
Table 8-14. Motherboard Assembly A16, Replaceable Parts

| 2236 A \& Below | Change A16 to HP Part Number 08559-60066, Check Digit 0. Change A16C3 and A16C21 to HP Part Number 0160-2055, Check Digit <br> 9. CAPACITOR-FXD . 01UF +80-20\% 100VDC CER. <br> Change A16C22 to HP Part Number 0180-2154, Check Digit 1, <br> CAPACITOR-FXD 1900UF +75-10\% 15VDC AL. <br> Delete A16Q1. <br> Change A16W1 to HP Part Number 08559-60067, Check Digit 1, HARNESS ASSEMBLY, MAIN RAME CONNBCTOR. <br> Change A16W2 to HP Part Number 08559-60008, Check Digit 0, CABLE ASSEMBLY, YIG. |
| :---: | :---: |
| 2208A \& Below | Change A16 to HP Part Number 08559-60020, Check Digit 6. Change A16W1 to HP Part Number 08559-60009, Check Digit 1, HARNESS ASSEMBLY, MAIN RRAME CONNECTOR Delete the following: <br> A16CR1, A16CR2, A16R10, and A16VR3. |
| $\begin{aligned} & \text { 1951A, 1945A } \\ & \& \text { Below } \end{aligned}$ | Delete A16C6, A16J3, and A16J4. |

Figure 8-76. Motherboard Assembly A16, Component Locations

| 2236A \& Below | Replace Figure $8-76$ with new Figure $8-76$ (SERIAL PREFIX 2236A) <br> included ic this Manual Backdating supplement. |
| :--- | :--- |
| 2208A \& Below Make the following changes to Figure $8-76$ (SERIAL PREFIX 2236A): <br> Delete CR1, CR2, R10, and VR3. <br> 1951A, 1945A <br> $\&$ Below Delete C6, 53, and 54. |  |

Figure 8-77. Motherboard Assembly A16, Interconnect Diagram
2236A \& Below Replace Figure 8-77 with new Figure 8-77 (SERIAL PREFIX 2236A) included in this Manual Backdating supplement.

2208A \& Below Chacge A16 to HP Part Number 08559-60020.
Make the following changes to Figure 8-77 (SERIAL PREFIX 2236A):
Delete CR2, VR3, and the 927 line.
Delete CR1 and the 8 line.
Delete R10 and the 928 line.
1951A,1945A At pin 18 of XA10P1, delete C6 and 53.
\& Below At XA10P2, delete 54 (CAL OUTPUT TO FRONT PANEL).

## A16 <br> MOTHERBOARD



FIGURE 8-76. MOTHERBOARDASSEMBLYA16,COMPONENT LOCATIONS(SERIAL PREFIX2236A)

## SECTION VIII SERVICE

## 8-1. INTRODUCTION

8-2. This section provides instructions for troubleshooting and repairing the HP Model 8559A Spectrum Analyzer. It includes circuit descriptions, general servicing hints and information, parts identification illustrations and lists, block diagrams, component locations diagrams, and schematics.

## WARNING

To troubleshoot and repair this instrument, it must be removed from the display mainframe and reconnected through an extender cable. Operating the spectrum analyzer outside the mainframe in this manner exposes high voltage points in the instrument that will, if contacted, cause personal injury. Maintenance and repair of this instrument should, therefore, be performed only by a skilled person who knows the hazards involved. Where maintenance can be performed without power applied, the power should be removed. When any repair is completed, be sure that all safety features are intact and functioning and that all necessary parts are connected to their positive grounds.
8.3. SCHEMATIC SYMBOLS, TERMINOLOGY, AND VOLTAGELEVELS

8-4. Symbols and terminology used on the schematic diagrams are explained in Figure 8-1. Test conditions for the signal and dc voltage levels shown on the block and schematic diagrams are provided in Figure 8-2.

## 8-5. TEST EQUIPMENT

8-6. Test instruments and accessories used to maintain the spectrum analyzer are listed in Table 1-4. If
the listed instrument is not available, another instrument that meets the required minimum specifications may be substituted.

## 8-7. MAJOR ASSEMBLY LOCATIONS

8-8. The major assembly location illustrations for the spectrum analyzer are located near the end of this section.

### 8.9. TROUBLESHOOTING

## 8-10. General Information

$8-11$. Troubleshooting is most easily accomplished by using the block diagram at the end of this section to follow the signal path. Once the problem is isolated to a particular circuit, the circuit description and schematic diagram can be used to locate the faulty component.

## NOTE

When a part is replaced, adjustment of the affected circuitry is usually required. For adjustment procedures, refer to Section V.

## CAUTION

Improper cleaning of the printed circuit board edge connectors can cause damage to the contact's gold plating, resulting in corrosion and intermittent electrical contact. Use only the recommended procedure.

## 8-12. Printed Circuit Board Edge Connector Contact Cleaning

## MATERIALS:

- Lint-free cloth or equivalent (HP Part Number 9310-0039, Check Digit 3).
- Solution of $80 \%$ electronics-grade isopropyl alcohol and $20 \%$ water.
- Static-free work station.


## PROCEDURE:

1. Dampen the cloth with the alcohol and water solution and scrub the edge connector contacts vigorously, using a circular motion. Polish one side of the board at a time until the contacts shine, keeping the cloth damp to dissolve contaminants and reduce static electricity.
2. Using a clean cloth, dry the contacts by wiping from their inside to outside edge. This prevents particles from building up on the contact edges.

## CAUTION

Do not use erasers to clean the edge connectors They cause microscopic damage to the contact surface, removing the thin gold plating and exposing the nickel under-plating, which eventually corrodes. Erasers also leave a film on the contact and generate static electricity.

Do not use paper of any kind to clean the edge connector contacts. Paper or lint particles left on the edge contact surface can cause intermittent electrical connections.

Do not touch contact or trace surfaces with bare hands. Always handle the board by its edges.

## SYMBOLS USEDIN SCHEMATICS AND BLOCK DIAGRAMS

## BASIC COMPONENT SYMBOLS

Sariable Resistor: Clockwise
rotation of shaft moves wiper
towards end of resistor mark-
El CW.

## SYMBOLS USED IN SCHEMATICS AND BLOCK DIAGRAMS

## BASIC COMPONENTSYMBOLS

$\leftarrow$
$-$



Oscillator


Operational amplifier


Tuneable cavity
Oscillator

Connection symbol indicating a Jack (except for PC board edge connectors)

Point: Terminal provided for test probe.

COMMONLY USED ASSEMBLY AND CIRCUIT SYMBOLS
$\perp \quad$ Earth ground





Jumper wire
Q, Front-panel control

Measurement Point: Used to indicate a convenient point for measurement. No terminal provided for test probe.
Connection symbol indicating a Plug (except for PC board edge connectors)

Instrument chassis ground. May be accompanied by a number or letter to specify a particular ground

Screwdriver adjustment

Front-panel control code. Color code same as resistor color code. First number indicates base color, second and third numbers indicate colored stripes.


Mixer

Inverter, buffer


Transmission Line

## SYMBOLS USED IN SCHEMATIC AND BLOCK DIAGRAMS

## BASIC LOGIC SYMBOLS

## Distinctive-Shape Symbols



## AMPLIFIER/BUFFER

SCHMITT TRIGGER

## AND FUNCTION

OR FUNCTION

## EXCLUSIVE-OR FUNCTION

## WIRED AND

 FUNCTIONWIRED OR FUNCTION

Output is active when input is active.

Output changes abruptly as a fixed DC level is crossed by the input signal.

Output is active only when all inputs are active.

Output is active when one or more inputs are active.

Output is active when only one input is active.

Two or more elements are joined together to achieve the effect of an AND function.

Two or more elements are joined together to achieve the effect of an OR function.

## SYMBOLS USED IN SCHEMATIC AND BLOCK DIAGRAMS

## BASIC LOGIC SYMBOLS

Indicator Symbols (positive logic assumed)


EDGE-TRIGGERED (dynamic) inputs
 are indicated by the presence of the dynamic input symbol.

Input is active only on the positive-going transition.

ACTIVE PERIOD


ACTIVE-HIGH inputs and outputs are indicated by the absence of the negation symbol, O.


FIGURE8.1. SYMBOLSUSEDINSCHEMATICAND BLOCK DIAGRAMS(40F 4)

Nominal power levels, voltages, and waveforms shown on schematic diagrams were measured using the test setup shown below. Note that signal characteristics shown on schematic diagrams are provided as a troubleshooting aid only. They should not be used for making instrument adjustments.


## EQUIPMENT:



## PROCEDURE:

1. Set HP 8559A Spectrum Analyzer controls as follows:
TUNING .035 GHz
FREQ SPAN/DIV ..... 1 MHz
RESOLUTION BW ..... 300 kHz
INPUT ATTEN ..... 0 dB
REFERENCE LEVEL ..... $-10 \mathrm{dBm}$
REFERENCE LEVEL FINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEP TRIGGER ..... FREE RUN
VIDEOFILTER ..... OFF
BL CLIP ..... OFF
SIGIDENT ..... OFF
ALT IF ..... OFF
2. Connect equipment as shown. Set signal generator for a $35 \mathrm{MHz},-10 \mathrm{dBm}$ output signal. Center the Cal signal on the display and adjust for top graticule.
3. Using board extenders when necessary, check voltages and waveforms indicated on schematic diagrams. Trigger oscilloscope on negative transition of AUX B PENLIFT/BLANKING signal from rear of display mainframe.
4. To measure RF power levels, set RESOLUTION BW control to $\mathbf{3} \mathrm{MHz}$ and FREQ SPAN/DIV to 0 (zero span). The first LO is not swept in zero span, allowing signal levels to be checked with a second spectrum analyzer (use adapter cables as necessary). DO NOT use a power meter (harmonics and LO signals will contribute to give erroneous levels).

## THE HP 8559A SPECTRUM ANALYZER THEORY OF OPERATION

## General Information

The HP 8559A is a wideband spectrum analyzer plug-in module for use with either the HP 180 series or HP 853 A display mainframes. It tunes from 10 MHz to 21 GHz and displays frequency spans as wide as 9 GHz (in bands 5 and 6) and as narrow as 100 kHz (in band 1). A zero span feature enables the analyzer to operate as a tunable, fixed-frequency receiver. Resolution bandwidths of 3 MHz to 1 kHz are selectable in a 1-3-10 sequence. CRT display calibration can be maintained by coupling the frequency span, resolution bandwidth, and video filter to an automatic sweep time control. A five-LED numerical display allows direct readout of the display center frequency or the tunable marker frequency.

The adjustable reference-levelcontrol is calibrated to allow direct readout of amplitudes ranging from -111 to +30 dBm . Continuous wave (CW) signals at or below the Reference Level, the top display graticule, are automatically below the analyzer's gain compression specification. Dynamic range is greater than 70 dB .

The resolution bandwidth and frequency span controls can be locked together to function as a "zoom" control. Signal identification, in spans from 100 kHz to 10 MHz per division, and an alternate IF are also available. This latter feature eliminates problems caused by IF feedthrough (baseline lift) and allows measurement of all signals within the frequency range of the analyzer.

The typical spectrum analyzer comprises three main sections (see Figure 8-3): the RF section, the IF section, and the display section. Since it is a plug-in designed to work with a display mainframe, the HP 8559A houses only the RF and IF sections. The display and power supply are contained in the mainframe.

## RF Section

The HP 8559A RF section resembles a triple-conversionsuperheterodyne receiver; input signal frequencies are converted three times before processing for display. Triple conversion makes possible wide frequency coverage and permits filtering and amplification at more easily controlled frequencies.

RF Attenuator. The stepped RF Input Attenuator Assembly A3, at the input to the RF section, attenuates the input in precise 10 dB steps from 0 to 70 dB . Precise and repeatable attenuation and gain in the signal path are necessary to preserve amplitude calibration and direct reading of signal amplitudes on the CRT. RF attenuator adjustment establishesthe optimum signal level applied to the First Mixer Assembly A4.

First Mixer. Within the First Mixer Assembly A6, the incoming signal mixes with the first local oscillator, generating the first IF. The first converter consists of a single microwave diode, a 4.8 GHz Low-Pass Filter Assembly FL1 contained in a short RF cable, and - housed in the Second Converter Assembly A5 - a 3 GHz bandpass filter with a 17 to 23 MHz bandwidth.

First LO. A YIG-Tuned Oscillator Assembly A6, or YTO, is used as the first LO. YIG, yttrium-iron-garnet, is a ferro-magnetic material which is polished into a small sphere and precisely oriented in a magnetic field. Changes in this magnetic field alter the frequency generated by the YTO. For the YTO in the HP 8559A, a frequency range of 3.01 GHz to 6.04 GHz is used. Voltage control of the magnetic field surrounding the YIG sphere allows the analyzer to be swept or tuned within these frequency limits. A control voltage, derived from the sweep generator, tunes the YTO in sync with the horizontal deflection of the CRT beam. A tuning voltage offsets the sweep to establish the center frequency. Voltage control of the analyzer's frequency is convenient, since low frequency circuits, like operational amplifiers and transistors, can generate and modify the control voltage.

Second Converter. The Second Converter Assembly A5 houses the 3 GHz bandpass filter, the second mixer, and the second LO. The 3 GHz filter uses the resonant characteristics of three precisely machined cavities, or
holes, in the aluminum block housing to filter the first IF. A fourth cavity is used as the resonant circuit for the second LO, which operates at one of two fixed frequencies. After mixing with the first IF, the second LO produces the second IF at 321.4 MHz .

The need for operating the second LO at two separate frequencies becomes apparent when measuring a signal at or near the first IF frequency, 3 GHz . The signal passes through the first mixer and first IF unaffected by first LO tuning and appears as an equally strong signal at all frequencies. This response is called IF feedthrough or baseline lift. Changing the frequency of the second LO shifts the feedthrough response away from the frequency being measured by effectively altering the first IF. Two LO frequencies may be selected with the ALT IF control, 2.6861 GHz (regular IF) and 2.6711 GHz (alternate IF). The LO shift ( 15 MHz ) is reflected in the first IF and fits within the 17 MHz to 23 MHz 1 dB passband of the 3 GHz bandpass filter.

Third Converter. The Third Converter Assembly A10 contains the second IF amplifier, the second IF bandpass filters, the third mixer, the third LO, and the third IF filters and compensation amplifiers. The second IF amplifier consists of a single-transistor amplifier with a 321.4 MHz bandpass filter at its input. It provides about 15 dB of gain before passing the signal to a second 321.4 MHz bandpass filter at its output. The net 1 dB bandwidth is 6 MHz to 9 MHz , narrow enough to reject the second mixer's image frequency. The doublebalanced third mixer produces sum and difference frequencies, as do other mixers, but rejects input and LO frequencies, simplifying subsequent filtering. Two transistors form the third LO, fixed at 300 MHz , which, when mixed with the 321.4 MHz second IF, produces a difference frequency at the final IF, 21.4 MHz .

Three conversions or frequency translations are necessary before the input signal reaches the final IF, where the analyzer's major bandpass filtering and calibrated gains occur. The circuits used in the final IF are more easily controlled at 21.4 MHz than they would be at the higher input frequencies. The RF section's function is to down-convert the input signal accurately so the analyzer can control and display it.

Harmonic Mixing. To extend the frequency range of the HP 8559A, harmonic mixing is employed. Instead of limiting the first mixer input to the fundamental range of the first $\mathrm{LO}(3.01 \mathrm{GHz}$ to 6.04 GHz$)$, harmonics of the LO are allowed to mix with the incoming signal. Each of the six FREQUENCY BAND GHz buttons on the front panel selects a different mixing mode. A mixing mode is characterized by the number of the LO harmonic used and the relationship of the incoming signal frequency to the LO frequency. For example, in the first band ( .01 to 3 GHz ) the incoming signal is below the frequency of the LO. If the incoming signal is 2 GHz , the LO must tune to 5 GHz to produce a difference frequency at the required IF, 3 GHz . This band is characterized as the " 1 - " mixing mode. This relationship is expressed by the fundamental mixing equation:

$$
\mathrm{F}_{\mathrm{LO}}-\mathrm{F}_{\mathrm{IN}}=\mathrm{F}_{\mathrm{IF}}
$$

Band two ( 6 to 9 GHz ) uses the " $1+$ " mixing mode. In this band, the incoming signal frequency is higher than the first LO frequency. Now an 8 GHz incoming signal mixes with the 5 GHz first LO , producing an IF response at 3 GHz . The mixing equation also reflects this change by becoming:

$$
\mathrm{F}_{\mathrm{IN}}-\mathrm{F}_{\mathrm{LO}}=\mathrm{F}_{\mathrm{IF}}
$$

Higher frequency bands are realized by using the second harmonic ( 6 to 12 GHz ) or the third harmonic ( 9 to 18 GHz ) of the first LO. Adjusting the dc bias of the first mixer diode enhances operation at these frequencies. As with the fundamental mixing mode, each harmonic mode has two possible frequency bands creating a total of six bands: $\mathbf{1 +}, \mathbf{1 -}, 2+, 2-, 3+$, and $\mathbf{3 -}$. Section 3, Figure 17 shows the tuning curves for the six mixing modes and the LO fundamental. The mixing equations for the harmonic mixing modes are:

$$
\mathrm{F}_{,,}, \mathrm{NF}_{\mathrm{Lo}}=\mathrm{F},, \quad \text { (for plus modes) }
$$

and

$$
\mathrm{NF},,-\mathrm{F}_{\mathrm{IN}}=\mathrm{F},, \quad \text { (for minus modes) }
$$

where N is the harmonic number of the mode.

Regardless of which harmonic is used for mixing, image frequencies can create problems. Image frequencies occur when a signal not in the band being viewed mixes with the LO to produce a response. It is possible to be in the 1 - band and have a signal at 5 GHz produce a response at 2 GHz ; the opposite can occur in the $1+$ band. As can be seen, it is necessary to be able to differentiate these signals. In the HP 8559A, this is the function of the signal identifier.

Signal Identifier. Several methods of eliminating image responses are used in spectrum analyzers: low-pass filters, preselectors, and signal identifiers. Low-pass filters eliminate all upper out-of-band frequencies from the mixer; this works well for single band analyzers. A preselector (a YIG-tuned bandpass filter) tracks the LO frequency; this allows multi-band operation, but can degrade input sensitivity. The signal identifier allows identification of in-band signals without losses in sensitivity. This is the scheme used in the HP 8559A.

Signal identification simultaneously shifts the display frequency down 1 MHz and decreases the display amplitude about 5 dB . If the signal is an image, it will do something other than shift down 1 MHz . The SIG IDENT button on the front panel activates this function by simultaneously shifting the frequency of the second LO and varying the level of the video signal during alternate sweeps.

## IF Section

The IF section comprises the third IF filters and amplifiers, and the step gain and logarithmic amplifiers. It also includes the video detector, video filters, and video amplifiers. The IF section processes the 21.4 MHz output of the Third Converter Assembly A10 and applies it to the vertical deflection circuitry in the display mainframe.

The 21.4 MHz third converter output is processed by the Bandwidth Filter No. 1 Assembly A11, the Step Gain Assembly A12, the Bandwidth Filter No. 2 Assembly A13, and, finally, the Log Amplifier Assembly A14. Each assembly occupies a separate printed circuit board, which is shielded by extrusions mounted on the Motherboard Assembly A16.

Bandwidth Filters. Bandwidth Filter No. 1 Assembly A11 and Bandwidth Filter No. 2 Assembly A13 are identical; each contains two synchronously-tuned filter poles isolated by buffer amplifiers. Synchronouslytuned filter poles have identical center frequencies, unlike stagger-tuned poles. The bandwidth of these poles, varying from 3 MHz to 1 kHz , is changed simultaneously by the front panel RESOLUTION BW control. Because the variable bandwidths are so much narrower than any of the RF section bandpass filters, the RESOLUTION BW control setting determines the analyzer's overall bandwidth. Parallel LC filters provide bandwidths from 3 MHz to 100 kHz . Crystal filters provide the narrow, 30 kHz to 1 kHz , bandwidths.

Step Gain Amplifier. Located between the bandwidth filter assemblies, the Step Gain Assembly A12 provides precise and selectable gain in three stages, a 10 dB stage followed by two 20 dB stages. Each stage can be turned "on" for full gain or "off" for unity gain. By turning on the amplifiers in combination, gains of 0 to 50 dB may be selected. This action is performed by the REFERENCE LEVEL control. Concentric with the REFERENCE LEVEL knob is the REF LEVEL FINE potentiometer, which controls the 0 to 12 dB PIN diode attenuator. In addition to the gain circuits described, circuitry providing biasing to the first mixer diode and flatness compensation to the third converter is included on the Step Gain Assembly A12.

Logarithmic Amplifier. The second bandwidth filter is followed by the Log Amplifier Assembly A14. The gain of this amplifier is a logarithmic function of the input signal, which allows a greater range of signal amplitudes to be simultaneously displayed on the CRT. This logarithmic amplification of the signal before detection results in the vertical display axis being calibrated in decibels (relative to a milliwatt), rather than volts. Linear amplification from 0 dB to 40 dB may also be selected from the front panel.

The video detector, located on the Log Amplifier Assembly A14, is basically a half-wave rectifier and a filter. This circuit produces a voltage proportional to the signal level, called the video signal. This signal passes through a video filter and a vertical deflection amplifier before leaving the H P 8559A.

## TROUBLESHOOTING HINTS

Begin troubleshooting by measuring the mainframe-supplied voltages as close to the HP 8559A as possible. The Vertical Driver/Blanking Assembly A15 offers three test points (A15TP6, A15TP7, A15TP8) to make the measurements. The +100 V supply is available at A15TP6, the +15 V supply at A 15 TP 7 , and the -12.6 V supply at A15TP8. If any of these voltages are low, refer to the mainframe Operation and Service manual and make the necessary adjustments before continuing. Common symptoms caused by low mainframe-supplied voltages include: increased residual FM (caused by a low +15 V supply) and poor frequency accuracy or intermittent lockup of the frequency display LED's (also caused by a low power supply).

## Residual FM

Residual FM is a short-term jitter or an undesired frequency modulation of a local oscillator (LO). It appears as noise riding on the displayed trace and may be random or cyclical (usually as a function of the line frequency). The following procedure is a guide for isolating a source of residual FM. Further troubleshooting hints concerning residual FM are included following the circuit descriptions of the indicated assemblies.

Set HP 8559A controls as follows:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... 010 GHz
FREQ SPAN/DIV ..... 0
RESOLUTION BW ..... 300 kHz
INPUT ATTEN ..... 0 dB
REFERENCE LEVEL ..... $-10 \mathrm{~dB}$
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} /$ DIV
SWEEP TIME/DIV ..... AUTO
SWEEPTRIGGER ..... OFF
VIDEOFILTER ..... OFF
BLCLIP ..... OFF
SIGIDENT ..... OFF
ALT IF ..... OFF

- Verify that the mainframe supply voltages are correct at the Vertical Driver/Blanking Assembly A15 of the HP 8559A by checking the voltages at A15TP6, A15TP7, and A15TP8.
- Use a second spectrum analyzer to check each LO of the HP 8559A for FM.

First LO: check at the HP 86559A front-panel RF input jack with test analyzer tuned to about 3 GHz (LO power is $-8 \mathrm{dBm} \pm 3 \mathrm{dBm}$ ).
Second LO: check at A5J3 on Second Converter Assembly A5.
Third LO: check at A10J1, the 300 MHz output on Third Converter Assembly A10.

- If the source of FM is the first LO, check the Frequency Control Assembly A7 and the YIG-Tuned Oscillator Assembly A6.
- If the source of the FM is the second LO, short A5A2TP1 to ground while observing the second LO with the second spectrum analyzer. This isolates the possible source of FM to the Second Converter Assembly A5 by removing the varactor bias voltage. Note that removing this bias voltage will cause the second LO frequency to shift. If FM is still present, check the Second Converter Assembly A5 as the source. If the FM disappears, check the bias voltage source on the Marker Board Assembly A8.
- If the source of the FM is the third LO, check the Third Converter Assembly A10.


## DPM Accuracy

The following is a guide to troubleshooting poor DPM accuracy. Further information is included following the circuit descriptions of the indicated assemblies.

- Check +14.5 V supply on the Frequency Control Assembly A7 (A7TP3).
- Perform and verify Frequency Display Adjustment (Paragraph 5-30).
- Verify Tuning Accuracy (Paragraph 4-12).
- Check Marker Board Assembly A8.
- Check frequency accuracy of first and second local oscillators.

First LO: DPM inaccuracies become worse as the higher bands are selected (i.e., increases in harmonic mixing mode).
Second LO: DPM inaccuracies are constant in all bands.

Bes.ek


# DIGITAL PANEL METER ASSEMBLY AI, CIRCUIT DESCRIPTION 

The Digital Panel Meter (DPM) Assembly A1A1/A1A2 is a dc voltmeter that measures a tuning voltage from Marker Assembly A8, and converts it to a front-panel frequency readout. The DPM electronics are contained on two assemblies: the DPM Display Assembly A1A1 and the DPM Driver Assembly A1A2.

## DPM Display Assembly A1A1

The DPM Display Assembly comprises five seven-segment displays with Darlington-transistor switches, Q1 through Q5. The seven-segment displays (DS1 through DS5) are the common-cathode type. The cathode of a display is pulled negative (to about -10.5 V ) when the Darlington-transistor switch associated with it is turned on. With the cathode at a negative potential, the output of A1A2U4 can light the display segments. The transistor switches are strobed so the displays light sequentially. The refresh rate is determined by the clock (block C) and is fast enough (about 300 Hz ) that the displays appear to be lit simultaneously.

## DPM Driver Assembly A1A2

Contained on the DPM Driver Assembly A1A2 are the analog-to-digital converter, power supplies, and display interface circuits. Analog processor IC (U2) and digital processor IC (U3) are each one-half of an analog-todigital converter (ADC). Analog comparator circuits in U2 control counter logic in U3. To accomplish the analog-to-digital conversion, U2 and U3 interact on three control lines: the M/Z (measure/zero logic) line, the COMP (comparator) line, and the U/D (up/down) line. The ADC, U3, produces two outputs. The first comprises five sequential four-line BCD outputs that are fed to BCD-to-seven-segment converter U4. The second consists of five sequential digit strobes that are fed to Darlington-transistor switches A1A1Q1 through A1A1Q5 on the DPM Display Assembly A1A1.

The input signal applied across connector pins J1-3 and J1-6 of the DPM Driver Assembly A1A2 is a dc level of OV to -4V, representing an instrument tuning-range of 0 to 20 GHz (a 1 V change of the input level represents a tune frequency change of 5 GHz ). This OV to -4 V input signal is divided by precision resistors R33 and R27, providing a OV to -2.000 V signal across pins 2 and 15 of the analog processor IC, U2.

Transistors Q1, Q2, and Q9 interface the "sign/or/ur" (sign/over-range/under-range) output of U3 with segment " $g$ " of numeric display A1A1DS5. Transistor Q2 and CR2 provides a "wired AND" function so that the minus sign is shown only in the most-significant-digit position (when both "D5" and "sign/or/ur" are high). Transistor Q1 serves to shift the signal level and Q9 supplies drive to the segment when a minus sign is displayed.

Field-effect transistor Q8 and its associated circuitry form a Colpitts oscillator that provides a clock of about 225 kHz . Inductor L 1 and the series combination of C 1 and C 2 determine the nominal clock frequency.

## Power Supplies and Reference (G) (A)

The power supply circuitry provides the necessary voltage reduction, protection, and filtering for the dc supply voltages: $+12 \mathrm{~V},-12.6 \mathrm{~V}$, and +5 V . The supply voltages are filtered as they enter the board to reduce interference between the DPM and the rest of the instrument. The +15 V supply is used to derive the +12 V supply and the +5 V supply. Zener diode VR1 is used to reduce the +15 V supply to +12 V , while regulator U8 reduces the +15 V supply to +5 V . The -12.6 V supply is filtered to offer two supply lines: $-12.6 \mathrm{VF}_{1}$ and $-12.6 \mathrm{VF}_{2}$. Operational amplifier U7 and its associated circuitry provide a constant dc voltage reference of approximately +6.2 V to the analog IC, U2.

## Display Interface (E)

During the period the DPM drive input is being converted, the BCD output circuitry in U3 is shut off. Once the conversion in U2 and U3 is complete, the four-line BCD is sent to U4 where it is converted to a seven-line (segment) drive. This seven-line output from U 4 is fed in parallel to the displays on the Display Assembly A1A1. Coincident with the BCD-to-seven-segment conversion, U3 supplies a digit strobe drive that, by turning on one of the DPM Display Assembly A1A1 transistors (A1A1Q1 - A1A1Q5), activates one of the seven-segment displays.

Multiplexed BCD data from the digital processor IC (U3) are level shifted by transistors Q3, Q4, Q5, and Q6 and decoded by the BCD-to-seven-segment decoder-driver IC, U4. The decoder-driver sinks the current that drives the paralleled LED display segments on the DPM Display Assembly A1A1. The digit strobe outputs from U3 are level shifted by Q7, A11, A12, Q13, and Q14 and subsequently drive the Darlington-transistor switches A1A1Q1 through A1A1Q5 on the DPM Display Assembly A1A1.

## DIGITAL PANEL METER ASSEMBLY AI, TROUBLESHOOTING

Check supply and reference voltages first.
Display digits freeze intermittently: Be sure the clock oscillator signal goes at least -7 V negative and appears as in Figure 8-4. Low gain (Gm) of A1A2Q8 is the most probable cause for failure. Resistor A1A2R1 is factory selectable; increasing its value increases the amplitude of the clock output,

Least Significant Digit (LSD) dithers: A1A2U2 is the most probable cause; however, noise from A1A2R24, A1A2R25, or A1A2C5 also causes this symptom.

The same segment in each digit does not light: A1A2U4 failure.


TABLE 8－1．DIGITAL PANEL METER ASSEMBLY A1，REPLACEABLE PARTS（1 OF 2）

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1 |  |  |  | DIGITAL PANEL METER ASSEMPLY |  |  |
| A1A1 | 08559－60079 | 5 | 1 | DIGITAL PANEL，METER DISPLAY ASSEMELY | 28480 | 08559－60079 |
| A1A1DS1 | 1990－0693 | 7 | 5 | DISPLAY－NUM－SEG 1 －CHAR 3 H | 28488 | 1DS $1-3533$ |
| A1A1DS2 | 1990－0693 | 7 |  | DISPLAY－NLM－SEG 1－CHAR－3－H | 28480 | 1DS $1-3533$ |
| A1A1DS3 | 1990－0693 | 7 |  | DISPLAY－NUM－SEG 1－CHAR ， $3-\mathrm{H}$ | 28486 | 1DS1－3533 |
| A1A1DS4 | 1790－0693 | 7 |  | DISPLAY－NUM SEEG 1－CHAR－3－H | 28480 | 1 DS 1－3533 |
| A1AIDSS | 1990－0693 | 7 |  | DISPLAY－NUM－SEG 1－CHAR ． 3 H | 23480 | 1DS1－3533 |
| AlA1Q1 | 18540472 | 2 | 5 | TRANSISTOR NPN SI DARL PD $=50$ amW | 04713 | MPS－A14 |
| A1A1Q2 | 1854－0472 | 2 |  | TRANGISTOR NPN SI DARL PD 5000 MW | 04713 | MPS－A14 |
| A1A103 | 1054．0472 | 2 |  | TRANSISTUR NPN SI DARL PD $=503 \mathrm{MW}$ | 94713 | MPS A14 |
| A1A1Q4 A1A125 | $1854-0472$ 1854 | 2 |  | TRANSISTOR NPN SI DARL PD $=500 \mathrm{MW}$ | 04713 | MPS－A14 |
| AIA1RS | 18540472 | 2 |  | TRANSTSTOR NPN ST DARL PD $=503 \mathrm{KL}$ | 04713 | MPS－A14 |
| A1A1XDS A1A1XDS | 1200－0834 | 5 | 5 | SOCKET－IS 10 －CONT DIP DIP－SIDR | 28480 | 1260－0834 |
| A1A1XDS2 | 1200－9834 | 5 5 |  | GOCKET－TC 10－CONT DIP DIP SLDR SOCKET－IC $10-\mathrm{CONT}$ DIP DIP－SLDR | 28483 | 1200－0834 |
| A1A1XDS3 | 1200－0834 | 5 |  | SUCKET－IC SOCKRT－TC 10－CONT 10－CONT | 28480 28480 | $1206-0834$ $1200-0834$ |
| A1A1XDS5 | 1200－0834 | 5 |  | SOCKET－IC 10－CONT DIP DIP ST．DR | 23480 | 12060834 |
| A1AE | 30557－60078 | 4 | 1 | DPM DRIVER ASSEMEI．Y | 28480 | 08559－60378 |
| $\mathrm{Al}_{1} \mathrm{C}_{2} \mathrm{C}_{1}$ | 0160－3751 | 4 | ？ | CAPACITOR－FXD $2200 P \mathrm{C}$＋ $5 \%$ SOUDC CER | 28480 | 016.0 .3751 |
| A1A2CL | 3160－3751 | 4 |  | CAPACITOR FXD 220 BPF $\because 5 \%$ SJUDC EER | 28483 | 3160－3751 |
| A1 A2C3 | 0160－3661 | 5 | 1 |  | 29480 | 0140－3661 |
| AlA2C4 | 9140－0200 | － | 1 | CAPAECITGR－FXD 390PF＋ $5 z$ 300UDC MICA | 7213／3 | DW15\％ 391 J 0300 UV 1 CR |
| A1A2C5 | 0160－2220 | 0 | 1 | CAPACITOR－FXD 1200PF＋－5\％300UDC MICA | 28480 | 0160－2220 |
| A1A2C． 6 | 01600177 | 8 | ？ |  | 56289 | $150 \mathrm{D} 255 \times 9020 \mathrm{~A}$ |
| A 1 A2C］ | 0180－1746 | 5 | $?$ | CAPACITOR FXI 15： $15 \% 10 \%$ 2CUDC TA | 58.2889 | 15015 $56 \times 9020 \mathrm{mF}$ |
| A1AECB | 3189－1746 | 5 |  | CAPACITIR－FXD 15UF＋ $13 \%$ 20VDC TA | 56.287 | $1500156 \times 902052$ |
| A1 ARC9 | 0180－0291 | 3 | 2 | CAPACITOR FXD 1UF＋ $10 \%$ 35VDC TA | 56,089 | $150105 \times 90354.5$ |
| A1AこC10 | 3180－0291 | 3 |  | CAPACITIR－$\times$ XD 1UF． $13 \%$ BENDC TA | 56.289 | $1500105 \times 9035.42$ |
| A1 ARC11 | c180－0197 | 8 |  | CAPACITOR－FXD $2.205+10 \%$ 2CUDC TA | 5：2899 | 150n225x9020at |
| A1ACC12 | 3180－3116 | 1 | 1 | CAPACI1GR F XD 6．f．UF， $10 \%$ 3EVEC TA | 56289 | 1530685×90352a |
| A1 A2C13 | 0160－4014 | 8 | 1 | CAPACTIOR EXD 1uF＋20\％SaUDC CER | 23480 | 01604084 |
| A1A CC14 | 3160－3432？ | 2 | 1 | CAPACITIR－FXD 1UT， 1 S\％SOULE，MET－PE1 YC | 28480 | 0163－3402 |
| A1 ALC 15 | 0100－2144 | 9 | 1 | CAPACITOR－FXO 20CUF $+75-10 \%$ 2SUDC AL | $5 \% 289$ | 36D2676025m4 |
| A1AECR1 | 17310350 | 3 | 3 | dreor EwITCHING nau zoama zew do 35 | 28480 | 19010050 |
| A1 A2CR？ | 1201－0050 | 3 |  | DIODF SWITCHING BOU 2G6MA 2NS DO－35 | 251480 | 1901－0050 |
| AlaÉCR3 | 17910250 | 3 |  |  | 58483 | 1701－0050 |
| A1A ${ }^{3} \mathrm{JI}_{1}$ | 1251－4797 | 4 | 1 | CUNNECTOR 10 PIN M POST TYCE | 2R480 | 1251－4797 |
| A1ARL 1 | an5s\％nanta | 6 | 1 | INDUCTIR，10ROID | 28480 | 0855980310 |
| A1ARL？ | 9140．0129 | 1 | ？ |  | Pa480 | 71400129 |
| A1AOL 3 | $7140-3137$ $9140-0120$ | 1 | 1 | INDUCTIGR 2 F CH－HID 1 MH ，$\%$ ， $2 \mathrm{DX}, 451 \mathrm{G} \quad \mathrm{G}=63$ | 28483 | 7140－0137 |
| A）ARL 4 | 9140－6129 | 1 |  |  | 20480 | 91408129 |
| A ACRO1 | 15553 －0920 | 4 | 11 |  | 58483 | 11553－0320 |
| Al Azqe | 1853－6020 | 4 |  | TRANSTSTOR PNP ST PD 306 CLH FT $=150 \mathrm{E}: 2$ | 2ת480 | $19 \times 300080$ |
| A1AC03 | 195380300 | 4 |  | TRANEISTIRR PNP ：I PD＝3aJMW TI－153m17 | 214880 | 48533 －0320 |
| A1 A2Q4 | 1953－0620 | 4 |  |  | 274888 | 13：5－0026 |
| A1AEQS | 16：53 0：323 | 4 |  | IRANETGTHR PNP SI PO 303n4 ：T－153k：1\％ | 28480 | 14536－0320 |
| Alazab | 18530020 | ， |  |  | 22180 | 10：3 00：0 |
| A1ACG7 | 165530970 | 4 |  |  | －10480 | 1553 －0ate |
| A1 A2Q8 | 135s－6420 | 2 | 1 | TRAN：TETR J TTI $2 N 4891$ N－CHAN D MODF | 81295 | 2N4391 |
| A1ACOP A1 A 20010 | 1054 115 115 040804 | ${ }_{3}^{3}$ | 1 |  | 20483 | 185．4－9404 |
| A1ARQ10 | 11554－6071 | 7 | 1 | IWANSTSTOR NPN SI PDU300mW IT T $=20 \mathrm{MmHz}$ | 29480 | 10540071 |
| MACR211 A1 ACD12 |  | 4 |  |  | C84n3 | 105．3－0020 |
| A1ARQ12 | 1453－0020 | 4 |  | TRAN：IESTRP PNI SI PD－368KW FT－150MH／ | 2ヵヶ8\％ | 108．5－8020 |
| A1ACD13 | 145380008 | 4 |  |  | 28480 | 11553－3930 |
| AIARQ14 | 1053－00：0 | 4 |  | TRAN：TETO：PNP St PD－3E0MW FT＝15，0m：\％ | P＋：¢8\％ | 1035 0020 |
| AIAER1x | 375\％24：n | 1 | 1 |  | ： 25.546 |  |
| A1 A2R2 | 1757－1．7\％ | － | 2 |  | 24：96 |  |
| AIAERA |  | a |  |  | 29：46 | C4 1／3－70－3161 F |
| A1 A2R 4 | 8\％．98－10604 | 9 | 5 |  | 24：46 | C． $1 / 8$－Th 215：F |
| AIA：RL | 16\％\％：3014 | ？ |  |  | $5 \cdot 4516$ | ［4 1／8－19－2151 T |
| AIA 2 R6 | 8698－8084 | 9 |  |  | 24：46 | ［A 1／8 18 31：， |
| A：A：R7\％ | 1650 338， | 9 |  |  | 24：46， | CA 1／0．T3 31515 |
| A：A2R8 | 1，698－01．84 | 9 |  |  | 2¢， 46 |  |
| A1A $A^{2} 9$ |  | $\stackrel{1}{4}$ | \％ |  | 2 $2: 414$ | $c=1 / 3 \cdot 13 \cdot 619: * 1$ |
| A：ARR10 | 66．78－3447 | 4 | 7 |  | 24：76 |  |
|  | 36.888487 | 4 |  |  | 25：46． |  |
| A1 ARR12 | C69\％1－3447 | 4 |  |  | 24，46 |  |
| A1ACR13 | 378．7 3416 | 7 | $?$ |  | 2\％96－ | C4 $41 / 8.13$ 511：2 |
| A ：A2R 14 | c6．69－3447 | 4 |  |  | 24， 26 | F4 1／8－12．42er r |
| AlAF＇R1：． | 6558－3447 | 4 |  |  | 212， 46 | 14 1：9717 428R 1 |

TABLE81. DIGITALPANEL METER ASSEMBLYAI, REPLACEABLEPARTS(2 OF 2)

| Reference Designation | HP Part Number | $\left.\begin{aligned} & c \\ & 0 \end{aligned} \right\rvert\,$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1ARR16 | 0693-3447 | 4 |  |  | 24546 | C4-1/8-T0-4228-F |
| A1A $12 R 17$ $A 1 A=R 18$ | 0698-3447 $3757-0469$ | ${ }_{1}^{4}$ |  |  | 24546 24546 | C4. 1/E-TE-422R-F C4 $1 / 8-\mathrm{T} 0-6192 \mathrm{~F}$ |
| A1ARR19 | 0, $0757-0460$ | 1 |  |  | 24546 | C4-1/8-T0-6192 F |
| Alacrea | 0757-0460 | 1 |  | RESISTGR 61.9K 1 K . 125 FW F TC=3+-139 | ${ }_{24546}$ | C.4-1/8-T3-6192-F |
| Alazrzi | 6757-6460 | $\frac{1}{1}$ |  |  | 24546 24546 |  |
| A1ARR23 | 3757-3179 | c |  |  | 24546 | C4-1/8-70-2152-r |
|  | 6757-0442 $0311-3640$ | 5 | 3 |  | 24546 28489 | C4-1/8-70-1802-F $3811-0640$ |
| A1 A2R25 | 0811-0696 | 1 | 1 |  | 20480 | 0811-0696 |
| A1azrzen | 9757-9274 | - | 1 |  | 24546 | CA 1/8-T0-1211-F |
| A1A2R27 | 0811-0640 | 5 |  | RESISTOR $100 \mathrm{~K}, 01 \mathrm{Z}, 125 \mathrm{~N}$ PWU TC=C+-16 | 28480 | 0811.064 C B2PR13K |
| A1AER28 | 2130-1738 | \% | 1 |  | 73138 <br> 73138 <br> 758 | ${ }_{8}^{\text {B2PRR13k }}$ |
|  | $2100-2655$ $0670-3155$ | 1 1 | 1 |  | 73138 24546 | $82 P \mathrm{R} 100 \mathrm{~K}$ $\mathrm{C} 41 / \mathrm{B}-\mathrm{T} 0-4641-\mathrm{F}$ |
| A1 A2R 31 | 0757-0460 | 1 |  | RESTETOR $61.9 \mathrm{~K} \quad 1 \% .125 \mathrm{~N} \mathrm{~F}$ TC $=0+-100$ | 245.46 | C.4-1/8-TC-6192-F |
| A1ARR32 | 0690-3162 | - | 1 | 2ESISTOR 46.4 K 1\% , 12SU F TC $=0+-133$ | 24546 | C4-1/8-73-4642.F |
| A1 ARR33 | 0811-0640 | 5 |  | RESISTOR $100 \mathrm{CK}, 01 \%$, 12 SW PUW TC=0+-10 | ${ }_{2}^{23480}$ | C811.0646 |
| A1ARR34 | 0757-0442 | S |  |  | 24546 | C4. 1/8-70-1032-F |
| A1 ARR35 | 6698-3442 | 9 | 1 | RESISTOR $2371 \%$.125w F TC=6+-160 | 24546 | C.4-1/8-T6-237R-F |
| A1A 22336. | 3757-0416 | \% |  | RESTSTCR $511{ }^{1 \%}$, 125L F TC=30-133 | 24546 | C4-1/8-T0-511R-F |
|  | c757-0438 | ${ }_{4}^{3}$ | 1 |  | 24546 78483 |  |
| A1Acr3e: A1 ARR39 | 0311-1385 $0698-3136$ | ${ }_{8}$ | 1 | RESISTOR $17.8 \mathrm{BK} 1 \mathrm{1z}$.1254 F TC=04-106 | 24546 | C4-1/8-T0-1782-F |
| A1ARTP1 | 0360-1788 | $\overline{7}$ | 1 | CONNECTLR SCA toint pin oas in hac sis So | 28480 | 3360-1788 |
| ${ }_{\text {Al }}{ }^{\text {a }}$ A2U1 | 1810-0398 | 9 | , | NETUNZK-RES 16-SIP22. OK OHM $\times 9$ | 11236 17556 | 750 101-R22k |
| A1A2UL A1A2U3 | $1026-0588$ $1826-0587$ | 2 1 1 | 1 | IC CONV 16 DlP-? PKG IC CONV 18-DIP-P PKG | 17856 17856 | LD123CJ L.E121CJ |
| A1A2IJ4 | 1020-2716 | a |  | IC DRUR CMMS DSPL DRUR | 34713 | MC14513ECL |
| A1 A2US | 1810-0347 | a |  | NETWORK-RES 8-SJP2.2k OHM $\times 4$ | 01121 | 2086252 |
| A1A2U6 | 1810-0347 |  |  | NETWORK-RES B STP⿳. 2 K OHM $\times 4$ | 31121 28480 | 2088232 |
| A1 A2U7 A1ACUB | $1826-1059$ $1826-0367$ | $\stackrel{3}{5}$ | 1 |  | 28480 04713 | 18261059 r.C7BM05C6 |
| Alazur 1 | 1902-3024 |  | 1 | DIODE-ZNP 2.87U 5 C DO-7 PD=.4W $\mathrm{TC}=-67 \%$ | 23480 | 1902-3024 |
| A1ARUR2 | 1732-3149 |  | 1 | DTODE-ZNR 9.37U $5 \times$ D0-35 PD $=.44$ | 28480 | 1932-3149 |
| A1 ARUR3 A1ARUR4 | $1902-0625$ $1902-1286$ | a | 1 |  | 04713 04713 | ${ }_{1}^{1} 1 \mathrm{Naz3}{ }_{1}$ |
| A1A2UR4 | 1902-1286 | ${ }^{1}$ | 1 | DIDOE ZNR 1NEBACH 6 BU 52 PD |  |  |
| A1AEXA1 | 1251-3403 | 7 | 1 | CONNFCTOR PC EDCC 10 -CONT/ROW 2 ROM: <br> al miscellanecus parts | 28488 | 1251-3403 |
|  | $\begin{aligned} & 0570-0130 \\ & 1205-0095 \\ & 2420-0014 \\ & 08559-00042 \\ & 2360-0113 \\ & 3050-0010 \end{aligned}$ | 6 <br> 6 <br> 0 <br> 6 <br> 6 <br> 2 | 1 1 1 | SCREW-MACH 637 , 375 IN LC EDC HD-GI I hFAT SINK <br> NUT-HEX-DHI -CHAM 6-37 THD . 125 IN TH: INSUL.ATDR <br> SCREW-MACH 6-32 .25-IN-LG PAN-HD-POZI <br> WASHER-FL. MTLC NO. 6 . 147 -IN-TD | 28480 <br> 30161 <br> 28480 28480 <br> 28480 <br> 28480 | $0570-0130$ <br> 32:5B <br> 2420-0014 <br> 08559 - 00342 <br> 2360-0113 <br> 3050-0010 |

A1A2 DPM DRIVER ASSEMBLY



FIGURE8.5. DIGITALPANELMETER ASSEMBLY AI, COMPONENT LOCATIONS

Bes.ek


## FRONT SWITCH ASSEMBLY A2, CIRCU!T DESCRIPTION

Functions of the switches and potentiometers on the Front Switch Assembly A2 are covered in the circuit descriptions for the electronic assemblies they control.

## FRONT SWITCH ASSEMBLY A2 DISASSEMBLY AND REPAIR

## REMOVAL OF FRONT SWITCH ASSEMBLY FROM HP 8559A CHASSIS

1. Turn HP 8559A upside down on a flat work surface.

## NOTE

Numbers in parentheses match the numerical callouts on Figure 8-10 Front Switch Assembly (exploded view). All illustrations referenced in these procedures follow the last procedural step.
2. Use a $9 / 16$-inch nut driver (drilled out, if necessary, to fit over front panel BNC connectors, and covered with heatshrink tubing or tape to avoid scratching enameled front panel) to remove dress nut holding CAL OUTPUT connector to front panel.
3. Remove bottom guide rail. Use a $5 / 16$-inch open-end wrench to carefully disconnect semi-rigid Cable W2 from Input Attenuator Assembly A3 to First Mixer Assembly A4.
4. Disconnect two 40-conductor Ribbon Cables, A2A1W1 (46) and A2A1W2 (47) from Motherboard Assembly A16.
5. Turn HP 8559A right-side up, with front panel facing you.
6. Remove screw holding cable clamp to Second Converter Filter Assembly A5A2. Remove screw located below cable clamp that was removed.
7. Remove the four screws attaching Front Switch Diecast (1) to left and right side gussets. Remove Front Switch Assembly A2, with Front Panel and RF Input Attenuator Assembly A3, from H P 8559A chassis and set chassis to one side.

## DISASSEMBLY OF FRONT SWITCH ASSEMBLY

8. Remove the following front panel knobs: FINE TUNE, COARSE TUNE, RESOLUTION BW, FREQ SPAN/DIV, REF LEVEL FINE, and REFERENCE LEVEL (including Index Disc, Retaining Cup, Nylon Spacer Washer(s), Conical Spring, and Input Attenuator pointer).
9. Remove SWEEP TRIGGER, MANUAL SWEEP, and SWEEP TIME/DIV knobs using a no. 4 hex wrench.
10. Use a no. 4 hex wrench to loosen the two set screws in Lock Knob. Remove Lock Knob.
11. Remove VIDEO FILTER and BASELINE CLIPPER knobs using a no. 2 spline (Bristol) wrench.
12. Remove retaining ring on coarse tune shaft. Remove the three flat washers and two wavy washers. Remove front panel hex nut and lockwasher on Coarse Tune Bushing (36) using a $1 / 2$-inch nut driver (covered with heatshrink tubing or tape to avoid scratching enameled front panel).
13. Loosen hex nut attaching RF Input Cable Assembly W1 to Front Switch Assembly A2 using a 5/8-inch open-end wrench. Carefully disconnect input cable assembly from RF Input Attenuator Assembly A3 using a 5/16-inch open-end wrench. Remove input cable assembly from Front Switch Assembly A2.
14. Disconnect 10-conductor ribbon cable connected to DPM Driver Assembly A1A2. Remove screw holding DPM Display Assembly A1A1 to diecast. DPM window will fall out.
15. Use a $5 / 16$-inch nut driver to remove the two nuts attaching front panel to Front Switch Diecast (1). Remove front panel from Front Switch Diecast.
16. Place Front Switch Assembly A2 on flat working surface with remaining knobs face-down and lock mechanism facing you. Prop sides of switch assembly to allow knobs and shafts to clear working surface (be careful not to scratch front panel enamel).
17. Remove screw and washer attaching Attenuator Bracket (49) to Front Switch Diecast (1). Remove RF Input Attenuator Assembly A3 from Front Switch Assembly A2.
18. Disassembly of REFERENCE LEVEL Switch:
a. Cut tiewrap holding REF LEVEL FINE wires to rear switch board.
b. Remove the three screws (48) attaching Ref Level Fine Pot Plate (68) to Standoffs (62).
c. Remove Index Disc Locator and Ref Level Fine assembly (30, 31, and 64 through 69) from Front Switch Assembly A2 (set to one side, without detaching wires).
d. Remove three standoffs (62) used to support Ref Level Fine Pot Plate (68). Use a no. 6 hex wrench to loosen the two set screws on Miter Gear (51) attached to Attenuator Shaft Assembly (18); then remove Miter Gear from shaft.
e. Use a no. 4 hex wrench to loosen Rotating Lockout (63) attached to Ref Level Shaft (6), and remove lockout from shaft. Remove Ref Level Detent (61) from Front Switch Assembly A2. Be careful to keep Ball Bearing (10) and Spring (11) with Ref Level Rotor (60).
f. Remove the three Studs (53) used to support Ref Level Detent (61).
g. Use a no. 4 hex wrench to loosen the two set screws on front Anticrush Drive Hub Assembly (7) (between Front Switch Board A2A1 and Front Switch Diecast (1) on Ref Level Shaft (6); accessible from side of Front Switch Assembly). Remove Ref Level Rotor (60) and Ref Level Shaft (6) with rear Anticrush Drive Hub Assembly (7) still attached.

## NOTE

Rear Anticrush Drive Hub Assembly (7) on Ref Level Shaft (6) is preset at 9.525 mm ( 0.3 in .) from end of shaft (see Figure 8.7A). Do not remove drive hub unless necessary for repair.
19. Disassembly of RESOLUTION BW Switch.
a. Remove Retaining Clip (21) from RESOLUTION BW Shaft (55).
b. Use a $1 / 4$-inch Nut Driver to remove two Hex Nuts (20) attaching Bandwith Switch Board (59) to Front Switch Assembly, and set board to one side (without detaching wires).
c. Remove Bandwidth Rotor (56). Be careful to keep Ball Bearings (10) and Springs (23) with rotor.
d. Remove Bandwidth Shaft (55), with rear Drive Hub (15) still attached, from Front Switch Assembly.

## NOTE

Rear Drive Hub (15) on Bandwidth Shaft (55) is preset flush with collar on shaft (see Figure 8-7B). Do not remove drive hub unless necessary for repair.
e. Use a no. 4 hex wrench to loosen the two screws on Coupling Hub (54) attached to Frequency Span Shaft (9), and remove hub from shaft.
f. Remove the two Studs (53) used to support Bandwidth Switch Board (59). Remove Bandwidth Detent (52) from Front Switch Assembly.
20. Remove the remaining Screws (48) attaching Front Switch Board Assembly A2A1 to Front Switch Diecast (1).
21. Twist the left side of Front Switch Board Assembly A2A1 down approximately $1 / 8$-inch to provide clearance from Front Switch Diecast support arm (upper left corner). Lift Front Switch Board Assembly A2A1 from Front Switch Diecast (1) and set aside.
22. Removal of Rotor Assemblies:
a. Remove Attenuator Drive Rotor (8), front Anticrush Drive Hub Assembly (7), and Attenuator Shaft Assembly (18) from Front Switch Diecast (1), and set these parts aside.
b. Remove Frequency Span Rotor (14) with associated parts (9-12, 15-17) from Front Switch Diecast (1), and set aside. Be careful to keep Ball Bearings (10) and Springs (11) with Frequency Span Rotor (14).

## NOTE

Drive Hub (15) on Frequency Span Shaft (9) is preset at 12.954 mm ( 0.510 in .) from end of shaft (see Figure 8-7C). Do not remove drive hub from shaft unless necessary for repair.
c. Remove both remaining rotor assemblies from Front Switch Diecast (1), and set aside. Be careful to keep Ball Bearings (10) and Springs (11) with their respective rotors.
23. Disassembly of Lock:
a. Press Locking Link (5) into Front Switch Diecast (1) to release pressure on Dowel Pin (4). Remove Dowel Pin through cutout in Front Switch Diecast. (Individual parts are identified in Figure 8-9.)
b. Remove Locking Link (5), Locking Shaft (3), and Lock Spring (2) from Front Switch Diecast.

## CLEANING AND INSPECTION OF FRONT SWITCH ASSEMBLY

1. All switch contacts must be totally clean and grease-free for proper operation. Use a $50-50$ mixture of isopropyl alcohol and distilled water to thoroughly clean switch rotor contacts and Front Switch Board Assembly A2A1. Avoid touching contacts with fingers.
2. Inspect for bent or damaged shafts, worn or broken contacts, weak or broken springs, rough feeling potentiometers, cracked castings, and damaged PC boards. Check for signs of corrosion or rust. Replace any suspect parts.
3. A special Instrument Grease (HP Part Number 6040-0584) is recommended exclusively for use during switch reassembly. Lubrication is essential for proper operation of switches and lock. A small brush is recommended for applying the Instrument Grease.


#### Abstract

CAUTION Misapplied grease might cause intermittent switch connections. Utmost care must be taken during reassembly to avoid excessive application of grease and contamination of switch contacts. Avoid getting grease on fingers.


## ASSEMBLY OF FRONT SWITCH ASSEMBLY

1. Assembly of Lock:
a. Lightly grease Locking Shaft (3) and insert into Front Switch Diecast (1). Lightly grease bearing surfaces of Locking Link (5).
b. Insert Lock Spring (2) into Front Switch Diecast (1). Press Locking Link (5) fully into Front Switch Diecast and insert Dowel Pin (4) through access cutout (left side of lock boss) to hold lock mechanism in place. Check for correct lock operation.
2. Installation of Rotor Assemblies:
a. Lightly grease all switch rotor detent holes on back of Front Switch Diecast (1).
b. Place Front Switch Assembly on flat working surface with front panel face-down and lock mechanism facing you. Prop sides of switch assembly to provide clearance for knobs and shafts during assembly (be careful not to scratch front panel enamel).
c. Inspect SWEEP TRIGGER rotor assembly (10-12, 24-27). Stop Arm (26) and Horseshoe Spring (27) are held in position by Push-on Retainer (25) and should move smoothly without binding (see Figure 8-8A). Roll Pins (12) should be positioned in hole 7 and hole 18 on SWEEP TRIGGER Rotor (24). Check that Spring (11) and Ball Bearing (10) are in position.
d. Lightly grease long side of SWEEP TRIGGER Shaft (24) and insert SWEEP TRIGGER rotor assembly into left-most bushing in Front Switch Diecast (1). Position rotor so that Ball Bearing (10) aligns with stop boss on left side of Front Switch Diecast.
e. Inspect SWEEP TIME/DIV rotor assembly (10, 11, 21, 22, 24), Figure 8-8B. MANUAL SWEEP Shaft (22) should be lightly greased and should turn freely inside SWEEP TIME/DIV Shaft (24). Check that Spring (11) and Ball Bearing (10) are in position. Note that there are no roll pins inserted in the SWEEP TIME/DIV Rotor (24).
f. Lightly grease long side of SWEEP TIME/DIV Shaft (24) and insert SWEEP TIME/DIV rotor assembly into next bushing in Front Switch Diecast (1).
g. Inspect FREQ SPAN/DIV rotor assembly (9-12, 14-17). If Drive Hub (15) has been loosened or removed from Frequency Span Shaft (9), refer to Figure 8-8C for correct dimensions for adjustment. Roll Pins (12) should be positioned in hole 15 and hole 17 on Frequency Span Rotor (14), as shown in Figure 8-8C. Slotted Bushing (16), Hairpin Spring (17), and Frequency Span Shaft must be lightly greased where they contact each other for proper operation of push-pull mechanism. Check that Springs (11), Ball Bearings (10), Slotted Bushing, and Hairpin Spring are in correct position.
h. Lightly grease long side of Frequency Span Shaft (9) and insert FREQ SPAN/DIV rotor assembly (9-12, 14-17) into next bushing in Front Switch Diecast (1). Position FREQ SPAN/DIV rotor assembly so that stop boss on Front Switch Diecast does not fall within small span between Roll Pins (12).
i. Inspect Attenuator Drive Rotor (8). Roll Pins (12) should be positioned in hole 1 and hole 9, as shown in Figure 8-8D.
j. Inspect front Anticrush Drive Hub Assembly (7). Note that pin is offset to one side of drive hub; place drive hub over right-most bushing in Front Switch Diecast (1) with this side down (i.e., pin as close as possible to Front Switch Diecast) for proper switch operation.

## NOTE

## Correct side of front Anticrush Drive Hub (7) must be oriented towards Front Switch Diecast (1) for proper operation of Front Switch Assembly.

k. Set Attenuator Drive Rotor (8) over Anticrush Drive Hub (7) with Attenuator Drive Rotor gear facing up. Long pin on Attenuator Drive Rotor should protrude through curved slot in diecast.

1. Lightly grease gear end of Attenuator Shaft Assembly (18) and insert into Front Switch Diecast (1). Place metal Washer (19) on shaft.
m . Clean contact fingers on all rotors using lint-free cloth and isopropyl alcohol/distilled water mixture. All rotors should be in proper position.
2. Installation of Front Switch Board Assembly A2A1:
a. Inspect Front Switch Board Assembly. Check switch traces for dirt, grease, or wear. Check interconnect wires, solder joints, pushbutton switches, and ribbon cables $(46,47)$.
b. Clean switch traces using lint-free cloth and isopropyl alcohol/distilled water mixture. No residue should be visible on traces.
c. Use a $3 / 8$-inch open-end wrench to tighten Hex Nut (31) and Lockwasher (30) attaching VIDEO FILTER Potentiometer (33) and metal Washer (32) to Front Switch Board Assembly.
d. Use a $1 / 2$-inch open-end wrench to tighten inner Hex Nut (28) and Washer (29) attaching Dual Tune Pot assembly (21, 28, 29, 34 - 42, 44) to Front Switch Board Assembly. Note that Roll Pin (12) aligns with hole in switch board to locate Dual Pot Bracket (39); Washer (29) between bracket and switch board is critical to proper switch operation.
e. Check Dual Tune Pot assembly for smooth operation and proper gear meshing; disassemble and lightly grease shafts if necessary. Install second Hex Nut (28) mid-way onto Coarse Tune Shaft Bushing (36).
f. Set Front Switch Board Assembly into place on partially-assembledFront Switch Assembly and use a Stud (53) on right-most side of switch assembly to loosely fasten switch board to Front Switch Diecast (1).
g. With one Stud (53) in place but not tight, twist left side of Front Switch Board Assembly up approximately $1 / 8$-inch to fasten switch board under Front Switch Diecast support arm (upper left corner) and align switch shafts.
h. Loosely install the remaining Screws (48) used to fasten Front Switch Board Assembly to Front Switch Diecast (1).

CAUTION
Do not overtighten screws and studs into Front Switch Diecast(1).
i. Use a no. 4 hex wrench to temporarily install SWEEP TRIGGER, SWEEP TIME/DIV, MANUAL SWEEP, and FREQ SPAN/DIV knobs.
j. Tighten Stud (53) and left-most Screw (48) attaching Front Switch Board Assembly to Front Switch Diecast (1). Check all switch rotors for smooth, free switch action. Readjust position of Front Switch Board Assembly as necessary for proper switch action.
k. Tighten the two remaining Screws (48) attaching Front Switch Board Assembly to Front Switch Diecast (1).

1. Recheck all switch rotors for smooth, free switch action and readjust Front Switch Assembly as necessary.
2. Assembly of RESOLUTION BW switch:
a. Place Coupler Hub (54) on Frequency Span Shaft (9) with pin facing up (away from Front Switch Assembly). Do not tighten Coupler Hub at this time.
b. Center Bandwidth Detent (52) over Coupler Hub (54) with stop tab towards top of Front Switch Assembly, and fasten to Front Switch Assembly using two Studs (53).
c. If Drive Hub (15) has been removed or loosened from Bandwidth Shaft (55), refer to Figure 8-7B for proper adjustment. Lightly grease narrow end of Bandwidth Shaft (55) and detent holes on Bandwidth Detent (52). Insert Bandwidth Shaft (55) through Frequency Span Shaft (9).
d. Inspect RESOLUTION BW Rotor (56). Roll Pins (12) should be positioned in hole 16 and hole 17 as shown in Figure 8-8E. Check that Springs (23) and Ball Bearings (10) are in position.
e. Place RESOLUTION BW Rotor (56) onto Bandwidth Shaft (55). Position RESOLUTION BW Rotor assembly so that stop tab does not fall within small span between Roll Pins (12).
f. Clean contact fingers on RESOLUTION BW Rotor and switch traces on Bandwidth Switch Board (59) using lint-free cloth and isopropyl alcohol/distilled water mixture.
g. Use a $1 / 4$-inch nut driver to fasten Bandwidth Switch Board (59) to Front Switch Assembly with two Hex Nuts (20). End of Bandwidth Shaft (55) must not bind against hole in board. Align MANUAL SWEEP Shaft (22) with MANUAL SWEEP Potentiometer (58) by turning MANUAL SWEEP knob clockwise until shaft engages with MANUAL SWEEP Potentiometer.

## NOTE

## Depth of MANUAL SWEEP Shaft (22) can be adjusted if necessary by carefully tapping SWEEP TIMEJDIV Shaft (24) farther into the white plastic rotor.

h. Turn Front Switch Assembly over and remove FREQ SPAN/DIV knob using a no. 4 hex wrench.
i. Install Retainer Clip (21) on Bandwidth Shaft (55).
j. Use a no. 6 hex wrench and a no. 4 hex wrench to temporarily install FREQ SPAN/DIV and RESOLUTION BW knobs.
k. Pull and turn FREQ SPAN/DIV Knob until a set screw is visible on Coupling Hub (54). Push FREQ SPAN/DIV knob in and out to align pin on Coupling Hub with slots in Bandwidth Rotor (56). With FREQ SPAN/DIV knob pushed in and Coupling Hub flush again Bandwidth Rotor (pin aligned), tighten set screw using a no. 4 hex wrench. Turn FREQ SPAN/DIV knob until second set screw is visible, and tighten second set screw.

1. Push FREQ SPAN/DIV knob in and out while observing Bandwidth Rotor (56). Bandwidth Rotor will not move if Coupling Hub (54) is properly aligned. Readjust Coupling Hub as necessary for proper operation.
2. Assembly of REFERENCE LEVEL Switch:
a. Install remaining two Studs (53) on Front Switch Assembly. Check that all screws and studs have been tightened.
b. If rear Anticrush Drive Hub Assembly (7) has been loosened or removed from Ref Level Shaft (6), refer to Figure 8-7A for correct dimensions for adjustment.
c. Inspect Ref Level Rotor (60). Roll Pins (12) should be positioned in hole 1 and hole 9, as shown in Figure 8-8F. Check that Spring (11) and Ball Bearing (10) are in position. Insert Ref Level Shaft (6) through Ref Level Rotor so that rear Anticrush Drive Hub (7) seats properly into rotor.
d. Lightly grease long end of Ref Level Shaft (6) and insert through Front Switch Board Assembly A2A1, Attenuator Drive Rotor (8), front Anticrush Drive Hub (7), and bushing in Front Switch Diecast (1).
e. Lightly grease detent holes on flat side of Ref Level Detent (61). Mount detent on three Studs (53) and fasten tightly with three Standoffs (62).

## CAUTION <br> Hollow Ref Level Shaft (6) might be damaged if set screws in Rotating Lockout (63) are tightened excessively.

f. Place Rotating Lockout (63) on Ref Level Shaft (6) with teeth flat against Ref Level Detent (61). Lockout teeth should be aligned to miss pin on Ref Level Detent when Ref Level Shaft is pushed in (switch in any detent position). With Ref Level Shaft fully extended from front panel, use a no. 4 hex wrench to tighten Rotating Lockout.
g. Push Ref Level Shaft (6) in and out and check for smooth mechanical feel and proper Rotating Lockout (63) alignment. Rotating Lockout should not bind against Ref Level Detent (61) and should allow Ref Level Shaft to turn smoothly between detent positions. Adjust Rotating Lockout as necessary for proper operation.
h. Use a no. 4 hex wrench to lightly tighten one set screw in front Anticrush Drive Hub (7) visible between Attenuator Drive Rotor (8) and Front Switch Diecast (1).
i. Turn Attenuator Drive Rotor (8) so that long pin (for input Attenuator pointer) is at bottom of Front Switch Diecast (1). Hold Attenuator Drive Rotor in position and push in on Ref Level Shaft (6) to align front Anticrush Drive Hub (7).
j. Push Ref Level Shaft (6) in and out while observing Ref Level Rotor (60) and Attenuator Drive Rotor (8). Rotors will not move when front Anticrush Drive Hub (7) is properly adjusted.
k. Use a no. 4 hex wrench to firmly tighten both set screws in front Anticrush Drive Hub (7). Recheck Ref Level Shaft (6) as in step j, and readjust front Anticrush Drive Hub as necessary.

1. Slip Miter Gear (51) over Attenuator Shaft Assembly (18). Do not tighten at this time.
m. Inspect Ref Level Fine Assembly (30, 31, 65-69). Ref Level Fine Shaft (65) should turn smoothly. Check Ref Level Fine Potentiometer (69) and connecting wires for good electrical connections. Lightly grease Ref Level Fine Shaft and hollow Index Disc Locator (64) shaft.
n. Install Index Disc Locator (64) on Front Switch Assembly. Hole in locator bar rides over left-most Standoff (62) used to support Ref Level Fine Pot Plate (68). Install Ref Level Fine Assembly (30, 31, 65 - 69) on Front Switch Assembly with three Screws (48). Connecting wires should be routed. Ref Level Fine Shaft (65) should turn smoothly without binding over its full rotation. Adjust position of Ref Level Fine Pot Plate as necessary.
o. Use a new tiewrap to attach Ref Level Fine connecting wires to Standoff (62).
2. Installation of RF Input Attenuator A3:
a. Mount RF Input Attenuator to Attenuator Bracket (49) using two Screws (48). Check all eight attenuator positions by hand for proper detent action and smooth operation. Leave attenuator in full counter-clockwise position.
b. Slide Miter Gear (51) to end of Attenuator Shaft Assembly (18) against Ref Level Fine Pot Plate (68). Set Attenuator Assembly in place on Front Switch Assembly, with notch in Attenuator Bracket (49) lightly greased and aligned with Attenuator Shaft Assembly. Use Washer (50) and Screw (45) to fasten Attenuator Bracket to lower left corner of Front Switch Diecast (1). (Do not tighten Miter Gear at this time.)
3. Installation of Front Panel:
a. Remove the front panel knobs.
b. Use a $5 / 16$-inch nut driver and two hex nuts to carefully install front panel (with pushbutton bezels and DPM window installed) on Front Switch Diecast (1).
c. Insert RF Input Cable Assembly W1 through front panel and loosely attach with hex nut. Carefully connect cable assembly to RF Input Attenuator using a $5 / 16$-inch open-end wrench. Tighten cable assembly to front panel using a $5 / 8$-inch open-end wrench.
d. Use a no. 4 hex (Allen) wrench to install lock Knob on Locking Shaft (3). Base of Lock Knob should clear front panel when Locking Shaft is pushed in.
e. Install front panel nut and washer on Coarse Tune Bushing and tighten with special $1 / 2$-inch nut driver.

## NOTE

Front-panel control knobs and their attaching parts are identified in Figure 6.1. Numbers in parentheses match numerical callouts on Figure 8-10.
8. Installation of Knobs:
a. Turn SWEEP TRIGGER Shaft (24) fully clockwise (as seen from front of Front Switch Assembly) to spring-loaded SINGLE position and release. Use a no. 4 hex wrench to install SWEEP TRIGGER knob with SINGLE line aligned with painted arrow on front panel. Check for proper switch operation and alignment.
b. Turn SWEEP TIME/DIV Shaft (24) to align Ball Bearing (10) on SWEEP TIME/DIV Rotor with left-most edge of stop boss on Front Switch Diecast (1). This positions SWEEP TIME/DIV Rotor with Ball Bearing slightly right of 12 o'clock position (as seen from front of Front Panel Assembly). Use a no. 4 hex wrench to lightly tighten SWEEP TIME/DIV knob onto SWEEP TIME/DIV Shaft with approximately center of green AUTO position aligned with painted arrow on front panel. Turn SWEEP TIME/DIV knob to any calibrated sweep time position and align knob markings exactly with painted arrow on front panel. Tighten SWEEP TIME/DIV knob and check for proper switch operation and alignment.
c. Uncouple RESOLUTION BW Shaft (55) from FREQ SPAN/DIV Shaft (9) by pulling both shafts out. Turn each shaft fully clockwise. Use a no. 6 hex wrench to install FREQ SPAN/DIV knob with 100 MHz indicated, checking that the plastic indicator guide on back of knob does not completely bottom into hole in Front Switch Diecast (1). Use a no. 4 hex wrench to install RESOLUTION BW Knob with 3 MHz indicated. Check for proper operation and alignment of both switches. Push-pull action should be smooth and positive.
d. Set nylon shim washer(s) and Index Disc (see Figure 6-1) in place on REFERENCE LEVEL knob to check for proper shim width. Nylon washers should shim Index Disc slightly away from labelled ring on REFERENCE LEVEL knob to prevent rubbing against painted numbers. Add or remove shim washers as necessary to provide slight clearance.
e. Turn Attenuator Drive Rotor (8) fully counter-clockwise so that Input Attenuator Pointer guide pin (P/O 8) is at bottom of front panel. Turn Ref Level Shaft (6) fully clockwise. Place plastic Input Attenuator Pointer over guide pin (pointer should indicate 70 dB ). Place large end of conical spring against Input Attenuator Pointer and slide REFERENCE LEVEL knob, nylon washer(s), and Index Disc (from step d) onto Ref Level Shaft, securing with retainer clip.
f. Use a no. 6 hex wrench to adjust Miter Gears (51) for alignment of Input Attenuator Pointer with 70 dB front panel label and proper gear mesh (Input Attenuator A3 still in full counter-clockwise position).
g. Turn REFERENCE LEVEL knob to indicate level of -30 dBm signal and tighten knob securely with a no. 6 hex wrench. Check for proper operation and alignment of REFERENCE LEVEL and INPUT ATTEN controls, and readjust knob, gears, and Rotating Lockout (70) as necessary. Reference Level should range from -10 dBm to -100 dBm with 0 dB INPUT ATTEN selected.
h. Turn REF LEVEL FINE Shaft (65) fully counter-clockwise and use a no. 4 hex wrench to install REF LEVEL FINE knob with 0 dB indicated. Check for proper operation and alignment and readjust knob as necessary.
i. Turn BASELINE CLIPPER Shaft and VIDEO FILTER Shaft (33) fully counter-clockwiseand use a no. 2 spline wrench to install BASELINE CLIPPER and VIDEO FILTER knobs in OFF position. Check for proper operation and alignment and readjust as necessary.
j. Install flat and wavy washers on coarse tune shaft as indicated in Figure 6-1. Compress these washers with retaining ring. A torque of about 1 in -oz should be required to turn coarse tune shaft.
k. Use a no. 4 hex wrench to install COARSE TUNE and FINE TUNE knobs. Base of COARSE TUNE knob should clear front panel. Check for proper operation of TUNING control.

## INSTALLATION OF FRONT SWITCH ASSEMBLY INTO HP 8559A CHASSIS

9. Set Front Switch Assembly into place in chassis, being careful not to bend semi-rigid cables or pinch wires or ribbon cables. Attach Front Switch Diecast (1) to left and right side gussets with four screws.
10. Connect four wires $(0,916,918,923)$ to correspondingly-labelled pins in Front Switch Board A2A1.
11. Attach DPM Driver Assembly A1A2 to diecast with one Screw.
12. Connect 10 -conductor Ribbon Cable (46) to DPM Driver Assembly A1A2.
13. Connect the two 40-conductor Ribbon Cables A2A1W1 (46) and A2A1W2 (47) to Motherboard Assembly A16.
14. Use a 5/16-inch open-end wrench to carefully connect Semi-rigid Cable W2 from the Input Attenuator to the First Mixer.
15. Use special 9/16-inch nut driver to install CAL OUTPUT connector to front panel with one dress nut.
16. Slide HP 8559A into display mainframe, turn instrument ON, and verify proper operation of all controls.

## FACTORY PRESET

## SHAFT ASSEMBLIES



B
BANDWIDTH SHAFT


C
FREQUENCY SPAN SHAFT

NOTE
Arrows point toward rear of HP 8559A

FIGURE8.7. SHAFT ASSEMBLIES


A
SWEEP TRIGGER ROTOR


C
FREQ SPAN/DIV ROTOR



B SWEEP TIME/DIV ROTOR


D
ATTENUATOR DRIVE ROTOR


FIGURE \&-8. ROTOR ASSEMBLIES


FIGURE 8-9. MACHINED PARTS

TABLE 8-2. FRONT SWITCHBOARD ASSEMBLY A2A1, REPLACEABLE PARTS


Bes]e

| Reference Designator | HP Part Number | ${ }_{0}^{\text {c }}$ | aty | Description | Mfr Code | Mfr．Par Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | O8595．60065 |  |  | FRovT sulct assmal | ${ }^{268480}$ | Oesso |
|  |  | ${ }_{1}^{4}$ |  |  | coicce | cosis |
|  |  | $8$ |  | 边 |  |  |
|  |  | ? |  |  |  |  |
|  |  | , |  |  | coize |  |
|  |  | ： | ${ }_{6}$ |  | ${ }_{7807}$ | graotso |
|  | ${ }_{\text {L }}^{12880.0059}$ | ： | 1 |  | coick | （1ati．023 |
|  |  | ${ }_{5}^{5}$ | $\frac{1}{2}$ |  |  |  |
| ${ }_{17}^{16}$ | O8S5．2089 | ${ }_{2}^{2}$ | 1 | Eushlis | $\substack { 28480 \\ \begin{subarray}{c}{28480{ 2 8 4 8 0 \\ \begin{subarray} { c } { 2 8 4 8 0 } } \end{subarray}_{\substack{\text { a }}}$ | coicisise |
| ${ }^{18}$ |  | $6$ | 1 |  |  | 5022. |
|  | coicle | ${ }^{3}$ | ${ }_{5}$ | Neter | $\underbrace{2080}_{\substack{28880 \\ 28880}}$ | coin |
| ce ${ }_{24}^{23}$ |  | \％ | $\frac{1}{2}$ |  | coick | ${ }_{\substack{502 \\ \text { So．} \\ \text { S0．}}}$ |
|  |  |  |  | $\substack{\text { contact } \\ \text { REAMNER }}$ |  | （0565．20108 |
| $\underbrace{26}_{28}$ | Ois | ${ }_{5}^{8}$ | 1 |  | ${ }_{28880}$ |  |
|  |  |  |  |  |  |  |
| $\underset{\substack{29 \\ 30 \\ 31}}{ }$ |  | ${ }_{4}^{4}$ | ${ }_{2}^{4}$ |  | $\substack{2988 \\ 2880}_{2}$ |  |
|  | 3050．0028 | 2 | 1 | WNSTHER L L MTCL |  |  |
|  |  |  |  | Resiltor，VAR Sok 20\％SW |  |  |
|  | 08558－201 | ${ }_{3}^{4}$ | 1 | SHAET FINE TUEE |  |  |
|  |  | $\frac{1}{9}$ |  | ， |  | cisisi．296 |
| 80 |  | ${ }_{6}$ | 1 |  | $\substack{28880 \\ 2880}_{\text {220 }}$ | coill |
| ${ }^{1}$ | ${ }^{2100.359}$ |  | 1 |  | 28880 | ${ }^{2100.3452}$ |
|  |  | 8 |  | SK 100 （cioarse t ine） |  | （e．3593 |
| ${ }_{44}^{43}$ |  | ${ }_{2}^{1}$ |  |  | coick | ${ }^{3050} 0$ |
| ${ }_{46}^{45}$ |  | ${ }_{6}^{4}$ |  |  | ${ }^{28880}$ | 22000 |
| ${ }^{47}$ | 08559．6000 |  |  |  | 2a80 | 08559.60 |
| ${ }_{49}^{48}$ | （220．010， | ${ }_{6}^{2}$ | 8 |  |  |  |
|  | cois |  |  |  |  | Sois |
| ${ }_{53}^{52}$ |  | ${ }_{3}$ |  |  | A80 |  |
|  |  | ${ }_{5}$ | 1 | Hubiciopling |  | cosis |
| 52184） |  |  |  | Rotors Sincte contact | ${ }^{28480}$ | 08558．00 |
|  | ${ }^{2100.333}$ | 3 |  | Resision trmp 10k 20\％CCC 1－TRN |  |  |
|  | （0859．2009 | $\stackrel{9}{4}$ |  | （tand | 退 | （osisi．azi |
|  |  |  |  |  |  | （sile |
| ${ }_{6}^{64}$ |  | ${ }_{8}$ |  | 边 |  |  |
| ¢69 |  | ？ |  | Sole |  |  |
|  | ${ }_{\substack{\text { OS5S5．0022 } \\ 2100.0542}}$ | － |  | （eate | $\substack{\text { che }} \substack{208880}_{2080}$ | cossiol |
| 70 | O8559．00022 |  |  | M LITREFLEVELINE） | （28880 | ${ }^{21200.0}$ |




A2A1W1
FANOUT RIBBON CABLE ASSEMBLY


A2A1W2

## RIBBON CABLE ASSEMBLY



PIN ARRANGEMENT
SHOWN FOR A16.J2 IS AS
SHOWN FOR A16.J2 IS AS
SEEN FROM TOP
(COMPONENTSIDE) OF
MOTHERBOARD.



ASSEMBLY NUMBERS REFER TO SCHEMATICS WHERE DIAGRAM OF INDICATED SWITCH OR CONTROL IS LOCATED. DIAGRAMS OF ALL SWITCHES AND CONTROLS ARE ALSO LOCATED ON THE A2 FRONT PANEL SWITCH ASSEMBLY SCHEMATIC.

FIGURE8-13. CROSS-REFERENCEOF FRONT PANELSWITCHES AND CONTROLS TORELATED ASSEMBLIES

| ERVICE | MODEL |  |
| :---: | :---: | :---: |
| MNEMONIC | DESCRIPTION |  |
| ALTIF | ALTERNATE IF (LOW = ALT IF $=2.9925 \mathrm{GHz}$ ) |  |
| BL CLIP | baseline clipper voltage |  |
| BW1 |  |  |
| BW2 |  |  |
| BW3 | BANDWIDTH CONTROL LINES |  |
| BW4 |  |  |
| BW5 |  |  |
| CTUNE | COARSE FREQUENCY TUNING VOLTAGE |  |
| EXPAND | SELECTS EXPANDED DISPLAY FOR $1 \mathrm{~dB} / \mathrm{DIV}$ LOG MODE |  |
| FINE TUNE | FINE FREQUENCY TUNING VOLTAGE |  |
| FREQ ZERO | FREQUENCY ZERO ADJUST VOLTAGE |  |
| FS1 |  |  |
| FS2 |  |  |
| FS3 |  |  |
| FS4 | FREQUENCY SPAN CONTROL LINES. |  |
| FS5 | FS6 SELECTS YTO FM OR MAIN COIL INPUT (+15V=FM COIL). |  |
| FS6 | FS9 SELECTS FULL SPAN OR PER DIVISION ( $+15 \mathrm{~V}=\mathrm{FULL}$ SPAN). |  |
| FS7 |  |  |
| FS8 |  |  |
| FS9 |  |  |
| GAIN | VERTICAL GAIN VOLTAGE |  |
| H2 | LOW=SECOND HARMONIC BAND |  |
| H3 | LOW=THIRD HARMONIC BAND |  |
| IFG1 |  |  |
| IFG2 | CONTROL IF STEP GAIN AMPLIFIERS |  |
| IFG3 |  |  |
| IFG4 |  |  |
| IFG5 | CONTROL LOG/LINEAR AMPLIFIERS |  |
| IFG6 |  |  |
| LINE TRIG | LINE TRIGGER SIGNAL |  |
| LOG/LIN | SELECTS LOG OR LINEAR DISPLAY ( $+15 \mathrm{~V}=$ L0G; -10V=LIN) |  |
| MAN SCAN | MANUAL SCAN VOLTAGE |  |
| NOISE MEASURE | SELECTS MAXIMUM VIDEO FILTERING |  |
| PENLIFT | PENLIFT SIGNAL |  |
| PM | SELECTS PLUS OR MINUS HARMONIC CONVERSION |  |
| REF LEVEL CAL | REFERENCE LEVEL CALIBRATION VOLTAGE |  |
| REF LEVEL CW | REFERENCE LEVEL FINE UPPER LIMIT VOLTAGE |  |
| REF LEVEL WP | REFERENCE LEVEL FINE CONTROL WIPER VOLTAGE |  |
| SIG ID | SIGNAL IDENTIFIER CONTROL ( $G$ ROUND $=0 \mathrm{~N}$ ) |  |
| SINGLE | SINGLE SWEEP TRIGGER VOLTAGE |  |
| ST1 |  |  |
| ST2 |  |  |
| ST3 |  |  |
| ST4 | SCAN TIME CONTROL LINES. ST6 ENABLES FAST SCAN TIMES. |  |
| ST5 |  |  |
| ST6 |  |  |
| ST7 |  |  |
| SYNC | SWEEP SYNC CONTROL (LINE OR VIDEO) |  |
| TRIG | SWEEP TRIGgER (SINGLE OR FREE RUN) |  |
| TUNE REF | FREQUENCY TUNING REFERENCE VOLTAGE |  |
| VERT | VERTICAL VIDEO SIGNAL VOLTAGE |  |
| VERT POSN | VERTICAL POSITION VOLTAGE |  |
| VIDEO | VIDEO SIGNAL |  |
| VIDEO FILTER | VIDEO FILTER LEVEL VOLTAGE |  |
| VIDEO TRIG | VIDEO SWEEP TRIGGER VOLTAGE |  |




## RF SECTION CIRCUIT DESCRIPTIONS

List of parts included in RF Section.

## INPUT ATTENUATOR ASSEMBLY A3, CIRCUIT DESCRIPTION

The HP 8559A Input Attenuator Assembly A3 is a 50 ohm, precision, coaxial step attenuator. Attenuation in $10-\mathrm{dB}$ steps from 0 dB to 70 dB is accomplished by switching the signal path through one or more of three resistive pads in a predetermined sequence by the INPUT ATTEN control. The Input Attenuator Assembly A3 is not field serviceable.

## FIRST MIXER ASSEMBLY A4, CIRCUIT DESCRIPTION

The First Mixer Assembly A4 is a sealed microcircuit (shown in Figure 8-19), that is not field serviceable and must be replaced with either a new or factory rebuilt unit. In the mixer assembly, the .01 to 21 GHz input signals are combined with the first LO signal ( 3.01 to 6.04 GHz ) generated by the YIG-Tuned Oscillator Assembly A6. Fundamental mixing is used for the two lowest mixing bands, while harmonic mixing is used for the remaining four bands. Fundamental mixing produces the sum and difference frequencies of the input and the LO frequency. The fundamental mixing equation is:

$$
\text { Where: } \begin{aligned}
\mathrm{F}_{\mathrm{s}} & =\mathrm{F}_{\mathrm{lo}} \pm \mathrm{F},, . \\
\mathrm{F}_{\mathrm{s}} & =\text { signal frequency } \\
\mathrm{F}_{10} & =\text { local oscillator frequency } \\
\mathrm{F}_{\mathrm{if}} & =\text { intermediate frequency }
\end{aligned}
$$

Harmonic mixing alters the mixing equation as shown:

$$
\begin{aligned}
& \mathrm{F}_{\mathrm{s}}=\mathrm{NF},, \pm \mathrm{F},, \\
\text { Where: } & \mathrm{N}=\text { the harmonic number }
\end{aligned}
$$

An alternate first IF is used to eliminate the problem of IF feedthrough (baseline lift) that occurs when a signal of the same frequency as the IF frequency $(3.0075 \mathrm{GHz})$ is present at the input. The second LO frequency is lowered by 15 MHz (from 2.6861 GHz to 2.6711 GHz ) to establish the alternate first IF at 2.9929 GHz . The first LO is also shifted to keep the signal on screen. The shift equation is:

$$
\text { Frequency Shift }= \pm \frac{15 \mathrm{MHz}}{\mathrm{~N}}
$$

Where: $\mathrm{N}=$ the harmonic number
A $17-23 \mathrm{MHz}$ bandpass filter, in the Second Converter Assembly A5 housing, follows the first IF and is centered at 3 GHz . The wide bandpass accommodates signals in either the regular or alternate IF modes.

A schematic of the First Mixer Assembly A4 is shown in Figure 8-25. The output of the YTO is coupled into the signal path ahead of the internal mixer. Mixing diode bias is supplied from the Step Gain Assembly A12. A different bias current is used for each harmonic to minimize conversion loss and flatness problems. In addition to mixer bias, the First Mixer Assembly A4 requires a +14.5 V and -10 V to power and bias the transistor buffer amplifier at its output. Conversion loss of the mixer is about -12 dB .

## FIRST MIXER ASSEMBLY A4, TROUBLESHOOTING

Typically, a bad first mixer results in at least a 15 to 20 dB loss in sensitivity (i.e., the amplitude of displayed signals is 15 to 20 dB low). There are, however, other factors that can affect spectrum analyzer sensitivity that should be checked. The measurement of power levels along the signal path can give a good indication of where the loss is occurring. The output of the Second Converter Assembly A5 offers a convenient point to isolate the RF front-end from the IF section. If the loss appears to be in the front-end, measure the power levels of the first and second local oscillator with a second spectrum analyzer. Next, measure the supply and bias voltages at the first mixer. To access the push-on connectors of the first mixer's bias and supply lines, it is helpful to remove the instrument's bottom guide-rail.

## CAUTION


#### Abstract

The First Mixer Assembly A4 can be damaged by electro-static discharge. Tools and hands should be grounded before handling this assembly. It is also possible to damage the mixer diode with an ohmmeter. Damage may occur with as little as 3 V open-circuit-voltage between the ohmmeter probes. Therefore, dc testing of the assembly is not recommended. If it becomes necessary to remove the rigid coaxial cable connecting the first mixer output and the second mixer input, be careful not to damage the Low Pass Filter Assembly FL1 internal to the cable. The filter assembly is very sensitive to bending.


Set HP 8559A controls as follows:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... 035 GHz
FREQ SPAN/DIV ..... 1 MHz
RESOLUTIONBW ..... 1 MHz
INPUT ATTEN ..... 10 dB
REFERENCELEVEL ..... $-10 \mathrm{~dB}$
REFLEVELFINE
$1 \mathrm{~dB} / \mathrm{DIV}$
Amplitude Scale
AUTO SWEEP TIME/DIV ..... FREE RUN
VIDEOFILTER ..... OFF
BLCLIP ..... OFF
SIGIDENT ..... OFF
ALTIF ..... OFF

## NOTE

Before making the following adjustments, measure and note the first mixer bias voltage (A16TP1). This permits the instrument to be returned to calibration if the first mixer is good.

Adjust the V1 potentiometer (A12R72 on the Step Gain Amplifier Assembly A12) through its range and observe the changes in the displayed signal peak and the bias voltage. With a good mixer, two changes are observed: the displayed signal peaks at some point in the adjustment (usually with about -5 V or -6 V of bias voltage) and the bias voltage (A16TP1) ranges from -9 V to $+2 \pm 0.5 \mathrm{~V}$. If all of these characteristics are not present, the mixer is probably damaged.

## SECOND CONVERTER ASSEMBLY A5, CIRCUIT DESCRIPTION

The IF from the First Mixer Assembly A4 is coupled into the Second Converter Assembly A5 bandpass filter through coupling loop L3. Three circular, slug-tuned cavity resonators, operating as an inductive transmission line, make up the bandpass filter. The filter forms a high-Q circuit centered at 3 GHz with a 23 MHz bandwidth that is required to accommodate the regular and alternate IFs. Coupling loops L4 and L5 provide coupling between the cavities. Loop coupling is also used to couple the 3 GHz IF signal to the second LO output at the mixer diode CR1.

The second LO contains varactor diodes that are controlled by a voltage from the Marker Assembly A8. The diodes shift the frequency of the second LO either 15 MHz (ALT IF) or $\pm 1 \mathrm{MHz}$ (SIG ID). The varactor control voltage is always between 1 V and 28 V and corresponds to the oscillator frequency; increasing the voltage increases the frequency.

Both the second LO and the 3 GHz IF signal are coupled into mixing diode CR1, generating a difference frequency of 321.4 MHz that is coupled through the matching filter (C3, L2, C4) to the Third Converter Assembly A10. The matching filter is a passive network designed to match the impedance of the second mixer to the 50 ohm impedance of the Third Converter Assembly A10. The match is optimized in both IF modes by adjusting L2 (2nd MIXER MATCH).

## SECOND CONVERTER ASSEMBLY A5, TROUBLESHOOTING

Verify that the Second Converter Assembly A5 supply voltages are correct.
If the displayed signal amplitude varies between ALT IF and REG IF, perform and verify the bandpass and second LO frequency adjustments.

Second LO Frequency: A failure in the Second Converter Filter Assembly A5A2 can cause the Second Converter Oscillator A5A1 to oscillate at about 3 GHz . This symptom can occur when the delay circuit in the filter assembly does not delay the application of the +13 V bias voltage. To test the delay, observe the +13 V bias as the instrument is turned on. There should be a noticeable delay before the +13 V is applied to the line. The -10 V supply, on the other hand, should rise gradually. If the +13 V and the -10 V respond properly, check the varactor voltage, varactor diodes, and the cavity adjustment as the possible source of the second LO frequency error.

Second LO Fails to Oscillate: The Second Converter Oscillator Assembly A5A1 can intermittently fail to oscillate after turn-on. If this symptom occurs, replace the entire assembly. Before removing the defective circuit board, note the orientation of components, leads, and hardware; orientation is critical to proper operation. To prevent damage to the replacement circuit board, do not over-tighten the hex-head antenna screw during installation.

Second Converter Bandpass Shape: Low signal power from the First Mixer Assembly A4 can distort the second converter bandpass filter shape. Excessive ripple in the bandpass can be the result of a mismatch in the signal path preceding the Second Converter Assembly A5. An input attenuator setting of 0 dB can cause such a mismatch. The second converter mixer diode or Mixer Match adjustment can also affect the bandpass ripple.

Residual FM: Residual FM can originate from the Marker Assembly A8 Second LO Driver, which supplies the varactor bias voltage, or from within the second LO itself.

## YIG-TUNED OSCILLATOR ASSEMBLY A6, CIRCUIT DESCRIPTION

The YIG-Tuned Oscillator Assembly A6 consists of three parts: a sealed magnet assembly that encloses the YIG sphere and oscillator; a bias board that uses discrete components to establishthe oscillator and amplifier bias, as well as protect the bias supply from noise and voltage overloads; and a mu-metal magnetic-shield can. Field service of the YIG-Tuned Oscillator Assembly A6 is limited to replacement with a new or factory rebuilt unit.

The YIG-Tuned Oscillator A6 is a transistor thin-film microcircuit. It uses a Yttrium-Iron-Garnet(YIG) sphere as the frequency determining structure. The YIG sphere is placed in the gap of an electromagnet to provide a magnetic tuning structure whose field (and thereby the oscillator's frequency) is linearly proportional to the drive current from the Frequency Control Assembly A7.

The Main coil is used for wide range sweeping and tuning with the coil current varying from approximately 69 mA to 138 mA . The FM coil performs these functions for narrow spans ( $1 \mathrm{MHz} / \mathrm{div}$ and less) with its coil current varying from approximately -18 mA to +18 mA .

## YIG-TUNED OSCILLATOR ASSEMBLY A6, TROUBLESHOOTING

Power Holes: Power holes that occur at the same point of the sweep in all bands are most commonly caused by the YIG-Tuned Oscillator Assembly A6.

Power holes above 18 GHz are most commonly caused by the type-N RF input connector on the HP 8559A front panel.

Residual FM: The primary cause of residual FM involving the first LO is the Frequency Control Assembly A7.

TABLE8-3. RFSECTION, REPLACEABLEPARTS


Bes]e


| Reference <br> Designation | HP Part <br> Number | Qty | Description | Mfr. <br> Code | Mfr. Part <br> Number |
| :---: | :---: | :---: | :--- | :---: | :---: |
| J2 | $86290-60005$ | 1 | Connector Assy (Type N) | 28480 | $86290-60005$ |
| J2MP1 | $1250-0914$ | 1 | Body: RF Connector (Type N) | 02660 | $131-150$ |
| J2MP2 | $1250-0915$ | 1 | Contact: RF Connector (Type N) | 02660 | $131-149$ |
| J2MP3 | $5040-0306$ | 1 | Insulator | 28480 | $5040-0306$ |
| J2MP4 | $08555-20093$ | 1 | Center Conductor | 28480 | $08555-20093$ |
| J2MP5 | $08555-20094$ | 1 | Body: Bulkhead | 28480 | $08555-20094$ |
| J2MP6 | $2190-0104$ | 1 | Washer: Lock 0.439" ID | 0000 | OBD |
| J2MP7 | $2950-0132$ | 1 | Nut: Hex 7/16-28 | 0000 | OBD |
| J2MP8 | $08761-2027$ | 1 | Insulator | 28480 | $08761-2027$ |
|  |  |  |  |  |  |

FIGURE8-16. RF INPUTCONNECTORJ2


FIGURE8-17. INPUT ATTENUATOR ASSEMBLYA3


FIGURE8-18. 3dB ATTENUATOR ASSEMBLY


FIGURE 8-19. FIRST MIXER ASSEMBLY A4


FIGURE 8-20. 4.8GHzLOWPASS FILTER ASSEMBLY FL1



FIGURE 8-21. SECONDCONVERTER ASSEMBLY A5, COMPONENTLOCATIONS(10F2)


A5A2
SECOND CONVERTER FILTER ASSEMBLY


FIGURE8-21. SECONDCONVERTERASSEMBLYA5, COMPONENT LOCATIONS(2OF 2)


FIGURE8-22. YIG-TUNED OSCILLATORASSEMBLY A6 AND SHIELDCOMPONENTS


FIGURE8-23. RF SECTION, BLOCK DIAGRAM


FIGURE8-24. RF SECTION,COMPONENTLOCATIONS


## FREQUENCY CONTROL ASSEMBLY A7, CIRCUIT DESCRIPTION

The Frequency Control Assembly A7 drives the YIG-Tuned Oscillator Assembly A6 and provides the regulated +14.5 V and -10 V supplies to the First Mixer Assembly A4, the Second Converter Assembly A5, and the Marker Assembly A8. Inputs to the Frequency Control Assembly A7 consist of the tuning voltage and the band information from the Front Switch Assembly A2, as well as the attenuated sweep from the Marker Assembly A8. The tuning voltage is routed to the Marker Assembly A8 while the sweep plus tune $(\mathrm{S}+\mathrm{T})$ voltage goes to the Step Gain Assembly A12 and Vertical Driver/Blanking Assembly A15. The YIG Tune Voltage (YTV) is applied to the biasing circuitry of the YIG-Tuned Oscillator Assembly A6.

## Tune/Full Span Voltage (B)

Coarse and fine tune voltages from the front panel are summed and buffered by U12 and resistors R77, R78, and R79. This summed voltage is routed to the YTO Main Coil Tune Driver through Q13. It is also routed to the Marker Assembly A8 to be conditioned for the Digital Panel Meter Assembly A1. Resistors R64 and R65 divide the -10 V supply to develop -5 V at the noninverting input of U11, which buffers the voltage for use as the mid-band tune voltage required for full sweep operation.

With the selection of full sweep operation, P1-41 (FS9) goes to +15 V and Q11 turns off. Without current flowing in R90, Q10 is off. This allows Q9 to turn on because Q10 no longer supplies the positive gate-source voltage that holds Q9 off. At the same time, Q12 turns on, shutting Q13 off. This routes the -5 V supplied by U11 to the YTO Main Coil Tune Driver tuning the YTO to mid-band. When full band is not selected, P1-41 (FS9) is close to ground potential due to A8CR19, A8R91, and A8R92, on the Marker Assembly A8 (block B). This results in Q10 turning on, holding Q9 off. Transistor A12 is now turned off, removing the pinch-off voltage on Q13. The tune voltage from the front panel now adjusts the YTO center frequency.

## YTO Main Coil Tune Driver (D)

Operational amplifier U10 and resistors R61, R62, R72, R76, R80, and R82 sum and offset the applied tuning and sweep voltages and convert them to the current required to tune the YTO. The current is set by the voltage across R 48 and the 6 GHz adjustment R47. Shaping of the voltage-to-current function is necessary to maintain the linearity of the YTO sweep. This shaping is accomplished by using CRS, in conjunction with R59* and R60*, to establish two break points in the sweep ramp. MOSFET Q8 adds current drive capacity to the output of U10. Offset and buffering of the sweep plus tune voltage takes place in U9. It supplies the sweep plus tune voltage to the limit comparator on the Vertical Driver/Blanking Assembly A15 and to the first converter band tilt circuit on the Step Gain Assembly A12. Operational amplifier U9b supplies the YIG Tune Voltage (YTV) at IV per GHz to the biasing circuitry of the YTO. This adjusts the YTO, controlling its harmonic output. Delay compensation for main coil sweeps is provided by C12* and R58.

## FM/Main Coil Sweep Switch (A)

Quad switch U15 routes the attenuated sweep ramp to the YTO Main Coil Tune Driver or to the YTO FM Coil Driver while grounding the unused inputs. Transistor Q16 provides level shift for the switch drive and is controlled by the FREQ SPAN/DIV control.

## YTO FM Coil Driver (G)

The YTO FM Coil Driver sweeps the YTO in spanwidths of 1 MHz per division and narrower. Operational amplifier U13 inverts the sweep voltage and drives the push-pull current driver comprising Q14 and Q15.

Resistor R92 is an adjustable current limiter that makes possible sweep width adjustment by changing the gain of the stage. Delay compensation for FM coil swept spans is provided by U14, C14, R96*, and potentiometer R83, the delay compensation adjustment.

## YTO Main Coil Fixed Driver (F)

This driver supplies current to the YTO main coil to set the start frequency of the first LO (YIG-Tuned Oscillator Assembly A6) at approximately 3 GHz . Resistor R8 adjusts this frequency by changing the reference voltage at U3 and, therefore, the drive to Q5. MOSFET Q5 buffers the operational amplifier's output and supplies current drive to the YTO main coil.

## Alternate IF Driver (YTO) (C)

A voltage divider, R18 and R19, form a nominal +5 V source that supplies U 7 and establishes pull-up voltages on the H2, H3, and PM lines. When alternate IF is selected, current to the YTO main coil changes, shifting the sweep-center frequencies by $\pm 15 \mathrm{MHz} / \mathrm{N}$, where N is the harmonic number associated with the selected band. Four-to-ten-line decoder U4 decodes front panel band information and activates the appropriate section of U1. This selects the resistor that is paralleled with R9 in the YTO Main Coil Fixed Driver. Altering the effective resistance of R9 changes the current drive to the YTO main coil by changing the gain of the YTO Main Coil Driver circuit.

## YTO Main Coil Filter (E)

When FM coil spans ( $<1 \mathrm{MHz} /$ div) are selected, A16Q1 connects A16C22 (both located on the motherboard) across the main coil of the YTO to filter noise and line related signals. During wide spans ( $>1 \mathrm{MHz} / \mathrm{div}$ ), the charge on A 16 C 22 is maintained by U5, Q1, Q3, and associated circuitry. Diodes CR3 and VR1 protect the filter from excessive back EMF (electromotive force) generated by the YTO.

## Voltage Regulators (H) (I) (K)

Precision, temperature compensated, zener diode VR2 provides the reference for the voltage regulators. The output of the +14.5 V supply is fed back through R39 to bias VR2, while VR3 ensures that VR2 initially turns on. Transistor Q4 is a series pass element driven by U6 and Q5, while R35, R40, and R41 sample the output voltage and provide adjustment.

The -12 V supply tracks the +14.5 V supply and consists of a pass element, Q 7 , driven by U 8 .
The -10 V regulator supplies the voltage to the TUNING control, and is heavily filtered by C3 and R33. Transistor Q6 is the series pass element driven by U7 and resistor R29 adjusts the output voltage level.

## FREQUENCY CONTROL ASSEMBLY A7, TROUBLESHOOTING

The Frequency Control Assembly A7 is the principal cause of excessive residual FM of the YIG-Tuned Oscillator's output. The following are a series of tests to help isolate the source of FM to a function block on the Frequency Control Assembly. Components most likely to be the source of the FM in each block are also listed. Be sure to check the following power supply voltages, for correct level and excessive ripple, before proceeding: the +14.5 V Regulator (block H), the -10 V Regulator (block I), the -12 V Regulator (block K), and the +15 V and - 12.6V Power Supplies (block J).

## RESIDUAL FM TROUBLESHOOTING FLOWCHART ANNOTATION


#### Abstract

CAUTION In the next steps, edge connector contacts on the circuit board are taped over to isolate portions of the circuit. After completing a step where taping is necessary, remove the tape and clean the circuit board edge contacts with an 80120 solution of isopropyl alcohol and water before continuing to the next step. Refer to PRINTED CIRCUIT BOARD EDGE CONNECTOR CONTACT CLEANING at the beginning of this section for a detailed description of the cleaning procedure. Care should also be taken whenever instructed to unsolder components during the test.


Set HP 8559A controls as follows:
FREQUENCY BAND GHz .....  $01-3$
TUNING ..... 010 GHz
FREQ SPAN/DIV ..... 0
RESOLUTIONBW ..... 300 kHz
INPUTATTEN ..... 0 dB
REFERENCE LEVEL ..... $-10 \mathrm{~dB}$
REFLEVELFINE ..... 0
Amplitude Scale ..... $10 \mathrm{~dB} / \mathrm{DIV}$
SWEEP TIME/DIV ..... AUTO
SWEEP TRIGGER ..... SINGLE
VIDEOFILTER ..... OFF
BLCLIP ..... OFF
SIGIDENT ..... OFF
ALTIF ..... OFF

## NOTE

Use the Residual FM Troubleshooting Flowchart to guide you through the test. Refer to this annotation as indicated by the steps in the flowchart.
a. To observe the first LO, connect a second spectrum analyzer to the HP 8559A RF input (a significant fraction of the first LO power is coupled to the RF input by the First Mixer Assembly A4). When measured in this manner, the first LO power should be $-8 \mathrm{dBm} t 3 \mathrm{dBm}$ at about 3 GHz for the listed control settings. This setup is used to observe the first LO in all of the following tests.
b. Begin by isolating the YTO Main Coil Tune Driver from the remainder of the frequency control circuit. This is accomplished by taping over $\mathrm{P} 1-3$ on the circuit board edge-connector contacts.
c. If the residual FM is unchanged, assume that the YTO Main Coil Tune Driver and the circuits feeding it are not the source of FM. The next step is to isolate the YTO FM Coil Driver from the circuit by taping over PI-15 and P1-37.
d. If the residual FM is unchanged, assume that the YTO FM Coil Driver is not the source. Proceed by placing a short across C1. This isolates the YTO Main Coil Fixed Driver from the circuit. Since the YTO Main Coil Fixed Driver supplies the majority of the YTO operating current, the YTO will not operate when the YTO Main Coil Fixed Driver is isolated from the circuit. To compensate for this, it is necessary to increase the current supplied by the YTO Main Coil Tune Driver. Adjust the TUNING control of the HP 8559A under test for a frequency display of 3 GHz ; this supplies enough current from the YTO Main Coil Tune Driver to allow the YTO to oscillate at about 3 GHz .

e. If the residual FM is unchanged, assume that the YTO Main Coil Fixed Driver is not its source. Retune the HP 8559A to minimum, .010 GHz . Isolate the YTO Main Coil Filter from the circuit by mounting the Frequency Control Assembly A7 on an extender board and taping over P1-19, P1-20, P1-25, while shorting P1-2 to P1-19.
f. If the residual FM is unchanged, the probable source is the YIG-Tuned Oscillator Assembly A6.
g. If isolating the YTO Main Coil Tune Driver from the frequency control circuit eliminates the residual FM, proceed to further isolate the source by shorting the sweep from block A to ground. This is best accomplished by shorting the input side of R80 to the ground side of R63. Use a short jumper to prevent the induction of line frequency noise into the circuit.
h. If the residual FM is eliminated, the source is probably the FM/Main Coil Sweep Switch. The most common failure is U15.
i. If residual FM is present after shorting the input sweep, remove the jumper and substitute a battery for the tune voltage. Do this by carefully unsoldering the input side of R82 and inserting a battery ( 5 V to 10 V ) between the free end of R82 (the " - " terminal) and the grounded end of R63 (the " + " terminal). Use the shortest possible leads to prevent line frequency noise pickup.
j. If residual FM is unchanged, the probable source is the YTO Main Coil Tune Driver. The most common failures are: U10, R72, R76, R61, R80, R63, and R62, in that order.
k. In this step, the -10 V regulator is replaced with a battery. Replace R82 and tape over P1-5. Attach the negative ( - ) battery lead to pin 3 of U12; attach the positive $(+)$ lead to the grounded end of R63. If the residual FM is eliminated, the probable source is the Tune/Full Span Voltage (block B). If the residual FM is unchanged, remove the battery and the tape. Tune the FINE TUNE control to minimum, remover the (945) wire from the COARSE TUNE control (A2R1), and attach the battery's negative ( - ) lead to the COARSE TUNE control in place of the (945) wire. Attach the positive (+) battery lead to the ground side of R63. This test is necessary to eliminate the TUNING control as a source of residual FM.

1. If using the battery in place of the -10 V regulator eliminates residual FM , the -10 V regulator is the probable source. All of the regulator parts can cause instability; however, the most common failures are: U7, R30, R33, R32, C3, R29, and VR2 (block H), in that order. Also, verify that all supplies are properly adjusted.
m. If the Tune/Full Span Voltage (block B) is the probable source of the FM, the most common failures are U12 and Q13.
n. If isolating the YTO FM Coil Driver eliminates the residual FM, short the incoming sweep to ground. Install a jumper between the input side of R97 and the ground side of R95. Use the shortest possible lead to minimize line frequency noise pickup.
o. If the residual FM is unchanged, the source is probably the YTO FM Coil Driver. The most common failures are U13 and U14.
p. If the residual FM is eliminated, the source is probably the FM/Main Coil Sweep Switch. The most common failure is U15. If the residual FM is unchanged, short TP8 to ground. If this eliminates the residual FM, the source is probably on the Marker Assembly A8.
q. If isolating the YTO Main Coil Fixed Driver eliminates the residual FM, it is probably the source of the FM. The most common failures are: U2, C1, R1, and R2, in that order.
r. If removing the YTO Main Coil Filter from the circuit eliminates residual FM, it is probably the source of the FM. The most common failure is Q5. If the FM is not eliminated, the most common failures are A16Q1 and A16C22.

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TABLE 8-4. FREQUENCY CONTROL ASSEMBLY A7, REPLACEABLE PARTS (1 OF 3)

| Reference Designation | HP Part Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A7 | 00559-60377 | 3 | 1 | FRESENEY CONTRDL ASSEMEIT | ว-3 8 \% | -8559-69077 |
| A7C1 | 0180-0180 | 3 | 1 | CAPACITOR-FXR 4.7UF+-10\% 3FSUC TA | 5seag | $150 n 475 \times 903562$ |
| A7CL | 3169-4384 | ${ }^{8}$ | ? |  | 28433 | 016.4084 |
| A7C3 A7C4 | ¢180-2207 $3180-3197$ | 5 | 1 $?$ |  | 56.739 <br> 56259 |  |
| A7C5 | C. 160-4810 | 8 | 1 | CAPACITOR-FXO 330CT +-5\% 16GUDC CER | 20400 | 01664810 |
| A7C6 | 3183-1746 | 5 | 3 | CAPARITIR-FXD 15UF-13\% RavEC TA | 56257 | 159D156×9023:12 |
|  | c160-3457 31603661 | 7 | 1 | CAPACITOS-FXD CAPGCITR-F S | -23480 | $8160-3457$ $3160-3661$ |
| A7CB ATC9 | 31603661 $0180-0197$ | S | 1 |  | -8483 5R.289 | $3169-3661$ $1505235 \times 9026 A 2$ |
| A7C13 | 2183-1746 | 5 |  | CAPACTTCR-5×D 151F-13\% 20VCC TA | 5.8269 | $15.30156 \times 902058$ |
| A7C11 | 0180-1746 | 5 |  | CAPACITOR-FXD 15AF+-10x 2CUDC TA | 55.089 | 1505156x9020ni |
| A7C12x | 0180-3291 | 3 | 1 | CAPAM:ITOR-F XO 1UF,-10\% 35VLC. TA | 56289 | $1530135 \times 9035.82$ |
|  | $0160-4812$ $7160-4984$ | - | 1 |  | ? ${ }^{2+868}$ | 0160.4812 $3163-4384$ |
| A7CR1 | 1901-6518 | 8 | 2 | DIODE SM SIC Schotiky | 2a4ac | 1961.0518 |
| a7cre | 1731-0518 | 日 |  | DIODE SM SLG Echintiky | [3480 | 1731-0518 |
| A7CR3 | 1901-0058 | 3 | 7 | DITDE- SWITCHING B6U 26ema 2 Na do-35 | 32480 | 1761-0050 |
| A7CR4 | 1701-3358 | 3 |  |  | 28480 | 1931-0350 |
| ATCRS | 1961-0650 | 3 |  | DIDDE-SWITCHING BGU 26GKA 2 NS do 35 | Ра480 | 1701-0050 |
| ATCR6 A7CR7 | $1731-0350$ $1961-0050$ | 3 |  |  | 28483 20480 | 1931-0350 |
| A7CR7 | $1961-0650$ $1701-2959$ | 3 3 3 |  |  | 23480 | 19610050 $1791-0350$ |
| ATCR9 | 1901-0640 | 1 | 2 | dTODE SNITCHING 300 SOMA 2 NS do-35 | ааяво | 1201-004n |
| A/CR13 | 1701-0048 | 1 |  | dicte swithling 3.30 53MA :NS to 35 | дея80 | 1731-0040 |
| A7CR11 | 1901-6050 | 3 |  | dIodr sultchinc acu zegha ens da-35 | 23480 | 1981.0050 |
| A731 | 1251-4700 | , | 1 | CONN:CTGR S-PTN M POST TTPE | 72489 | 1:51-4700 |
| A781 | 1855-0420 | 2 | 1 | TRANCISTOR J-FET 2 N4391 N -ChAN D-MODF | 01293 | 204391 |
| A782 | 1855-0251 | 7 | 2 | translsior masfet n-chen e mode, to 37 St | 28483 | 1855-3251 |
| A7Q3 | 1855-0278 | 8 | 1 | TRANGISTOR J-FET 2NS116 P CHAAN D-MAD | 17858 34713 | 2NS116 |
| A789 A705 | 1853-2213 | ? | 1 2 |  | 34713 29480 | 2n4:36 |
| A786 | 1054-3637 | 1 | 3 | TRANSTSTUR NPN ENE219A SI TO 5 PD=0a3M | 31295 | 2 N 2210 A |
| A787 | 1954-0637 | 1 |  | TRANSISTOR NPN 2NP219A St T0-5 PD=36EMAd | 01295 | 2N.2219A |
| A788 | 1855-9251 | 7 |  | TRANSTSTGR MOSFET N CHAN E MODE. TO- 39 St | 20483 | 15,55-0251 |
| A 789 A7819 | $1855-0421$ $1853-0281$ | 3 | 3 | TRANSISTOR J-FET 2NSITA P-CIAN D-MDDE | ${ }_{\substack{17854 \\ 0 \rightarrow 713}}$ |  |
| A7Q11 | 1853-0281 | 9 |  | TRANSISTOR PNP 2N2907A SI TO-18 PD-AGCMW | ¢4713 | 2N.9907A |
| A7912 | 11553-3281 | ${ }^{\circ}$ |  | TRANSTSTGR PNP ZN2907A ST T0-18 PD=400R4 | 34713 | 2182937 A |
| A7013 | 1855-0421 | 3 |  | TRANGISTOP J-FEI 2NS114 P CHAN D-made | 17356 | $2 \mathrm{NS114}$ |
| A7814 A7Q15 | 1653 $1054-0314$ | ? | 1 | TRANSISTGR PNP NNEYASA SI | 34713 01295 | $2122935 A$ 2N1219A |
| A7016 | 1554-3404 | 0 |  | TRANSTSIOR NPN SI TO-18 PD=360ML | 28483 | 11554-9404 |
| ATR1 | 0699-0304 | 8 | 1 |  | 2а480 | 0699-0384 |
| A7R2 | $0679-3900$ $0698-6359$ | 0 2 2 | $!$ |  | 28480 23480 | 3699-0390 |
| A7RS | 3757-0458 | 7 | 1 |  | 24546 | C4 1/8-T0-511: F |
| A7R6 | 0757-0464 | 5 | 1 |  | 24.546 | C4 1/8-70-9097-F |
| ATR ${ }^{\text {ATR }}$ | 9698-6362 | ${ }^{8}$ | 2 | RESISTOR $1 \mathrm{~K}, 1 \%, 12 S \mathrm{~F}$ F $1 \mathrm{C}=01-25$ | 28480 | 36\%8-6,362 |
| A7R8 | 2100-4020 | 8 | 1 |  | 2R480 | $210 \mathrm{Cc}-4020$ |
| A7R A7R10 | ${ }^{0811}$-3581 | ? | 1 |  | 21480 | 3011-3501 |
| A7R11 | 3757-0442 | 9 | 12 |  | 24546 | C4 1/8-T3-1032-F |
| A7R12 | 0757-0465 | 6 |  | RTSISTOR 100k 12 L . 125 L F TC=0+-100 | 24546 | C4-1/8-T0-1003-F |
| A7R13 | 0757-0465 | 6 |  | RESTSTOR 103 K 12.125 .4 T TC=3t-100 | 24546 | C4-1/8-70-1033-F |
| ATR14 ATR15 | 0757-0465 $0757-0465$ | 6 |  |  | 24546 24546 | C4-1/8-T0-16c3-F |
| A7R16 | 0757-0.465 | 6 |  | RESISTOR 100 12 .1254 F TC $=0+160$ | 24546 | C4-1/8-T0-1603-F |
| A7R17 | 0757-0465 | 6 |  |  | 24546 | C4-1/8-T0-1033-F |
| A7R18 ${ }_{\text {A }}$ | 0698-3153 | ? | 1 |  | 24546 | C4-1/8-T0-3831-F |
| ATR20 | 0757-0465 | 6 | 1 | RESISTOR 100 K 12 Z 12SU F TC=0t-100 | 24546 | C4-1/8-TE 1603-F |
| A7R21 | 0698-6320 | 日 | 1 |  | ${ }^{3} 3888$ | PMES5-1/8 - T9-5031-B |
| A7R22 | 0698-8861 | ${ }^{6}$ | 1 | RESISTO9 $6.66 \mathrm{~K} \quad 1 \mathrm{X} \quad 125 \mathrm{~F}$ F TC $=0+25$ | 28480 | 0698-8861 |
| A7R23 | 0698-6614 | 3 | 1 | RESISTUR 7.5K ${ }^{112}$, 125U F $\mathrm{TC}=0+25$ | 28480 | 0698-6614 |
| ATR26 | 0698-6630 | 3 | 1 |  | 284880 28480 | 0678-6619 0630 |
| A7R27 | 0757-0465 | 6 |  | RESTSTOR $100 \mathrm{~K} 1 z, 125 \mathrm{~L}$ F IC $=0+-100$ | 24546 | C4 1/8-T0-1033-F |
| A7R28 | 0757-0465 | 6 |  | RESISTOR 100k 12 y -125W F TC $=0+100$ | 24546 | C4-1/8-70-1003-F |
| A7R29 | 2100-2851 | ? | $?$ | RESISTOR-TRMR 2 K 10x WW SIDE-ADJ 20 TRN | 32660 | 3813P-202 |
| A7R30 A7R31 | 0699-0901 $0757-0382$ | 1 | $\frac{1}{2}$ |  | 28480 19701 | 0699-0901 |
| A7R31 | 0757-0382 |  |  | RESTSTOR 16.2 iz 12SU F TC=0+-100 | 19701 | MFAC1/8-T0-16R2-F |

TABLE 8-4. FREQUENCY CONTROL ASSEMBLY AT, REPLACEABLE PARTS (2OF 3)

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & \mathrm{C} \\ & \mathrm{D} \end{aligned}\right.$ | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A7R32 | 0699-9993 | 3 | 6 |  | 28480 | 3699-3903 |
| A ARP33 | 6699-0903 3757.0418 | 3 | 1 |  | 23480 24546 |  |
| A7R35 | 0811-1175 | 8 | 1 | RESTSTOR 4.22k 12.1254 PWW TC=0,10 | ${ }^{2} 7088$ | kP6, 1-42? 1-1 |
| A7R36 | 3678-0383 | B | 1 |  | 2.4546 | C4 1/8 T0-1961-F |
| A7837 | 0757-0438 | 3 | 2 |  | 24546 | C4. 1/8-70 S $5111-\mathrm{F}$ |
| A7838 | 3757. 94:8 | ${ }_{7}^{1}$ | 1 |  | 21546 | C4 1/8-73-1621 F |
| A7R A 784 | 0757-0424 3011 | 7 | 1 |  | 24596 23719 |  |
| A7R41 | 2100-3123 | 0 | 1 | RESISTOP-TRMR 50 E 10\% C GIDF-ADS 17 -TRN | 05111 | 43 F 501 |
| A7R42 | 3678-636.2 | - |  |  | 20483 | 3698-6362 |
| ATR43 | 06998-6360 | ${ }^{6}$ |  | RESISTIR $10 \mathrm{k}, 1 \mathrm{z}, 125 \mathrm{~L} \mathrm{~F}^{\text {F }}$ TC $=0+25$ | 28486 | 8699 6360 |
|  | 3757. 3444 | $\stackrel{1}{9}$ | 1 |  | 24546 | C4-1/8-10-121.-F |
| ATR4S | - $\begin{aligned} & 6757-0442 \\ & 3757-6382\end{aligned}$ | 9 |  |  | 24546 19731 |  |
| ATP47 | 2100-1753 | ${ }^{8}$ | 1 | RESTSTOR-TFMR 20.52 Wh Stide Ad. 1-TEN | 28480 | 2 men 1753 |
| A7R48 | 3811-3472 | 1 | 1 | PRSISTIER 133 1\% 126 PW TC=3+2 | 78483 | 3811-3492 |
| A 7 RA9 | 0757-0230 | 3 | 2 |  | 24:46 | C4-1/8-70-166, -F |
| ATR51 | 0698-3136 | 8 | 1 |  | 24546 24546 | C4-1/8-T0 1782.F |
| A7REs | 9757-0317 | ? | 1 |  | 24546 | C4 1/8- T9-1331-5 |
| A7R53 | 6698-3160 | 8 | 2 |  | 24546 24546 | C4. 1/8-76-316. C |
| ${ }_{\text {ATR5S }}$ | 6.693-0685 | ? | 2 |  | 24546 24546 |  |
| A7RS6 | 0757-0421 | 4 | 1 | PEGISTGR BES 12 , 1254 F TE=3t-133 | 24596 |  |
| ${ }_{\text {A }}^{\text {ATR5 }}$ A | 6757-0442 | 9 |  |  | 24546 24546 | [4-1/8-TC-166: F |
| ATRS日 | 3757-0279 $0757-0459$ | \% | 1 |  | 24546 24596 |  |
| A726a* | 0678-3454 | ${ }_{3}^{8}$ | 1 |  | 24546 | C4 1/8- Tn -2153-F |
| A7R61 | 6699-0903 | 3 |  | RCSISTOR 16K 12 z , 1W F TC=6 +10 | 28480 | 0695-0903 |
| A7R62 | 3698-3456 | 5 | 2 |  | 24546 | C4 1/8-T0-2873-F |
| A AR63 Pr | $0679-3456$ $3757-0442$ | $\stackrel{5}{9}$ |  |  | 24.46 24546 | $\mathrm{CA}-1 / 8-\mathrm{TC}-2873-\mathrm{F}$ $\mathrm{CA} 1 / 8-\mathrm{Ta}-1002 \mathrm{~F}$ |
| A7R6S | 1757-0442 | 9 |  | RESISTOR 10K 12.125 F F TE=0 + - 100 | 34546 | C4 1/8-TC-16.62-F |
| A7R66 | 3757-0442 | 9 |  | RESTSTOR $13 \mathrm{~K} \quad 1 \mathrm{~K}, 125 \mathrm{~W}$ F $\mathrm{TC}=0+-103$ | 245.46 | CA - 1/8- Ta-1002 F $^{\text {c }}$ |
| A7R67 | 0696-3156 | 2 | 1 |  | 24:56 | C4-1/8-T0 1472-F |
| A7R68 | 3698-3450 | ? |  |  | 24546 | C4 1/8 T3-422e-F |
| A7R69 A | $0757-0442$ $0696-0035$ | $\stackrel{\square}{9}$ |  |  | 24546 24546 |  |
| A7R71 | 0699-3442 | 9 | 2 | RESISTOP 237 1\% .125W F TCmet-160 | 245.46 | C4 1/8-т0 - 237P-F |
| A7R72 | 0699-3903 | 3 |  |  | 28430 | 0699-3903 |
| A7R73 | 0757-0442 | 9 |  | RESISTOR ${ }^{\text {EK }}$ L $1 \%$, 125W F TE $=0+100$ | 24546 | C4 1/8-T6-1662 F |
| A) ${ }^{\text {A } 74}$ | 3757-0442 | 9 |  | RESISTIR $10 \mathrm{~K} 1 \%$, 125 W F TC- $=0+103$ | 24546 | C4 1/8-50-1002-F |
| A7R75 | 2100-2851 | 9 |  | RESISTOR-TRMR 2 K 10\% HL SIDE ADJ 20-TRN | 02660 | $3810 \mathrm{P}-202$ |
| A7R76 | 0697-0903 | 3 |  | RESTSTOR 10K .1\% , 14 F $1 \mathrm{C}=3+-13$ | 28483 | 3699-0903 |
| ATRT7 | 0698-3260 | , | 4 |  | 2 P 480 | 06933260 |
| A7R78 ATR79 | $0.978-3160$ $0757-0280$ | 9 3 |  |  | 24546 24546 | C4-1/8-T0-3162-F $\mathrm{C4-1/8-T8-1061-F}$ |
| A7R日 | 0679-3703 | 3 |  | RESISTIR 1aK 1 z , 14 F TC=0+-13 | 28480 | ${ }_{0699-3903}$ |
| A7R81 | 2100-3053 | 5 | 1 | RESIGTOR-TRMR 20202 C SIDF-ADJ 17 TRN | 02111 | 43P200 |
| A7RR2 | 0698-3442 | 7 |  |  | 24546 | C.4-1/R-T0-23/R-F |
| ATR83 A 7 Re4 | $2100-3054$ $0757-0465$ | 6 | 1 |  | 0.2111 24546 | ${ }_{\text {C4-1/8-T0-1093-F }}$ |
| ATR85 | 0757-0465 | 6 |  | RESISTOR 100k $1 \%$, 125W F TC=0+100 | 24546 | C4-1/8-70-1003-F |
| A7R86 | 0690-3260 | 9 |  | RESISTOR 464K 1 K , 125W F TC=04-100 | 28480 | 0678-3260 |
| A 7 AR87 ATREB | $0757-0465$ $0698-3260$ | 6 9 |  |  | 24.46 28480 | $\begin{aligned} & \text { C. } 1 / 8-T 0-1003-F \end{aligned}$ |
| A7R89 | 0757-0438 | 3 |  | RESISTOR 5.11 K 1 X . 125 SW F TC=0,-100 | 24546 | C4-1/8-T0-5111-F |
| A7R90 | 3757-0465 | 6 |  |  | 24546 | C4-1/8-70-1003-F |
| A7R91 | 0698-3? 60 | 9 |  | RESISTOR 464k 12.125 F F TC= $0+-180$ | 28480 | 0698-3260 |
| A7R92 | 2100-1756 | 1 | 1 | RESTGTUR-TRMR 2005 S WU SIDE-ADJ 1-TRN | 28480 | $2100-1756$ |
| A7R93 | 0698-3622 | 7 | 1 | RESISTOR 120 5\%, $24 . \mathrm{MO}$ TCOOT-200 | 28480 | 06983622 |
| ${ }^{\text {A }}$ AR94 | 0698-7212 | 9 | 1 |  | 24546 19701 | C3-1/B-T0-103R-F |
| A7R96* | 0757-0462 | 3 | 1 | RESISTOR 7SK 1 K , 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-7502-F |
| ATR97 A7R93 | $0757-0.990$ $0757-0401$ | 5 | 1 |  | 19701 24546 | MF AC1/8-T0-6191-F C4-1/3-T0-101 F |
| A7R99 | 0757-0290 | 5 |  | RESISTOR 6.19k 1 z . 12 SW F TC $=0+-100$ | 19701 | MFAC1/8-T0-6191-F |
| A7R100 | 0757-0290 | 5 |  | RESTSTOR 6.19 K , 12.125 L F $\mathrm{TC}=0+-100$ | 19701 | MF4C1/8-T0-6191-F |
| A7R101 | 0757-0465 | 6 |  | RESISTOR 100 K 12.125 W F TC $=0+\cdots 100$ | 24546 | C.4-1/8-T0-1003-F |
| A7R102 | 0678-3428 | 1 | 2 | RESISTOR 14.7 $12 \mathrm{X}, 1254 \mathrm{~F}$ TC $=0+100$ | 038888 | PMES5-1/8-TO-14R7-F |
| ATR103 A7R104 | $0698-3428$ $0757-0442$ | $\stackrel{1}{6}$ |  |  | 03488 24546 | PMESS-1/8-10 1427-F $C 4-1 / 8-T 0-1002-F$ |
| A7R105 | 06.98-3157 | 3 | 1 | RESISTOR 19.6k 1 X , 1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-1962-F |
| A7R106* | 0698-3450 | ? | 3 | RESISTOR 42.2K 12 .125W F TC=0+-103 | 24546 | C4-1/8-T0-4222-F |

TABLE 8-4. FREQUENCYCONTROLASSEMBLY A7, REPLACEABLEPARTS (30F3)


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FIGURE 827. FREQUENCYCONTROLASSEMBLY A7, BLOCKDIAGRAM


FIGURE8-28. FREQUENCY CONTROLASSEMBLY A7, COMPONENT LOCATIONS




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## MARKER ASSEMBLY A8, CIRCUIT DESCRIPTION

The Marker Assembly A8 comprises the Marker Generator, the DPM and Second LO Drivers, the ALT IF and SIG IDENT circuits, the Auto Scan Time Drivers, and the Scan Attenuators.

## Marker Generator (F)

The Marker Generator is basically a zero voltage detector. The four summed resistor voltages at pin 5 of U14 equal OV only when the sweep voltage and the tune voltage correspond to the same frequency. The marker is then displayed at that frequency. If the input of $\mathrm{U} 14 \mathrm{~b}(\operatorname{pin} 5)$ is at 0 V , the outputs (pins 7 and 1 ) should be at 0 V . The anodes of CR7 and CR10 should therefore be at OV also. Resistor R45 pulls their cathodes down to about -0.5 V . This turns on U 6 c , which normally has its emitter held to about $+0.7 \mathrm{~V}(+1.2 \mathrm{~V}$ in fullband). As the emitter voltage of U6c increases, it turns on Q1. This pulls the video shift line down, shifting the signal and noise at the Log Amplifier Assembly A14 about one division toward the bottom of the screen. The output of the Log Amplifier Assembly A14 is permitted to be pulled low by the log shift resistor (A14R119) at its output.

## DPM Driver (D)

The DPM Driver is an inverting operational amplifier circuit. The appropriate combination of input, offset, and feedback resistors is selected by U5 for the chosen frequency band (see Figure 8-30). Input control lines H2, H3, and PM carry the encoded band information. A truth table on the schematic, Figure 8-33, shows the levels of these lines during each band.


| Band | R Input | R offset | R Feedback $^{\text {1 }} 10$ R64 |
| :---: | :---: | :---: | :---: |
| 2 | R67 | R68 | R66 |
| 3 | R70 | R71 | R72 |
| 4 | R73 | R74 | R75 |
| 5 | R76 | R77 | R78 |
| 6 | R79 | R80 | R81 |

## Second LO Driver (E)

The Second LO Driver varies the voltage applied to the varactors in the second LO cavity (A5CR2 and A5CR3). The upper limit of this voltage is dependent on the second LO sensitivity and varies during operation from about IV to between 7 V and 30 V . An increase in the drive voltage increases the second LO frequency. The SIG IDENT and ALT IF buttons both change the second LO frequency.

ALT IF. When ALT IF is not selected, TP2 is at -7.5 V , setting the collector of Q 2 to $+15 \mathrm{~V}( \pm 7 \mathrm{~V})$. When ALT IF is selected, TP2 goes to -2.5 V , setting the base of Q 2 to about +5 V . The voltage on the collector of Q2 varies within the range of 1 V to 28 V as needed to drive the varactors in the Second Converter Assembly A5. The shift in drive voltage serves to offset the second LO to the alternate IF.

SIG IDENT. When SIG IDENT is not selected, U10 pin 4 is low and pin 11 is high. This supplies a current through R37 and R38 to bias the second LO 1 MHz away from its minimum frequency. When SIG IDENT is selected, pins 4 and 11 both are either high or low together, depending on the sense of the PM line (PM is low for bands 1, 3, and 5). This either raises or lowers the frequency of the second LO 1 MHz . Resistor R39 provides additional shift, if necessary, when ALT IF is not activated (the second LO may be less sensitive at that frequency). Flip-flop U3 alternates both the frequency shift and level shift on every other retrace.

## Auto Scan Time (AST) Drivers (C)

As scan and bands change, sweep times must be changed to maintain amplitude calibration. The AST (auto scan time) line, which goes to the Sweep Generator/Bandwidth Control Assembly A9, varies the sweep time by varying the amount of current it carries. More current speeds the sweep rate, less current slows it. The current is controlled through a current mirror on the Marker Assembly A8, comprising U6a and U6d. The current mirror is a common-emitter amplifier with a current gain of -1 . Collector current changes through U6a (caused by U11a, U11b, or U11c turning on) are mirrored in U6d.

## Scan Attenuator (B)

Operational amplifiers U13 and U17 are buffer amplifiers that are not directly involved in the switchable scan attenuation, but, if one fails, the scan becomes uncalibrated. The switching is done by Q4, Q6, and U12. For fundamental mixing bands 1 and 2, U12b is on, all others are off. Resistors R22 and R23 form a voltage divider with R24, R25, and R26. The division ratio is changed depending on whether Q4 and Q6 are on or off. For higher mixing modes (bands 3 through 6), U12a or U12d is switched on, picking off the sweep from a lower amplitude point on the voltage divider. For full span operation, U12c is enabled so that no attenuation is added for higher mixing modes.

## MARKER ASSEMBLY A8, TROUBLESHOOTING

DPM Accuracy: DPM inaccuracy is often traceable to the calibrated-gain circuit in the DPM Driver (block D). The most common cause is the gain determining resistors associated with U15. A generalized model of U15, with associated resistors, is shown as Figure 8-30. Variations in the input resistors or in the feedback resistors will cause DPM inaccuracies throughout its range. Offset resistor variations primarily affect the low end of the range. When troubleshooting DPM inaccuracies, always start with the components related to the worst band.

Marker Accuracy: The marker accuracy is dependent on the frequency accuracy of the first LO and the frequency accuracy of its sweep end-points (i.e., the frequencies that correspond to the $\pm 5 \mathrm{~V}$ extremes of the sweep).

Spanwidth Accuracy: Observe the positions of the FREQ SPAN/DIV switch and how they relate to the spanwidth errors. The problem could be originating from either the Marker Assembly A8 or the Sweep Generator/Bandwidth Control Assembly A9 or both.

Auto Scan Time (AST) Accuracy: Observe front panel switch positions to isolate the problem area. Auto scan time can also be affected by circuits on the Sweep Generator/Bandwidth Control Assembly A9 and the VIDEO FILTER control position. If the AST problem is band-related, the Marker Assembly A8 is the most probable cause. If the AST problem is either bandwidth- or scanwidth-related, the most probable cause is the Sweep Generator/Bandwidth Control Assembly A9. The greater the load on the AST line, the greater the current demand. The greater the current demand, the faster the sweep rate.

Residual FM: Residual FM can originate from the Second LO Driver (block E). The most common failures are: R88, R87, R33, R34, U1, U7, R37, and R38, in that order.

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TABLE 8-5. MARKER ASSEMBLY A8, REPLACEABLE PARTS (10F 3)


TABLE 8-5. MARKER ASSEMBLY A8, REPLACEABLE PARTS (2OF3)

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Reference Designation \& HP Part Number \& $$
\begin{aligned}
& \mathbf{C} \\
& \mathrm{D}
\end{aligned}
$$ \& Qty \& Description \& Mfr Code \& Mfr Part Number <br>
\hline AmR4 \& 37570442 \& $?$ \& \&  \& 24546 \& C4- - /3-T3 1032-F <br>
\hline  \& $0698-7794$
0757
0.442 \& 2
7 \& 2 \&  \& 19761

29546 \&  <br>
\hline AOPR 44 \& -6698-3160 \& 8 \& 3 \&  \& 24546
24546 \&  <br>
\hline criras \& 3757-1465 \& 6 \& \&  \& 24546 \& C4 1/8-13 1303-r <br>
\hline ${ }^{\text {AtiR }} 46$ \& 8757-0465 \& ${ }_{7}$ \& \&  \& . 24596 \& C4 1/8-Ta 16.5-f <br>
\hline EERR 47
ABR 43 \& 06985416
$6688-3458$ \& 7 \& 1 \&  \& 23489
23680 \& $7678-5.446$
6. 0.37 .3450 <br>
\hline Actisiv \& 2690-3163 \& B \& \& RESTSTOR 34.ck $1 \%, 1854$ F $\quad 1 \%=3+-109$ \& ${ }_{2}^{245460}$ \& CA 1/8-73-3162-F <br>
\hline AB250 \& -698-0094 \& 9 \& 1 \& RLSISTOR 2.15\% $1 \%$, 125 \% F TC=04-166 \& 24546 \& C.4 1/8-T6-2151-F <br>
\hline Atirs ${ }^{\text {a }}$ \& ${ }^{9659} 0 \cdot 3157$ \& 3 \& \&  \& 24546 \& Cs 1/8-13-196.2-F <br>
\hline  \& $6699-3157$
$3757-0465$ \& 3
6
6 \& \&  \& 24546 \& C4 1/8-TE 126.a F <br>
\hline ${ }_{\text {ATR }}$ \& 3, $3757-0465$ \& 6 \& \& ReStstur 130 ll \& 24546
24546 \&  <br>
\hline f.fREs \& 37570165 \& 6 \& \&  \& 24546 \& ci 1/3-19-1093-F <br>
\hline ARRS 6 \& 0683-3355 \& 2 \& 1 \& RESISTOR 3.3M 5\% .25w FC TC--960/1160 \& 01121 \& cer $3^{5} 5$ <br>
\hline ARRS
ASRSE \& ${ }^{3} 50332255$ \& ? \& 1
3 \&  \& 31121 \&  <br>
\hline ABRSE
AGR5\% \& $06.99-0378$
$0.699-0378$ \& 6 \& 3 \&  \& 26480
20480 \& 06990378
$0699-8378$ <br>
\hline Agr60 \& 6.757-0442 \& 9 \& \&  \& 24594 \& C4 1/8-T0-16ch-F <br>
\hline Ema 61 \& 2100-3161 \& 6 \& \& RESTSTGR-TRMR 23 K 13\% C SDDE-ADJ 17.12 N \& 32111 \& 43 ¢293 <br>
\hline  \& $2160-3161$
3757
0438 \& ${ }_{6}^{6}$ \& \&  \& ${ }_{2}^{2} 2111$ \& $43 \times 263$
$C 61 / 8-50-5111-F$ <br>
\hline  \&  \& 3
9 \& 1
3 \&  \& 24596
284880 \& C4 4 1/8-70-5111-F
06978371 <br>
\hline A6R65 \& 3757-0431 \& 3 \& 2 \&  \& 21546 \& C4 1/8-10-1,31 F <br>
\hline ABR56 \& 0699-6376 \& 4 \& 2 \&  \& 20480 \&  <br>
\hline ABR68 \& $3679-3371$
$0699-0374$ \& ${ }^{2}$ \& 1 \&  \& 20480 \& $\begin{array}{ll}10699 & 6371 \\ 66 \% 9374\end{array}$ <br>
\hline Catir69 \& 36990376 \& 4 \& \& acstatur 11.76 K . $325 \%$, 16 F IC=36 5 \& 28483 \& 3699-0376 <br>
\hline AOR70 \& 8699-0.379 \& 7 \& 3 \& RESISTOR 68.1k .02S\% , 1W F TC=0 - 5 \& 28480 \& 06.9980379 <br>
\hline AnR71
AORT2 \& 069990379 \& ${ }^{8}$ \& 1 \& REGISTIR 196.995k . $225 \%$, 14 F F TC=3, 5 \& -e480 \& 0679-0370 <br>

\hline  \& | $6699-0,375$ |
| :--- |
| 3699 |
| 0371 | \& 3

9 \& 1 \&  \& ${ }^{23480}$ \&  <br>
\hline ASR 74 \& 0699-0372 \& 0 \& 1 \& RESICIOR 100.974 ${ }^{\text {a }}$.025\%, 1W F TC-01-5 \& 23400 \& 1665\% 0372 <br>
\hline CtiR7S \& 3599-0378 \& 6 \& \& RESTSTAR 23.52 K , 325\% , 14F TC $=6.5$ \& :8483 \& 3679-0378 <br>
\hline A8R76 \& 8.699-0.379 \& ? \& \& RESIST09 68. 1 K , 023z 16 FF TC=0.-5 \& 28400 \& 06970379 <br>
\hline Atripl
ASR78 \& $2699-0373$
$0694-0377$ \& $\stackrel{1}{5}$ \& $\frac{1}{2}$ \&  \& 28889 \& 0699-0373 <br>
\hline  \& 86894-0377
$8699-0379$ \& 5 \& 2 \&  \& 2ac80 \& 060990377
$3659-0379$ <br>
\hline ATR80 \& 18699-0380 \& 0 \& 1 \&  \& 28480 \& 06.97-8380 <br>
\hline Erinot \& 3699-9377 \& 5 \& \&  \& 20480 \& 3659-9377 <br>
\hline A8R83 \& 0698-7794 \& 2 \& \&  \& 1976.1 \& MFAC1/8 T0 1002 C <br>
\hline  \& 3680-3169 \& ${ }^{3}$ \& \&  \& 24546 \& C4 1/8-70-3162 F <br>
\hline A3R85 \& 0757-0442 \& 9 \& \& RESISTRR 10 K 1\% . 125 SW F $\mathrm{TC}=0+100$ \& 24546 \& C4-1/8-T0-1002-F <br>
\hline AERB6 \& 37570442 \& 9 \& \&  \& 3.4546 \& C4 1/8-70-1032-F <br>
\hline A8pa7 \& 0699-0901 \& 1 \& \&  \& 28480 \& 06,99-0901 <br>
\hline Astres \& 0699-3931 \& 1 \& \&  \& 28483 \& 3699-0901 <br>
\hline ATR9? \& $06989-3162$
0757.0465 \& , \& 1 \&  \& 24546 \&  <br>
\hline ATR93 \& 0757-0440 \& 7 \& 1 \&  \& 24546 \& C4 1/8-T0-7509-F <br>
\hline Arirg 4 \& 3757-0459 \& 8 \& 1 \&  \& 29546 \& C4 1/8-T0-5622-F <br>
\hline ABR9S \& 0757-0465 \& ${ }^{6}$ \& \& RTSISTOR $100 \mathrm{k} 1 \%$, 12Sid F TC=0+-100 \& 24546 \& $\mathrm{CA}^{4}$ 1/8-T0-10.3-F <br>
\hline ASR96 \& 3757-0470 \& 3 \& 1 \& RESTSTGR 162k $1 \%$, 1254 F TC-0, 139 \& 24546 \& C4.1/8-T9-1623-F <br>
\hline A0297 \& 0757-0280 \& 3 \& \& RESISTOR 1k 12.125 F F TC=01-100 \& 24546 \& C4-1/8-T0-1001-F <br>
\hline AGR98 \& 3757-0280 \& 3 \& \&  \& 24546 \& C4-1/8-70-1001-F <br>
\hline A8R99 \& 0757-0467 \& - \& 2 \& RESISTOR 121k 12.1254 F Tr $=0+100$ \& 24546 \& C4-1/8-T0-1213-F <br>
\hline  \&  \& 6 \& 1 \&  \& 28489
24.546 \& 0598-3457
C. $41 / 8-10-196.3-F$ <br>
\hline ARR 132 \& 9757-0467 \& 8 \& \& RESISTUR 121K iz .12SW F TC=0t-100 \& 24546 \& C4-1/8-T0-1213-F <br>
\hline ARR103 \& 0757-0465 \& 6 \& \& RESISTOR 100K 1\% .125W F TC=0+-100 \& 24546 \& C4 1/8-T0-1003-F <br>
\hline AER 104 \& 0757-0465 \& 6 \& \& RESISTCR 100 K 1\% .125W F TC=0+-100 \& 24546 \& C4-1/8-T0-1003-F <br>
\hline ARR 105
ARR 106 \& 0757-0465 \& 6 \& \& RESISTOP 100K $12.125 W$ F TC=0+100 \& 24546 \& C4. 1/8-T0-1003-F <br>
\hline ABR 106
AgR108 \& $0757-0401$
$0698-7270$ \& $\stackrel{0}{9}$ \& 1 \&  \& 24546
24546 \&  <br>
\hline Atir 139 \& 0698-7285 \& 6 \& 1 \& RESISTUR 113 K 1 X , 35W F TC $=0+-100$ \& 24546 \& C3-1/8-T0-1193-F <br>
\hline A日R110 \& $06699-0903$
$0699-0903$ \& 3
3 \& 2 \&  \& 28480

28480 \& $$
\begin{aligned}
& 0669-0903 \\
& 0699-0903
\end{aligned}
$$ <br>

\hline A8TP 1 \& 1251-0600 \& 0 \& 5 \& CONNECTOR-SGL CONT PIN 1.14-MM-bSC-sZ SQ \& 28480 \& 1251-0600 <br>
\hline ${ }_{\text {ABTP2 }}$ \& 1251-0600 \& 0 \& \& CONNECTIR-SGL CONT PIN 1.14-MK -ESC-32 SQ \& 28480
28480 \& 125110600 <br>
\hline ${ }_{\text {ABTP4 }}$ \& $1251-0600$
$1251-0600$ \& 0 \& \& CONNECTOR-SGL CONT PIN 1.14 -MM-GSC-S7 SQ \& 28480
23480 \& $1251-0600$
$1: 51-0600$ <br>
\hline ABTP5 \& 1251-0600 \& 0 \& \& CONNECTOR-SGL CONT PIN 1.14-MM-hSC-s7 SR \& 23480 \& 1251-0600 <br>
\hline ABU1 \& 5180-2315 \& 1 \& 4 \& IC OSC M1OPAMP \& 28480 \& 5180-2315 <br>
\hline ABUZ \& 1820-1548 \& 4 \& 1 \& IC SWITCH ANLG QUAD 14-DIP-C PKG \& 34585
31585 \& CDA066AY <br>
\hline ${ }_{\text {abus }}^{\text {abu4 }}$ \& $1820-1530$
$1826-0092$ \& 4 \& 1
2 \& IC \& 32585
28480 \& CD4027AF <br>
\hline ABUS \& 1820-1547 \& 3 \& 1 \& IC MULTIPLXR 8 -GHAN-ANLG 16 - DIP-C PKG \& 28480
04713 \& MC140518CL <br>
\hline
\end{tabular}

TABLE 8-5. MARKER ASSEMBLY AB, REPLACEABLEPARTS(30F3)

| Reference Designation | HP Part Number | $\left\lvert\, \begin{gathered} \mathrm{c} \\ \mathrm{D} \end{gathered}\right.$ | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\left\|\begin{array}{l} 5 \\ 1 \\ n \\ 8 \\ 8 \end{array}\right\|$ | 3 |  |  |  |
|  | 1858-1083: <br> 13260416 <br> $1880-2315$ 1026 <br> $1036-1058$ | $\left\|\begin{array}{l} 8 \\ 5 \\ 1 \\ 3 \\ 3 \end{array}\right\|$ | 1 1 $:$ | tpansistor arpay 14 - Pin pisicte pil Ir. S,WILCH ANLS <br>  <br> 1c an Amp gr a to 99 Pkg |  |  |
| $\begin{gathered} \text { Anu16 } \\ \text { AROMT } \\ \text { ARH1 } \end{gathered}$ | $1520 \cdot 1542$ <br> 5180-2515 <br> $1856 \cdot 1358$ <br> $2030-3177$ |  | 1 | IC HFR CMOS INU HEX 1-IN: <br> IC ES: MIOPAM <br> tC tip fimp r.p B th 99 PKG <br> AR MISCEILANEDUS PARTS <br> SIRFW MACII 4 4 43 .375-1N-1 C: PAN-:1D-POZI | 31.555 $2848!$ -8480 -848 <br> 28480 | CD4049AF $5180-2315$ $1526-1058$ <br> 2200-0107 |

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MARKER ASSEMBLY


FIGURE 8-32. MARKER ASSEMBLY A8, COMPONENT LOCATIONS








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## SWEEP GENERATOR/BANDWIDTH CONTROL ASSEMBLY A9, CIRCUIT DESCRIPTION

The Sweep Generator/Bandwidth Control Assembly A9 consists of the sweep generator circuit, the sweep trigger circuits, the resolution bandwidth control circuits, the video filtering circuits, the sweep attenuator circuit, and the sweep offset circuit.

A linear sweep from -5 V to +5 V is provided by the sweep generator circuit. Normally, the sweep operates in a free run mode with sweep times automatically generated as a function of the FREQ SPAN/DIV, RESOLUTION BW, VIDEO FILTER, and BAND settings.

Fixed calibrated sweep times are available, ranging from 2 microseconds per division to 10 seconds per division. This equals a full sweep time ( 10 divisions) of 20 microseconds to 100 seconds. Fixed sweep times are set with the SWEEP TIME/DIV control and are used mainly in zero span to determine the modulation frequency of an input signal. Modulation frequency determination is possible because during zero span operation the analyzer displays the signal in the time domain rather than the frequency domain. The sweep can also be controlled manually from the front panel with the MAN sweep control.

Besides internal triggering, SINGLE, VIDEO, and LINE triggering modes are also available. SINGLE starts or stops a single sweep from the front panel. VIDEO triggering allows the sweep to be synchronized with the displayed video signal. LINE mode synchronizes the sweep with the line frequency. Single sweeps can be initiated via HP-IB if an HP 853A Spectrum Analyzer Display is being used.

The resolution bandwidth control circuit has three functions: First, it provides bandwidth-filter-control current to the PIN diodes on the Bandwidth Filter assemblies (A11 and A13). Second, it provides current to the sweep generator current source (via the AST line) to control the automatic sweep time circuit as a function of resolution bandwidth. Third, it switches in capacitance to the video filter to provide video filtering as a constant percentage of resolution bandwidth.

The sweep attenuator circuit attenuates the sweep ramp to the Frequency Control Assembly A7 in proportion to the FREQ SPAN/DIV selected. It also provides current to the sweep generator current source (via the AST line) to control the automatic sweep time circuit as a function of the FREQ SPAN/DIV control setting. Note, the sweep ramp passes through the Marker Assembly A8 before being attenuated by the sweep attenuator.

## Sweep Generator

The sweep generator circuit comprises the current source, the buffer amplifier, the comparator, and the retraceout buffer amplifier. A simplified schematic is shown in Figure 8-34.

When AUTO sweep is selected, the voltage ramp is generated as follows: The ramp begins when the dead time capacitor (comprising C10 and C11 in block L) charges to about +1.2 V through R44. This turns Q33 on and drives pin 2 of the comparator (block H ) below +2.78 V . The output of the comparator then rises to about +14 V , reverse biasing reset-diode CR2 (block I).


FIGURE 8-34. SIMPLIFIED SCHEMATIC OF SWEEP GENERATOR IN AUTOMODE

With CR2 off, the current source begins charging the timing capacitor (C3 and C4, block I). As the timing capacitor charges, the output of the buffer amplifier increases linearly. Transistor 433 is on and its collector voltage is about +0.5 V . The voltage at U 1 pin 2 is mainly established by sweep voltage divider R29, R39, and R47*. (Components VR1, CR4, and R40 feed back some of the comparator's output to pin 2 and act upon the divider. These components have been omitted to simplify the model; see block L on the main schematic.)

When the ramp voltage reaches +5 V , the U1 pin 2 is approximately +2.78 V . Consequently, the comparator's output swings to about -4 V . This negative change reverse biases CR6 and turns 433 off. Resistors R42*, R39, and R29 form a divider that, when combined with the feedback loop and the buffer amplifier, sets the ramp voltage at -5 V during the dead time. (Factory selected resistor R42* adjusts the dead time voltage.)

The timing capacitor is discharged by the comparator and quickly reaches -5 V . The ramp remains at -5 V until the dead time capacitor charges to +1.2 V and the sweep cycle is repeated.

Other components in the sweep generator have the following functions: Capacitor C6 speeds up the switching of U1. Capacitor C8 and resistor R33 desensitize U1 from power spikes. Frequency compensation for U1 is provided by C9, feedback compensation by C7. Zener diode VR1, switching diode CR4, and resistor R40 bring U1 out of saturation at the end of the ramp to improve switching time.


FIGURE8-35. SIMPLIFIED SCHEMATICOF FASTISLOW SWEEPTIMEOPERATION

## Fast/Slow Sweep Time Operation

Timing capacitors C3 and C4 provide fast and slow sweep operation (refer to Figure 8-35). When a sweep time less than or equal to 1 millisecond per division is selected with the SWEEP TIME/DIV switch, sweep control line ST6 is grounded. This turns sweep dead time switch Q6 (block K) and fast sweep switch Q7 (block J) off. With Q7 off, C3 and C4 are in series; C4 effectively becomes the timing capacitor. With Q6 off, +15 V at R46 reverse biases CR9 and CR8, switching C10 out of the dead time circuit. Capacitor C11 now sets a short dead time of about 0.4 millisecond.

In sweep times greater than or equal to 1 millisecond per division or in automatic sweep, control line ST6 is open, turning both Q6 and Q7 on. Transistor Q7 grounds C3 and it becomes the timing capacitor. Transistor Q6 forward biases CR8 and CR9, paralleling C10 and C11. The dead time is effectively established by C10 at about 8.0 milliseconds.

## Pulse Shaper (M)

The pulse shaper circuit (block M) consists of an FET switch, a Schmitt trigger, a differentiator, and an emitter follower (see Figure 8-36). Field-effect transistor Q56, and its associated components, disconnects the base of 435 during the sweep cycle to prevent the Schmitt trigger from firing during a sweep. Transistors 434 and 435 make up the Schmitt trigger. Transistor 435 is normally off; 434 is conducting. On the positive portion of the input signal (either video or line), 435 is driven into conduction, turning 434 off. The switching speed of 434 and 435 is increased by feedback (between the collector of 435 and the base of 434) through C13 and R58.

When 435 switches on, the negative change at the collector is differentiated by C14 and R60 and coupled through Q36 to the emitter of 433. The negative pulse causes 433 to turn on. Zener diode VR1 switching diode CR5, and resistor R41 keep 433 on while the ramp is generated. When the ramp is completed, the circuit returns to its dead time state until another negative trigger pulse begins a new sweep cycle.


FIGURE8-36. SIMPLIFIEDSCHEMATIC OF VIDEO, LINE, AND AUTO TRIGGER MODES

## Free Run

During the FREE RUN (internally triggered) mode, the trigger switch grounds the sync line, which removes the pulse shaper (block M) from the circuit. At the same time, the switch applies +15 V through the trigger (TRIG) line to voltage divider R52 and R53 (block L). This divider sets the voltage at the cathode of CR1O at approximately +1.4 V . Since the voltage drops across CR1O and CR6 are equal but opposite, they cancel. For this reason, the base of 433 is also about +1.4 V . Transistor 433 turns on and drives the comparator to about +14 V , initiating free run operation as described in the sweep generator section.

## Video Triggering

When the TRIGGER switch is in the VIDEO position, the trigger line is open and the video signal (from the Vertical Driver/Blanking Assembly A15) is applied to the pulse shaper (block M) through the sync line. With the trigger line open, Q33 is held off until a negative pulse turns 433 on and begins the sweep cycle outlined in the sweep generator description. At the end of the sweep, 433 is again held off until the next pulse.

## Line Triggering

The sweep may be synchronized with the ac line voltage in the same manner as described for video triggering. With the TRIGGER switch in the line position, the ac line from the mainframe power transformer is connected
to the Pulse Shaper. Resistor A16R2 and capacitor A16C8 on the motherboard attenuate the ac line signal to approximately 1V peak-to-peak (at the base of 435) and filter line spikes.

## Single Sweep Triggering and Abort

When the TRIGGER switch is in the single sweep position, the sync line is grounded and the single line open. Transistor 433 is held off by the voltage developed across CR10 and R53. The voltage at the collector of Q33 is at +10 V , putting the emitter of Q 38 at +9.4 V . This charges C 15 to +2.4 V through voltage divider R 48 and R49.

A sweep is initiated when the trigger switch is set to the spring-loaded SINGLE position and +15 V is applied to the single trigger switch (block N). When 437 turns on, a negative pulse is produced at the emitter of 433 due to voltage stored by C15. This pulse turns 433 on and starts the sweep cycle.

The sweep may be aborted (reset to -5 V ) by pressing the single sweep switch while the sweep is in progress. During the sweep, the collector of 433 is at +0.5 V . This puts the emitter of Q 38 at OV and charges C 15 to -4 V through voltage divider R48 and R49. Now when +15 V is applied to the single trigger switch (block N ), 437 turns on and a positive pulse appears at the emitter of 433. Consequently, 433 turns off and the sweep is aborted.

## Manual Sweep

Manual sweep control is obtained when the SWEEP TIME/DIV switch is set to MAN. In the manual position, ST7 is open (see Figure 8-37). Transistor Q40 turns 433 on by supplying current to its base and 439 acts as a


FIGURE 837.MANUALSWEEPMODE, SIMPLIFIEDSCHEMATIC
switch that connects R34 to the comparator. Turning the manual sweep control (A2R4) adjusts the voltage at the control side of R34.

Operational amplifier U1, operating in a linear mode, fixes the voltage at pin 2 by feedback through CR2, the buffer amplifier, and R29. This fixed voltage is applied through Q39 to one side of R34. As the manual sweep potentiometer is adjusted, the voltage across R34 changes, varying the current supplied to pin 2 of the comparator. This current is forced through R29 and develops the voltage offset that varies the ramp voltage.

## Current Source (F)

The current source provides a constant charging current to the timing capacitors (block I) at a rate selected by either the SWEEP TIME/DIV switch or the automatic sweep time (AST) line.

Temperature compensation of the current source is accomplished by the nominal +10 V supplied by the temper-ature-dependent power supply (block P). The 1 MS (one millisecond) adjustment fixes a voltage at pin 3 of U2a, while the 5 MS adjustment varies the feedback around U2a.

During calibrated sweep time settings, the Sweep Cal. Switch (Q11 in block G) is off. This allows the feedback ratio of U2a, the voltage source, to be varied by grounding different input resistor combinations (R21 through R24) with the SWEEP TIME/DIV switch. In the automatic sweep mode, Sweep Cal. Switch Q11 is turned on by current through Q9 and R25. The feedback ratio now varies with the resistors attached to the AST line and switched in by various settings of the FREQ SPAN/DIV and RESOLUTION BW switches. When the video filter is on, it also affects the feedback and, therefore, the sweep time, by varying the voltage at the emitter of Q8a.

The voltage applied to the emitter of Q8a from voltage source U2a is proportional to the logarithm of the sweep time. Transistor Q8a converts this voltage to a current directly proportional to the sweep time, which charges the timing capacitors in the buffer amplifier. A current limiter composed of Q5 and R15 limits the automatic sweep time to about 1.5 milliseconds per division.

## Xtal Resolution Bandwidth Control (B)

When the RESOLUTION BW switch selects a crystal filtered bandwidth ( $\leq 30 \mathrm{kHz}$ ), bandwidth control line BW5 is open and pulled to -0.5 V by Q12 and Q10 in the Xtal PIN Driver Buffer (block D). As a result, four simultaneous changes occur in the analyzer: the crystal poles on the Bandwidth Filter assemblies are activated, the LC poles are disabled, the crystal bandwidth-control current is established, and the automatic sweep time is scaled for the crystal bandwidths.

Control line BW5, from the RESOLUTION BW switch, is routed to the Bandwidth Filter assemblies (A11 and A13) where it activates the crystal filter poles. (Refer to Bandwidth Filter Assembly No. 1 All, Circuit Description and Schematic.) It reverse biases A11/A12CR2 (block D) and A11/A13CR13 (block G). At the same time, A11/A13Q3 and A11/A13CR8 (block D), and A11/A13Q6 and A11/A13CR15 (block G) are turned on.

The LC poles on the Bandwidth Filter assemblies are disabled by a positive voltage on the BW7 control line. Voltage for BW7 is generated in the LC PIN Driver Buffer (block C) on the Sweep Generator/Bandwidth Control Assembly A9. Control line BW5 turns A11/A13Q22 off, allowing BW7 to be pulled to a level greater than +10 V by A11/A13CR17 and A11/A13R105. This turns off the LC filter sections.

Crystal filter bandwidth is determined by the current on BW6. Transistor Q13 in the Xtal PIN Driver Buffer (block D) is turned off, allowing Q14 to establish the bandwidth control current. Depending on the setting of the RESOLUTION BW switch, one of the bandwidth control lines (BW1 through BW3) is at +15 V while the remaining two are open and pulled to a negative voltage. The positive voltage turns on one of the transistor switches in the Xtal Resolution Bandwidth Control (Q42, Q44, or Q46 in block B). The current on BW6 is now established by one of the factory selected resistors, R109, R110, or R111, and the setting of R72 (the crystal bandwidth adjustment, block D). When the 30 kHz bandwidth is selected, no current is drawn through Q14 and the bandwidth-control PIN diodes (A11/A13CR4 and A11/A13CR12 on the Bandwidth Filter assemblies) are off.

The automatic sweep time (AST) is determined by combinations of resistors switched into the current source circuit by front panel settings. (See the Current Source circuit description.) These resistors are located in blocks A, F, 0 , and the VIDEO FILTER switch A2S2. The contribution of the RESOLUTION BW occurs in the LC Resolution Bandwidth Control (block A). Resistors R117, R119, R121, and R122 are switched into the AST circuit by 4 31, Q26, Q27, and Q28, respectively, when the proper control line is activated. Control lines BW2 through BW4 and the noise measure position of the VIDEO FILTER switch apply +15 V to their respective control lines. The same lines are used to control sweep times in both crystal and LC modes. Since the same resistors are used to establish the automatic sweep time for both crystal and LC modes, scaling is necessary. To scale the sweep time, Q24 in block A switches R75 in or out of the AST circuit. During crystal filter operation, BW5 turns Q24 off and removes R75 from the circuit, allowing a longer sweep time.

## LC Resolution Bandwidth Control (A)

When an LC filtered bandwidth ( $\geq 100 \mathrm{kHz}$ ) is selected, control line BW5 is pulled to +15 V by the RESOLUTION BW switch. This results in four simultaneous changes in the analyzer: the LC poles on the Bandwidth Filter No. 1 and No. 2 Assemblies A11 and A13 are activated, the crystal poles are disabled, the LC bandwidthcontrol current is established, and the automatic sweep time is scaled for LC bandwidths.

With +15 V routed to the Bandwidth Filter assemblies by BW5, A11/A13Q3, A11/A13Q6, A11/A13CR8, and A11/A13CR15 are turned off and A11/A13CR2 and A11/A13CR13 are on. (Refer to Bandwidth'Filter Assembly No. 1 A11, Circuit Description and Schematic.) This blocks any signal from passing through the crystal filter sections. Transistor Q13 (on the Sweep Generator/Bandwidth Control Assembly A9, block D) turns on and control line BW6 is pulled to -4 V , which further inhibits the crystal filters.

The defeat of the crystal filter poles and the application of bandwidth-control current on the BW7 line activates the LC filter sections. The LC bandwidth is controlled by the current through BW7 to the Bandwidth Filter assemblies. Transistor 422, in the LC PIN Driver Buffer (block C), is turned on, allowing the current on BW7 to be controlled by 421 . The position of the RESOLUTION BW switch, via BW2 through BW4, turns one of the transistor switches (Q26, Q27, or Q31) in the LC Resolution Bandwidth Control (block A) on. The band-width-control current on BW7 is now determined by a factory selected resistor, either R116, R118, or R120, and R85 (LC bandwidth adjustment, block C). If the 100 kHz bandwidth is selected, 422 is turned on, but BW7 is pulled up to greater than +10 V through R106. The bandwidth-control PIN diodes (A11/A13CR3 and A11/ A13CR11 on the Bandwidth filter assemblies) are reverse biased by BW7.

Automatic sweep time scaling for LC occurs when BW5 turns Q24 (block A) on. This switches R75 into the AST circuit and decreases the sweep time. The effect on the automatic sweep time is determined by the parallel combination of R75 and the resistor (R117, R119, R121, or R122) selected by the active control line.

## Video Filter

The video filter comprises control A2R6, RESOLUTION BW switch A2A1S5, and eight capacitors on the Sweep Generator/Bandwidth Control Assembly A9 (blocks A and B). VIDEO FILTER control A2R6 varies the resistance of the RC filtering network that it forms with the video filter capacitor. The RESOLUTION BW setting determines which video filter capacitor will be switched in by the transistor switches (Q41, Q43, Q45, and Q47 in crystal bandwidths, and Q54, Q32, Q30, and Q55 in LC bandwidths). Increased capacitance is switched in to provide increased filtering as the bandwidth narrows.

The output of the Xtal PIN Driver Buffer (BW6) is applied to the bases of Q42, Q44, Q46, and Q47 via CR18 through CR21. This holds the transistors off and prevents the crystal mode, video filter capacitors from being switched into the circuit during LC mode operation. It is not necessary to switch the LC mode video filter capacitors out of the circuit during crystal operation; their values are so much smaller that they are effectively out of the circuit.

Switch A2S2 applies maximum video filtering for noise measurements by turning on Q55, which switches in C28.

## Sweep Attenuator ( 0 )

The Sweep Attenuator circuit attenuates the full span sweep ( -5 V to +5 V ), before it is applied to the Frequency Control Assembly A7, as a function of the FREQ SPAN/DIV setting. The circuit also varies the automatic sweep time (AST) as a function of the frequency span. Attenuation takes place in the 1-2-5-10 sequence that results in the FREQ SPAN/DIV control sequence. The circuit has two voltage dividers separated by U3, the unity gain sweep buffer. The input divider provides divide-by-two and divide-by-five; the output divider provides divide-by-tenand divide-by-one-hundred.

To select any of the input dividers, $\mathbf{+ 1 5 V}$ is applied to activate the associated control line. For example, if FS3 is activated, Q51 and Q50turn on and ground R102 and R73. Resistor R102 becomes part of the AST circuit; R73 forms a divider with R70 that results in the ramp voltage being divided by two. The divided ramp is then applied to the sweep buffer.

The dividers at the output of the sweep buffer have reversed control-logic. That is, they are normally connected to +15 V by the FREQ SPAN/DIV switch and open (0V) when selected. Transistor Q19 is a gate to drive Q17. When FS4 and FS5 are connected to $+15 \mathrm{~V}, \mathrm{Q} 19$ is off. As a result, Q17 is on and opens a path for the sweep buffer's output to P1-12. No attenuation takes place. If either FS4 or FS5 opens, Q17 shuts off. When FS4 opens, Q16 turns on and a divide-by-ten (R81/R82 + R83) is provided. When FS5 opens, Q15 turns on and provides a divide-by-one-hundred (R81 + R82/R83).

Automatic sweep is varied as a function of frequency span by transistors Q53, Q51, Q49, Q29, Q25, and Q23. Transistor A29 is switched on in narrow spans ( $<1 \mathrm{MHz} / \mathrm{div}$ ) when the YIG FM coil is swept. All of these transistors act as switches connecting resistors from the AST line to ground. This varies the sweep time. (See the Current Source circuit description.) As the FREQ SPAN/DIV is narrowed, the sweep time is decreased.

## Sweep Offset

Transistor Q20 in the sweep attenuator (block $\mathbf{O}$ ) makes it possible to offset the sweep ramp in response to the position of a start-center (ST-CTR) switch. This capability is not required in the HP 8559A. So, the +15 V from the Motherboard Assembly A16 is applied to Q20, holding it off. The circuit is always in the center position.

## SWEEP GENERATOR/BANDWIDTH CONTROL ASSEMBLY A9, TROUBLESHOOTING

## CAUTION <br> When making measurements at or near test points, be careful not to short adjacent points or circuit components together.

Auto Scan Time (AST) Accuracy: Observe front panel switch positions to help isolate the problem area. Auto scan time can also be affected by circuits on the Marker Assembly A8 and the VIDEO FILTER control position. If the AST ŋroblem is band related, the Marker Assembly A8 is the most probable cause. If the AST problem is bandwidth or scanwidth related, the most probable cause is the Sweep Generator/Bandwidth Control Assembly A9. The greater the load placed on the AST line, the greater the current demand. The greater the current demand, the faster the sweep rate.

Failure to Sweep: Check the +10 V (nominal) supply. If it is greater than +11.5 V , the sweep will be inhibited.

If the +10 V (nominal) supply is low, check the Bandwidth Filter No. 1 and No. 2 Assemblies A11 and A13 for a shorted crystal filter pole. Test from A11/A13TP2 to ground and A11/A13TP5 to ground with an ohmmeter to locate the possible short.

Begin troubleshooting the sweep generator by determining if the Current Source (block F) is operating and if the Comparator (block H) will toggle.

The inability to trigger retrace, during the beginning of a sweep, is commonly caused by the failure of U 1 or CR7.

Bes]e

TABLE8-6. SWEEP GENERATOR/BANDWIDTH CONTROL ASSEMBLY A9, REPLACEABLEPARTS (10F 4)

| Reference Designation | HP Part Number | $\begin{aligned} & c \\ & c_{0} \end{aligned}$ | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| As | 01559-600n3 | 1 | 1 |  | гвяз | 09559-60.983 |
| ${ }_{\text {a }}^{\text {apcl }}$ |  |  | 3 |  |  |  |
|  |  |  |  | ction | cinco | (12.3020 |
| a9c6 |  |  |  |  | 28498 | ${ }^{3160-3466}$ |
|  |  |  | , |  |  |  |
|  | (in | ${ }^{3}$ | : |  |  | ${ }^{\text {dit }}$ |
| ${ }_{\substack{\text { A9ccil } \\ \text { accie }}}$ |  |  | = | capaction-xxo |  |  |
|  |  |  |  |  | ${ }_{\substack{23900 \\ 72130}}^{290}$ |  |
| A9Cis | 0160-3094 |  |  |  | 28880 | 011.60-3094 |
|  |  |  |  |  | $5: 8.89$ |  |
|  |  | ${ }^{8}$ |  |  |  |  |
| ${ }^{\text {anc } 22}$ | $0100-0.168$ |  |  |  | ${ }^{\text {2namo }}$ | ${ }^{01760.0169}$ |
| ${ }_{\substack{\text { a }}}^{\text {afcci }}$ |  |  |  | comer |  |  |
|  |  |  |  |  |  | (2160-0.155 |
| ${ }_{\text {a }}^{\text {Apcrez }}$ | (160-1134 |  |  |  |  |  |
|  |  |  | : |  | $\underset{\substack{\text { 20409 } \\ \text { 20as }}}{ }$ | ${ }_{\text {19012 }}^{19050}$ |
|  | 19910950 $\substack{1901050 \\ 1901-0.50}$ | $3_{3}^{3}$ |  |  |  |  |
| ${ }_{\text {afcrs }}$ | 1991-0050 | 3 |  |  | 23480 | 1971-0050 |
| (encri | (191-0.059 | $3_{3}^{3}$ |  | Mrobe surchrng piv 260 mazas dn 35 | cient |  |
|  | (1901-0.050 | 宷 |  |  | (ention |  |
| ${ }_{\text {ata }}^{\text {Afre }}$ | ${ }^{1901-0050}$ | 3 |  |  |  |  |
| and | 边 $11.01-0.0050$ | 3 |  |  |  |  |
| ${ }_{\text {and }}^{\text {Apcria }}$ | $1901-0000$ <br> $1901-0050$ <br> 100 | $3_{3}^{3}$ |  |  | ${ }_{\substack{\text { 2a400 } \\ \text { 20803 }}}$ | ${ }^{12012} 1200050$ |
|  | - 1901 -00050 | 3 |  |  |  | - 1901 1-0050 |
|  | (1901-0.0050 |  |  |  |  |  |
|  |  |  |  | diode sutiching bju 20ora zns do-35 |  | 1931-2 |
|  |  | 3 |  |  | cisation |  |
|  | 1991-0.050 | 3 |  | Dioue silchlng gil | ${ }_{\substack{\text { 20490 }}}^{\text {2680 }}$ | - 129120.0050 |
|  | (1901-0050 | 3 |  |  |  | - 1901 10050 10050 |
|  |  | $\stackrel{?}{2}$ |  |  |  | (102198 |
|  |  | $\ldots$ | \% |  |  |  |
| ${ }_{\text {apab }}^{\text {apa }}$ |  | $?$ |  |  |  | ${ }_{\text {cose }}^{1054} 10071$ |
|  |  | $\cdots$ | 1 |  |  |  |
| A8910 | 1854-0071 |  |  | TRANSISTOR NPN SI PD=300m4 FTT=200ntz |  | 1854-0871 |
|  |  |  | ${ }_{5}^{2}$ |  <br>  |  |  |

TABLE8-6. SWEEP GENERATOR/BANDWIDTH CONTROLASSEMBLY A9, REPLACEABLEPARTS(2OF 4)

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A5016 | 1655-0382 | E |  | IRANSTSTITR J FST P-CHAN D-MODE SI | - 17480 | 1855-0382 |
| A9Q17 | 1055-0.02 | 2 |  | TRANSISTOR J-FET P-CHAN D-MODE SI | 28480 | 1955-0082 |
| APQ18 A9219 | $11554-0404$ $1853-0020$ | $a$ 4 |  | 1RANSTSTGR ${ }^{\text {NPN }}$ SI $10-18 \mathrm{PD}=360 \mathrm{MW}$ TRANGISTOR PNP SI PD=300MW FT $=150 \mathrm{MH} 7$ | , 9489 | $1554-0404$ $1858-0020$ |
| APD219 Asq23 | $1853-0620$ 1353 | 4 |  |  | 29480 | $1858-0020$ $1553-0320$ |
| A9Q23 | 1854-0404 | 0 |  | TRANSISTOR NPN ST TO-18 PDV 368 EL | ? 2488 | 18.5-0464 |
| ASRES A 223 | 1954-0071 | 7 |  |  | 29380 | 1654-0371 |
| A7223 | 1055-0082 | 2 |  | TRANGISTOR J-FET P CHAN D MODE SI | 20480 | 1955-0082 |
| Aspeat | $1854-0371$ $1855-0082$ | 7 |  | TRANSISTCR TRAN SI P PD | . 2480 | $11554-8371$ $1855-0082$ |
| A) 026 | 15:54-0371 | 7 |  | TRANGTSTOR NPN SI PD=303MW [T= 2.J3MHZ | c 8480 | 1654-0971 |
| A9Q27 | 1954-0071 | 7 |  | TRANSISTOR NPN SI PD $=360 \mathrm{MW}$ FT=2G日M ${ }^{\text {S }}$ | 28.480 | 135.4-0071 |
| A9828 | 1854-0071 | 7 |  | TRANSISTSJR NPN SI PD=30nM.4 $\mathrm{FT}=200 \mathrm{mH}$ \% | . 8480 | 1654-0071 |
| A7029 | 1855-0414 | 4 | 2 | TPANSISTOR J-FLT $2 N 4393$ N-CHAN D-MODE | 04713 | 2N4393 |
| AFQ33 | 18540371 | 7 |  | TRANSTSTGR NPN $51 \mathrm{PD}=303 \mathrm{MW} \mathrm{FT}=203 \mathrm{MLIZ}$ | 28480 | 1854-3071 |
| A9031 A 933 | $1854-0071$ $1054-0071$ | 7 |  | TRANSISTOR NPN SI $\mathrm{PD}=30 \mathrm{CMW} \mathrm{FT}=20 \mathrm{CMHZ}$ | 28480 | 1854-0071 |
| A9832 | 1354-0071 | 7 |  | TRANSISTRR NPN SI PD=300KLW :T $=203 \mathrm{MH}$ | \% 89480 | 10554-0.371 |
| A)934 | 15154-0371 | 7 |  | TRANSTSTGR NPN SI PD=33aKW ! T= 203MMZ | 8480 | 15554-0.371 |
| A9035 | 1854-0071 | 7 |  | TRANSISTOR NPN S1 PD=3COMU FT $=200 \mathrm{MH}$ \% | 30400 | 1054-0071 |
| A8036 A9037 | $1853-0320$ $1055-0417$ | 4 |  |  | . 84800 | 1853-0320 |
| A9037 A 938 | $1855-0417$ $1854-0404$ | 7 0 |  |  | 28480 <br> 78480 <br> 88480 | $1855-0417$ $1854-0404$ |
| A9039 | 1654-0671 | 7 |  | TRANSTSTOR NPN SI PD $=300 \mathrm{MW} \mathrm{FT}=2 \mathrm{COMHz}$ | 28480 | 185:4-0071 |
| A3Q43 | 1853-3320 | 4 |  |  | 28480 | 1553-0020 |
| A9Q41 | 1854-0071 | 7 |  | TRANGISTOR NIN SI PD $=300 \mathrm{ML}$ FT $=200 \mathrm{M} / 17$ | 111400 | 105.4-0071 |
| A9842 | 1354.0071 | 7 |  | TRANSTETGR NPN SI PD=300NL $5 T=200 \mathrm{MH}$ | 28.483 | 1654-0071 |
| A9G43 A9844 | 1854-0071 | 7 |  | TRANSISTOR NI'N ST PD $300 \mathrm{MW} \mathrm{FT}=20 \mathrm{GMiNZ}$ | 28490 | 1854-0071 |
| A7Q45 | 1854-0071 | 7 |  | TRANSISTOR NIN ST PD $300 \mathrm{MW} \mathrm{FT}=200 \mathrm{M} 2 \mathrm{Z}$ | 20480 | 1854-0071 |
| AS846 A9647 | 1854 $1854-0371$ 1854 | 7 |  |  | 68480 <br> 26480 <br> 88480 | 1854-0371 |
| A9Q4] | 1654-0971 | 7 |  |  | 78480 | 1654-0071 |
| A9849 | 1854-0071 | 7 |  | TRANGIGTOR NPN SI PD=300kL $\mathrm{FT}=20 \mathrm{MmHz}$ | 28480 | 1854-0071 |
| ASLS 3 | 1654.0071 | 7 |  | TRANGTSTUR NPN SI PD=303rM FT 203mbl | ,04880 | 1:554-0371 |
| A9RS 1 | 1854-0071 | 7 |  | TRANSISTOR NPN ST PD 300 MW FT=200MHZ | 28480 | 195.4-0071 |
| A945.2 | 1854.0071 | 7 |  | TRANSISTCiR NPN SI PD=300riW FT $=200 \mathrm{mH}$ | 28480 | 15554-0071 |
| A9853 | 1854-0071 | 7 |  | TRANSISTOR NPN SI PD $=300 \mathrm{MW}$ FT $=200 \mathrm{MH} 7$ | 26480 | 1854-0071 |
| ASGS 4 | 1054-0071 | 7 |  |  | 26480 | 1654-0071 |
| A9Q55 | 1854-0071 | 7 |  | TRANSTSTER NPN ST PD $=300 \mathrm{MW}$ FT $=200 \mathrm{mlit}$ | 28480 | 185.4.0071 |
| ASQ56 | $1855-0414$ | 4 |  | TRANSTSTOR J-FET 2N4393 N CAGA D-NADE: | 04713 | 2N4393 |
| A9R1 | 0698-3450 | 9 | 1 | RESISTOR 42.2k $1 \%$, 125w F TC $=0+100$ | 24546 | C4-1/8-70-4222-F |
| A9R3 | 0757-0277 | 0 | 4 | RESISTUR $3.16 \mathrm{~K} 1 \%$, 125w F TC $=0.103$ | 24546 | C4 1/8-T0-3161 F |
| APR4 | 0757-0419 | - | 1 | RESISTOR $6011 \%$, 125 W F $\mathrm{TC=0+-100}$ | 24546 | C4 1/8-TB-681R-F |
| A9RS | 0757.0459 | 8 | 4 | RESISTOR S6.EK 1 x , 125W F TC $00+100$ | 245,46 | C4-1/8-T0-5622-F |
| A9R6 | 0698-3152 | B | 1 | RESISTOR 3.48K $1 \%$, 125 F F TC=0 + 100 | 24546 | C4-1/8-T0-3481-F |
| A9R7 | 0757-0442 | 9 |  |  | 24546 | C4-1/8-Ta-1092-F |
| A9R8 | 0755-0442 | $\stackrel{7}{7}$ |  | RESISTOR $10 \mathrm{~K} 1 \%$, 125 F F TC=0 - 100 | 24546 | C4-1/8-T0-1062-F |
| A7R9 | 0757.0444 | 1 | $?$ | RESISTOA 121 K 1 x 12EW F TC $=0+100$ | 24546 | CA-1/B-T0-1212-F |
| A9R10 | 2100-3109 | 2 | 1 | RESISTOR TRMR 2 K 10x C SIDE ADJ 17 TRN | 02111 | 43 P ? 02 |
| AYR11 | 0698-3457 | 6 |  | RCSISTOR 316k 1\% 125w F TC=0 100 | 23480 | 3698-3457 |
| A9R 12 | 10698-3446 | 3 | 1 | RESISTOR 383 1\% , 125w F TC: $=0+-100$ | 24548 | C4-1/8-T0-383R-F |
| A9R13 | 2100-3052 | 4 | 1 | RESTSTGR -TRMR $5010 \%$ C SIDE ADJ 17-TRN | 02111 | 43 P 500 |
| APR 14 | 06,98-3442 | 9 | 1 | RESISTOR $2371 \%$, 125w F TC=0+-100 | 24546 | C4 1/8-T0-237R-F |
| APR15 | 0757-0424 | 7 | 1 | RESISTOR $1.1 \mathrm{~K} 1 \%$, 125w F TC=0 + 100 | 24546 | C4-1/8-T0-1101-F |
| A9R16 | 0757-0279 | 0 |  | RES ISTOR 3.16k 1\% .125w C TC=0+-100 | 24546 | C4-1/8-T0-3161-F |
| A9R17 | 0698-3444 | , | 1 | RESISTIOR $3161 \%$, 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-316R-F |
| A9R18 | 0757-0280 | 3 | 1 | RESISTOR $1 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A9R19 | 0757-0346 | 2 | 2 | RESISTOR $101 \%$ 125w F TC=0 +-100 | 24546 | CA-1/8-T0-10R0-F |
| A9R20 | 0757-0465 | 6 | 11 | RCSISTOR 100 K RESISTOR 13 | 24546 | C4- 1/8-T0-1003-F |
| A9R21 | 0698-3451 | 0 | 2 | RESISTOR 133K 1\% . 125 W F TC= $=0+100$ | 24546 | C4-1/8-T0-1333-F |
| A9R24 | 0698-3194 | 3 | 3 | RCSISTOR 20K . 25 \% . 125 W F TC $=0+50$ | 03888 | PMES5-1/8-T2 2002-C |
| A9R25 | 0698-7794 | 2 | 3 | RCSISTOR 10 K . 25 T . 125 W F TC $=0+-100$ | 19731 | MF4C1/8-T0-1002-C |
| A9R26 | 0757-0289 | 2 |  | RESISTOR 13.3k $1 \%$. 125 W F T $\mathrm{C}=0+-100$ | 19701 | MF4C.1/8-T0-1332-F |
| A9R27 A9R28 | $\begin{aligned} & 0757-0199 \\ & 0757-0465 \end{aligned}$ | 3 6 | 6 | RESISTOR 21.5K $1 x$. 125 W F TC $=0+-100$ RESISTOR 100 K ix . 125 W F TC=0+-100 | 24546 24546 | $\begin{aligned} & \text { C4-1/B-T0-2152-F } \\ & \text { C4-1/B-T0-1003-F } \end{aligned}$ |
| A9R29 | 0698-6360 | 6 | 5 | RESISTOR $10 \mathrm{~K}, 1 \chi$. $12 \pm W F$ TC=0+-25 | 28480 | 0698-6360 |
| A9R30 | 0698-3934 | 4 | 1 |  | 20480 | 0698-3934 |
| A9R31 | 0698-7794 | 2 |  | RESISTOR $10 \mathrm{~K} .25 \times$. 125 W F TC $=0+-100$ | 19701 | MF4C1/8-T0-1032-C |
| A9R 32 A9R33 | $0683-3355$ $0683-3355$ | 2 | 3 | RCSISTOR 3.3M 5X .25W FC TC $=-900 /+1100$ RESISTOR 3.3M 5X .25W FC TC $=-900 /+1100$ |  | CB3355 |
| A9R33 A9R34 | $0683-3355$ $0757-0289$ | 2 |  |  | 01121 19701 | C83355 ${ }_{\text {MF4C1/8-T0-1332-F }}$ |
| A9R35 | 0757-0442 | 9 |  |  | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T} 0-1002-\mathrm{F}$ |
| A9R36 | 0757-0465 | 6 |  | RESISTOR 100 K 1 x . 125 W F TC. $\times 0+-100$ | 24546 | C4-1/8-T0-1003-F |

TABLE 8-6. SWEEP GENERATOR/BANDWIDTH CONTROL ASSEMBLY A9, REPLACEABLE PARTS (3 OF 4)

| Reference Designation | HP Part Number | $\begin{aligned} & \mathbf{C} \\ & \mathbf{D} \end{aligned}$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AsR33? | 0757-0465 | 6 |  | RCSISTOR $100 \mathrm{~K} 1 \%$, 1254 F $T C=0+-166$ | 24546 24546 | $\mathrm{C} 4-1 / 8-\mathrm{TO} 1063 \mathrm{~F}$ |
| A9R38 A9R39 | 0757-0458 $0698-8360$ | 7 |  | RESTSTGR $51.1 \mathrm{~K} \quad 1 \mathrm{X}, 125 \mathrm{~W}$ F $\mathrm{TC}=0+-103$ RESISTOR $10 \mathrm{~K}, 1 \mathrm{X}, 125 \mathrm{~W}$ TC $0+-25$ | 24546 28480 | $\begin{aligned} & \mathrm{C} 4-1 / 8-\mathrm{T})-5112-\mathrm{F} \\ & 0693-6360 \end{aligned}$ |
| A9R39 ASR43 | 0698-6330 $0757 \cdots 0442$ | 6 9 |  | RESISTOR 10 K RESISTOR 13 K iz | 26480 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T} 10-1032-F$ |
| A9R41 | 06,98-3160 | 8 | 3 | RESISTOR 31,6K 1\% , 125w F TC=0+-16G | 245.46 | C4 1/8-TC-318.2 F |
| A5R42x | 0698-3935 | 5 | 1 |  | 28480 24546 | $3698-3735$ |
| A9R43 | $0698-3160$ $3693-3260$ | 8 |  |  | 245.46 882800 | $\begin{aligned} & \text { C4-1/8-T0-3162 F } \\ & 3698-3260 \end{aligned}$ |
| AFR44 AFR 45 | $3693-3260$ $6757-0465$ | 6 | 2 | RESTSTOR RESISTOR 160 K R 1\% R | 68480 24546 |  |
| ASR 46 | 3757-0439 | 4 | 3 |  | 24546 | C4 1/8-T0-6.811-F |
| ATR47* | $0698-4037$ $3693-6845$ | 1 | 2 |  | 240.46 31121 | $\mathrm{C} 4-1 / \mathrm{B}-\mathrm{TC}-4 / . \mathrm{R} 4-\mathrm{F}$ $\mathrm{CB} / 3 \mathrm{~B} 45$ |
| AFR 48 A9R49 | $3693-6845$ $0698-3457$ | 1 | 1 |  | 31121 23480 | CEABA5 <br> c69a 3457 |
| ASRS0 | 3757-0439 | 4 |  |  | 24546 | C4 $1 / 8-19-6811-\mathrm{F}$ |
| A ${ }^{\text {PS }} 1$ | 6698-4C37 | 0 |  | RESIGTOR 46, 4 1\% , 1254 F TC=0+-160 | 24546 | C4 $1 / 8$ T6-4684-F |
| A9RS2 | 0598-3160 | ${ }^{8}$ |  | RESISTOR 31.6 K 1\% $1 \%$ 125, \% TC $=3+139$ | 24546 34546 |  |
| A9RS3 AVRS4 | 0757-0279 $0757-0442$ | 0 |  |  | 24546 24546 |  |
| A7RSS | 0757-0464 | 5 | 1 | RESIGTOR 9C. 9 K 12.125 L F $\mathrm{TC}=0+-166$ | 24,546 | C4-1/8-T0-7692-F |
| A\%R56 | 3757-3279 | 3 |  | RESTSTOR 3.16K $1 \%$, 12SW F TC $=3+103$ | 24546 | C4 1/8-T3-3161-F |
| A9R57 | 6757-0439 $3757-0469$ | 4 1 1 |  |  | 245.46 24546 | C.4-1/0-T0-6811-F C4 $1 / 8-70-6192 \cdots \mathrm{~F}$ |
| APRSE A9RS9 | $3757-0463$ $6757-0442$ | 1 |  | RESTSTOR 61.9 K 12.125 W F TC $\mathrm{T}=0+-133$ RESISTOR 1 Eh 12.125 W TC $=0+100$ | 24546 24546 | C4 C4 C4 1/8-T0-619-16-F CA |
| AsR69 | 3757-9442 | $?$ |  | RESISIOR $13 \mathrm{~K} 1 \%$, 125, F F TC $=04-109$ | 24546 | C4 1/8-T3-1092-F |
| A9R61 | 0757-0465 | 6 |  | RESISTOR 100 K 1\% , 125 F F TC=0t-100 | 2.45 .46 | C4 1/8-T6 1003-F |
| ASR62 | 3757-0465 | 6 |  |  | 24546 24546 | $\begin{aligned} & \mathrm{C} 4 \mathrm{1} / 8-\mathrm{TO}-1093-\mathrm{F} \\ & \mathrm{C} 4-1 / 8-\mathrm{T} 0-1063-\mathrm{F} \end{aligned}$ |
| A9R64 A R 65 | 0757-0465 $0757-0459$ | 6 |  |  | 24546 24546 | C4- $1 / 8-\mathrm{T} 0-1063-\mathrm{F}$ $\mathrm{CA} 1 / 8-\mathrm{TO}-5622-\mathrm{F}$ |
| A9R66 | 0757-0442 | 9 |  | RESISTOR 10 K 12.125 W F TC $=0+100$ | 24546 | C4-1/8-T0-1062-F |
| A9R67 | 3690-3154 | 3 | 1 | RESIGTGR 4.22K $1 \%$, 125\% F $10 \times 3+100$ | 24546 | C4 1/8-73-4221-F |
| A9R68 ASR69 | $0698-3457$ 0757 07440 | 6 7 | 3 1 |  | 28480 24546 | $\begin{aligned} & 06.98-3457 \\ & C 4-1 / 8-10-7531 \quad F \end{aligned}$ |
| ASR69 A9R70 | 07570440 $0698-6360$ | 7 | 1 |  | 24546 28480 | $\begin{aligned} & C 4-1 / 8-T 0-7531 \mathrm{~F} \\ & 6692-6360 \end{aligned}$ |
| A $/ 2 \mathrm{R} 71$ | 0757-0442 | 9 |  | RESISTCR $13 \mathrm{~K} 1 \%$, 12 ESW F TC $=0+-109$ | 24546 | C4 1/8-73-1032-F |
| AFR72 | 2160-2856 | 8 | 2 | RESISTOR-TRMR 10 K 10\% WW SIDE-ADJ 26 - TRN | 02660 | 3810r-103 |
| A 2873 A PR74 | $0698-6369$ $0757-0459$ | 6 8 8 |  | RESTSTOR RESISTOR R | $28+80$ $245.46$ | $\begin{aligned} & 0678 \cdot 6360 \\ & C 4 \quad 1 / 8-T B-56.22-F \end{aligned}$ |
| AYR74 A 2 R | $0757-0459$ $0698-7794$ | 8 |  | RESISTOR SESISTOR RES R | 24546 19731 | $\begin{aligned} & \text { CA } 1 / 8-T B-56 \sin -F \\ & \text { MFAC1/B-T3-1002-C } \end{aligned}$ |
| A9R76 | 0698-3238 | 1 | 1 | RESISTOR 2.5K .25\% . 1254 F TC=0+-50 | 28480 | 0698-3238 |
| ASR77 | 07570465 | 6 |  | RESTSTER 133K 12.1254 F $1 \mathrm{C}=3+-13 \mathrm{a}$ | 24546 | C4 1/8- ${ }^{\text {co-1033-F }}$ |
| A9R78 | 6698-8827 | 4 | 3 | RESISTOR $1 \mathrm{M} 1 \%, 125 \mathrm{~W}$ F TC=0,-106 | 29480 | 069a-8827 |
| ASR79 | 0690-6827 | 4 |  | RESSISTGR 1M $1 \%$ 12SU F TC-3+-130 | 28480 | 3698-ER27 |
| A9R80 | 0757-0465 | 6 |  | RESISTOR 100 K 1\% , 125W F TC=0+-100 | 24546 | C4-1/8-T0-1063-F |
| A7R31 A?R82 | 3698-6363 $0698-6362$ | 6 | 1 |  | 6.8483 22480 | $0698-6360$ 0692 |
| A9R83 | 0698-7912 | 6 | 1 | RESTSTGR $111.1 \quad 25 \%$, 125W F TC $=0+100$ | 19701 | MFAC1/8-T0-111R1-C |
| A9R84 | 0698-7421 | 2 |  | RESISTOR 40 K . 258 \% 1254 F $\mathrm{TC}=0+-100$ | 19701 | Mr AC, $1 / 8-\mathrm{TO}$ - $4 \mathrm{CO2-C}$ |
| A9R85 | 2130-2850 | 3 |  | RESTSTICR-TRMR 12 K 13\% LU SIDE-ADJ 20 TRN | 32663 | 3813P-133 |
| A9R86 ASR87 | 0757-0447 $9757-0461$ | 4 2 2 | 1 |  | 24546 24546 |  |
| A9R88 | 0757-0442 | 9 |  | RESISTOP 10K $12.125 \%$ F TC-0\%-160 | 24.546 | C4 1/8-T0-1602 F |
| A9R87 | 0757-0442 | 9 |  | RESISTAR $10 \mathrm{~K} 1 \%$. 125 LW F TC $=00 \% 109$ | 24546 | C4 1/B-T0-1032 F |
| A9R90 | 0757-0289 | 2 |  | RESISTOR $13.3 \mathrm{~K} \quad 12 \quad 1254 \%$ F $\mathrm{CC}=0+100$ | 19701 | Mr 4C1/8-T0-1332-F |
| A9R91 | 0683-3355 | 2 |  | RESISTGR 3.2M $5 \%$, SSL FC TCa $903 / 11100$ | 31121 | cri3355 |
| A9R92 | 0757-0346 | 2 |  | RESISTRR $101 \%$, 12SW F TCu 01.160 | 24546 | C4-1/8-T0-1CPC-F |
| AYR92 | 2100-3154 | 7 | 1 | RESISTGR-TRMR 1 K 10 Z C SIDE-ADJ 17-TAN | 32111 | 43 P 102 |
| A9R93 | 0757-0465 | 6 |  | RESISTOR $100 \mathrm{~K} 1 \%$, 125W F TC=0 0 - 100 | 24546 | C. 4 1/8-T0-1003-F |
| A9R94 | 9757-0199 | 3 |  | RESTSTLR 21.5 K 1\% , 125W F TC=01-103 | 24546 | C4-1/8-T0-2152-F |
| A9R95 | 0698-3157 | 3 | 1 | RESISTOR 19.6 K 1\% , 1254 F TC=0+166 | 24546 | C4- 1/8-T0-196.2-F |
| A9R96 | 0698-3136 | 8 | 1 | RESISTOR 17.8K $1 \%$, 125 W F TC=3t-100 | 24546 | C4-1/8-T3-1782-F |
| A9R97 | 0757-1094 | 9 | 1 | RESISTOR $1.47 \mathrm{~K} 1 \%$. 125 W F $\mathrm{TC}=0+-100$ | 24546 | C4-1/8-T0-1471-F |
| A9R98 | 0757-0289 | 2 |  | RESISTAR 13.3K $1 \%$, 12SW F TC=0+-100 | 19731 | MFAC1/8-T0-1332-F |
| A9R99 | 0757-0199 | 3 |  | RESIGTOR 21, 5 K $1 \%$, 125 W F TC $=0+100$ | 24546 | C4-1/8-TC-2152-F |
| ATR 101 | 0757-0179 | 3 |  | RESISTUR $21.5 K 12$, 12SW F TC=0 1 - 100 | 24546 | C4-1/8-T0-2152-F |
| A9R102 | 8698-3451 | 0 |  | RESISTOR 133 K 1 x , $125 \pm$ F $T C=0+-100$ | 24546 | C4-1/8-T0-1333-F |
| A9R103 | 0757-0199 | 3 |  | RESISTOR 21.5 K 1 X , 125W F TC=3+100 | 24546 | C4-1/8-T0-2152-F |
| A9R104 | 0757-0199 | 3 |  | RESISTOR $21.5 \mathrm{~K} 1 \%$, 125W F TC $=0+100$ | 24546 24546 | C4-1/8-T0-2152-F |
| ATR135 | 0698-0.005 | 0 | 1 | RESISTOR $2.61 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~F}$ F TC $\mathrm{T}=0+100$ RESISTOR $464 \mathrm{~K} 1 \chi$, 125 F F $\mathrm{TC}=0+160$ | 24546 28480 | $\begin{aligned} & C 4-1 / B-T 0-2611-F \\ & 0698-3260 \end{aligned}$ |
| A9R106 | 0698-3260 | 9 |  | RESISTOR RESISTOR 4 R | 28480 74546 | $\begin{aligned} & 0698-3260 \\ & \mathrm{C} 4-1 / 8-\mathrm{TO}-1212-F \end{aligned}$ |
| A9R107 | 0757-0444 | 1 |  | RESISTOR $12.1 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-1212-F |
| A9R108 | 0698-3194 | 8 |  | RESISTOR 20K , 25\% , 12SU F TC $=0+-50$ | 03888 | PMES5-1/8-T2-2002-C |
| APR109* A9R110* | 0698-3151 | 7 | 13 | RESISTOR $2.87 \mathrm{~K} 1 \chi$. 125 W F $\mathrm{TC}=0+100$ RESISTOR RES | 24546 24546 | C4-1/8-T0-2871-F $\mathrm{C} 4-1 / 8-\mathrm{TO}$-1002-F |
| ASR111* | 0757-0458 | 7 | 2 | RESISTOR 51.1 K 1 x , 125U F TC $=0+-100$ | 24546 | C4-1/8-T0-5112-F |
| A9R116* | 0757-0460 | 1 | 2 | RESISTOR 61,9K 1z , 125W F TC $=0+100$ | 24546 | C4-1/8-T0-6192-F |
| A9R117 | 0698-7421 | 2 |  | RESISTOR $40 \mathrm{~K}, 25 \%$, 125W F TC=0+-100 | 19701 | MF4C1/8-T0-4002-C |

TABLE86. SWEEPGENERATORIBANDWIDTHCONTROLASSEMBLYA9, REPLACEABLEPARTS(4OF4)



FIGURE838. SWEEP GENERATOR/BANDWIDTH CONTROLASSEMBLYA9, BLOCKDIAGRAM


FIGURE8-39. SWEEPGENERATOR/BANDWIDTH CONTROLASSEMBLY A9, COMPONENTLOCATIONS



## THIRD CONVERTER ASSEMBLY A10, CIRCUIT DESCRIPTION

The Third Converter Assembly A10 contains a 321.4 MHz amplifier followed by a 321.4 MHz bandpass filter, a double balanced mixer, a 21.4 MHz IF preamplifier, a flatness compensation amplifier, and a band conversion loss compensating amplifier. Also included in the Third Converter Assembly A10 are the 35 MHz calibration oscillator and the 300 MHz third local oscillator. The 321.4 MHz signal from the Second Converter Assembly A5 is amplified in the 321.4 MHz amplifier and filtered in the 321.4 MHz bandpass filter before being mixed with the 300 MHz oscillator in the balanced mixer. The output of the mixer is the difference frequency, 21.4 MHz , which is applied to the IF preamplifier where gain is added for the reference level calibration. The signal now passes through two amplifiers to compensate for flatness across the bands and the varying conversion loss of the bands before leaving the Third Converter Assembly A10 at a power level of approximately 0 dBm .

### 321.4 MHz Amplifier (A)

The 321.4 MHz Amplifier provides a broad-band fixed gain of approximately 18 dB to the incoming 321.4 MHz IF signal. The amplifier is a single-stage common-emitter transistor amplifier whose gain is determined by the high frequency characteristics of Q10, the input matching bandpass filter, and the output matching elements L 3 and C8. The 3 dB bandwidth of the input bandpass filter is approximately 500 MHz (with 150 MHz and 650 MHz as the 3 dB points). The filter comprises series capacitor C 1 , two shunt capacitors, C 2 , and C 3 , and series inductors L1 and L2. This bandpass filter attenuates the first and second LO feedthrough to prevent overloading of the amplifier and to minimize spurious responses. Bias to RF amplifier transistor Q10 is provided by Q9 and R3 through L25. Note that Q9 and associated components are RF decoupled by C6 and C7.

### 321.4 MHz Bandpass Filter <br> (C)

The 321.4 MHz Bandpass Filter rejects the image frequency from the Second Converter Assembly A5 and limits the signal power applied to the mixer in the Third Converter Assembly A10 to a 3 dB bandwidth of about 9 MHz . The filter consists of four LC resonators that are tap-coupled at the input and output of the filter and capacitively coupled between sections by traces on the printed circuit board. The center frequencies of the four poles are adjusted by $\mathrm{C} 9, \mathrm{C} 10, \mathrm{C} 11$, and C 12 .

## 300 MHz Oscillator (D)

Transistor Q1 and associated circuitry form a grounded-base Colpitts oscillator. Direct collector current for Q1 is supplied through L8, whose internal parallel capacitance causes it to self-resonate at 300 MHz . Inductor L12 and capacitors C15, C16, and C17, form a tank circuit that feeds back the collector current of Q1 to its emitter. The frequency of the tank circuit is selected by tuning L12. Power is tapped out of the tank circuit through C18 and L11 and sent to Q2, a buffer amplifier that distributes the power and provides a constant load to the oscillator.

The 300 MHz buffer amplifier isolates the oscillator from the mixer and provides the high-level signal required to drive the mixer. The buffer amplifier is a common-emitter amplifier in which R10 and R11 set the emitter current. Base current is supplied, through self-resonant L9, from R5 and R6. Inductor L13 and capacitor C19 form a matching network that matches the impedance of the signal applied to the mixer's (U1) LO input. A test port is provided, through R4 and J1, to monitor frequency and amplitude of the 300 MHz Oscillator (Third LO). Voltage regulator U2 and its associated circuitry provide a regulated power supply for Q1 and Q2.

## Double Balanced Mixer (E)

The Double Balanced Mixer (U1) mixes the 321.4 MHz second IF from the 321.4 MHz Amplifier with the 300 MHz Oscillator. This produces the sum and difference frequencies, 621.4 MHz and 21.4 MHz , that are sent to the IF Preamplifier. The 621.4 MHz mixing product is removed by the matching filter at the input of the IF Preamplifier. Inherent in the double balanced mixer is excellent port-to-port isolation.

## IF Preamplifier (F)

The IF Preamplifier voltage gain is provided by Q8 in a common-emitter amplifier configuration. Circuit gain is controlled with collector-to-base feedback through PIN diode CR4. The current through CR4 is adjusted from the front panel by the REF LEVEL CAL control and can vary the gain of the IF Preamplifier over a 10 dB range. Transistor Q7 functions as an emitter follower buffer amplifier.

## Flatness Compensation Amplifier (H)

Approximately 20 dB of compensation is available in the Flatness Compensating Amplifier to compensate for small changes in conversion efficiency that occur while sweeping through individual bands. Larger betweenband changes in conversion efficiency are compensated for in the Band Conversion Loss Amplifier. The gain of the Flatness Compensation Amplifier is controlled by the Non-Linear Current Source, which draws current through PIN diode CR1. The more current it draws, the lower the gain.

## Non-Linear Current Source (G) <br> (G)

The flatness voltage from the Step Gain Assembly A12 sets the base voltage of Q3. Resistors R41, R42, R43, and diode CR5 establish the emitter current and cause it to vary non-linearly in response to changes in the base voltage. This non-linear current drives CR1 and enables the gain of the Flatness Compensation Amplifier to be proportional to the base voltage (and flatness voltage) at about 0.4 V per dB of gain.

## Band Conversion Loss Compensating Amplifier (I)

The Band Conversion Loss Compensating Amplifier changes gain in discrete steps to compensate for the changes in conversion Ioss associated with RF section harmonic band switching. In the fundamental mixing bands (Bands 1 and 2), the circuit has unity gain. During second harmonic mixing (Bands 3 and 4), CR2 is forward biased, allowing the gain to be set by R34 as shown in the following equation: Gain $=1+\mathrm{R} 32 / \mathrm{R} 34$. In the third harmonic mixing mode (Bands 5 and 6), CR3 is forward biased and R36 establishes the gain as follows: Gain $=1+\mathrm{R} 32 / \mathrm{R} 36$. See Figure $8-41$ for a simplified schematic of the Band Conversion Loss Compensating Amplifier gain switching. A gain-versus-band table is shown on the Third Converter Assembly A10 schematic below function block I.


## 35 MHz CalibrationOscillator (B)

The 35 MHz Calibration Oscillator consists of a differential amplifier formed by Q11 and Q12. A frequency determining tank circuit (L21, C45, and C46) is connected to the base of Q11. The base of Q12 and one side of the tank are at RF ground due to C48. Capacitor C45 temperature-compensatesthe oscillator; R13 controls the bias current and output amplitude. As the base voltage of Q11 increases, the voltage at the emitters of Q11 and Q12 increases. Since the base of Q12 is effectively at signal ground, the increase in voltage at its emitter reverse biases its emitter-base junction, shutting Q12 off. As Q12 shuts off, the voltage at its collector increases and is fed back in phase to the tank at the base of Q11 through C47. The output is taken from the collector of Q11, filtered to lower harmonic content, and sent to the CAL OUTPUT connector on the front panel.

## Power Supplies (

Three supply voltages power the Third Converter Assembly A10: $+15 \mathrm{VF},-10 \mathrm{~V}$, and -10.6 VF . The +15 VF is derived from the +15 V supply line and is filtered as it enters the board. The -10 V and the -10.6 VF originate from the -12.6 V supply line. After filtering, the -12.6 V supply feeds a shunt regulator comprising R48, C53, VR1, and VR2 and develops the -10 V supply. The filtered -12.6 V supply also feeds three-terminal regulator U2, which develops the -10.6 VF supply. Regulator U2 improves isolation of the 300 MHz Oscillator from the supply lines and reduces spurs caused by oscillator harmonics.

## THIRD CONVERTER ASSEMBLY A10, TROUBLESHOOTING

## CAUTION

Spring contacts are used on the circuit board to ground portions of the circuitry to the aluminum extrusion walls. Care is required when removing the circuit board to prevent damaging these springs. The circuit board must be installed in the extrusion before attempting to adjust the 321.4 MHz Bandpass Filter (block C).

Low Gain: Most common failures are: CR1, CR4, the PIN diodes in the IF preamplifier, and the Flatness Compensation Amplifier.

300 MHz Oscillator off Frequency: Most common failures are C16, C17, and C18.
35 MHz Oscillator off Frequency: Most common failures are C45 and L21.

Bes]e

TABLE 8-7. THIRDCONVERTER ASSEMBLY A10, REPLACEABLE PARTS (1 OF3)

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A10 | 05359-60040 | 8 | 1 | THIPD CONUERTCR ASSEMELY | 28483 | 38559-60380 |
| A10C: | 0160-3974 | 2 | 1 | CAPACITOR FXD 10 CF +-. SPF 2gCUDC CER | 28480 | 016.0 .3874 |
| 41, ${ }^{\text {a }}$ ( | 31603673 | 1 | 3 | CAPACTTGR-FXD 4.JPF $-\cdots .5 P T$ 2JJVLC CER | 28480 | 3160-3873 |
| A10C3 | c160-3873 |  |  | CAPACITOR-FXD $4.7 \mathrm{PF}+.59 \mathrm{~F}$ 20EUDC CER | 28480 | $0160-3873$ |
| A1 114 | 3169-2055 | $\stackrel{?}{5}$ | 32 | CAPAECTTGR-FXD , 31UF 180-23\% 103VDC CER | 28483 | 3160-2355 |
| Al 0 CS | 0160-3877 | 5 | 2 | CAPACITOR-「XL 1605 C +-26\% 26OUDC CER | 28480 | c16.0 3877 |
| A10CE, | 0160-3878 | 5 | $?$ | CAPACIIOR-FXD 1333PF - $23 \pm$ 10JVUC CER | 23480 | 0168-3878 |
| A10C7 | 0160-3978 | ¢ |  | CAPACITOR-FXD $10005 F+-202$ 10DUDC CEE | 28480 | 6160-3878 |
| A10CG A 10 CO | 3160-3873 | 1 |  | CAPACTTTR FXD A.7PF 1 -, SP F 2JJVDC CER | 28480 | 3163-3873 |
| A11C. 3 | 3121 0453 | 5 | 4 | CAPACITOR-U TRMR-AIR $1.3-5.4 P T$ 17SU | 74970 74770 | 107-0303-125 $187-3333-125$ |
| ATGC11 | 0121-0453 | 5 |  | CAPACITRR-U TFMR-ATR 1.3 S.4PF 1750 | 74970 | 107-0303-135 |
| Ataric | 0121.0453 | 5 |  | CAPARITER-U TRMR A12 1.35 S. APF 1750 | 74975 | 187-3393-1:5 |
| A) 0 C13 | C160-3456 | 6 | 8 | CAPACITOR-FXD 100 EPT + $10 \% 1$ KUDC CER | 20480 | $0160-3456$ |
| A10¢14 A10C15 | $3160-3456$ $0150-0059$ | E | 1 |  | 28489 28480 | $3160-3456$ $0150-0059$ |
| A10¢16 | 3160 22954 | 0 | 1 | CAPACITIR FXD 7.5.9F, ESPF SOOULC CER | 28485 | 2160-2254 |
| A10C17 | 0150-0115 | 7 | 2 | CAPACITOR-FXD 27PF + $16 \%$ S0CUDC CER | 28480 | $6150-0115$ |
| A10C18 | 0160.345.6 | 6 |  | CAPACIITIR-FXD $1030 \mathrm{PF}+-10 \%$ 1KULC CER | 28483 | 3160-3456 |
| A10C19 A1 ces | $0160-3456$ $0163-3456$ | 6 6 |  |  | 23488 78480 | 816.0-3456 $3160-3456$ |
| A 10001 | 6160-345 6 | $t$ |  | CAPACITOR-FXD $10 \mathrm{GORF}+\cdots 10 \% ~ 1 K U D C ~ C E R ~$ | 23480 | 616.0-3456 |
| A19C2? | $3160 \cdot 3533$ | c | 1 | CAPARETTCR FXD 47OPF + 58 33JVDC MTCA | 28480 | 9150-3533 |
| Al $0 \mathrm{C}_{2} 3$ | 0160-2655 | 9 |  |  | 23480 | $016.0-2055$ |
| A10re 4 | 0160-2055 | 2 |  | CAPACTIOR-FXD OIUF \%80-23\% 100NDE CER | 28489 | 3160-2055 |
| A10C25 | 0160-2055 | 9 |  | CAPACITOR-FXL , C1UF + $30-20 \%$ 100UDC CER | 20480 | $016.0-2055$ |
| Alarst | 0160.2055 | 5 |  | CAPACIITIR-FXD . 314 F +83-23\% 1330 VEC CER | 28480 | 0160-2a55 |
| Al $10 C 27$ A 1053 | 6160-2055 | 9 |  | CAPACITOR - $5 \times D$. $014 \mathrm{UF}+8 \mathrm{C}-20 \%$ 100UDC CER | 28480 | 016.6-2055 |
| Aloces | 3160 $0160-2655$ | 9 |  |  | 23480 28480 | $3160-2055$ $0160-2055$ |
| A1)039 | 0160.2355 | 5 |  | CAPACITIR-FXD .01UF 130232 130UEC IER | : 0480 | 3160-2355 |
| A. 0C31 | c160-2055 | 9 |  | CAPACITRR-FXD .01UF +80-26\% 10RUDC CER | 28480 | 016.62055 |
| Albe: | 0160 2355 | 2 |  | CAPAETTGR FXD 3113F $+83-23 \%$ 1JJVLC CER | 5.3480 | 3160-2055 |
| A10C33 | 0160-2055 | 9 |  |  | 20480 | e160-2055 |
| A1] 3.4 | 31533 2as5 | 5 |  | CAPAC, 1 TGR FXD - 31UF - $83-23 \% 1000 \mathrm{CC}$ C:R | 28483 | 3160-2355 |
| Al0C3: | c160-265s | 9 |  | CAPACITOR - FXD , 01UF + RG-20\% 10CUDC CRE | 28480 | 016.c-2055 |
| 013036 | 0160-2055 | 5 |  |  | -848: | 3160-2055 |
| A10C37 | 0160-2655 | 9 |  | CAPACTTOR-FXL , O1UF + 30-2R\% 100UDC CEF | 29480 | 0160 205s |
| A13530 | 2160-3456 | 6 |  | CAPACIITR-FXD 1399PF + 13\% 1KULC CER | 28480 | 3160-3456 |
| A10039 | 0160-2cs5 | 9 |  | CAPACITOR - EXD CE1UF + $30-28 \% ~ 100 \cup D C ~ C F E ~$ | 23480 | c160-2055 |
| A10cma | 0160-3456 | A |  | CAPACITUR-FXD 1a3GPF + $13 \%$ IKULC CER | 28480 | 3160-3456 |
| $\mathrm{A}_{10 \mathrm{C}} \mathrm{A}_{1}$ | 0160-205s | 9 |  |  | 28480 | C16.0-2055 |
| A10c42 | 3160-2055 | 7 |  |  | 28488 | 3160-2055 |
| A10C43 | 0160-2253 | 9 | 1 |  | 28400 | 0160-2253 |
| A10C 14 | 3160-2355 | 7 |  |  | 2:8489 | 3160-2055 |
| a $10 \mathrm{C45}$ | 0150-0115 | 7 |  | CAPACITOR -FXD 27PF + $10 \%$ 53SUDC CER | 20480 | c150-0115 |
| A10C46 | 0121-9195 | 4 | 1 | CAPACTTGR-V TRMR-CER 9-35PF 2030 PC-MTG | 52763 | 304324 9/35PF 16650 |
| A10C47 | 0160-3877 | 5 |  | CAPACITOR - $\times$ XD $106 P F+-20 \% ~ 200 U D C ~ C E R ~$ | 28480 | $0160-3877$ |
| ${ }^{\text {A } 10 C 48 ~}$ | 0160-2055 | 9 |  | CAPACTICR-FXD , J1UF +80-33\% 130ULC CFR | 28480 | 0160-2355 |
| A10C49 | 0160-2055 | 9 |  |  | 28480 | 0160-2055 |
| A10C50 | 0160-4457 | 9 | 1 | CAPACITUR-FXD S1PF +-5\% 330UDC MICA | 29480 | 0160-4457 |
| A10C51 | 0160-2529 | 2 | 2 | CAPACITTOR-FXD 16OFF - 22 300UDC MICA | 20488 | 0160-2529 |
| A10C52 | 0160-2529 | 2 |  | CAPACITOR-FXD 160PF + $2 \times 300 \mathrm{VDC} \mathrm{MTCA}$ | 28483 | 3160-2529 |
| A 10 CLS 3 | 0180-0197 | 8 | 1 | CAPACITOR FXD 2. 2 UF $+10 \%$ 2CUDC TA | 56.289 | $150 \mathrm{Da25} \mathrm{\times 9020A2}$ |
| A10C54 | 0140-0199 | 6 | 1 | CAPACITGR-FXD 243PF +-5\% 330VDC MICA | 72136 | DMISF241J9300WU1CR |
| A10C55 | 0160-2205 | 1 | 1 | CAPACITOR-FXD 120PF +-5\% 300UDC MICA | 28480 | 0160-2205 |
| A1 0 OL56 A 10 O 57 | $0160-4490$ $0160-4084$ | ${ }_{0}^{9}$ | 1 | CAPACITCR -FXD 1. GPF 1-.25PR 200ULC CER | 23480 | 3160-4490 |
| A $10 \mathrm{CL5}$ | 0160-4084 | 8 | 1 | CAPACITOR-FXD 1UF +-20\% 50UDC CFR | 29480 | 01664084 |
| A10C58 | $0180-0291$ $0180-1746$ | 5 | 1 | CAPACITOR-FXD 1UF $-10 \times 35 \mathrm{SVCC}$ TA | 56239 | 15JD135 9035 AL |
| A10CS9 | 0180-1746 | 5 | 1 | CAPACITOR-FXD 15UF-10\% 20UDC TA | 58289 | 150D156×902082 |
| A1 JCR 1 | 1901-1070 | 7 | 2 | DIODE PJN 1100 | 28433 | 1901-1070 |
| A10CR 2 A1 OCR A | 1901-0050 | 3 | 3 | DIODE SWITCHING QOU 200MA TNS DO 35 | 28480 | 1901-0050 |
| A10CR 3 A $10 C R 4$ | 1901-0050 | 3. |  |  | 28480 | 1731-0050 |
| A10CRS | $1901-1070$ 19010050 | 9 3 |  | DIODE FIN 110 C DIODE SWITCHING BOU 2DOMA ENG DO 35 | 28480 28480 | $1901-1070$ $1901-0050$ |
| A10E1 | 9170-0029 | 3 | 4 | CORE-SHIELDING ERAD | 28480 | 9170-0029 |
| A1 0E2 | 9170-0029 | 3 |  | CORE-SHIELDING EEAD | 28480 | 9170-0029 |
| A10E3 | 9170-0029 | 3 |  | CORE-SHIELDING BTAD | 28480 | 9176-0029 |
| A1OE4 | 7170-0029 | 3 |  | CORE-SHIELDING EEAD | 28480 | 9170-0029 |
| A10.1 | 1250-0691 | 7 | 1 | CONNECTOR RF Snn m Scl-hot E-Fr 50\%OHM | 28480 | 1250-0691 |

TABLE8.7. THIRDCONVERTER ASSEMBLY A10,REPLACEABLEPARTS (2OF3)

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A1321 | 55683-60937 | 3 |  | INDUCTOR 35 NH | 23483 | 95t30-80019 |
| A1012 A1313 | 85880-86069 $7130-7671$ | 4 |  |  | 28480 -8480 | $83606-86009$ $9131-2571$ |
|  | 85660-86062 | ${ }^{2}$ | 2 | COIL TAPPED | 28480 | $05,665-8600 ?$ |
| A1345 | 8355980812 | E |  | COIL FILTER | - 8 \%80 | 38559-80312 |
| A1006 A1917 | 68559-86012 $\square 5669-8032$ | $\stackrel{8}{8}$ |  | COIL PILTER COIL TAPPED | 28480 28480 | 188359-86.612 $65660-80032$ |
| ${ }_{\text {Al }}^{\text {Al } 1917}$ | $98100-2236$ | 5 | 6 | INDUCTOP RF-CH-MED $560 \mathrm{NH} 10 \%$, 1650X, 26LG | 23480 | ${ }_{9100-2256}$ |
| A1319 | 9130-2256 | 5 |  | INTLCTIR RF-CH-mid S63NH $13 \% .1350 \times .26 L 6$ | 2R483 | 2190-2256 |
| AlOL10 | 9100-2256 | 5 |  | INDUCTOR RF-CH-mLD $560 \mathrm{NH} 16 \%$.16SDX. 26 LG | 28480 | 9160-2256 |
| 6130.11 | 2130-2250 | 7 | 1 | INELCTGR RF-CH-MLD $183 \mathrm{NHH} 13 \%$, 135DX. 26 L G | 88480 | 2120-2259 |
| A10L12 | 68557-80001 $7130-2256$ | 3 | 1 |  | 28436 <br> 28480 <br> 180 | $08357-86601$ $9133-2256$ |
| A10L14 | 9100-2256 | 5 |  |  | 23488 | 7100-2256 |
| A10115 | 9130-1613 | 3 | 1 | INDICHITR RF-CH-m, | 28483 | 7133-1610 |
| A10101 16 A11 A | $9140-6111$ $7140-2112$ | 1 2 | 1 |  | ${ }_{238489}^{23489}$ | $\begin{aligned} & 914 \mathrm{C}-0111 \\ & 9140-3112 \end{aligned}$ |
| A10L18 | 9100-1618 | 1 | 1 | INDICTOR RF-CH-MLD 5.60 H 1 cz | 23480 | $7100-1618$ |
| A13L19 | 9130-2247 | ${ }^{4}$ | 2 |  | 20480 | 9130-2247 |
| A 10 L 20 | 9100-2247 | 4 |  | INDUETOR R - CH-MLD $160 \mathrm{NH} 16 \%$.105DX, 26LS | 284日 | $9106-2247$ |
| A 10121 | 2130-2252 | 1 | 1 | INDUCTGR RF-CH-大aD 273mat 13\%, 135DX, 265 | 28480 | $9130-2252$ |
| Al0l2z A10L23 | $9140-0179$ $7109-2256$ | $\frac{1}{5}$ | 1 |  | 28480 78480 | $914 \mathrm{C}-0179$ $9130-2256$ |
| A10L24 | 9100-2251 | 0 | 1 |  | 28480 | 9106-2251 |
| A19125 | 7100-2255 | 4 | $t$ | INDLCTOR RF - CA-mLD 47364132 , 1350x, 26LG | 28483 | 9130-2255 |
| A10126 A10L 27 | $9100-6368$ $9100-1613$ | 6 | 1 |  | 23480 28489 | 91000369 $9100-1613$ |
| A1001 | 1854-0546 | 1 | 2 | TPANGISTOR NPN SI TO-72 PD=2COMW | 28480 | 185.4-0546 |
| A1002 | 1054-3247 | $\stackrel{7}{7}$ | 4 |  | 20480 | 1854-0247 |
| A1003 A 11004 | $1854-0023$ $1354-3546$ | 9 | 1 | TRANGTGTOR NPN ST TO 10 PV 360MW |  | $1854-0023$ $1654-0546$ |
| Al 1005 | 1853-0007 | 7 | 1 |  | C 4713 | 2N3251 |
|  | $1854-9247$ $1854-0247$ | 9 |  |  | 28480 25480 | 1654-9247 |
| A1:103 | $1654-0247$ | 9 |  | TRANSTSTTR NPN SI Ti-39 PD=1W FT=803MHZ | 28489 | 1554-3247 |
|  |  |  |  |  |  |  |
| $\begin{aligned} & A 10 Q 11 \\ & \text { A13Q12 } \end{aligned}$ | $\begin{aligned} & 1854-0019 \\ & 1554-0319 \end{aligned}$ | $\stackrel{3}{3}$ | 2 | TRANSTDTOP NPN ST TO 18 FD 360 MW TRANGTSTOR NPN SI TO 18 PD=36BMW | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 1854-0019 \\ & 1554-0319 \end{aligned}$ |
| A OR1 | 0757-0260 | 7 | 1 |  | 24546 | C4-1/8-T0-5621-F |
| A1 OR? A 1083 | $3757-3288$ $0757-0416$ | 1 | 1 | RESISIOR RESISTOR 5111 S | 19731 24546 |  |
| A1JR4 | 0698-0082 | 7 | 2 | RESISTER 464 ix , 125W F TC=34-100 | 24546 | C4-1/8-70-4640-F |
| A1 OR5 | 0757-0280 | 3 | 2 | RESISTOR 1 K 12.125 W F TC=0+-100 | 24546 | C4-1/8-T0-1061-F |
| Aljrg | 0757-0419 | 0 | 1 | RESISTOR GB1 1\% , 125L C TC=0t-100 | 24546 | C4-1/8-T0-681R-F |
| A 10 R 7 A 10 RB | $0757-0401$ $0698-0002$ | $\stackrel{0}{7}$ | 4 |  | 24546 24546 | $\mathrm{CA}-1 / 8-\mathrm{TO}-101-\mathrm{F}$ $\mathrm{C} 4-1 / 8-\mathrm{TO}-4640-\mathrm{F}$ |
| A 10 R9 | 0757-0346 | 2 | 5 | RESISTOR $101 \%$. 1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-10R0-F |
| Alorio | 0757-0346 | 2 |  |  | 24546 | C4-1/8-T0-10R ${ }^{-5}$ |
| Alor 11 A1 A 12 | $0757-0401$ $0698-3155$ | 0 |  | RCSISTOR RESISTOR a | 24546 24546 | C4-1/8-T0-101-F $\mathrm{C4-1/8-70-4641-F}$ |
| Aloriz | 269800545 $2100-054$ | 4 | 1 | RESISTOR-TRMR 1 K ( $10 \%$ C SIDE ADJ 17 TRN | 32997 | 3292x-1-102 |
| A1 JR14 | 0757-0279 | a | 1 | RESISTOR 3.16K $1 \%$ 125W F TC $=0+100$ | 24546 | C4-1/8-70-3161-F |
| A10815 | 0757-0438 | 3 | 2 | RESIGTOR 5 11k $1 \%$. 125 L F TC=0+-100 | 24546 | C4-1/8-T0-5111-F |
| Al0rib | 0698-0035 | $a$ | 1 | RESISTGR 2.61 K 1\% 12.125 W F TC=0t-100 | 24546 | C4-1/8-T0-2611-F |
| A10R17 A $10 R 18$ | $0698-3449$ $0698-3440$ | ${ }^{6}$ | $\stackrel{1}{2}$ |  | 24546 24546 | C4-1/8-T0-2872-F $\mathrm{CA-1/8-T0-196R-F}$ |
| A10R19 A1 10 R 19 | $0698-3440$ $0698-8821$ | $\stackrel{7}{8}$ | 2 | RESISTOR $5.62 \%$ 1\% 12554 F TC $C=0+-160$ | 28480 28480 | 8698-8821 |
| A10R20 | 0698-3440 | 7 |  | RESISTOR $1961 \%$ 12SW F TC=0+-109 | 24546 | C4-1/8-T0-196R-F |
| A1 OR21 A 10 R 22 | $\begin{aligned} & 0757-0280 \\ & 0757-0346 \end{aligned}$ |  |  | RESISTOR 1 K 1 X .125 W F TC=C $\mathrm{C}-100$ RESISTOR $101 \%$. 125. W F TC $=0+\cdots 130$ | 24546 24546 24546 | C4-1/8-T0-1001-F C4-1/8-T0-10R0-F $C 4$ |
| ${ }^{\text {A } 10 R 23}$ | 0757-0440 | 7 | 2 |  | 24546 24546 | C4-1/8-T0-7501-F $\mathrm{C4-1/8-70-7531-F}$ |
| A10R24 A10R25\% | 0757-0449 $0757-0397$ | $\stackrel{7}{3}$ | 1 |  | 24546 24546 | C4-1/8-T0-6881-F |
| A10R26 | 0698-3443 | a | 4 | RCSISTOR $2871 \%$. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-287R-F |
| A1 OR27 | 0757-0346 | 2 | , | RCSISTOR $101 \% .125 W \mathrm{~F} T \mathrm{~T}=0+100$ | 24546 | C4-1/8-T0-10R0-F |
| A10R28 A 10 R 29 | -0757-0442 | $\frac{5}{3}$ | 2 |  | 24546 24546 | C4-1/8-T0-5111-F |
| A10R30 | 0757-0346 | $\underset{\text { a }}{ }$ |  | RESISTOR 10 1\% . 12 Siw F TC $=0+-100$ | 24546 | C4-1/8-T0-10R $0-F$ |
| Al OR31 | 0698-3443 | a |  | RESISTOR $2871 \% .125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-287R-F |
| A10R32 | 0757-0418 | 5 | 1 |  | 24546 24546 | C4-1/8-T0-619R-F |
| A10R33 A10R34 | $0698-3444$ $0698-3446$ | $\stackrel{1}{3}$ | 1 |  | 24546 24546 24546 | $\mathrm{C4}-1 / 8-\mathrm{T} 0-316 \mathrm{P}-\mathrm{F}$ $\mathrm{C4-1/8-T0-383R-F}$ |
| A10R35 | 0698-3443 | a |  | RESISTOR 287 1\% .125W F TC=0+-100 | 24546 | C4-1/8-T0-287R-F |

TABLE 8-7. THIRD CONVERTER ASSEMBLY A10, REPLACEABLE PARTS(3OF3)


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FIGURE 8-42. THIRDCONVERTER ASSEMBLYA10,BLOCK DIAGRAM


FIGURE8-43. THIRDCONVERTER ASSEMBLY A10,COMPONENT LOCATIONS


## BANDWIDTH FILTERS No. 1 and No. 2 ASSEMBLIES A II and A13, CIRCUIT DESCRIPTION

Bandwidth Filters No. 1 and No. 2 Assemblies A11 and A13 are identical except for some off-board connections. Bandwidth Filter No. 1 Assembly A11 is described here. Bandwidth Filter No. 1 Assembly A11 operates at 21.4 MHz with a variable bandwidth of 3 MHz to 1 kHz . The RESOLUTION BW switch selects one of the following eight available bandwidths: $3 \mathrm{MHz}, 1 \mathrm{MHz}, 300 \mathrm{kHz}, 100 \mathrm{kHz}, 30 \mathrm{kHz}, 10 \mathrm{kHz}, 3 \mathrm{kHz}$, or 1 kHz .

Four stages of filtering are used for all eight bandwidths; each assembly contains two stages. The bandwidths from 30 kHz to 1 kHz are obtained from synchronously-tuned crystal filters. The remaining four bandwidths ( 100 kHz to 3 MHz ) use synchronously-tuned LC tank circuits. The four crystal filter stages contain factory selected and matched crystals (A11Y1, A11Y2, A13Y1, and A13Y2) that must be replaced as a set. If replacement of a bandwidth filter assembly is necessary, the new assembly is shipped with two crystals installed and two packaged separately to replace the crystals on the other assembly. In addition to the filter stages, each board contains a 10 dB Buffer Amplifier, a Unity Gain Buffer Amplifier, and an Output Buffer Amplifier.

## 10 dB Input Buffer Amplifier <br> (B)

The 10 dB Input Buffer Amplifier is shown as a noninverting operational amplifier in Figure 8-45. Gain for the amplifier is expressed in the equation: Gain $=1+\mathrm{R}_{\mathrm{t}} / \mathrm{R}_{\mathrm{in}}$. The total resistance of R5, R6, and R7 forms the feedback path $\left(\mathbf{R}_{\mathrm{f}}\right)$; R3 forms the input resistance $\left(\mathrm{R}_{\mathrm{i}}\right)$. This ac model of the amplifier's operation is true for all but the narrowest bandwidths, as illustrated later.


FIGURE 8-45. 10 dB INPUT BUFFER AMPLIFIER GAIN MODEL
Two current paths are used for dc bias in the input buffer amplifier, one for crystal filter poles, another for LC filter poles. When a crystal filtered bandwidth ( $\leq 30 \mathrm{kHz}$ ) is selected, Q3 (block D) and Q1 are the sources for the current through Q2 (see Figure 8-46). The base voltage of Q2 is fixed by the divider R9 and R10, while the

emitter is fixed by R8. The collector, therefore, becomes a constant-currentsink for 20 mA of current supplied by Q1 and 43. A decrease in the current supplied by Q3 results in increased current through Q1, keeping the current through Q2 constant. If an LC filtered bandwidth is selected, BW5F (filtered bandwidth control line 5 in block C) supplies current via CR1 and R13 (see Figure 8-47); Q3 is effectively removed from the circuit.


FIGURE 8-47. DC BIAS PATH DURING LC POLEOPERATION
To understand how $\mathbf{Q} 3$ functions during crystal filtering modes, a new model is needed. (See Figure 8-48.) Resistor R7 has been omitted to simplify the model. The emitter load of $\mathbf{Q} 3\left(\mathrm{R}_{\mathrm{t}}\right)$ is the series combination of the internal resistance of $\mathrm{Y} 1\left(\mathrm{R}_{\mathrm{s}}\right)$ and a resistance determined by the bandwidth selected (see First Xtal Pole description). The crystal's series resistance at resonance $\left(R_{s}\right)$ is constant at about 10 ohms. In the 30 kHz bandwidth, R23* is in series with $R_{8}$. Since R23* is very large by comparison, it represents the total load on $43\left(\mathrm{R}_{1}\right)$. When R23* is substituted into the gain equation for $R_{r}$, a gain of $2.7(8.6 \mathrm{~dB})$ results. This is roughly equal to the gain without 43 in the circuit. In fact, the larger $R_{r}$ becomes, the closer the gains become.



Then: OAIN $-\frac{1+\frac{185.7}{110}}{1-\frac{23.7}{82.50}}-2.89$ OAIN $2.70 \simeq 8.6 \mathrm{~dB}$

FOR 1K BW:
When: $R_{t}=70 \Omega$
Then: OAIN $-\frac{2.69}{.66} \simeq 4.0 \simeq 12 \mathrm{~dB}$

When the 1 kHz bandwidth is selected, CR4 is biased on and has a resistance of about 60 ohms . This resistance forms a voltage divider with $\mathrm{R}_{\mathrm{s}}$ that results in signal amplitude loss across the crystal. Increased gain in the input buffer amplifier, caused by the load on 43, compensates for these losses. The gain increase occurs when the reduction in $R_{t}$ turns 43 on even harder, resulting in some of the feedback from R6 being shunted to ground through the collector of 43. This reductionin negative feedback increases the gain of the input buffer amplifier. By substitutinginto the gain formula the 1 kHz bandwidth $\mathrm{R}_{\mathrm{t}}(10+60=70 \mathrm{ohms})$, a new gain of $4.0(12 \mathrm{~dB})$ is derived.

## First Xtal Pole (D)

Crystal filtering is used for bandwidths of $1 \mathrm{kHz}, 3 \mathrm{kHz}, 10 \mathrm{kHz}$, and 30 kHz . Individual poles have a bandwidth about 2.3 times the selected bandwidth, and each filter board assembly (two poles combined) has a bandwidth of about 1.5 times the selected bandwidth. For example, when the 1 kHz bandwidth is selected, each pole has a 3 dB bandwidth of about 2.3 kHz , each assembly a bandwidth of 1.5 kHz . The signal from the input buffer amplifier is routed to 43 and to compensation amplifier 44. (The action of 43 is discussed in the 10 dB Input Buffer Amplifier description.) From 43 the signal is applied to the crystal (Y1), where it is filtered before going to the unity gain buffer amplifier.

The crystal functions as a series-resonant filter tuned to 21.4 MHz . An equivalent circuit is shown in Figure 8-49. Parallel capacitance $C_{0}$ is the result of terminal and case capacitances in the crystal; $R_{s}$ is the effective resistance at resonance (about 10 ohms ). Both $\mathrm{C}_{0}$ and $\mathbf{R}_{s}$ are detrimental to the pole's performance, so compensation is used to nullify their effects. Because they are cancelled, $\mathrm{C}_{\mathrm{o}}$ and $\mathrm{R}_{\mathrm{s}}$ are not shown in the simplified crystal pole schematic.


FIGUREJ3-49. CRYSTALMODEL

Pin diode CR4 (see Figure 8-50) controls the filter's bandwidth by functioning as a variable resistance at 21.4 MHz. The voltage applied to BW6F controls the current through CR4 and its resistance. An increase in current decreases the resistance and narrows the bandpass.

The crystal presents a low impedance ( $\mathrm{R}_{\mathrm{s}}$ ) to the signal at resonance, hence signal voltage is developed across CR4. As the signal frequency varies from the center frequency ( 21.4 MHz ), the impedance of the crystal increases, making it part of a voltage divider with CR4 and causing more signal voltage to be developed across the crystal. The frequencies at which crystal impedance and PIN diode resistance become equal are the 3 dB points of the bandpass. Varying the PIN diode resistance, therefore, varies the bandwidth.


FIGURE8-50. FIRST CRYSTALPOLE, SIMPLIFIEDSCHEMATIC

The case capacitance of the crystal ( C , ) would cause a second resonant point, or dip, in the bandpass if compensation were not used to nullify its effects. Compensation is provided by Q4 as a current equal to and opposite in phase with the current flowing through C,, as shown in Figure 8-51. Capacitor C15 (SYM) adjusts the phase of the compensating current.


The input capacitance of the unity gain buffer, the trace capacitances, and the capacitance of the PIN diode add, causing the center frequency of the filter to be altered. Compensation is used to eliminate this effect. These capacitances are tuned out by including them in a parallel resonant circuit (at 21.4 MHz ) formed with L 7 and fine tuned by C25 (CTR). Adjusting C25 tunes the circuit to present a high impedance at resonance.

When LC filtering is selected, BW5F forward biases CR2, effectively grounding the emitter of Q3. During crystal filtering, CR2 is reverse biased.

## First LC Pole (C)

LC filtering is used for bandwidths of $100 \mathrm{kHz}, 300 \mathrm{kHz}, 1 \mathrm{MHz}$, and 3 MHz . The relationship of an individual pole's bandwidth to the selected bandwidth is the same as the crystal pole's ( 2.3 times per pole and 1.5 times per assembly). The LC filter pole comprises a metallized inductor (L6) in parallel with four capacitors: the series combination of C16* and C20*, C21 (temperature compensation), and C23 (center adjust). This resonant circuit is driven through CR3, which functions as a variable resistor. Bandwidth control line BW7F establishes the current through CR3 and thereby controls the pole's bandwidth. Feedback from the unity gain buffer replenishes losses in the resonant circuit.

A simplified model of the LC pole is shown in Figure 8-52. At resonance, a voltage divider is formed between CR3 and the resonant circuit. The 3 dB points of the bandpass occur when the PIN resistance and the impedance of the resonant circuit are equal. Varying the PIN resistance varies the filter's 3 dB points. The higher the PIN resistance, the narrower the bandwidth. When the 100 kHz bandwidth is selected, CR3 is reverse biased and R19* sets the bandwidth; if one of the other bandwidths is selected, the parallel combination of R19* and CR3 is utilized. The intrinsic capacitance of PIN diode CR3 affects the bandpass, if not compensated for. Adjustable capacitance C73 (LC DIP) and L5 are in parallel with the PIN capacitance and allow it to be tuned out of the circuit.


FIGURE8-52. LCPOLEMODEL

A simplified schematic of the first LC pole is shown in Figure 8-53. The fundamental frequency-determining components are L6 and the center-tapped capacitance $\mathbf{C 1 6 *}$ and $\mathbf{C} 20^{*}$. Positive feedback is applied to the centertap at 21.4 MHz to compensate for losses in the tank circuit. The application of feedback makes it important that C16* and C20* be about the same value for proper pole operation. The level of the feedback is controlled by CR5, acting as a variable resistance. LC feedback control R26 establishes the current through CR5 and its resistance.


FIGURE 8-53. FIRSTLC POLE, SIMPLIFIEDSCHEMATIC

When an LC filtered bandwidth is selected, BW5F is at +15 V ; BW7F is at a voltage greater than or equal to +6.8 V and supplies bandwidth-determining bias current to CR3. Supply line + VF BIAS is always at +6.8 V . Control line BWSF reverse biases CR8 (block B), disabling the crystal pole, and forward biases CR1 (block B), opening the dc bias path to Q2 (see Figure 8-47). During LC operation, CR6 is reverse biased, keeping C28 out of the circuit. When a crystal filtered bandwidth is selected, BWSF forward biases CR6 and allows C28 to ground the signal path.

## Unity Gain Buffer Amplifier

Operation of the Unity Gain Buffer Amplifier is similar to the 10 dB Input Buffer Amplifier, except that it has an FET input (Q5) and unity gain. The input signal path is activated by the BWSF line, which switches on CR9 (during LC mode) or CR8 (during crystal mode).

When the crystal mode is selected, the current through the input FET (Q5) is determined by Q6 and constant current sink Q7 (which sinks about 4 mA ). During LC mode, current is supplied through R37 and CR10 from BWSE The input FET current is a good indication of the stage's operation and can be monitored by measuring the gate-to-source voltage. This voltage should be between +0.2 V and +1.5 V (an increase in current decreases the voltage).

Capacitor C68 and L19 form a feedback circuit that tunes Q7 to 21.4 MHz. Trimmer Resistor R31 (XTL FEEDBACK) adjusts the feedback and controls the stage gain as did R5 and R6 in block B.

## Second Xtal Pole (G)

The operation of the Second Xtal Pole is identical with the First Xtal Pole.

## Second LC Pole (F)

Operation of the Second LC Pole is the same as the First LC Pole, except that R56* performs the same function as PIN diode CR5.

## Output Buffer Amplifier (H)

The Output Buffer Amplifier is a complementary pair of transistors in which Q9 acts as a source follower with its output current boosted by Q10. The current through input FET Q9 is established by R53:

$$
\mathrm{L}_{m}=\mathrm{V}_{\mathrm{be}}(\mathrm{Q} 10) / \mathrm{R} 53
$$

Which becomes:

$$
\mathrm{I}_{m}=.7 / 196 \text { or about } 3 \mathrm{~mA} .
$$

The total current through Q9 and Q10 is set by R54. The input signal path is selected by either CR15 (during crystal mode) or CR16 (during LC mode).

## BANDWIDTH FILTERS No. 1 and No. 2 ASSEMBLIES A11 and A13, TROUBLESHOOTING

Observe front panel switch positions in relation to the problem to isolate the area of the failure.
Check for leaky diodes and capacitors. Loading of the signal path can alter either a pole's gain or bandpass shape or both.

Isolate crystal poles from LC poles to prevent interaction of failure symptoms. Isolation of the crystal poles from the circuit is best achieved by removing CR8 and CR15 (blocks D and G). Isolation of the LC poles is best achieved by removing CR9 and CR16 (blocks C and F).

TABLE88. BANDWIDTHFILTERNO. 1 ASSEMBLY AII, REPLACEABLEPARTS(1OF3)

\begin{tabular}{|c|c|c|c|c|c|c|}
\hline Reference Designation \& HP Part Number \& C \& Qty \& Description \& Mfr Code \& Mfr Part Number <br>
\hline A11 \& 00559 -60059 \& 0 \& 1 \& bandwtith Filter no. 1 astembly \& 28483 \& 9859.9-63353 <br>
\hline A11C1
A11c2 \& - $0160-2655$ \& ${ }^{2}$ \& 38 \&  \& 28496
F248 \& c160-2055
$3160-3127$ <br>
\hline  \& $0169-127$
$0160-2055$ \& 2 \& 1 \&  \& -28898 \& $3160-9127$
0166055 <br>
\hline Alics \& 0169-2355 \& ? \& \& CAPACITHR-FXD DILF VB0-23\% 1030 CLC CER \& 20480 \& 3160-2355 <br>
\hline A1 1 Cb \& 0160-2055 \& , \& \& CAPACITOR-FXD .01UF + 36 -20\% 100UDC CRR \& 23486 \& 616.62855 <br>
\hline Al1c7 \& 9160-2055 \& ? \& \& CAPACITGR-FXD J14F 103 23\% 130 OLCL CER \& 28489 \& 3160-2355 <br>
\hline ${ }^{\text {A } 11128}$ \& $0160-2207$
$0160-2055$ \& 3 \& 2 \&  \& 28,480
28489 \& ¢16.e-2207
$3160-2055$ <br>
\hline Al1c9
Al 1610 \& $3160-2055$
$0160-2055$ \& ? \& \&  \& 28483
2¢480 \& $3162-2355$
$0160-2055$ <br>
\hline ${ }_{\text {A11 }}{ }^{\text {A1 }} 11$ \& 0160-2055 \& \% \& \&  \& 20483 \& 3163-2355 <br>
\hline A11C12 \& 6160-2055 \& \% \& \&  \& 28986 \& $0166-2655$
$3160-3456$ <br>
\hline A112C13
A1 1 Cl 14 \& $3160-3456$
$0160-2249$ \& ${ }_{6}^{6}$ \& , \&  \& \%8483 \& - $1160-34566$ <br>
\hline A11C15 \& 0121-3359 \& 7 \& ? \& CAPACIIDR-U 1amR-CER 2 -fPF 3530 PC -mIG \& 52763 \& 334324 2/8PF NPO <br>
\hline A11C16* \& c160-0134 \& 1 \& 4 \& CAPACTTOA-FXD 22EPF +-5\% 30GVDE MICA \& 23480 \& 016.61384 <br>
\hline A11c17 \& 0160-2055 \& ? \& \&  \& 28493 \& 3160-2355 <br>
\hline A11C18 ${ }_{\text {Al1 }}^{\text {Al }}$ \& $6160-2655$
$3160-2055$ \& ? \& \&  \&  \& $6160-2055$
$3160-2355$ <br>
\hline A $11 \mathrm{Cl20*}$ \& 0180-0134 \& 1 \& \& CAPACITOR-FXD 22OPF +5\% 360VDC MTCA \& 2a896 \& 0160-0134 <br>
\hline A11c21 \& 0160-0437 \& 7 \& 2 \& CAPGCITCLR-FXD TEPF $+5 \%$ STOVLC CER \& 22483 \& 3160-0437 <br>
\hline A11622 \& c160-4084 \& ${ }^{\text {a }}$ \& 3 \&  \& 2anco \& 0160-400.4 <br>
\hline ${ }^{\text {A1 } 11023}$ \& 0121-0036 \& ? \& ? \& CAPACTITR-U TRMR-EER 5.5-119PF 3530 \& 5:763 \& $3043245.5 / 108 \mathrm{~F}$ NPO <br>
\hline A11C24
A11C25 \& $0160-2055$
$0121-2446$ \& ? \& ? \&  \& 20480
2.480 \& $0160-2055$
$3121-0446$ <br>
\hline A11c26 \& 0160-2655 \& , \& \& CAPACITOR FXD -011F + 06 26\% 108UDC CER \& 23480 \& E160 2055 <br>
\hline Allcas \& 3160-2055 \& \% \& \&  \& 28480 \& 3160-2355 <br>
\hline  \& $0160-2055$
$3163-3456$ \& B \& \&  \& 28480
28489 \& $6160-2055$
$3160-3456$ <br>
\hline A11c30 \& 0160-2055 \& ? \& \& CAPACITOR-FXD C1UF +3C-20\% 100VDC CEF \& 28486 \& 616.62055 <br>
\hline hlic31 \& 0160-4298 \& 6 \& 1 \&  \& 54.269 \& C3675:51147:M522-CDH <br>
\hline  \& 0160-4084 \& ${ }^{8}$ \& \&  \& 28438 \& ${ }^{61616.64084}$ <br>
\hline ${ }_{\text {Al }}{ }_{\text {Al } 11634}$ \& 160-2237
$0160-2055$
01605 \& ${ }_{3}$ \& \& CAPACITIR-FXD
CAPACITOR F \& 28483
204880 \& $3160-2237$
616.02055 <br>
\hline A11c35 \& 3160-20.55 \& ? \& \&  \& 23483 \& 0160-2355 <br>
\hline A11c36 \& 0160-2655 \& , \& \& CAPACITOR-FXD . $110 \mathrm{~F}+36.26 \% ~ 100 v D C$ CER \& 28480 \& 016.0 .2055 <br>
\hline A11c37
A1 11038 \& $0160-2247$
$0121-0659$ \& 3 \& \&  \& 28.480
$5 \times 2763$ \& $3160-2249$
364324
3 <br>
\hline A11 11638
A11C40 \& - $0121-0.659$ \& ? \& \& CAPACITOR-U TRMA-CER $2-8 \mathrm{Cr} 3$ SOU PC-MTE \& 5.2763
88460 \& $31643242 / 8 \mathrm{CF}$

3160.2055 <br>
\hline  \& $6160-3456$
$0160-2355$ \& ${ }^{6}$ \& \& CAPACITOQ-FXD 1060RF +-10\% 1KUDC CER \& 234n0 \& c160-3456 <br>
\hline A11C42 \& 0160-2355 \& , \& \& CAPACIILR-FXD .01UF +63-23\% 1JJULC CER \& 28480 \& 3160-2055 <br>
\hline A1 1143**
A1 1644 \& $0160-0134$
$0160-0437$ \& $\frac{1}{7}$ \& \& CAPACITOR - F
CAPACITOR \& 28488
28489 \& 01600134
$3160-0437$ <br>
\hline A11 1 C45 \& 0121-0036 \& , \& \& CAPACITOR - TRMR-CER 5.5 P 8 CF $3510 \cup$ \& 52763 \& $3043245.5 / 102 \mathrm{~T}$ NPO <br>
\hline ${ }^{\text {Al1 }} 11 \mathrm{C46}$ \& 0160-4384 \& ${ }^{3}$ \& \& CAPACITRR-FXD. 1 UF $+23 \%$ SavBC CER \& 28483 \& 3160-4384 <br>
\hline A11 478 \& 0160-2055 \& - \& \&  \& 28480 \& 6160-2055 <br>
\hline A11C48 \& 0160-2055 \& ? \& \& CAPACITOR-FXD A1UF +00-20\% 10NUDC TER \& 29883 \& 3163-2055 <br>
\hline A11C49 \& 0160-2055 \& ? \& \&  \& 28480 \& 016.0 -2055 <br>
\hline Alics0 \& $0160-2055$
$0160-2055$ \& $?$ \& \&  \& 28480 \& $3160-2355$
01602055 <br>
\hline A11c52 \& 0160-2055 \& 9 \& \& CAPACITJR-FXD . 01115 F 'B0-23\% 130 VDC CER \& 28480 \& 3160-2355 <br>
\hline A11 1153
A $11 \mathrm{CS4}$ \& $0160-2055$
$0121-0446$ \& ? \& \&  \& 28480
28480 \& c 1 $160-2055$
$3121-0446$ <br>
\hline A1 1 Css \& 0160-2055 \& ? \& \& CAPAC ITOR FXD O1uF +80 $20 \% 100 \cup D C$ CER \& 28488 \& $0160-2055$ <br>
\hline A11C60 \& 0160-2055 \& ? \& \&  \& 28480 \& 3160-2355 <br>
\hline A11c61 \& 0160-2655 \& - \& \& CAPAC ITOR FXD 01UF +80-20\% 100UDC CER \& 28480 \& 0160-2055 <br>
\hline ${ }_{\text {A }}^{\text {A } 11212663}$ \& -0160-2055 \& ? \& \&  \& 28480
28480 \& - $\begin{aligned} & 31600-2055 \\ & 0160-2055\end{aligned}$ <br>
\hline A11164* \& 0160-0134 \& 1 \& \& CAPACITOR FXD STOPF $+5 \times 303 \mathrm{VDC} \mathrm{MICA}$ \& 28480 \& ${ }^{3160-0134}$ <br>
\hline ${ }^{\text {A1 } 11655}$ \& 0160-2055 \& ? \& \& CAPACTITR-FXD - BIUF +GO-20\% 100UDC CER \& ${ }^{28480}$ \& 0160-2055 <br>
\hline A11C66 \& 0160-2055 \& , \& \& CAPACITOR-FXD . O1UF +B0-20X 10SUDC CER \& 28480 \& 0160-2055 <br>
\hline  \& $0160-2055$
$0160-2258$ \& $\stackrel{7}{4}$ \& 1 \& CAPATITOR-FXD
CAPACITOR FXD
O1PF
O \& 28480
28480 \& 0160-2055
$3160-2258$ <br>
\hline A11669 \& 0160-2055 \& ? \& 1 \& CAPACTTOR-FXD O1UF + 00 20x $200 \cup 10 \mathrm{DC}$ CER \& 28480 \& $0160-2055$ <br>
\hline A11c73 \& 0121-0452 \& 4 \& 2 \& CAPACITOR-U TRMR AIR 135 APF 175U \& 74\%70 \& 187-0103-028 <br>
\hline A11074 \& 0121-0452 \& 4 \& \& CAPACITOR-V TRMR-AIR 1.3 5.APF 1750 \& 74970 \& 187-0103-0.88 <br>
\hline  \& $1901-0047$
$1901-0047$ \& ${ }_{8}^{8}$ \& 6 \&  \& 29480
28480 \& 1931-0047 <br>
\hline A11CR3 \& 1901-1070 \& ? \& 5 \& DIODE PIN 110 J ( ${ }^{\text {d }}$ \& 28480 \& 1951.1370 <br>
\hline A11CR4 \& 1901-1070 \& $?$ \& \& DIDDE PIN 1100 \& 28480 \& 1901-1070 <br>
\hline Al1CR5 \& 1901-1070 \& , \& \& DIODC PIN 1100 \& 28480 \& 1901-1070 <br>
\hline
\end{tabular}

TABLE 8-8. BANDWIDTH FILTER NO. 1 ASSEMBLY A11, REPLACEABLE PARTS (2 OF 3 )

| Reference Designation | HP Part Number | $\begin{aligned} & \mathrm{C} \\ & \mathrm{D} \end{aligned}$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A116RG | 173125035 | $?$ | 5 | DTECE SM 515 SE:,01TKY | 28480 | 1931-3535 |
| A11CR8 Alicra | 1761-0535 | 9 |  | DIOLE SM SIG SChattky | 28486 | 1961-0535 |
|  | 19310047 $1901-0047$ | A |  | OTGE5 SWITCHINS 230 TSiPa 10 NS | 28480 | 1731-0347 |
| Alicrit | 1931-1370 | 8 |  | DIGDI SWITCHING $200 ~ 75 M A ~ 1 C N: ~$ DTODE PTN 113 V | 28486 | $1701-0047$ $1931-1.370$ |
| AtICR12 | 1961-1070 | 9 |  | DIODE-PIN 118 | 20480 | 1261-1070 |
| A1ICR13 | 17313047 | ${ }^{8}$ |  | DICDE SWITCA1NG DJU 7ETA TJNS | 28480 | 1931-0047 |
| A11CR14 | 1901-0535 | 9 |  | DIODE SM SIG SEHOTTKY | 28480 | 1761-6535 |
| A11CR15 | 1731-3535 | $?$ |  | DTODE SH SIG SE: 017 KY | 23483 | 1931-3535 |
| A11CR16 | 1901-6047 | 8 |  | DLODR-SWITCHING 2CU 75*A 10 NS | 24480 | 1701-0047 |
| A11CR17 | 1731-3535 | ${ }^{7}$ |  | DIODE SM STG EC:DOTKY | 28480 | 1931-9535 |
| AlIEI | 9170-0029 | 3 | 0 | CORE SHIELDING RTAD | 28486 | 9176-0027 |
| Al1E2 A 1123 | 71730329 | 3 |  | CORE SAHELDTNG EEAD | \%8483 | 7170-0329 |
| Alif 4 | 9175 0.22 | 3 3 3 |  | CORE SHIEIDING BTAD | 28489 | 9176.0029 <br> $9170-3329$ <br> $176-0029$ |
| Al 125 | 9170-0029 | 3 |  | CORE SHIELDING RTAD | 28480 | 9176-0029 |
| A1156 | 71703059 | 3 |  | COIRE SHIELDING EFAD | 28483 | 9173-0329 |
| A11E7 | 9176-66.99 | 3 |  | CIRE-SHIELDING BFAD | 28436 | 9170.0029 |
| A1158 | 9170 032? | 3 |  | CLIPE -SHTELDING ETAD | 28483 | 9173-0329 |
| A1111 | 9140-0112 | 2 | 1 | INDUCTOR RF CH-MLD 4. 7 UH $10 \%$ | 29486 | 914C-8112 |
| A1112 | 2193-1641 | 3 | 1 |  | 28483 | 9130-164: |
| A11L3 | 9140-0114 | 4 | 3 |  | 28480 | 914 C 0114 |
| A1114 A11LS | $7139-1624$ $9140-0179$ | $?$ | 3 2 |  | 28483 | 7130-1624 |
|  |  | . |  |  | -2480 | 9140-8179 |
| A1116 | $9130-2813$ $9140-0390$ | 0 | $?$ | TNDERIGR $403 \mathrm{NHA} 13 \%, 312 \mathrm{P} \times 1.316 \mathrm{LG}$ Q $2=150$ | 28483 | 7130-2813 |
| A1117 | $7140-0379$ $7140-3170$ | 7 | $?$ |  | 29480 | 714C-0399 |
| A1118 A1 11.9 | $7140-3178$ $9160-1619$ | 3 2 | 1 |  | 28483 | 9140-0178 |
| A11LIO | 7143-0114 | 4 | . | lele | 28480 23480 | 71601617 $7140-3114$ |
| A11L11 | 9100-1624 | 9 |  | INDUCTOR RT-CH MLD 3014 $5 \% .1660 \times$, 38\% G | 20480 | 91061624 |
| A116.12 | 9149-0179 | 1 |  |  | $2 \mathrm{E4B3}$ | 7140-3179 |
| A111.13 | 5140-0399 | 7 5 |  | INDUCTOR RF-CH-MLD $2.20415 \% ~ 166 D X, 385 L 5$ | 29488 | 91460397 |
| A11L14 | $7100-16.20$ $9100-2813$ | 5 | 1 | INLLECTOR RF ( INDUCTOR A MLD | 23483 28480 | $9109-1620$ $9106-2813$ |
| A111.16 | 914:-0144 | 3 | 2 | INDUCTOR RF (H-MLD 4.7UH 13\% , 13SDX, 26LG | 28480 | 7140-0144 |
| A11L17 | 9100-1624 | 2 |  | INDUCTOR RT-CH-MLD 3CU: 58 , 1660X. 3855.6 | 28480 | 910c-1624 |
| A11L18 | 9100-16.19 | 2 |  | INDUCTGR RF-CH-M.D 6. Et in $10 x$ | 28480 | 9150-1619 |
| A11L19 | 9140-0144 | 0 |  | INDUCTOR RF-CH Mt D 4.7UH 10X , 105DX, 26 L G | 28480 | 9146 0144 |
| A1191 | 10540345 | - | 1 | TRANSISTIR NPN ENS 179 SI TO-72 PD=233ru | 04713 | 215179 |
| A1102 | 1854-0404 | 0 | 2 | TRANGISTOR NPN ST TO-18 PD=360ML | 29480 | 1054-0464 |
| A1193 | 10530007 | 7 | 5 | TRANSISTGR PNP ENK2S 1 SI TO-13 PD=363ML | 04713 | 2N3251 |
| A1194 | 1853-0007 | 5 |  | TPANSISTOR PNP 2N3251 SI TO-18 PD=360MW | 64713 | 2N3251 |
| A1/GS | 1055-0267 | 5 | 2 | TRANSTSTGR J-FET N-CHAN D-MCDE TO-92 SI | 28480 | 1855-3267 |
| A1106 | 1853-0007 | 7 |  | TRANSISTOR PNP 2 N3251 ST TO-18 PD $=366 \mathrm{MW}$ | 04713 | 2N3251 |
| A1107 | 10540404 | 3 |  | TRANSTSTCR ${ }^{\text {NPN }}$ SI TO-18 PD $=369 \mathrm{hW}$ | 28480 | 1054-0404 |
| A1108 | 1853-0007 | 7 |  | TRANSISTOR PNP 2N32S1 SI TO 18 PD=36CMW | 04713 | 2N3251 |
| A1189 | 10550267 | 5 |  | TRANSISTOR J FET N-CHAN D-MODE TO-92 SI | 28483 | 1855-3267 |
| A11910 | 1953-0007 | 7 |  | TRANGISTOP PMP 2N32S1 SI TO-18 PD=360KU | 04713 | 2N3251 |
| A11R1 | 0757-0444 |  |  | RESISTOR $12.1 \mathrm{~K} 1 \%$, 125W F TC=0 0 - 100 | 24546 | C4-1/8-T0-121?-F |
| A11R2 | 0698-3156 | 2 |  | RESISTOR 14,7K 1 X , 1254 F TC $=0+-100$ | 24546 |  |
| A1IR3 | 0757-0402 | 1 | ? | RESISTOR $1101 \%$, 1254 F TC 00 , -100 | 24546 | C4-1/8-70-111-F |
| A1 1R4 | 0757-0442 | 9 | 8 | RESISTOR 10k 12.1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-1002-F |
| A11R5 | 0757-0405 | 4 | 1 | RESTSTOR 1621 X (125U F TC $=04-130$ | 24546 | C4-1/8-T0-162R-F |
| A11R6 | 6698-3431 | 6 | 1 | RESISTOR $23.71 z, 1254$ F TC $=0+-100$ | $03888$ | PMES5-1/8-T0-23R7-F |
| A1187** | 0598-8821 | - | 1 | RESTSTIJR $5.621 x, 12 S W$ F TCaOt-100 | 28488 | $0698-8021$ |
| A11R8 | 0757-0401 | 0 | 3 | RESISTOR $1001 \%$, 125w F TC $=0+100$ | 24.546 | C4-1/8-T0-101-F |
| Al1R9 | 0757-0439 | 4 | 1 | RESISTGR $6.81 \mathrm{~K} \quad 1 \mathrm{X}, 1254 \mathrm{~F}$ TC $=0+100$ | 24546 | C4 1/8-T0-6811-F |
| A11R10 | 0757-1094 | 9 | 1 | RESISTOR $1.47 \mathrm{~K} \quad 1 \mathrm{z}$, 125W F TC $=0+-100$ | 24546 | C.4-1/8-T0-1471-F |
| A11R11 | 0757-0440 | 7 | 1 | RESISTOR 7.5K $1 \chi$, 125以 F TC $=0+200$ | 24546 | C4-1/8-T0-7501-F |
| At 1812 | 0757-0447 | 4 | 1 | RESISTOR 16, 2K $1 \mathrm{z}, 125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8-T0-16.22-F |
| A11R13 | 0698-0082 | 7 | 1 | RESTSTER $4641 \mathrm{X}, 1254$ F TC $=0+100$ | 24546 | C4-1/8-T0-4640-F |
| A1 1814 | 0757-0346 | 2 | 4 | RESISTOR $101 \chi$, 1254 F F $T C=0+-100$ | 24546 | C4-1/8-T0-1080-F |
| A11R15 | 0698-3440 | 7 | 2 | RESTSTIR $1961 \mathrm{X}, 125 \mathrm{~L}$ F $1 \mathrm{C}=3+-100$ | 24546 | C4-1/8-T0-196R-F |
| A 11816 | 0757-0419 | 0 |  | RESISTOR 681 12.125 W F TC $=0+-100$ | 24.546 | C4-1/8-T0-681R-F |
| A11R17 | 0698-3442 | 9 | 2 | RESTSTIOR 2371 x , 1254 F TC $=0+100$ | 24546 | C4-1/B-T0-237R-F |
| A1 1R18 | 0698-3154 | 0 | 2 | RESISTOR 4.22k 12.1254 F TC $=0+-100$ | 24546 | C4-1/8-T0-4221-F |
| A11R19* | 0698-3155 | 1 | 2 | RESTSTOR $4.64 \mathrm{~K} 1 \mathrm{z}, 125 \mathrm{~W}$ F TC $=0+-100$ | 24546 | C4-1/8-T0-4641-F |
| A11R20 | 0757-0442 | 9 |  | RESISTOR $10 \mathrm{~K} 1 \mathrm{X}, ~ 1254 \mathrm{~F}$ TC $=0+-10 \mathrm{C}$ | 24.546 | C4 1/8-T0-1002-F |
| A11R21 A11822 | $\begin{aligned} & 0757-0442 \\ & 0757-0442 \end{aligned}$ | 9 |  | RESISTIR $10 \mathrm{KK} 1 \mathrm{x}, 125 \mathrm{~W}$ F TC $=0+200$ <br> RESISTOR 10K 1 K . 125W F TC $=0+-100$ | $\begin{aligned} & 24546 \\ & 24546 \end{aligned}$ |  |
| A11R23* | 0757-0288 | 1 | 2 | RESISTOR RESISTOR 9.09 K R | 24546 $1 \% 731$ | $\begin{aligned} & \text { C4-1/8-T0-1002-F } \\ & \text { MFAC1/B-T0-9091-F } \end{aligned}$ |
| A11824 | 0757-0465 | 6 | 2 | RESISTOR $100 \mathrm{~K} 1 \chi$, 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |
| A11R25 | 0757-0465 | 6 |  | RESISTGR 100K $12.125 W$ F TC $=0+-100$ | 24546 | C4-1/8-T0-1003-F |

TABLE 8-8. BANDWIDTHFILTERNO. 1 ASSEMBLYAII, REPLACEABLEPARTS (3OF 3 )

| Reference Designation | HP Part Number | $\left\|\begin{array}{l} c \\ D \end{array}\right\|$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A11R26 | 2130-3163 | ${ }^{8}$ | 1 | RESTSTTR-TRKR 1 M 2JX C SIDE ADJ 17 -T2N | 32111 | 43 P 135 |
| A11R27 A1 11 REB | $0757-0444$ $3757-9443$ | 1 | 2 |  | 24.46 <br> 24546 <br> 2.46 | $\mathrm{C} 4-1 / 8-\mathrm{TC}-1212-\mathrm{F}$ $\mathrm{CA-1/8-T9-1132-F}$ |
| A11R29 A1tR3 | $0698-0 \cos$ $3757-0432$ | 8 | 2 |  | 24546 24546 | C4 $1 / 8-\mathrm{TO-1961-F}$ $\mathrm{C} 4-1 / 8-\mathrm{T}-111-\mathrm{F}$ |
| Al1R31 | 2100-3052 | 4 | 1 | RESISTOP-TPM $5810 \%$ C SIDE-ADJ 17-TPN | 02111 | 43 P 50 |
| Al1R23\% | ${ }^{0698-3454}$ | 3 | 1 | RESISTER 215k $1 \%, 1254 \mathrm{~F}$ TC $=3+109$ | 24546 | C4-1/8- ${ }^{\text {c }}$ |
| A11R33 | 0757-0442 | 9 |  | PESISTOR 10 K 1 L , 125 S F TC=0+100 | 24546 | C4-1/8-T0-1062-F |
| A11R34 | -3757-3199 | 1 | 1 |  | 24546 19701 | $\mathrm{C} 4-1 / 8-\mathrm{T} 3-2152-\mathrm{F}$ $\mathrm{M}=4 \mathrm{Cl} / 8 \mathrm{TC}-9691-\mathrm{F}$ |
| A11R36 | 9698-0083 | ${ }^{8}$ |  |  | 24546 | C4-1/8-T0-1961 = |
| A11R37 | 0757-0416 | 7 | 2 | RESISTOP $51112.1254 \mathrm{~F}^{\text {F }}$ TC $=0+100$ | 24546 | C.4-1/8-T0-511R-F |
| A11238 | 0558-3441 | 8 | 1 | RESTSTIR 215 1z 1250 F IC=3+103 | 24546 | C4-1/8-T0-215R-F |
| A11239 A1 1 R 40 | - $\begin{aligned} & 0757-0419 \\ & 0698-3442\end{aligned}$ | ${ }_{9}$ |  |  | 24546 24546 | $C 4-1 / 8-T 0-681 R-F$ $C 4-1 / 8-T 3-23 / R-F$ |
| A1 1R41 | 0698-3154 | 0 |  | RESISTO $4.22 \mathrm{~K} 1 \mathrm{1} \mathrm{\%}, 125 \mathrm{WF}$ TC $=0+16 \mathrm{C}$ | 24.46 | C4-1/8-T0-422, ${ }^{\text {c }}$ |
| A11R42 | 3757-0442 | ? |  |  | 24546 | C4-1/8-T0-1032-F |
| A1 1R43* | 6698-3155 | 1 |  |  | 24546 | C4-1/8-T8-464t-F |
| Al1R44 A1 1845 | - $\begin{aligned} & 0757-0442 \\ & 0757-0401\end{aligned}$ | \% |  | RESISİR ${ }^{\text {R }}$ | 24546 245.46 | C4-1/8-TJ-1032-F $\mathrm{C4-1/8-TE-161-F}$ |
| A11R46 | 0757-0431 | 0 |  | RESIGTOR $100{ }^{12}$ \% 125 SW F TC=0+-103 | 24546 | C4-1/8-T0-131-F |
| A11R47 A11R48* | 0757-0346 $3757-0444$ | ? | 4 |  | 24.546 24546 | C4-1/8-T0-16Fa-F $\mathrm{C4-1/3-T0-1212-F}$ |
| A 11 R 49 | 0757-0444 | 1 | 4 | RESISTOR 12.1 K 12, 12S ${ }^{\text {R }}$ F TC $=0+100$ | 2.4546 | C4-1/8-T0-1212-F |
| Al1R53 | 3757-9346 | 2 |  | RESISTOR $131 \%$, 12SW F TC=3+-100 | 24546 | C4-1/8-T0-10R3-F |
| $\mathrm{Al}^{11 R 51}$ | $0757-0346$ $0757-0443$ | a |  |  | 24546 | CA-1/8-T0-10R0-F |
| A11R52 A1 1R53 | 9757-0443 $0698-3440$ | 0 |  |  | 24546 24546 | $\mathrm{CA}-1 / 8-\mathrm{Ta-132-1}$ $\mathrm{C4-1/8-TC-1968-F}$ |
| A11R54 | 3757-0416 | 7 |  |  | 24546 | C4-1/8- $\mathrm{T}^{\text {a }}$-511R-F |
| A11R5S | 6757-0442 | 9 |  | RESISTOR 10K 1\% . 125 SW F TC 8 $8+160$ | 24546 | C4-1/8-T0-1062-F |
| A11R56* A11 125 | 9757-0274 | 5 | 1 |  | 24546 | C4-1/8-70-1211-F |
| A11R57 A11R5B | 0757-0180 $3678-3152$ |  | 2 |  | 28480 24546 |  |
| A11R5B A1 1859 | ${ }_{0}^{36757-0180}$ |  | 1 | RESISTOR $31.61 \mathrm{~K}, 1254 \mathrm{~F}$ TC $00+-100$ | 28480 | 0757-0180 |
| Al1R69 | 0698-3153 | 9 | 1 | RESISTGR 3.03 K 1 X . 125 SW F TC=34-133 | 24546 | C4-1/8-T0-3831-F |
| A 11 1PP 1 | 0360-1788 |  | 4 | CONNECTOR SGI CONT PIN.04E IN ESE S7 50 | 28480 | c360-1788 |
| A11TP2 | $0360-1788$ $1251-060$ | 7 | 7 |  | 28480 28480 | $9360-1788$ $1251-0600$ |
| ${ }_{\text {Al }} 11 \mathrm{TPP}^{4}$ | ${ }^{0360-1788}$ | 7 | 7 | CONNECTOR SGL CONT PIN . 045 IN FSC SI2 SQ | 28480 | ${ }^{12360-1788}$ |
| A11TP5 | 0360-1788 | 7 |  | CONNECTOR-SGL CONT PIN. O4E IN-ESC S\% SQ | 20480 | 03/0-1783 |
| A11TP6 | 1251-3600 |  |  | CONNECTOR SGL CINT PIN 1.14-mm ESC Sz 90 | 28480 | 1251-0600 |
| A11 TP8 A11TP9 | $1251-0600$ $1251-0600$ | 0 |  | CONECTOR-SEC CONT PIN 1.14 MM-ESC 97 SO | 28480 28480 | $1251-0600$ $1251-0600$ |
| A11TP 10 | 1251-0600 | , |  | CONNECTOR-SGI CONT PIN 1.14 MM -ESC-S2 SQ | 28480 | 1251-0600 |
| A11TP11 | 1251-0600 | 0 |  | CONNECTOR-SGL CONT PIN 1.14-MM-EEC $\leqslant \mathrm{Z}$ S SQ | 28480 | 1251-0600 |
| A11 TP 12 | 1251-0600 | 0 |  | CONNECTOR-SGL CONT PIN 1.14 MM-ESC 97 SQ | 28480 | 1251-0600 |
| Al1uri | 1902-0048 | 1 | 1 | DIODE ZNR 6.81V 58 vo-35 PD=.4U | 28480 | 1902-0048 |
| Allyi AliYz | $\begin{aligned} & 0410-0776 \\ & 0410-0776 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \end{aligned}$ | 2 | CRYSTAL-QUARTZ 21.4 MHZ HC 25/U-HLDR CRYSTAL-QUARTZ 21.4 MHZ HC 25/U-HLDR Al। miscellaneous parts | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 6410-0776 \\ & 0410-0776 \end{aligned}$ |
|  | $\begin{aligned} & 0403-0026 \\ & 08559-000025 \\ & 08559-00007 \end{aligned}$ | $\begin{aligned} & 6 \\ & 5 \\ & 3 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \end{aligned}$ | PLug hile bdr-hD for . 107 D hole nyl BAFFLE INDUCTOR <br> cover, EW Filter no. 1 | $\begin{aligned} & 32768 \\ & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 237-120241-03-3101 \\ & 08559-00025 \\ & 08559-00007 \end{aligned}$ |

Bes]e


FIGURE8-54. BANDWIDTHFILTERNO. 1 ASSEMBLY A11,BLOCK DIAGRAM

A11


FIGURE8.55. BANDWIDTHFILTER NO. 1 ASSEMBLY AII, COMPONENT LOCATIONS


## STEP GAIN ASSEMBLY A12, CIRCUIT DESCRIPTION

The Step Gain Assembly A12 provides from 0 to 50 dB amplification of the 21.4 MHz IF in 10 dB steps, as selected from the REFERENCE LEVEL control. A zero to - 12 dB REFERENCE LEVEL FINE attenuator control is also included on the front panel. Generated on the Step Gain Assembly A12 are the first mixer diode bias and a flatness control voltage proportional to the sweep plus tune $(\mathrm{S}+\mathrm{T})$ voltage.

## Step Gain Amplifiers (E) (F) (G)

There are three step gain amplifiers, one 10 dB and two 20 dB , cascaded as shown in the schematic diagram. Full gain of any amplifier is selected by grounding the appropriate IFG line. The three step gain amplifiers can be considered as operational amplifiers. An equivalent circuit for the three stages is shown in Figure 8-57. The gain for each amplifier is: Gain $=1+\mathbf{R}_{\mathrm{r}} / \mathbf{R}_{\mathrm{i}}$. The feedback resistance, R ,, for the 10 dB amplifier is $\mathbf{R 8}, 562$ ohms; for the 20 dB amplifiersit is 233 and R 31 , each 750 ohms . The input resistance, $R$,, is a combination of a fixed series resistance ( 56.2 ohms ) and the controlled resistance of the PIN diodes. The resistance of the PIN diodes is approximately 10 to 1000 ohms and increases as the forward bias current is decreased from 100 milliamperesto 1 microampere. The input resistance, $\mathrm{R}_{\mathrm{i}}$, for the 10 dB amplifier is approximately 260 ohms ; for the 20 dB amplifiers, it is about 83 ohms .


FIGURE8-57. STEP GAIN AMPLIFIERS, SIMPLIFIEDDIAGRAM

Selection of the correct combination of step gain amplifiers is accomplished with the REFERENCE LEVEL switch. Rotating the switch grounds the emitter circuit of the selected amplifier (or amplifiers), allowing current to flow through the PIN diode (or diodes). The possible switch combinations allow the gain to vary from unity (all switches open) to 50 dB maximum with all three emitter circuits grounded.

Test/Norm Switch. In the emitter paths of the 20 dB step gain amplifiers are the TEST/NORM switches used to disable both 20 dB amplifiers during log amplifier adjustment.

```
0-12dB Control (H)
```

The REFERENCE LEVEL FINE control provides approximately 0.3 to 12.3 dB of attenuation at the base of Q6 in the $0-12 \mathrm{~dB}$ control circuit. By regulating the current flow through PIN diode CR7, the amount of signal attenuation is controlled. For example, if PIN diode current flow is increased, more RF signal is shunted or bypassed to ground. Capacitor C23 provides the RF ground path.

A minimum current flow through the PIN diode, which provides the maximum allowable diode resistance, is established by -12 dB potentiometer R39 so that the diode is never completely cut off. Adjustment of R39 sets the 0.3 dB point and is adjusted with the REFERENCE LEVEL FINE control set fully clockwise ( -12 position).

The maximum current flow through the PIN diode is set with the $\mathbf{0} \mathrm{dB}$ potentiometer R35. Resistor R35 is adjusted to the 12.3 dB attenuation point with the REFERENCE LEVEL FINE control set fully counterclockwise ( 0 position).

Transistors Q5 and Q7 are identical current sources. The maximum current is set with the 0 dB adjustment, R35, in the common base circuit. Diode CR5 provides temperature compensation for the transistors.

Transistor Q5 provides current for a bias voltage applied to the anode of the PIN diode. The voltage source consists of R39, R38, and CR6. Diode CR6 provides temperature compensation for the PIN diode. Inductor L8 isolates the diode current source from the RF signal.

Transistor Q7 provides current for a variable voltage source at the cathode of PIN diode CR7. Fixed resistor R40 is effectively in parallel with the negative side ( -12.6 V ) of the REFERENCE LEVEL FINE control potentiometer. Its purpose is to match the FINE control to changes in the PIN diode resistance. The FINE control varies the voltage at the PIN diode cathode, this varies the diode current flow. When the FINE control is fully clockwise, the PIN diode is at minimum conduction and maximum signal is applied to the base of Q6. Conversely, when the FINE control is fully counterclockwise, the PIN diode is forward biased into maximum conduction and minimum signal is applied to Q6. Buffer amplifier Q6 operates as an emitter follower, providing isolation between the $0-12 \mathrm{~dB}$ control circuit and the 21.4 MHz bandpass filter.

### 21.4 MHz Bandpass Filter (I)

The 21.4 MHz Bandpass Filter at the output of the $0-12 \mathrm{~dB}$ control circuit is a two-pole type used to reduce the out-of-band noise produced by the step gain amplifiers and $0-12 \mathrm{~dB}$ control.

## NOTE

For minimum step gain error, the ground plane on the Step Gain Assembly A12 must be firmly connected to the chassis extrusion and the Motherboard Assembly A16 common ground. This means that before you can make any step gain measurements or adjustments, the Step Gain Assembly A12 must be fully seated in its connector socket and all of its cover screws must be in place and tightened. You can, however, leave the gold secondary cover off for these measurements.

## BandSelect Decoder (A)

Band select decoder U3 is a 4-to-10 line decoder. It decodes the three band-select lines (H2, H3, and PM) to select one of six output lines. The selected line goes low while the remaining five lines stay high. The status of the decoder's outputs controls the tilt, offset, and bias circuits.

## Band Tilt (C)

Band tilt is controlled with a variable, voltage-controlled voltage source comprising operational amplifier U4b, current boosting transistor Q2, and related adjustable resistor networks. The signal input to this circuit is the sweep plus tune $(\mathrm{S}+\mathrm{T}$ ) voltage. Normally, this signal is a ramp extending from +1.2 V to +4.8 V or some level in between, depending on the position of the FREQ SPAN/DIV and frequency TUNING controls.

When the $\mathrm{S}+\mathrm{T}$ ramp is at its low point $(+1.2 \mathrm{~V})$, the level at test point 3 should be $+10.6 \mathrm{~V} \pm 0.1 \mathrm{~V}$. When the $\mathrm{S}+\mathrm{T}$ ramp is at its peak $(+4.8 \mathrm{~V})$, the level at test point 3 can be adjusted from about +9.6 V to +10.9 V with the circuits's potentiometers and factory selected fixed resistors. Potentiometers R47, R48, R49, R51, R53, and R55 adjust the overall tilt for each band. Two factory selected resistors, R50 and R52, and potentiometers R54 and R56 provide additional tilt adjustment for harmonic mixing bands $2+, 2-, 3+$, and $3-$ after a breakpoint at approximately midband.

## Band Offset (D)

Operational amplifiers U4a, U4d, U4c, and their associated circuits provide offset and gain for the tilt voltage. Potentiometers R57, R58, R59, R60, R61, and R62 are used to adjust the offset of each band. A fixed negative offset is provided for all bands by operational amplifier U4c. The resulting flatness output voltage is applied to a voltage-controlled amplifier on Third Converter Assembly A10.

## Mixer Diode Bias (B)

Bias of the First Mixer Assembly A4 depends on the desired harmonic mixing number. Quad switch U1 and operational amplifiers U2a, U2b, and U2c with their associated components form the mixer diode bias sources. Varying power levels are coupled into the mixer diode due to irregularities in the YTO's swept power output, causing variations in the mixer diode bias conduction angle, or total bias power. The bias sources adjust to these instantaneous changes in the mixer bias conduction angle by increasing or decreasing bias in order to maintain a constant conduction angle. The circuit includes separate bias adjustments for bands $2-, 2+, 3-$, and $3+$. Bands 1 - and $1+$ use a common bias adjustment potentiometer.

The four switches in U1 are normally closed, but the individual switches open when selected by a logic-high control voltage. Since the outputs from the band select decoder U3 are all high except one, the normal status of the switches in U1 is open until a low control input allows one to close. The switch then connects one of the three potentiometers (R70, R71, R72) through a factory selected fixed resistor to the positive input (pin 10) of operational amplifier U2c, forming a voltage source at that point. The table below shows which potentiometers and factory selected resistors apply to which band.

TABLE 8-9. MIXERDIODEBIAS ADJUSTMENTS

| Band | Control Name | Bias Adjust <br> Resistor | Range Adjust Resistor <br> (Factory-Select) |
| :---: | :---: | :---: | :---: |
| $.01-3$ | V1 | R72 | R73 |
| $6-9$ | V1 | R72 | R73 |
| $3-9$ | $\mathrm{~V} 2-$ | R83 | R84 |
| $9-15$ | $\mathrm{~V} 2+$ | R87 | R88 |
| $6-15$ | $\mathrm{~V} 3-$ | R71 | R74 |
| $12.1-21$ | $\mathrm{~V} 3+$ | R70 | R75 |

Operational amplifier U2c forms a negative impedance converter that increases or decreases bias as needed to maintain a constant angle of conduction at the first mixer. This is necessary to maintain a constant insertion loss through the first mixer. Operational amplifier U2c is connected to the voltage source at the junction of R73, R74, R75, and Q1. This circuit multiplies its input source resistance by approximately $-1 / 110$, thus converting the input voltage source and series resistance into an equivalent voltage source and negative impedance (here, approximately $\mathbf{- 1 0 0 0} \mathrm{ohms}$ ).

Because of this conversion, as current increases in the circuit, the resultant output voltage decreases, just as it would if a negative resistance value ( -R ) were substituted for R in the familiar expression for Ohm's Law. The expression would then be rewritten as: $\mathrm{E}=\mathrm{I}(-\mathrm{R})$. Notice now that an increase in current (I) results in a decrease in voltage (E). This is the equivalent action of this circuit. If all of U1's switches are open (as in band 2 - or $2+$ ), transistor Q1 forces the junction positive, turning off CR15 and thereby removing the negative impedance converter from the bias output at P1-24. One of the other operational amplifiers in U2 is activated, providing voltage sources and positive resistances to the bias output (TP1 or P1-24). When one of the operational amplifiers is selected, the diodes at the outputs of the other two are reverse biased, and disconnect the outputs from P1-24.

## +5.1V Reference (K)

Transistor Q 4 and its associated circuitry operate off the +15 V supply to furnish a regulated +5.1 V reference for the flatness and mixer diode bias circuit.

## Power Supplies (J)

Extensive filtering of the $+15 \mathrm{~V},+12 \mathrm{~V}$, and -12.6 V inputs is needed to reduce coupling between each step gain amplifier and between the Step Gain Assembly A12 and the other assemblies.

## STEP GAIN AMPLIFIER ASSEMBLY A12, TROUBLESHOOTING

## CAUTION

## Tubular ceramic capacitors will short to the aluminum extrusion if allowed to touch it during testing.

Always check the supply voltages. If the +15 V supply drops (even slightly), the +5.1 V Reference becomes unregulated.

Linear or Log Fidelity Errors: First readjust REFERENCE LEVEL FINE to the -12 dBm position and test again. If the problem is not present, gain compression may be occurring in one of the circuit's amplifiers. The 10 dB Amplifier (block E) is the most probable source, and improper biasing of CR1 is the most probable cause. Insufficient dc biasing of CR1 allows signal voltage to vary the bias, causing the stage gain to vary as the signal level varies. Diode CR1, not transistor saturation, is the most common cause of compression.

Reduction of the losses in the $0-12 \mathrm{~dB}$ Control (block H) allows the first amplifier stage to operate at a lower input level, thus reducing compression. To decrease the losses, hand-select CR7 and C23 for minimum circuit loss.

Poor Linearity of the $\mathbf{0} \mathbf{- 1 2} \mathbf{d B}$ Control: The most probable cause is CR7.

TABLE8-10. STEP GAIN ASSEMBLY A12, REPLACEABLEPARTS(10F3)

| Reference Designation | HP Part Number | $\left\|\begin{array}{l} c \\ \mathbf{D} \end{array}\right\|$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A12 | 0555s-60326 | 2 | 1 | Step gain assemily | 78483 | 06559-60.326 |
| A12C1 | ${ }^{\text {c 1 1 }}$ 60-26.55 | $\stackrel{7}{7}$ | 27 | CAPACITOR-FXD , C1uF +80-20\% $160 \cup \mathrm{DC} \mathrm{CRR}$ | 2 cas | 016.0. 2055 |
| A12Cl A12C3 | 9169-3457 $\mathrm{c} 160-2655$ | $\stackrel{7}{9}$ | 3 |  | - 84888 | 3160-3.457 |
| A12C3 A12C4 | c160-265s $3180-3291$ | 4 | 2 | CAPACITOR FXD Cille | ${ }_{56889}^{26886}$ | 15JD13599335A2 |
| Al2Cs | 0160-265s | 9 |  | CAPACTTOR FXD . 1 IUF +00-26\% 10QUDC CLF | 28498 | $6160 \cdot 2055$ |
| A12c6 | 3160-2355 | , |  | CAPACITGR-FXD 013F 1 Bn $23 \%$ 103ULC CER | 7 c 489 | 3160-2355 |
| A12C7 | 6160-2055 | 9 |  |  | 23430 | 6160-2055 |
| ${ }_{\text {Al }}^{\text {Al2cs }}$ | ${ }^{0160-2955}$ | ${ }_{9}$ |  |  | 28480 | (3160-2055 |
| A12C10 | 0160-2055 | 7 |  | CAPACITGR FXD Dilu vas a\% luavec irn | 23483 | 3160-2355 |
| $\mathrm{Al2Cl1}^{12}$ | 0160-2055 | 9 |  | CAPACITOR-FXD .G1uF +36-20\% 100UDC CLE | 28980 | ${ }^{016.62055}$ |
| A12C12 | 3150-2355 | 7 |  | CAPACITSR-FXD - O1UF $183-202$ 103VEC TER | . 11401 | 3160-2355 |
| ${ }^{\text {A } 12 C 13}$ | 0160-2055 | 9 |  |  | $\frac{28490}{1140.1}$ | ${ }^{C 164}$ |
| A12C1S | 0160-2055 | 9 |  | CAPACITOR-FXO. C1UF +86-20\% 100VDC CFF | 21980 | 616.02055 |
| A1EC16 | 3159-3.457 | , |  |  | \%'1400 | 3160-3457 |
| A12C17 | 0160-2055 | 9 |  |  | 239898 | 016.0.2055 |
| A12cis | 3163-2355 | \% |  |  | 33480 | 3163-2355 |
| A12C19 A1EC23 | c160-3457 | 7 |  | CAPACITOR-FXD 2EGECF + $10 \%$ 25AUDE CEER | 20480 | 61603457 $0160-2355$ |
|  | 7160-2355 |  |  |  |  |  |
| A12C21 | 0160-2055 | $\stackrel{9}{9}$ |  | CAPACITITR-FXD . $01 u \mathrm{~F}$ +86-20\% 10CUDC CRR | 2 aman | c14.0-2055 |
| ${ }^{\text {Alecen }}$ | 0163-2055 | 8 |  |  | ${ }^{-8489}$ | - 316302355 |
| A12C24 | 3160-2355 | ${ }_{8}$ |  | CAPGCITOR-FXD O1UF 180-23\% 13JVLC CER | 28439 | 3163-2955 |
| A12c2s | 6160-2199 | 2 |  | CAPACITO2-FXO 3GEr + 52 3Ggudd mica | 28498 | 016.6-2199 |
| A1こC26* | 0160-2199 | 3 | ? |  | 23780 | 3163-2199 |
| ${ }^{\text {A12C2\% }}$ | 0160-2055 | 9 |  | CAPACTIOR FXD - A1uF +atere | 20489 | 016.E. 2055 |
| Alscis A12c30 | 0160-2055 | ${ }_{9}$ |  |  | 23489 | 3160-2355 |
| Alec31 | -160-2655 | 9 |  |  | 28480 | $3160-2355$ |
| A12C32 | 0160-2655 | ${ }^{9}$ |  |  | 2:490 | 0160-2055 |
| ${ }^{\text {Al2C33 }}$ | 0160-2355 | 7 |  | CAPACITUR-FXD . $3115183-23 \%$ 103ULC CER | , 8483 | 3160-2055 |
| A12C34 |  | 9 |  | CAPACITOR-FXD . 114 F +8G-20X 100VDC CER | 38880 | 016.0-2055 |
| ${ }_{\text {A1 }}{ }^{\text {Al2C36 }}$ | $0160-2355$ $0160-0127$ | ${ }^{2}$ | 1 |  | 23480 | 0160-0127 |
| A12C40 | 0160-2253 | $\epsilon$ | 3 | CAPACLIDR-FXD 5.1PF + .aspy sioutc cer | -6489 | 3160-2250 |
| A12C41 | 0180-2250 | , |  | CAPACITOR-FXD 5.1PF +-.259F SOOUDC CFR | 29480 | 0160-2250 |
| A12C4? | 0160-2250 | , |  | CAPACIIDR-FXD S.1PF +-.2SPF SOJUEC CER | - 0483 | 0160-2250 |
| A1 2CR1 | 1901-1070 | 9 | 4 | DIODE-PIN 110 L | 28480 | 1901-1078 |
| A12criz | 17310059 | 3 | 17 | DIODE- SWITLHING 300 203iat ENS DO-35 | 26489 | 1731-0350 |
| A12CR3 | 1901-1070 | 9 |  | DIODE-PIN 1100 | 28489 <br> 18480 | $1761-1074$ 1201.1070 1902050 |
| A12CRS | 1791-0050 | $\stackrel{3}{3}$ |  |  | -8480 | 1901-0050 |
| AIECRG | 1931-0353 | 3 |  | diode simitching bou zomma mes do 35 | 28480 | 1901-0050 |
| A12CR7 | 1901-1670 | 9 |  | DTODE PIN 1100 | 284110 | 1761-1070 |
| Al2CRg A12CR9 | 1731-3050 |  |  |  | 28.880 | 1701-0950 |
| AlECR10 | 1901-0050 | 3 |  | drook switchiag gou zoma ang do 15 | 29480 | 1901-3050 |
| A12CR 11 $A 12 C R 12$ | 1901-0050 | 3 |  | DITODE SUITCHINE RIGU 2OIMA 2 NE DO 35 | 20480 | 1901-0050 |
| Aler 12 Alecr 13 | $1901-0.050$ $1901-0050$ | 3 <br> 3 |  | DTODE SH1TCHINE GRU 200MA a NS GO 15 | 26483 | 1731-0050 |
| A12CR14 | 19010050 | 3 |  | DTODE SWITCHING GAU 2aOMA ENS EO 35 | P11480 | 1931-0050 |
| A12CR15 | 1901-0050 | 3 |  | DIODE SWITCHING G0U 2GDMA 2NG da 35 | 20480 | 1901-0050 |
| A12CR16 | 1701-0950 | 3 |  | DIODE SWITCHING BJU 230MA ENS DO-35 | 29480 | 1931-0350 |
| A12CR17 A12CR18 | 1901-0050 | 3 |  | DIODE SWITCHING QGU 2GGMA ENS DO 35 | 29480 | 1591-0050 |
| A12CR19 | 1901-0050 | 3 |  | DTIDE SWITCHING EOU 2UOMA ZNS DO 35 | 28480 | 1901-0050 |
| Alzcreo | 1901-0535 | 9 | 2 | DIODE-SM SIG SCliotiky | 70480 | 1731-0535 |
| A12CR21 | 1901-0535 |  |  | DIODE: SM SIC SCHOTTKY | 28480 | 1901-0535 |
|  | 1901-0050 | 3 |  | Drooe-swithing bou cinha ens do-3s | 26480 | 1901-0050 |
| A12F, A1 $^{12 \ell 2}$ | 9170-0029 |  | 3 | CLIRE SHIELDJNG EFAD | 28480 | 9170-0329 |
| A12E3 | $9170-0029$ $9170-0329$ | 3 3 |  |  | 28480 68480 | 917000029 $9170-0029$ |
| ${ }^{\text {A } 2211}$ | $9140-0179$ | 1 | 8 | INDUCTOR RF-CH-MLD $22 U 4102.1660 \times .385 L G$ | 23480 | 9140-0179 |
| A12L2 | 7140-0179 | 1 |  | INDUCTRR RF-CH-MLD 22UH 102.166 DX . 3885 LG | 28480 | 914000179 |
| ${ }_{\text {A12L }}{ }^{\text {A12 }}$ | $9140-0179$ $9140-0179$ | 1 |  |  | 28480 28480 | $9140-0179$ $9140-0179$ |
| A12L5 | 9140-0179 | 1 |  | INDUCTOR RF-CH MLD 22IJH 10\%.166DX. 3 RSLG | P0480 | 9140-0179 |

TABLE 8－10．STEP GAIN ASSEMBLY A12，REPLACEABLE PARTS（2OF 3）

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A12l6 | 7140－0179 | 1 |  | INDUCTOR ar－CH－NLD 22UH $13 \%$ ．156DX．385LG | 28480 | 9140－3179 |
| A12L7 | 9140－0179 | 1 |  | INDUCTOR RF－CH－MLD 22.1 H $18 \% .1650 \times .383 L G$ | 28480 | 71460179 |
| A12L8 A12L9 | 714：－9179 | 1 |  | INCUCTIOR RF－CH－MLD 2CUH $19 \%$ ， 166 EDX ．365LG | 28480 | 9140－0179 |
| A12L9 A12Lis | $9100-2260$ $7140-3158$ | 1 6 | 1 |  | 28480 28483 | $9160-2260$ $9143-0158$ |
| A1201 | 1053－0291 | 9 | 1 | TRANSISTOR PNO 2N2907A SI TO－18 PD＝4CEMW | C4713 |  |
| A1202 | 1954－0323 | 7 | 2 | TRANSISTOR NP＇N SI TO－18 PD $=360 \mathrm{MW}$ ， | 28480 | 1654－0323 |
| A1203 | 1854－0．023 | 9 |  | TRANSISTOR NPN SI TO－18 PD 360 ML | 28480 | 185．4．0023 |
| A1204 | 1354－9637 | 1 | 1 | TRANSTSTGR NPN ŻN2217A ST TO－5 PD $=303 \mathrm{MW}$ | 31295 | 2N2219A |
| A1205 | 1953－0007 | 7 | 3 | TRANSISTOR PNP 2N3251 SI TO－18 PD $=360 \mathrm{MW}$ | 04713 | 2M3251 |
| A1296 | 1053－0007 | 7 |  | TRANSTGTOR PNP 2N3P5 SI $^{\text {S }}$ TO－18 PD $=363 \mathrm{MW}$ | 04713 | 2n3：51 |
| A1207 | 1953－0007 | 7 |  | TRANGISTOR PNP 2N3251 SI TO－18 PD $=366 \mathrm{MW}$ | 64713 | 2N3251 |
| A12c8 | 1053－0．715 | 7 | 3 | TRANSISTOR PNP SI PD $=203 \mathrm{KW}$ FT $=500 \mathrm{MHZ}$ | 28489 | 1853－3015 |
| A12 289 A12010 | $1854-0546$ $1053-0015$ | 1 | 3 | TRANSISTOR NPN SI $T 0-72$ PD＝20日MW | 28480 | 1854－0546 |
| A12Q10 | 1953－0015 | 7 |  | TRANSTSIGR PNP SI PD＝233KL FT＝5036n7 | 28483 | 1553－0315 |
| A12911 | 1954－0546 | 1 |  | TRANSISTOR NPN SI TO－72 PD＝200ML | 28480 | 1054－0546 |
| A12012 A12Q13 | 1854－0546 | 1 |  | TRANSTSTOR NPN SI TO－72 PD＝203mW | 28483 | 1354－0546 |
| A12Q13 | 1853－0015 | 7 |  | TRANSISTOR PNP SI PD $=20 \mathrm{CHW} \mathrm{FT}=500 \mathrm{~m} 4 \mathrm{Z}$ | 28480 | 1853－0015 |
| A12R1 | 9757－0279 | 0 | 4 | RESTSTUR 3．16K $1 \%$ ，125W F TC $=3+109$ | 24546 | C4－1／8－T3－3151－F |
| A1 2R2 | 0698－3444 | 1 | 4 | RESICTOP $3161 \%$ ， 125 S F $\mathrm{TC}=0+10 \mathrm{E}$ | 245.46 | C4－1／8－T0－3162－F |
| A12R3 A1 $12 R 4$ | 3757－9375 | 1 | 3 |  | 24546 | C4－1／8－T0 S6R2－F |
| A12RS | 2130－3752 | 1 | 1 | RESTSTCR－1RMR 530 K 13\％C STDE－ADJ 17－TRN | 24546 78480 | $2130-3752$ |
| A12Rg | 2100－36，11 | 1 | 1 | RESISTOR－TPMR S0K $10 \%$ C SIDE－ADJ 17－TRN | 32977 | 3？92x－1－503 |
| A1227 Al AR8 | 3757－3280 | 3 <br> 8 | 6 | RESTSTOR $1 \mathrm{~K} 1 \%$ ，125W F TCuBt－133 | 24546 | C4－1／B－T0－1031－F |
| A1 $2 R 8$ A12R9 Al | 6757－0417 | 8 3 3 | 1 |  | 24546 | CA－1／8－T0－56．2R－F |
| Al2R9 A1 $2 R 10$ | $0757-0280$ $0698-3155$ | 3 | 1 |  | 24546 24546 | C4－1／B－T3－1091－F C4－1／8－T0－46．41－F |
| AlcR11 | 3757－0465 | 6 | 2 | RESTSTRR 10 JK $1 \%, 1254$ F TC＝3＋－100 | 24546 | C 4 －1／8－T3－1033－F |
| A12R13 | 6757－0346 | 2 |  | RESISTOR $101 \% .125 W$ F TC $=0+100$ | 24546 | C4－1／8－TC－16PG－F |
| A1CR14 | 9757－0346 | 2 |  | RESTSTOR $131 \%$ ，12SW F TC＝0t－103 | 24546 | C4－1／8－T3－10R 3－F |
| A12R15 | 6757－0346 | 2 |  | RESISTOR 10 1\％ 12.125 W F TC Cot－100 | 24546 | C4－1／8－T0 1020－F |
| A12R16 | 1998－3433 | 日 | 2 | RESTSTOR $28.71 \%$ ，12SW F TC $=3+\sim 130$ | 33568 | PRE5S－1／8－T0－2ER7－F |
| A12R17 | 0757－0279 | 1 |  | RESISTOR 3． 16 K 1\％，125W F TC $=0+160$ | 24546 | C4－1／8－T0－3161－F |
| AlcR18 | 0698－3444 | 1 |  | RESISTOR $31612 \times 125,4$ F TC＝3＋－133 | 24546 | C4－1／8－T3－316R－F |
| A12R19 | 6698－3260 | 9 | 2 | RESISTOR 464k $1 \% .1254$ F TC $=0+100$ | 20480 | 0693－32b0 |
| A12R20 | 3757－9395 | 1 |  | RESTSTAR $56.21 \%$ ，12SW T TC＝34－103 | 24546 | C4－1／8－T3－56R2－F |
| A12R21 | 2100－3056 | 8 | 3 | RESISTOR－TPMP 5K 10\％C SIPE－ADJ 17－TRN | 02111 | 43 P 502 |
| A12R22 | 3757－0280 | 3 3 |  | RESISTAR 1 K 12.12 ESW F TC $=31-100$ | 24546 | C．4－1／8－T0－10．31－F |
| A12R23 A12R24 | －7557－0420 | 3 3 3 | 2 | RESISTOP RESTSTOR $1501 \%$ R 1\％ | 24546 24546 | C4－1／8－T0－751－F |
| A12R25 | 0757－0279 | 0 |  |  | 24546 24546 | C4－1／8－T0－1001－F $\mathrm{C} 4-1 / 8-\mathrm{TO}-3161-\mathrm{F}$ |
| A12R26 | 0698－3444 | 1 |  | RESTSTOR 31618 ． 12 SW F $1 \mathrm{C}=3+-100$ | 24546 | C4－1／8－T0－316R－F |
| A12R27 | 0698－3260 | 9 |  | RESISTOR $464 \mathrm{~K} \quad 17.1254$ F TC $=0+-100$ | 28480 | 8690－3260 |
| A12R28 | 3757－0395 | 1 |  | RESISTAR $56.21 \%$ ， 12254 F TC＝$=34-139$ | 24546 | C4 1／8－T3－56R？－F |
| A12R29 | 2100－3056 | 8 |  | RESISTIR－TRMR 5K 10\％C SIPE ADJ 17－TEN | 02111 | 43P582 |
| A12830 | 0757－3280 | 3 |  | RESTSTOR $1 \mathrm{~K} 1 \mathrm{~K}, 125 \mathrm{~L}$ F TC＝0t－100 | 24546 | C4－1／3－T0－1031－F |
| A12R31 | 0757－0420 | 3 |  | RESISTOR $7501 \chi$ ，125w F TC＝0＋－100 | 24546 | C4－1／8－T0－751－F |
| A12R32 | 0757－0280 | 3 |  | RESISTGR $1 \mathrm{~K} 1 \%, 12 \mathrm{SW}$ F TC＝3＋100 | 24546 | C4－1／8－T0－1091－F |
| A12R33 | 0757－0288 | ， | 4 | RESISTOR 9.09 K 17.125 W F TC＝04－106 | 15701 | MF4C1／8－T0－9091－F |
| A12R34 | 0757－0279 | 0 |  | RESISTOR 3．16K 1\％，125W F TC＝0t－109 | 24546 | C4－1／3－T0－3161－F |
| A12R35 | 2100－3103 | 6 | 3 | RESISTOR－TRMR $10 \mathrm{~K} 10 \%$ C STDE－AD． $17-$ TRN | 02111 | 43 F 103 |
| A12R36 | 0757－0288 | 1 |  | RESISTOR 9．09K 1 X ． 125 W F $\mathrm{TC}=0+-102$ | 19701 | MFAC1／8－T3－9091－F |
| A12R37 | 0698－3444 | 5 |  | RESISTOR 316 1\％，1254 F TC＝0 +100 | 24546 | C4－1／8－TG－316R－F |
| A12R38 | 0757－0290 | 5 | 3 | RESISTOR $6,19 \mathrm{~K} \quad 1 \mathrm{~K}$ ，12SU F TC＝02t－130 | 19731 | MFAC1／日－T0－6191－F |
| A12R39 | 2100－3056 | 8 |  | RESISTOR－TRMR 5 L 10\％C SIDF－－ADJ 17－TRN | 02111 | 43 P 502 |
| A12R40 | 0698－3457 | 6 | 1 | RESISTOR 316K 1\％，125W F TC＝0＋ 100 | 28483 | 3698－3457 |
| A12R41 | 0698－3433 | 8 |  | RESISTOR $28.71 \% .1254$ F T $¢=0+-100$ | сз8ав | PMF55－1／8－T0 2ERT－F |
| A12R42 | 0757－0290 | 5 |  | RESISTOR 6， $19 \mathrm{~K} \quad 1 \mathrm{X}, 1254$ F TC $=0+-100$ | 19731 | MF4C1／B－T2 6191－F |
| A12R43 | 0757－1094 | 9 | 1 | RESISTOR 1．47K $1 \mathrm{1z}$ ，125W F TC $=0+-100$ | 24546 | C4－1／8－T0－1471－F |
| A12R44 | 0698－3440 | 7 | 1 | RESISTOR $1961 \chi$ ， 1254 F TC $=0+100$ | 24546 | C4－1／8－T0－196R－F |
| A12R45 | 0757－0441 | 8 | 2 | RESISTOR 8．25K 12 ． 125 W F $\mathrm{TC}=0+100$ | 24546 | C．4－1／8－T0－0251－F |
| A12R46 | 0698－3136 | 8 | 1 | RESISTOR 17， BK 12 ， 125 W F $\mathrm{TC}=0+-100$ | 24546 | C4－1／8－T3－1782－F |
| A12R47 | 2100－0670 | 6 | 3 | RESISTOR－TRMR $10 \mathrm{~K} 10 \chi$ C SIDE－ADJ 17－TRN | 32997 | 3292x－1－103 |
| A12R48 | 2100－3103 | 6 |  | RESISTOR－TRMR 10 K 10 X C SIDE－ADJ 17－TRN | 02111 | 43 P 103 |
| A12R49 | 2100－3750 | 9 | 3 | RESISTOR－TRMR 20 K 10 X C SIDE－ADJ 17－TRN | 28480 | 2100－3750 |
| A12R50＊ | 0757－0458 | 7 | 2 | RESISTOR $51.1 \mathrm{~K} 1 \mathrm{~K}, 125 \mathrm{~W}$ F TC＝0＋-100 | 24546 | C4－1／8－T3－5112－F |
| A12R51 | 2100－3750 | 9 |  | RESISTOR－TRMR 20 K 10X C SIDE－ADJ 17－TRN | 28480 | 2100－3750 |
| A12R52 | 0757－0458 | 7 |  | RESISTOR 51， 1 K 1 K ，12SW F TC $=0+100$ | 24546 | C4－1／B－T0－5112－F |
| A12R53 | 2100－3161 | 6 | 3 | RESISTOR－TRMR 20K 10 X C SIDE－ADJ 17－TRN | 02111 | 435203 |
| A12R54 | 2100－3094 | 4 | 5 | RESISTOR－TRMR 100 K 10 X C SIDE－ADJ 17－TRN | 02111 | 43P104 |
| A12R5S | 2100－3161 | 6 |  | RESISTOR－TRMR 20K $10 \%$ C SIDE－ADJ 17－TRN | 02111 | 43 Pr 203 |
| A12R56 | 2100－3094 | 4 |  | RESISTOR－TRAR 100 K 10 X C SIDE－ADJ 17－TRN | 02111 | 43 P 104 |
| A12R57 | 2100－0544 | 3 | 3 | RESISTOR－TRMR 100 K 10 CK C SIDE－ADJ 17－TRN | 32997 | 3292x－1－104 |
| A12R58 | 2100－3094 | 4 |  | RESISTOR－TRRR 100 K 10 X C SIDE－ADJ 17－TRN | 02111 | $43 P 104$ |
| A12R59 | 2100－3094 | 4 |  | RESISTOR－TRMR 100 K 10x C SIDE－ADJ 17－TRN | 02111 | 43 P 104 |
| A12R60 | 2100－0544 | 3 |  | RESISTOR－TRAR 100K $10 \times \mathrm{X}$ C SIDE－ADJ 17－TRN | 32997 | 3292x－1－104 |
| A12R61 | 2100－0544 | 3 |  | RESISTOR－TRMR 100K 10 X C SIDE－ADJ 17－TRN | 32997 | 3292x－1－104 |

TABLE 8-10. STEP GAIN ASSEMBLY A12, REPLACEABLE PARTS (30F 3 )

| Reference Designation | HP Part Number | $\left\|\begin{array}{l} C \\ \mathrm{D} \end{array}\right\|$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A12R62 | 2193-3094 | 4 |  | PESTSTIR-TRMR 133 K 13\% C SIDE ADJ 17-TRN | 32111 | $43 P 134$ |
| A1 $12 R 63$ Al 1264 | $0698-3157$ $0698-3157$ | 3 3 | 2 |  | 24516 2.4546 |  |
| A12R65 | 0757-0199 | 3 | 1 | RESTSTOP 21.5X $12.125 \mathrm{~S}^{\text {F }}$ F TC=01-106 | 24546 | C.4 1/8-TC-2152.F |
| A12R66 | 3698-3266 | 5 | 1 | aESISTGR 237k 1\% , 12SW F TC=3 1-130 | 24546 | C4 1/8-T0-2373.F |
| A12R67 | 0757-0441 | 8 |  | REGISTOR 8.25\% $17,125 \mathrm{FF}$ TC=0 -106 | 24596 | C4 1/8-T0-2031-F |
| A1ERLB | 3757-3462 | 3 | 1 |  | 28546 | C4 1/3-Ta-75.92-5 |
| A12R69 | 0698-0084 | 9 | 1 | RESISTOR $2,15 \% 12,1254 \mathrm{~F}$ F TC=0+166 | 24546 | C4.1/8-T0-3151-F |
| A1E270 | 2133-0670 | 6 |  |  | 12897 |  |
| Al $2 R 71$ | 2100-3103 | 6 |  |  |  |  |
| A12r72 A12R73* | $2100-0673$ $0757-0463$ | 4 |  |  | 33597 24546 |  |
| A12R73* A1ER74* | $0757-0463$ $0757-0464$ | 4 5 | $\frac{1}{2}$ |  | 24546 7.4546 |  |
| A12R75* | 0757-0464 | 5 |  | RESISTOR $90.9 \mathrm{~K} 1 \mathrm{1z}, 123 \mathrm{~L}$ F TC $=0+100$ | 24546 | C.4. 1/8-T0 -7092-F |
| A12R76 | 9757-0442 | 7 | ? | RESTSTOR 13K 1\% .1254 F TC=34-139 | 24546 | C4 1/8-T9-1032-F |
| ${ }^{\text {A1 }} 12 \mathrm{R} 77$ | 0757-8465 | 6 |  |  | 245.46 24546 |  |
| Al2R78 A12R79 | -0757-0431 | $\stackrel{3}{9}$ | 1 |  | 24546 24546 |  |
| A12R80* | 3757-9346 | 2 | 4 | 2ESTSTOR 10 1\% .1254 F TC-3,-133 | 24546 | C4-1/8-T3-10R3-5 |
| A12R81 | 0757-c289 | 1 |  |  | 17761 |  |
| ${ }^{\text {A1PRE2 }}$ | 0757-0443 | 0 | $?$ |  | 24546 | C4-1/8-T0-1102-F |
| ${ }_{\text {A1 }}^{\text {A12R83 }}$ | 2100-3750 | 9 | 3 | RESISTOR-TRMR 20K 10\% C STEE-ADJ 17-TRN | 28480 24546 | 2106 3750 $\mathrm{CA} 1 / 8 \cdot \mathrm{ta}-1961 \mathrm{~F}$ |
| A12R85 | $0698-0283$ $0757-0288$ | - | 3 |  | 19761 | MF4C1/8-T0 $9691-\mathrm{F}$ |
| Alerbs | 3757-0443 | ${ }^{3}$ |  | RESTSTOR 11K 1 K , $1 \mathrm{ESG4} \mathrm{~F}$ TC $=3+-103$ | 24546 | C4 $1 / 8$ - $73-1132$ F |
| A12R87 | 2100-3161 | 6 |  | RESISTOR-TRMP 20 K 10 z C SIDE-ADJ $17-$ TRN | 02111 | $4 \mathrm{4P} 2 \mathrm{c} 3$ |
| A12R8B* | 0698-0.083 | ${ }_{8}^{8}$ |  |  | 24546 | C4-1/B-T0-1961-F |
| A12R89 A12R90 | $06988-0083$ $3757-0290$ | - |  |  | 24546 19731 | TFFAC1/8-Tシ-6191-F |
| A12S1 | 3101-1618 | 7 | 1 | SWITCH-SL DPDT GUBMIN . 5 A 12SUAC/DC PC | 28480 | 316.1-1610 |
| ${ }_{\text {A12TP1 }}$ | 1251-0600 | 3 | 7 | CONNECIGR-SEL CONT PIN 1.14-MM-ESC-s7 SR | ${ }_{28483}$ | $1251-0600$ |
| Al2TP2 ${ }_{\text {A1 }}$ | $1251-0600$ $1251-0600$ | 0 |  | CONNECTOR-SGL CONT PIN 1.14 HM- iSC--\%\% SQ | 28480 28480 | $1251-0606$ $1: 51-0600$ |
| A12TP4 | 1251-0600 | 0 |  | CONNECTOR-SGL CONT PIN 1.14-MM-BSC-S7 SQ | 28480 | 1251-0606 |
| A12TP5 | 1251-0600 | 0 |  | CENNFCTIR-SCL CONT PIN 1.14-MH-DSC-52 5R | 28483 | 1251-26.30 |
| A12TP6 | 1251-0600 | 0 |  |  | 28480 88480 | $1251-0660$ |
| A12TP7 | $1251-0300$ $1251-0600$ | 0 |  |  | 28480 | ${ }_{1251-0600}^{1251-0600}$ |
| A121P9 | 0360-0.077 | 5 | 1 | TERMINAL-STUD SGL-TUR SWGFİM-MTG | 28480 | 9360-0.977 |
| A12TP 10 | 1251-0600 | 0 |  | CONNECTOR-SGL CONT PIN 1.14-MM-ESC--57 SQ | 28480 | 1251-0600 |
| ${ }^{\text {A1220 }}$ | 1926-0582 |  | 1 | IC SUTTCH ANLG GUAD 16 DIP-C PKG | 27314 | 1.F613201d |
|  | $1826-0161$ $1820-1735$ | 7 | 2 | IC OP ARP GP RUAD 14-DIP-P PKG IC DCDR CMOS ECD-TD-DEC A-TO-10-LINE | 04713 27014 | MtM3icap |
| A12U4 | 1826-0161 | 7 |  | IC OP AMP GP quad 14-DIP-P PKG | 04713 | MLM324P |
| A12U5 | 1810-0208 | 0 | 1 | NETWORK RES 8-SIPb8.JK GHM $\times 7$ | 01121 | $208 A S 83$ |
| A12US A12U7 | $\begin{aligned} & 1810-0206 \\ & 1810-0206 \end{aligned}$ | - | 2 |  | 01121 01121 | 208,103 $208 A 103$ |
| A12UR1 A12UR2 | $1902-3070$ $1982-3070$ 19820 | 5 | 4 |  | 28480 28480 | $1902-3070$ $1902-3070$ |
| A12UR3 | 1902-3070 | 5 |  | DIODE-2NR 4.22 V 5 K DO-35 PD $=4 \mathrm{4W}$ | 28480 | 1902-3070 |
| A12UR4 A12UR5 | $1902-3070$ $1902-3094$ | 5 |  | DIODE-ZNR 4.22U DIODE-ZNR 5.114 SX | 28480 28480 | $1932-3070$ $1902-3094$ |
| A12VRS | 1902-3094 | 3 | 1 | al2 hiccellaneous parts | 28480 | 1902-3094 |
|  | 2200-0101 <br> 08559-0000日 <br> 86701-40001 <br> 2510-0279 | 0 4 9 0 9 | 1 2 1 2 | SCREW-MACH 4-40 , 188-IN-LG PAN-HD-POZI COVER, STEP GAIN <br> EXTRACTOR, PC <br> PLATE, CAÚTION <br> SCREW-MACH 8-32 . 125-IN-LC PAN-HD-SLT | $\begin{aligned} & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \\ & 28480 \end{aligned}$ | 2200-0101 0R559-00038 86701-4C001 06559-20044 $2510-0278$ |

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FIGURE 8.58. STEPGAIN ASSEMBLY A12,BLOCKDIAGRAM

A12


FIGURE 8-59. STEP GAIN ASSEMBLY A12, COMPONENT LOCATIONS


## BANDWIDTH FILTER No. 2 ASSEMBLY A13

Bandwidth Filter No. 2 Assembly A13 is very similar to Bandwidth Filter No. 1 Assembly A11, and corresponding components have the same reference designators. The differences between the two assemblies are in the TO/ FROM designations listed on the schematic diagrams. Refer to the Bandwidth Filter No. 1 Assembly A11 circuit description for complete information on circuit operation.

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TABLE 8-11. BANDWIDTH FILTER NO. 2 ASSEMBLY A13, REPLACEABLE PARTS (10F 3 )

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A13 | 085559 -6025n | 0 | 1 | SANDWIDI: FILTER NO. 2 ASSEMEAY | 78430 | 38559-60058 |
| ${ }^{\text {A }} 313 \mathrm{CL}$ | 0160-2055 | 9 | 38 1 |  | 2а480 | 0160.2055 316000127 |
|  | - $116.60-2655$ | 2 9 9 |  | CAPACSTOR-FXD ETUE +30-26\% 100UDC CIR | 23480 | $6160-2055$ |
| A13c5 | 3160-2355 | ? |  |  | 2e483 22480 | $3160-2355$ $0160-2055$ |
| A 13 Cb | 6160-2055 | 9 |  | CAPACITOR-FXO .eluF +00-20\% iecude cre | 22480 | 0160-2055 |
| Al:c7 | 31602055 | $?$ |  |  | 28480 | 3160-2355 |
| A13C8 | 0160-2267 | 3 | $?$ | CAPACTTOR-FXD 300RT + $5 \%$ 300UDC MICA | 22480 | 0160 220\% |
| A13C. | 3160-2055 | $?$ |  |  | 28483 | 3160-2055 |
| Al3C10 A1 15 C 11 | $0160-2055$ $0160-2355$ | 9 |  |  | 28488 28483 | $6160-2055$ $3160-2355$ |
| A 13612 | 11160-2655 | 9 |  |  | 2а¢80 | ©160-2055 |
| A13C13 | 111603456 | 6 | 3 | CAPAC:ITOR-FXD 10009F +-13\% 1 KVEC CER | 28483 | 3160-3456 |
| ${ }_{\text {A } 13 C 14}$ | 0160-2249 | 3 | 2 | CAPACITOP-FXD 4.7PT $+-.25{ }^{\text {² }}$ S SCOUDC CRE | 28488 | c160-2249 |
| ${ }^{\text {n } 13 \mathrm{SCL}} 15$ | 21210059 | ? | 2 | CAPACITR U TRMR -EER 2 ERF $35 J$ PC MTG | 5.2763 | 334324 2/BPF NPO |
| A13C16* | (0) 60-0134 | 1 | 4 | CAPACITO2-FXD 220PF +-5\% 3CEUDC MICA | 20480 | 0160-0134 |
| Alze.17 | 2163-2355 | 7 |  |  | 28980 | 3160-2355 |
| A13C18 | 0160-2655 | ? |  |  | 20480 | $0160-2055$ |
|  | $3160-2355$ $0160-0134$ | ? |  |  | 2R480 28480 | $0160-2055$ $0160-0134$ |
| ${ }_{\text {A13C21 }}$ | 21600437 | 7 | 2 | CAPACITIGR-FXD | 28480 | 3169-10437 |
| A13C22 | 0160-4884 | 8 | 3 | CAPACITOR-TXD -14F +-20\% SOUDC CER | 20480 | 016.0-4084 |
| ${ }^{\text {A13 }}$ A 23 | 01210336 | $\stackrel{3}{9}$ |  | CAPACITGR-U TRMR-CER S.5-13PF 3530 | 5.2763 | $3043245.5 / 18 P F$ NPO |
|  | $0160-21.55$ 01210446 0.046 | 6 | ? |  | 2\%480 | c16c-205S $3121-0446$ |
| A13626 | $0160-2655$ | 9 |  | CAPACITOR-FXID .O1UF +80-20\% 100UDC CER | 28480 | 0160-2055 |
| Alzes | 3163-2355 | 9 |  |  | 28483 | 3160-2955 |
| ${ }_{\text {A }} 13 \mathrm{3C28}$ | 0160-2055 | 9 |  |  | 28480 | c160-2055 |
| A13c29 | - 0160.3456 | ${ }_{6}^{6}$ |  |  | 28480 | ${ }^{3160-3456}$ |
| Al3r.31 | 0160-4250 | 6 | 1 |  | S4z89 | C0s\%F2514472msiz-CDH |
| A13C32 | 0160-4094 | 8 |  | CAPACXTOR-FXD 14 F + $26 \%$ SOUDC CER | 28486 | 8160-4084 |
| ${ }^{\text {A13 }} 13 \mathrm{C33}$ | $0160-2237$ | 3 |  | CAPACTIUR FXD $33625+5 \times 333$ DDC MICA | 23483 | 0160-2237 |
| A13C34 A13c35 | 0160-2055 | 9 |  |  | 28480 | $0160-2055$ |
| ${ }_{\text {A } 13 C 36}$ | $0160-2655$ | 9 |  | CAPACITOP-FXD .O1UF +8C-20X 100UDC CER | 28480 | 0160-2055 |
| ${ }_{\text {A13C37 }}$ | 01602249 | 7 |  | CAPACITOR-FXD 4.7PF, 2SPF 50, | 78480 50763 | $3160-2249$ |
| A13C38 A13C.40 | 0121-0659 | 9 |  |  | 5.2763 23480 | $3043242 / 8 \mathrm{PPT}$ NPO $0160-2055$ |
| A13C40 | $0160-2355$ $0160-3456$ | ? |  |  | 29480 | $016.0-3456$ |
| A13C42 $^{\text {a }}$ | 0160-2055 | ? |  | CAPACITOR-FXD - D1UF - B3-20\% 10JVDC CER | 28483 | 3160-2055 |
| A13C43* | 0160-0134 | 1 |  | CAPACTTOR-FXD 22OPF + $5 \times$ 300UDC MICA | 28480 | 016000134 |
| A13C4S | -3160-0437 | 7 |  |  | ${ }_{52760}$ |  |
| A13C46 | $0160-4034$ | B |  | CAPGC,ITOR-FXD, 1UF +-20x SOULC CER | ¢8480 | ${ }^{3160-4084}$ |
| A13C47 | 0160-2655 | 9 |  | CAPACITOR-FXD O1UF +80-20\% 100UDC. CCR | 28480 | c. $160-2055$ |
| ${ }^{\text {A } 13 C 48}$ | 0160-2955 | ? |  | CAPACITIR-FXD .01UF +80-20\% 100VDC CER | 28480 | 0160-2055 |
| A13C49 | 0160-2055 | 9 |  | CAPACITOP-FXD . 014 F + 80020 O 100UDC CCR | 28480 | 0160-2055 |
| A13C5a | 2160-2055 | ? |  |  | 28480 28480 | 3160-2055 |
| A13c52 | 0160-2055 | $?$ |  | CAPACITOR-FXD , 01UF + Ba-20x 100 VDC CER | 28480 | $3160-2055$ |
| ${ }_{\text {A13 }}{ }^{\text {a }} 3 \mathrm{CS5}$ | 0160-2055 | 9 |  | CAPACITRP-FXD O1UF +00-20\% 100UDC CCR | 28480 | 0160-2055 |
| A13C54 | 0121-0446 | 6 |  | CAPACITGR-U TRMR-CER 4.5-20PF 163 J | 28483 | 0121-0446 |
| A13css A13C60 | $0160-2055$ $0160-2055$ | 9 |  |  | 28480 28480 | $0160-2055$ $0160-2055$ |
| A13C61 | 0160-2055 | 9 |  | CAPACITOR-FXD O1UF + 00-20\% 100UDC CER | 28480 | 0160-2655 |
| ${ }^{\text {A } 13 C 62}$ | 0160-2055 |  |  | CAPACITOR-FXD .01UF + $00-202$ 100UDC CER | 28480 | 3160-2355 |
| ${ }^{\text {A } 13 C 63}$ | 0160-2055 | 9 |  | CAPACITOR-EXD O1UF + $00-20 x$ 100UDC CER | 28480 | 0160-2055 |
| A13c.64** | $0160-0134$ $0160-2055$ | 1 |  | CAPACITOR-FXD CAPACITOR-FXD | ${ }_{28480}^{28480}$ | 3160-9134 |
| ${ }_{\text {A1 }}$ | $0160-2055$ | 9 |  | CAPACITOR-FXD, 010 F + $80-202 \mathrm{Z}$ 100VCC CER | ${ }^{28480}$ | 0160-2055 |
| ${ }_{\text {A1 }}{ }^{13 \mathrm{C}} \mathrm{C} 67$ | 0160-2055 |  |  | CAPACITOR-FXD O1UF +80-20x 100UDC CER | 28480 | 0160-2055 |
| A13C68 A13C69 | 0160-2258 | $\stackrel{4}{4}$ | 1 |  | 28480 | 3160-2258 |
| A13C69 | $0160-2055$ $0121-0452$ | 4 | 2 |  | 28480 74770 | 0160-2055 $187-0103-028$ |
| A13C74 | 0121-0452 | 4 |  | CAPACITOR-U TRMR-AIR 1.3-5.APF 1750 | 74970 | 187-0103-028 |
| A13CR1 | 1901-0047 |  | 6 | diode -switching zou 75ma ions | 28480 | 1901-0047 |
| A13CR2 | 1901-0047 | 8 |  | DIOde-SUITCHING 20U 75MA 10NS | 28480 | 1901-0047 |
| ${ }^{\text {A13CR3 }}$ | 1901-1070 | ? | 5 | DIODE-PIN 1100 | 28480 | 1901-1070 |
| A13CR4 A13CR5 | $1901-1070$ $1901-1070$ | 9 |  | DIODE-PIN 1100 <br> DIODE-PIN <br> 1100 | 28480 28480 | $1901-1070$ $1701-1070$ |

TABLE8-11. BANDWIDTHFITTERNO.2ASSEMBLY A13, REPLACEABLEPARTS (2OF3)

| Reference Designation | HP Part Number | ${ }_{0}^{\text {c }}$ | Oty | Description | $\begin{aligned} & \text { Mfr } \\ & \text { Code } \end{aligned}$ | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 5 | drabe sh sit scuitity | ceich |  |
|  | (19010007 |  |  |  | ceat | 隹 |
|  | ${ }^{\text {cosen }}$ |  |  |  |  | ${ }^{\text {a }}$ |
|  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| ${ }^{\text {A1 35CR16 }}$ | 1901-0047 |  |  | drope-suitching 20w 75 KA 10 Ns | 29880 | 1901-0047 |
| ${ }^{\text {A1ECR17 }}$ | 1901--5535 |  |  | dtobe sh ste sciotiky | $\square_{\text {гяв }}$ | 1931-9535 |
|  |  |  | : |  | ¢ | \%170.009 |
|  |  | 3 |  |  |  |  |
|  | 9170-0629 | 3 |  | cone-Shitliming head | 28800 | 9170.0029 |
|  |  | $3_{3}^{3}$ |  |  | coich |  |
| ${ }_{\text {a } 234}$ | $9140-0112$ |  |  |  | zaasa | ${ }^{\text {914C }}$ |
| ${ }_{\text {a }}^{\text {atal }}$ |  |  |  |  | ¢naso |  |
| ${ }_{\text {Als }}^{\text {A13L4 }}$ |  |  |  |  | ${ }_{\substack{\text { zeabo } \\ \text { casoo }}}$ |  |
|  |  |  | 1 <br> 1 <br> $\frac{1}{2}$ <br> 2 <br> 2 <br> 2 <br>  |  | ${ }_{\substack{\text { zasa } \\ \text { 2пaba }}}$ | (9100-2613 |
|  |  | ${ }_{4}^{2}$ |  | INDUCTOR RI-CH-MCD $6,8 U H 10 \%$INDUC:TIR RF-CH-MID $10 U H 10 \%, 166 D X, 385 I, G$ | $\underbrace{}_{\substack{\text { zabab } \\ \text { casac }}}$ |  |
|  |  |  |  |  |  |  |
|  |  |  |  | INDUCTOR RF-CH-ME D $3 C U H 5 \%, 166 D X, 385 L G$ $\begin{array}{llll}\text { INDUSTOR RF-CH-MLD } & 22 U H & 10 \% & 166 D X, 385 L G \\ \text { INDUCTOR RF-CH-MLD } & 2.2 U H & 5 \% & .165 D X, 395 \mathrm{~L}\end{array}$ NDUCTOR |  |  |
|  |  |  | 1 |  |  |  |
| ${ }_{\text {a }}^{\text {Al13117 }}$ |  |  |  |  INEUCTOR RF-CH-MLD $6.6 U H$ <br> , | 28493 | , 9140-3194 |
|  |  | - |  |  |  |  |
|  |  |  | 2 |  | cistis | 2w5179 |
|  |  |  |  |  | (2atio | cose |
|  | (1835-0007 |  |  |  |  |  |
|  |  |  |  | TRANGISTOR PNP $2 N 3251$ SI TO-18 PD $=360 \mathrm{ML}$ TRANSTSTGR NPN SI TO-18 PD=363ML TRANSISTOR PNP 2N32S1 SI TO-18 PD $=36,6 \mathrm{MS}$ | ${ }_{\substack{\text { on7 } \\ \text { cis } \\ \text { 280 }}}$ |  |
|  | (1035-007 | 5 |  |  |  |  |
|  | 1853-000 |  |  |  <br> $\begin{array}{lllllll}\text { RESTGTOR } & 12,1 \mathrm{~K} & 1 Z & 125 \mathrm{~F} & \mathrm{~F} & \mathrm{TC}=0+-100 \\ \text { RESIGTOR } & 14,7 \mathrm{~K} & 1 \% & 125 \mathrm{H} & \mathrm{F} & \mathrm{TC}=0+-100\end{array}$ <br> RESISTOR 14.7K 12,1254 F TC=0t-180 |  | 2 N 351 |
|  |  | 2 | ? |  |  |  |
|  |  | ? |  |  | 边 |  |
|  |  |  | 1, | $\begin{array}{llllll}\text { RESISTOR } & 23.7 & 1 \% & .125 & F & T C=0+-100 \\ \text { RESISTOR } & 5.62 & 1 \% & 125 W & F & T C=0+-100\end{array}$ |  |  |
|  |  |  |  |  | cose |  |
|  |  |  |  |  | ${ }^{2}$ |  |
| ${ }_{\text {al }}^{\text {Ali } 13812}$ |  | 4 | + |  | ${ }_{2}^{24546}$ |  |
| cole |  |  | 1 |  |  |  |
| A 138 R 15 | 0659-3440 |  |  |  | 24546 | C4-1/8-To-1968-F |
|  |  | $\cdots$ | ${ }^{2}$ |  | ${ }_{\text {cole }}^{24546}$ |  |
|  |  | i |  | (RESISTOR 4.22 Sa | ${ }_{2}^{295964}$ |  |
| A13 320 | 0757-0442 | - |  |  | ${ }^{24596}$ | C4.1/8-T---1602-F |
|  |  | ? |  |  |  |  |
|  |  |  | 2 |  | ${ }^{24546}$ $\underset{\substack{12701 \\ 24546}}{ }$ |  |

TABLE 8-11. BANDWIDTH FILTER NO. 2 ASSEMBLY A13, REPLACEABLE PARTS (30F 3 )

| Reference Designation | HP Part Number | $\left\|\begin{array}{l} c \\ d \end{array}\right\|$ | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{A}_{1} 3 \mathrm{BL} \times 5$ | 9757-8465 | $\wedge$ |  |  | 27545 | Cat 1/8-19-1033F |
| A13R26 $A 12 R 2 \%$ | $2100-3163$ $3757-10444$ | $\stackrel{11}{7}$ | 1 |  |  |  |
| A13R28 | 0757-0443 | $\bigcirc$ | 2 |  | - 2458 | C4 1/8-TB 1102F |
| Alı3z? ${ }^{\text {a }}$ | 3698-0363 |  | 2 |  | 2454 |  |
| A1 3R 3 E |  | 3 | 1 | RESISTOR 215k :\% , 125w F TC=0+-100 | -4:\% | c.4 1/8-10 215.F |
| A13R 34 | 3757-3199 | 3 | 1 |  | 245\% | C4-1/0-T3-2152F |
| Al 3 385 | 0757-0288 | 1 |  | PCSTSTOR 9, b9\% 1\% . 123\% F TC=0+-160 | 1976, | MFAC1/8-T6.9091-F |
| ${ }^{\text {A } 13836}$ | n698-19383 | $\stackrel{8}{8}$ |  | RESISTGR 1.96\% $1 \%$, 125, FF TC=3+-139 | 24.45 | C4-1/8-70-1961 F |
| A 13837 | 0757-0416 | 7 | $?$ |  | 24544 | C. $1 / 8-78-5118-\mathrm{F}$ |
|  | $16986-3441$ $0757-0419$ | 8 0 0 | 1 |  | 24545 24545 | C.4-1/8-T0-6151R-F |
| A13R 49 | 16.98-3442 | ${ }_{9}$ |  | RESTSTOR z37 1\% , 12ew F $16=0+\cdots 100$ | 2-454; |  |
| A133841 | 06998.-3154 | ${ }^{11}$ |  | RESISTOR 4. 22k 1\%, 125is F TC $=01-160$ | \%45\% | C4 1/8-T0-4as 1-F |
|  | $0757-0442$ $0678-3155$ | Q |  |  | 2454.46 | C4. 1/8-73-1092-F |
|  | -0698-3155 | ' |  |  | 24.5046 | C4-1/8-70-1092-F |
| A13R45 | 0757-1461 | $\bigcirc$ |  | RESISTOR 106 1\%.125id F TC=0+-160 | 24:\% 6 | C4. 1/8- $010161-\mathrm{F}$ |
| 213846 | 97570401 | 0 |  | RESTSTGR 100 1\% .12sw F TC=0.-130 | 2.5545 | C4-1/0-T0-191-F |
| 213 S 47 | 0757-0346 | 2 | 4 | RESISTOR 10, $1 \%$ 125w F TC=0, 106 | 2455 | C4 1/6-T6 16R6F |
| 213 RSO | -0757-11346 | 2 |  |  | 24546 | C4-1/3-T0-1083-F |
| A13851 | 0757-6346 | 2 |  | RESISTOR $101 \%$, 125W F TC=0, 100 | 24:34, | C.4.1/8-Tb-1apt-F |
| A13REs | 3757-0443 | $\stackrel{3}{7}$ |  |  | 245,43 | C4 1/8-79 1102F |
| ${ }_{\text {A }} 13 \mathrm{zrs3}$ | 1698-3440 | 7 |  |  | ${ }^{345545}$ |  |
| A13855 | 0757-0442 | 9 |  | RESISTOR 10 K 1\% . 125 F F TC=04-106 | 24545 | C4 1/8-T0-1002-F |
| ${ }^{2} 13 \mathrm{REF}$ | 0757-9274 | 5 | 1 |  | 24.546 | C4-1/0-T0-1211-F |
| 213R57 | 8757-0190 $0658-3158$ | 3 | 2 |  | $\underbrace{284504}_{2}$ | $6757-0180$ $64.1 / 8-70 \cdot 3481$ |
| 213 R 57 | 0757-0180 | 2 |  |  | 20488 | 6757-0180 |
| 2 13 Rt 0 | 0678-3153 | , | 1 | RESTSTOR 3 82\% $1 \%$, 125W F TC=0+100 | 2.3543 | C4-1/8--T0-3831-F |
| ${ }^{\text {A }} 13 \mathrm{FP1}$ | 0360-1783 | ${ }^{\infty}$ | 4 | CONNECTOR-GEG CONT PIN O4F-IN-ESC-SZ 50 | ${ }^{20480}$ | $036.0-1789$ $3 \times 6.1788$ |
| ${ }^{\text {A } 137 P 2}$ | 0360-1788 | J |  |  | cesmo | 3361.1788 |
| A13TP3 A13TP.4 | 1251-0600 | ${ }^{\circ}$ | 7 | CONNECTOR GGE CONT PIN 1.14 -MM-ESC S7 SQ | - 288490 | $1251-0608$ $0360-1788$ |
| A13TP5 | 0360-1708 | 1 |  |  | 23480 | 036.0-1783 |
| 213176 | 1251-0600 |  |  |  | 28460 | 1251-0600 |
| 213TP8 813197 | $1251-0600$ $1251-0600$ | ${ }^{0}$ |  | CONNECTOR-SGL CONT PIN 1.14-M-ESCC SI SQ |  | 1251-0600 |
| ${ }_{2}{ }^{2} 151910$ | $1251-0600$ $1251-0600$ | ${ }_{0}$ |  | CONNECTOR-SGL CONT PIN 1.14 MM -HSC SX SQ | 2848日 <br> $\mathbf{2 8 4 9 0}$ | $1251-0600$ $1251-0600$ |
| 213TP1 1 | 1251-0600 | ${ }^{1}$ |  | CINNECTGR-SGL CONT PIN 1.14- Mm-bece sz SQ | 28487 | 1251-0600 |
| 213 P12 | 1251-0600 | 0 |  | CONNECTOR SGt. CONT PIN 1.14 MM-ESC--5Z SQ | 20480 | 1251-0600 |
| 213UR 1 | 1902-0048 | 1 | 1 | DIODE-7NR 6. $11 \mathrm{~V} 5 \mathrm{~K} \mathrm{DD}-35 \mathrm{PD}=.4 \mathrm{~L}$ | 2340 cr | 1902-0048 |
| $\begin{aligned} & A 13 V_{1} \\ & A 1312 \end{aligned}$ | $\begin{aligned} & 0410-0776 \\ & 0410-0776 \end{aligned}$ | $\left\|\begin{array}{l} \mathrm{a} \\ \mathrm{~B} \end{array}\right\|$ | 2 | CRYGTAL-qUARTZ 21.4 MHZ HC-25/I-HLDR CRYSTAL-GUARTZ 21.4 MHZ HC 25/U-HiDR alz higcellanedus parts | $284 \pi 0$ $28430$ | $\begin{aligned} & 0410 \cdots 0776 \\ & 0410-0776 \end{aligned}$ |
|  | 0403-0026 08559-0002כ 03559-00009 | $\left\|\begin{array}{l} 0 \\ \underset{\sim}{c} \\ \underset{\sim}{c} \end{array}\right\|$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \end{aligned}$ | PLUG-HOLE BDR-HI FUR . 167 D-HILE NYL baffle inductar <br> COVER, EW FTLTER ND. 2 | 122760 28480 28490 |  |

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A13


FIGURE8-62. BANDWIDTHFILTERNO.2ASSEMBLY A13,COMPONENT LOCATIONS


## LOG AMPLIFIER ASSEMBLY A14, CIRCUIT DESCRIPTION

The Log Amplifier Assembly A14 includes seven amplifier stages, each capable of providing linear and logarithmic amplification. A detector circuit following the amplifier stages detects the amplified $21.4 \mathbf{M H z} \mathrm{IF}$ signal, producing the vertical display signal. The offset circuit that follows the detector operates in Log mode to offset the vertical display signal in 100 mV steps. This steps the display in four $10-\mathrm{dB}$ increments of apparent gain and adds the last 40 dB of displayed step gain to the gain $(50 \mathrm{~dB})$ already provided in the IF section.

## Amplifier Stages (1st through 7th) (A) (C) (D) (E) (F) (G) (H)

The seven amplifier stages are similar in operation. Different stages are selected as linear or log amplifiers, depending on the setting of the Amplitude Scale switch.

Log Mode of Operation. In Log mode, the gain of the seven amplifier stages is sequentially limited as the signal level increases. Limiting starts with stage seven, since it sees the combined gains of the other stages, and continues sequentially as the signal level increases. Stage one is the last stage to begin limiting the signal. The total limiting process provides 70 dB of $\log$ display range. Each stage consists of an emitter follower voltagedriver and a common-base amplifier in which the gain is signal-level dependent. Increases in signal level decrease the gain.
A simplified schematic of a typical log stage (the second stage) is shown in Figure 8-64. In Log mode, the LOG/ LIN control line is high (about +15 V ); Q24 is on, forward biasing diodes CR1O and CR11 and the log diodes in all of the other stages. Diodes CR1O and CR1l are Schottky diodes with a forward bias voltage of approximately 0.4 V . Emitter follower Q13 is a voltage source that develops signal current flow through CR1O and CR1 1 . This signal-current drives Q20, a common-base amplifier tuned to approximately 21.4 MHz . The gain of this amplifier is set by the ratio of R52 to the total resistance, R,, between the emitters of Q13 and 420 (primarily the resistance of CR1O and CR11). The formula for computing the gain in dB is:

$$
\text { Gain }(\mathrm{dB})=20 \mathrm{LOG}\left(1+\mathrm{R} 52 / \mathrm{R}_{\mathrm{T}}\right)
$$



FIGURE 864. LOG MODEOPERATION,SIMPLIFIEDSCHEMATIC

Resistance $R_{T}$ is at a minimum (approximately 150 ohms) for small signals. The small signal gain of the stage (about 10 dB ) is established by the dc bias through the log diodes. As the signal level at the emitter of Q13 increases, signal current cancels bias current in the $\log$ diodes, increasing $\mathrm{R}_{\mathrm{T}}$. The gain of the stage for large signals is reduced to unity ( 0 dB ) as $\mathrm{R}_{\mathrm{T}}$ becomes very large.

Linear Mode of Operation. Two simplified schematics illustrating unity and 10 dB gain of a typical linear stage are shown in Figures 8-65 and 8-66. In linear mode, the signal level dependent components are removed from the signal path and a linear display is provided. The -8 VT is applied to the base of Q 24 , turning it off. This removes dc bias from CR10 and CR11. Total resistance $\mathrm{R}_{\mathrm{T}}$ (primarily the resistance of R56 and CR12) is high, since CR12 is reverse-biased. Control line IFG6 is high and the stage gain is near unity. The signal flow is through emitter follower Q13 and R52, to 420. In stages six and seven, an alternate signal path is used to fix the gain at about 5 dB per stage, allowing for scale differences between Log and Lin modes. Both stages are activated by the -8 VT from the Amplitude Scale switch through R34, R93, R101, CR25, and CR28. The combined stage gain is adjusted by R34 (LIN), which controls the dc PIN diode bias.


FIGURE 8-65. UNITY GAIN OPERATION IN LINEAR MODE, SIMPLIFIED SCHEMATIC

Stage $2,3,4$, and 5 each have an alternate signal path that switches in 10 dB of step gain for a total of 40 dB . The alternate path is selected by the REFERENCE LEVEL control. With the INPUT ATTEN at 0 dB and the REFERENCE LEVEL control at -60 dBm , the -8 VT is routed, via the IF gain control line (IFG4), to forward bias CR22 in stage 5. For each stepped increase in the REFERENCE LEVEL control, the - 8 VT activates the IFG lines associated with the stages of gain required, forward biasing the diodes in the signal path. Each IFG line has a potentiometer (block B) that controls the line's bias current and the stage gain. Note that IFG6 controls two stages (stages 2 and 3 ) that, when switched in, provide 20 dB of gain.

## Gain Control Lines (B)

The +15 V (in Log mode) or the -8 VT (in Lin mode) is routed through the REFERENCE LEVEL switch to the combination of IFG4, IFG5, and IFG6 corresponding to the referencelevel selected. In Log mode, the Log Offset circuit is activated through R24, R25, and R26. The LOG/LIN line is at $+15 \mathrm{~V}, \mathrm{Q} 24$ is saturated, and the


FIGURE866. 10 dB GAIN OPERATIONIN LINEAR MODE, SIMPLIFIEDSCHEMATIC
collector of $\mathbf{Q} 24$ goes to -8 VT , turning the $\log$ diodes on. In Lin mode, the LOG/LIN line is at $-8 \mathrm{VT}, \mathrm{Q} 24$ is turned off and current flows through R34 (LIN) to stages 6 and 7.

## Log Mode Temperature-Controlled Variable-GainAmplifier (J)

In Lin mode, when approximately $700 \mathrm{mV} \mathrm{rms}(+10 \mathrm{dBm})$ is applied to the input of the Log amplifier, the voltage at the output of stage 7 (TP5) is about 1.5 rms . With the same input in Log mode, the output at TP5 is about 2.0 V rms. To maintain an equal relationship with maximum input signal (the trace at top display), the output in Log mode must be attenuated. This attenuation is achieved with variable gain amplifier 47, the gain of which is determined by the ratio of its collector load to its emitter load.

In Lin mode, the LOG/LIN line is a -8 VT, CR4 is forward biased, and the output of U2b (TP1) is approximately +15 V . Diode CR29 is reverse biased and the gain of the variable gain amplifier is R104/R105 (100/316) or approximately 0.3. In Log mode, the LOG/LIN line is at +15 V , CR4 is reverse biased, and the output of U2b (TP1) is about -0.45 V . Diode CR29 is forward biased and exhibits an ac resistance of about 100 ohms. This resistance is in parallel with the 100 ohms of R104 for a total of 50 ohms. Since the collector load of 47 is about 50 ohms, the gain becomes $0.15(50 / 316)$. This gain depends upon the resistance of CR29, which is established by SLOPE adjustment R23.

## Detector (K)

The detector comprises a voltage-to-current converter, a half-wave rectifier, and a low-pass filter. The output of the variable gain amplifier is applied to 46, where voltage variations are converted to current variations. Transistor Q5 acts as a current driver for half-wave rectifier Q4, while CR1 biases 44 just below cutoff. When the signal is positive going, Q 4 conducts; during the negative half-cycle, Q 4 is cutoff. The detector's output goes to the low-pass filter, a series of pi-section filters that smooth the detector's output and remove RF signal components.

## Buffer Amplifier (L)

The detector's output, the video signal, is amplified by the Buffer Amplifier. Differential pair 421 and driver 422 approximate a noninverting operational amplifier with a gain calculated by the formula:

$$
\text { Gain }=1+\mathrm{R} 110 / \mathrm{R} 116
$$

Which becomes:

$$
1+619 / 619=2
$$

## Log Offset (M)

The offset circuit operates in Log mode to offset the video signal in four 100 mV steps. These appear on the display as 10 dB steps of apparent gain. This gain adds the last 40 dB of display step gain to the 50 dB of gain already provided by the Step Gain Assembly A12. The offset is provided by Q23 operating as a current source that steps the current through R119. When the Log mode is selected, +15 V via the REFERENCE LEVEL switch can be applied to IF gain control lines IFG4, IFG5, and IFG6. When an IFG line is activated, the associated log-shift diode (CR31, CR32, or CR33) is forward biased, causing current (determined by R123, R124, or R125) to flow in Q23. Each IFG line supplies a specific offset when activated; IFG4 and IFGS each provide 100 mV , while IFG6 provides 200 mV . The LOG GAIN adjustment (R121) establishes the operating point of Q23 as needed for 100 mV steps.

## TemperatureCompensation Power Supply (I)

Temperature compensating of the Log Amplifier Assembly A14 is provided by the -8 VT (both VT and VTV mean Volts Temperature Variable) and -1 VTV regulators while CR2 operates as the temperature-sensing element. Temperature variations cause diode voltage changes that, when amplified by Ula, regulate the -8 VT supply. Since the -1 VTV supply is coupled to the -8 VT supply through R17 and R132, its output is also temperature variable. The -8 VT provides bias for the log diodes in Log mode, and bias current for CR12, CR19, CR22, and CR28 in Lin mode. The - 1 VTV supplies bias to CR29 in the variable gain amplifier.

## +11V Regulated Power Supply (N)

A precise +5.4 V reference for the +11 V regulator is provided by VR1. This reference voltage is applied to the noninverting input of Ulb. Since the ratio of R5 to R6 establishes the gain of Ulb at 2.1, the output at TP2 is 2.1 times $+5.4(+11.3 \mathrm{~V})$. Emitter follower Q1 provides current drive for the +11 V supply.

## LOG AMPLIFIER ASSEMBLY A14, TROUBLESHOOTING

Check supply voltages.
Dead Stage: Use an oscilloscope along the signal path to locate a dead stage.
Check the dc levels along the signal path. Beginning after stage two, the dc level alternates between -0.7 V and OV with each successive stage because of the direct coupling of the stages. This is noted in the waveforms indicated on the schematic.

Log Fidelity Accuracy: Begin testing by establishing a top graticule reference (eighth graticule). Reduce the input signal level in 10 dB steps and observe the variations between each step. Now, establish a reference at the next graticule 100 mV lower (seventh graticule). Step the signal level again and observe the variation between the steps. Continue lowering the reference point until each step below the reference point is within specification. This will indicate at which step the inaccuracies are being introduced. If the error occurs between the 800 mV reference and the 700 mV reference, the problem is probably in the first stage. If the problem is present at all referencelevels except the last one, the problem is probably in the last amplifier stage, sinceit compresses first.

The most probable causes of failure are PIN diodes, Schottky diodes, transistors, capacitors, and resistors, in that order.

Schottky diodes have a dc resistance of about 300 to 330 ohms. The value varies, depending on the current supplied by the ohmmeter. The values should, however, all be within $10 \%$ of each other.

TABLE 8-12. LOG AMPLIFIER ASSEMBLY A14, REPLACEABLE PARTS (1 OF 4)

| Reference Designation | HP Part Number | c | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A14 | 5061-5411 | 2 | 1 | LCG AMPLIFIER ASSEMEL.Y | 28480 | 5361-5411 |
| A $14 C 1$ A14C2 | $0160-4554$ $3180-0197$ | 7 | 67 |  | P8480 S6287 | 816.0.4554 $15 \mathrm{SD} 225 \times 9023 \mathrm{~A}$ |
| ${ }_{\text {A1 }}^{\text {Al } 14 C 2}$ | $3180-0177$ $0160-4554$ | $\stackrel{8}{7}$ | 1 | CAPACITOR-FXD , D1UF +-26\% SOUDC CER | ${ }_{23480}$ | $0166-4554$ |
| A14C4 | 3160-4084 | 8 | 2 | CAPACIIOR-FXD . 14 F +-23\% SOUDC CER | 2¢480 | 3160-4084 |
| A14C5 | 0160-4084 | - |  | CAPACITOR-FXD , 14F +-20\% SOUDC CER | 28480 | 01604084 |
| ${ }^{\text {A } 14 C 6}$ | - 0160 - 0554 | 7 |  | CAPACITUR-FXD . D11F +-23Z SJUDC CER | 28483 | 3160-4554 |
| A14C7 Al ACB | $0160-3879$ $0160-4554$ | 7 | 1 |  | ${ }_{\substack{28486 \\ 28489}}^{\text {20, }}$ | $01600-3879$ $3163-4554$ |
| A14C9 | 0160-4554 | 7 |  | CAPACITOR-FXD OIUF + -2\% SOUDC CRR | 28480 | 0160.4554 |
| A14C10 | 3160-4554 | 7 |  | CAPGCITOR - $\times$ XD . D1uF --2az SJVDC CER | 28480 | 2169-455.4 |
| ${ }^{\text {A } 4 \mathrm{ACL}_{11}}$ | 0160-4554 | 7 |  | CAPACITOR-FXD 01UF +-20\% SOUDC CER | 28490 | c160.4554 $3160-4554$ |
|  | $0160-4554$ $0160-4554$ | 7 |  |  | ${ }^{28489}$ | $3160-4554$ 8166.4554 |
| A14C15 | 1160-4554 | 7 |  | CAPAC,ITGR-FXD , D1UF t-23\% SJUDC CER | \% 483 | 3160-4554 |
| A14C16 | 0160-4554 | 7 |  | CAPACITOR-FXD .OTUF +-202 SOUDC CER | 28480 | 0166.4554 |
| A14C17 | 0169-4554 | 7 |  | CAPGEITTOR-FXD , DIUF +-2J\% SJUDC CER | c3489 | 3160-4554 |
| A14C18 | 0160-4554 | 7 |  | CAPACITOR-FXD 01UF +-2\% SOUDC CFR | 23480 | 6160.4554 |
| A14C19 A14C20 | 0160-4554 | 7 |  |  | 28480 | 3160-4554 |
| Alacel | $6160-4554$ $3163-4554$ | 7 |  | CAPACITGR-FXD .31UF + 232 SJVDC CER | 29480 | 3160-4554 |
| A14C22 | 0160-4554 | 7 |  | CAPACITOR-FXD -01UF + $20 \%$ SOUDC CER | 28480 | 0160-4554 |
|  | $3160-4554$ $0160-4554$ | 7 |  |  | 28483 28480 | $3160-4554$ 016.6 .4554 |
| A14C25 | 0160-4554 | 7 |  | CAPACITGR-FXD DIUF +-23\% SJUDC CER | 28480 | 3160-4554 |
| A14C26 | 0160-4554 | 7 |  | CAPACITOR-FXD .01UF +-203 SOUDC CER | 28480 | 816. 4554 |
| A14c27 | 0160-4554 | 7 |  | CAPACIIUR-FXD .31uF +-230 S3VDC CER | 28480 | 1160-4554 |
| A1 4C28 A14C29 | $0160-4554$ $3160-4554$ | 7 |  |  | 28480 | $6160-4554$ $0160-4554$ |
| A14C30 | 0160-4554 | 7 |  | CAPACITDR-FXD . CIUF +-202 SOUDC CCR | 23489 | $8160-4554$ |
| A14C31 | 0160-4554 | 7 |  |  | 28483 | 3160-4554 |
| A14C32 | c 160-4554 | 7 |  | CAPACITPP-FXD CIUE + -2\% Sounc cer | 28480 | ${ }_{6}^{6160-4554}$ |
| ${ }_{\text {A } 14.383}$ | 0160-4554 | 7 |  |  | 20483 | 3160-4554 |
| ${ }^{\text {A1 }} 14 \mathrm{Cl34}$ | 0160-4554 | 7 |  | CAPACITRQ-FXD (01UF +-20\% 50UDC CER | 28480 | $0160-4554$ 0160.4554 |
| ${ }_{\text {A1 }}{ }^{\text {A } 14.373}$ | 0160,-45S4 $0160-4554$ | 7 |  | CAPACITOR-「XD .CUUF +-26\% SOUDC CRR | 28480 | $0168-4554$ |
| ${ }_{\text {A } 14 C 3 日 ~}^{\text {a }}$ | 3160-4554 | 7 |  | CAPACUTGR FXD . 314 F ,-23\% SJULC CER | 28483 | 3160-4554 |
| A14C39 A14C40 | $0160-4554$ $0169-4554$ | 7 |  |  | 204800 | 016,64554 $3160-4554$ |
| A14C41 | 0160-4554 | 7 |  | CAPACITOP-FXD .C1UF $-26 \%$ SOUDC CFR | 23480 | $016.0-4554$ |
| A14C42 | 9160-4554 | 7 |  | CAPACITUR-FXD , a1uF --23\% SJVEC CER | 28480 | 0160-4554 |
| A14C43 | 0160-4554 | 7 |  | CAPACITOR-FXD . 61 UF + $26 \%$ SOUDC CLR | 22480 | 014.0 .4554 |
| A14C44 A1 4 CaS | $0160-4554$ $0160-4554$ | 7 |  |  | 28489 23480 | 3160-4554 |
| A14C46 | 0160-4554 | 7 |  | CAPAC,TIGR-FXD . D1uF +-23\% SJU0C CER | 28489 | $3160-4554$ |
| A14C47 | 0160-4554 | 7 |  | CAPACITOR-FXD .01UF +-2c\% SOUDC CER | 28480 | 016.0-4554 |
| A14C48 | 0160-4554 | 7 |  | CAPGEITUR-FXD - DIUF +2J\% SJVde cer | 28480 | 3160-4554 |
| A14C49 | 0160-4554 | 7 |  | CAPACITRR-FXD , O1UF +-26\% SOUDC CER | 28480 | 0160-4554 |
| A14C50 | -160-4554 | 7 |  | CAPACITOR -FXD .CUVF +-2C\% SOUDC CCR | 29480 | 616.0 .4554 |
| A14C52 | 0160-4554 | 7 |  |  | 28480 | 3160-4554 |
| A1 Acs3 | 0160-4554 | 7 |  | CAPACITOR-FXD .C1UF +-20x SOUDC CER | 284ค0 | 016.0-4554 |
| A14C54 | 0160-4554 | 7 |  | CAPACITTR -FXD 01uF +-23X SJULC CER | 23480 | 3160-4554 |
| A14c5s | $0160-4554$ $0168-4554$ | ? |  | CAPACITOR-FXD $01010 \mathrm{~F}+262$ SOUDC CER |  | $0160-4554$ $0160-4554$ |
| ${ }_{\text {A1 }}$ A 1457 | $0160-4554$ | 7 |  | CAPACITOR-FXD .01UF + 20\% SOUDC CER | 28480 | $0160-4554$ |
| A1 $4 C 58$ A 14.59 | 0160-4554 | 7 |  | CAPACITTUR-FXD .01UF - $23 \times$ SJUDC CER | са480 | 3160-4554 |
| ${ }_{\text {A } 14 C 60}$ | $0160-4554$ $0160-4554$ | 7 |  | CAPACITOR-FXD CAPACITUR-FXD S | 23480 c8480 | $6160-4554$ $3160-4554$ |
| ${ }_{\text {A } 14 C 61 ~}^{1}$ | 0160-4554 | 7 |  | CAPACITOR-FXD , 01UF +-20\% SOUDC CER | 28480 | $0160-4554$ |
| A14C62 | 0160-4554 | 7 |  | CAPACITOR-FXD .OIUF +-23x SJUDC CER | 28489 | 3160-4554 |
| A1 AC63 A14C64 | $0160-4554$ $0160-4554$ | 7 |  |  | 28480 28480 | $0160-4554$ $0160-4554$ |
| A1 4 C65 | 0160-4554 | 7 |  | CAPACITTR-FXD.O1UF +202 SODC CER | 28480 | 0160-4554 |
| A14C66 A14C67 | $0160-4554$ $0160-4554$ | 7 |  |  | 28480 28480 | $3160-4554$ $0160-4554$ |
| A14C68 | 0160-4554 | 7 |  | CAPACITOR-FXD .OSUF +-20X SOUDC CER | 28480 | 0160-4554 |
| ${ }^{\text {A1 4C69 }}$ | 0160-4554 | 7 |  | CAPACITIR -FXD 01UF +-20X SQUDC CER | 20480 | 0160-4554 |
| A14C70 A14C71 | $0160-4519$ $0140-0195$ | 4 | 1 | CAPACITOR-FXD 9, 1PF +-.5PF 20JUDC CER | ${ }_{78480}$ | 0160-4519 |
| A14C72 | -0160-4386 | 3 | 1 | CAPACITOR-FXD 33PF +-5 2 200VDC CER $0+-30$ | 28480 | ${ }_{\substack{\text { b }}}^{\substack{\text { dico-4386 }}}$ |

TABLE 8-12. LOG AMPLIFIER ASSEMBLY A14, REPLACEABLE PARTS (2 OF 4)

| Reference Designation | HP Part Number | $\left\lvert\, \begin{aligned} & \mathrm{C} \\ & \mathrm{D} \end{aligned}\right.$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {A } 14 C 73}$ | 316n-3872 | 3 | 1 |  | 28480 | 3160-3872 |
|  | $0160-4554$ $3163-4554$ | 7 |  |  | 2048 C 70889 | 0160 $3160-4554$ |
| A14C76 | 6160-4554 | 7 |  | CAPACTTOS-F×0 C1UF, 26\% SOUDC CLR | 2848 C | 0160-4554 |
| A1AC\%7 | -160-4554 | 7 |  | CAPACTTCR-FAD 31UF +-23\% SJVDC CER | 2¢489 | 0160-4554 |
| A14CR1 | 1910-0016 | ${ }_{0}^{0}$ | 5 | DTODE-CE GOU G6MA 143 DD 7 \% | 28480 | $1916-0016$ |
| ${ }_{\text {A1 }}^{\text {Al }}$ ACR 4 | 1731-6353 | 3 | 5 | DTODE SHITLH3KG 33U 200 MA ins to-35 | ${ }^{28480}$ | 1931-0350 |
| Alacas | 1931-1955 | 6 | 17 |  | 2a480 c 8489 | $1961-0050$ $1931-1385$ |
| A14CR7 | 1701-1485 | 6 |  | dIODE - SM SIG SChottky | 28480 | 1961-1085 |
| A14\%Ra | 1791-1395 | ' |  | DTCEE SM SIG Sthotiky | 29480 | 1731-1385 |
| A1 ACR9 A1CRR1] | $1961-1685$ $1231-1365$ | 6 |  | DIDEE-SM SIG SCHOITKY DTOTE SM SIG Sc: | 28486 | $1761-1085$ $1901-1285$ |
| A1 ACR 11 | 1961-1085 | 6 |  | DIODF-SM SIG schotiky | 28480 | 1961-1085 |
| A19CR 12 | 1921-1979 | 9 | 7 | DIDDE-PIN 1130 | 28483 | 1731-1370 |
| A14CR 13 | 1961-1095 | 6 |  | DIODE-SM SIG Schiotiky | 28480 | 1961-1085 |
| A1 ACR 15 | $1731-1365$ $1901-1070$ | ${ }_{6}^{6}$ |  | DTODE SH SIG, SCliottky DIODE PIN 116 C | 28483 28480 | $1931-1385$ $1961-1070$ |
| A14CR16 | 1731.1273 | ? |  | DITDE PIN IIJU | ${ }_{88480}^{28880}$ | 1731-1970 |
| A14CR 17 | 1901-1085 | 6 |  | dIODE SM SIG SChottky | 28480 | 1501-1085 |
| Alacris | 1701-1085 | ${ }_{6}^{6}$ |  | DTCDE SH SIG SC:OTTKY | 88483 | 1931-1985 |
| A1 ACR 19 A14CR29 | $1901-1078$ $1731-1385$ | 9 |  | DIODE-PIN 116 C DIODE SM SIG SCHOTIKY | 28480 88489 | $1961-1876$ $1731-1785$ |
| A14CR21 | 1901-1085 | 6 |  | DIDDE SM SIG schirtik | 28480 | 1961-1085 |
| A14CR22 | 1931-0040 | 1 | 1 | DTODE SWITCHINS 3JV SJMA ENS DO 35 | - 2480 | 1931-0040 |
| A1 4CR23 A14CR24 | $1901-1085$ $1701-1385$ | 6 |  | DIODE SM SIE, SCHOTTKY | 28486 | 1961-1085 |
| A14CR2S | 1901-1078 | $\stackrel{6}{9}$ |  | DIDOR PIN 116U | 28480 28480 | 1931-1085 |
| A14CR26 | 1701-1085 | 6 |  | DIDDE SH SIG Schatiky | ᄃ8480 | 1731-1985 |
| A14CR27 | 1961-1085 | 6 |  | dIDDE -SM SIG, SCHOtTKY | 28480 | 1961-1085 |
| A14CR2 A14CR29 | $1731-1070$ $1901-1070$ | 9 |  | DIODE -PIN 1130 DTODE-PIN 1100 | 20489 28489 | $1931-1370$ 1961070 |
| A14CR33 | 1991-1335 | 6 |  | DTODE SM SIG $56 . H O T T \mathrm{KY}$ | 28889 <br> 8480 | 1901-1385 |
| ${ }^{\text {A } 14.4831}$ | 1901-0050 | 3 |  | DIODE-SWITCHING BOU 200MA 2NS DO-35 | 28480 | 1901-0050 |
| A14CR32 | 1931-0059 | 3 |  | diade-switchincs asu romea eins do-35 | ce4an | 1931-0050 |
| A14CR33 | 1901-0050 | 3 |  | diode-switching bou zcoma 2ns do-35 | 28480 | 1901-0050 |
| A14E1 | 91700929 | 3 | 1 | CORE Shitlding erad | 28480 | 9170-0.329 |
| A14L1 | 9100-1618 | 1 | 1 |  | 28488 | $9100-1610$ 914000144 |
| Al 1412 Al 412 | $7140-9144$ $9140-0165$ | ${ }_{3}^{2}$ | 1 2 |  | 28480 28480 | $9140-0144$ $9146-0105$ |
| A14L4 | 9100-1619 | 2 | 2 | INLIETOR RF-CH-MLD 6.61 H 13\% | 28480 | $9100-1619$ |
| A14L5 | 9100-1619 | 2 |  | INDUCTOR RT-CH-MLD 6.8UH 103 | 23488 | 9100-1619 |
| A14L6 | 9140-0114 | 4 | 3 |  | 28480 | 9140-0114 |
| A1 4 LT | $9140-0114$ $9140-0114$ | 4 |  | (1) | 28480 28489 | 9140-0114 |
| A14L9 | 9140-0112 | 2 | 1 | INDUCTOR RF-CH-MLD $4.7 \mathrm{UH} 10 \%$ | 28480 | $9146-0112$ |
| A14LIS | 9140-3105 | 3 |  | INDUCTOR RF CH-MID D. 2 HH 13 x | С8480 | 9140-3105 |
| A14L11 | 9100-1627 | 2 | 1 | INDUCTOR RF-CH-MLD 39 UH $52.166 \mathrm{DX}, 385: 6$ | 28480 | $9100-1627$ |
| A14L. 12 | 9100-1629 | 4 | 1 |  | 28480 | $9130-1629$ |
| A1 41213 A14L 14 | $9100-1622$ $9100-2257$ | 7 | 1 | INDUCTOR INDUCT-CH-MLD IN | 28480 c8480 | $9106-1622$ $9100-2257$ |
| A14Q1 | 1854-0637 | 1 | 1 | TRANSISTOR NPN 2N2219A SI TO-5 PD=B0OMA | 01295 | 2N2219A |
| A1402 | 1053-0281 | ? | 3 | TRANSISITR PNP ZN2907A SI TO-18 PD=400MM | 04713 | 2142907 A |
| A1 1483 A1 494 | $1853-0281$ $1053-0015$ | ? | 5 |  | 04713 28480 | 2N2907A $1053-0015$ |
| A1 495 | 1853-0015 | 7 |  |  | 28480 | 1853-0015 |
| A1496 | 1853-0007 | 7 | 12 | TRANSTSTOR PNP 2 N3251 51 TO-18 PD=360M | 04713 | 2N3251 |
| A1488 | 1854-0019 $1853-0815$ | 7 |  | TPANGISTOR NPN SI PO-18 PD=360MW | 28480 88480 | $1854-0019$ $1653-0315$ |
| A1499 | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-18 PD=360MW | 28480 | 1854-0019 |
| A14910 | 1853-0015 | 7 |  | TRANSISTOR PNP SI PD=200KW FT $=500 \mathrm{MHZ}$ | 28480 | 1853-0015 |
| ${ }^{\text {A }} 148111$ | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-10 PD=360ML | 28480 | 1854-0019 |
| A14 1412 A1 4813 A | $1853-0015$ $1854-0019$ | 7 |  |  | 28480 28480 | $1853-0015$ $1854-0019$ |
| A14814 | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-18 PD $=360 \mathrm{MH}$ | 28480 | 1854-0319 |
| A14815 | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-18 PD $=360 \mathrm{MW}$ | 28480 | 1854-0019 |
| A14916 A14017 | $1854-0019$ $1854-0019$ | 3 |  | TRANSTSTOR NPN SI TO-18 PD=360ML | 28480 | 1054-0919 |
| A14017 A14918 | 1854-0019 $1854-0019$ | 3 3 3 |  | TRANSISTOR NPN SI TRANSISTOR NPN SI TO- TO-18 | 28480 28480 | $1854-0019$ $1854-0019$ |
| A14919 | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-18 PD $=360 \mathrm{HL}$ | 28480 | 1854-0019 |
| A14R20 | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-18 PD=360ML | 28480 | 1654-0019 |
| A1 48221 A14022 | $1854-0475$ $1854-0404$ | 5 | $\frac{1}{2}$ |  | 28480 28480 | $1854-0475$ $1854-0404$ |
| A14823 | 1853-0291 | 9 |  | TRANSISTOR PNP 2N2907A SI TO-18 PD $=400 \mathrm{KW}$ | 28488 04713 | 1854-0404 2N2907A |
| A14024 ${ }_{\text {A }}{ }_{\text {A1 }}$ | 1054-0404 | 0 |  | TRANSISTOR NPN SI TO-18 PD=360MM | 28480 | 1854-0404 |
|  | 1854-0019 | 3 |  | TRANSISTOR NPN SI TO-18 PD=360M4 | 28480 | 1854-0019 |

TABLE 8-12. LOG AMPLIFIER ASSEMBLY A14, REPLACEABLE PARTS (30F 4)

| Reference Designation | HP Part Number | $\|c\|$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A14R1 | 0757-6317 | 7 | 1 |  | 24546 | C6. $1 / 8$ - T0-13,1-F |
|  | $3757-3280$ $0698-0884$ | 3 9 | 3 |  | 24546 24546 | CA 1/8-T3-1931-F |
| A1 AR3 A1 1 R 4 | $0698-0684$ $0698-3430$ | $\stackrel{9}{5}$ | 1 | RESTSTOR $21.51 \%$, 12SU F TC $23+\cdots 133$ | 33538 | pritss-1/8 T9 -2185- |
| A1 ARS | 0757-0443 | 0 | 1 | RCSISTOR 11K 12 z , 125W F TCa0+-166 | 24.546 | C4-1/8-te-116? |
| A14R6 | 3757-0442 | 7 | 4 |  | 22546 | C4 1/8-T9-1032-F |
| A14R7 | 0757-1465 | ${ }_{6}^{6}$ | 4 |  | 24546 34546 |  |
| A14R日 A1 4R9 | 3757.0442 $8698-3450$ | ${ }_{9}$ |  |  | 24546 24546 | C4 1/8-T0 4232. F |
| Al4R9 |  | 5 | 2 |  | 1, 3583 | 5153×132 |
| A14R12 | 0757-0453 | 7 | 2 | RESISTOR 51.1 K iz $125 \mathrm{~F} \mathrm{~F} \mathrm{TC}=0,-106$ | 34546 | CA 1/8-TC-5112 ${ }^{\text {c }}$ |
| Al4R13 | $3757-9431$ $0757-0460$ | 3 | 1 |  | 24546 | C4 1/8-T9-6192-F |
| A14R15 | 0757-0456 | 7 |  | RESTST0R 51.1 K 1\% 12 12 SW F TC=01-133 | 24546 | C4-1/8-79 5142-F |
| A14R16 | 0757-0130 | 2 | 1 | RESISTOR 31.6 1\% . 125 SH F TC=04-166 | 23480 | c75\%-0186 |
| Al AR17 | 0757-0464 | 5 | 1 | REEISTGR 73.8X 12.1254 F TC=31-133 | 24546 24546 |  |
| A14R18 A 1 PR19 | $0.698-3136$ $3,757-0123$ | ${ }_{3}^{8}$ | $\stackrel{2}{1}$ |  | 24546 <br> 8480 | C4 4 1/8-re $3757-3123$ |
| A1 AR20 | 0698-0083 | 8 | 2 | RESISTOP 1.86 K 12, 125\% F TC=6,-166 | 34546 | C4 1/8-70-1\%h. F |
| A14R21 | 2130-245? | ? | ? |  | 3.9583 | E153*592 |
| A14R22 | 16698-3453 | 2 | 1 | RESISTOR 196k 12. 1255 F F TC=0t-100 | 245,46 | C4 1/8-70-196.5: |
| Al4R23 | 2103-2514 |  | 1 |  | 33583 | 11534.203 |
| A14R24 | 0757-0274 | 5 | 3 | RLSISTR 1.21 K | $24: 46$ 24546 |  |
| Al 4 R 26 | - $0757-0274$ | 5 |  |  | $245: 46$ | C4-1/8-T0 1211-5 |
| A14R27 | 21302467 | ? |  | RCSESTICR-TRMR SK 13\% C Side adj i-ton | 33983 | ¢753x532 |
| Al 4R28 | 0757-0346 | 2 | 14 |  | 24546 | CA. $1 / \mathrm{A}-\mathrm{TO}$ 16F6-F |
| A14R2? | $3757-0346$ | 2 |  |  | 37546 36933 | C4 1/3-13-10R3.F |
| Al4R30 ${ }_{\text {A1AR31 }}$ | 2100-2522 $3757-3346$ | 1 2 2 | 3 |  | 24546 |  |
| A14R32 | 0757-6346 | 2 |  | RESISTOR $16.1 \%$, 12SW F TC= C1-100 | 24546 | CA 1/8-T0-10pC.F |
| A14R33 | 2100-2522 | 1 |  | RESTSTGR-TRMR 19 K 13\% C SIDE-ADJ $1-T 2 \mathrm{~N}$ | 33783 <br> 30973 |  |
| A14R34 A1 1 P35 | $2100-2521$ $3757-0346$ | $\stackrel{1}{2}$ | 1 |  | 30933 3.456 | C4-1/8-10-108. F |
|  | 0.757-0346 | $\frac{2}{2}$ |  | RESISTOP 10 12. 125 S F $\mathrm{TC}=6+-100$ | 24546 | C4 1/8-TC 16FG-F |
| A14R37 | 3757-0442 | 9 |  | RESTSTOR $13 \mathrm{~K} 1 \%$ 12SU F TC=3t-133 | 23546 | C4 1/8-T0-1092. 5 |
| A14R38 | 0696-3151 | 7 | 1 |  | 245.46 <br> 3.983 <br> 185 |  |
| A14239 A1 AR40 | 2100-2520 | 9 | 1 | RESISTOR 10k $1 \% .125 \omega^{\text {r }}$ K TC $=0+-1 \mathrm{CG}$ | 245.46 | C4.1/8-T0-1002F |
| A1 ARA1 | 1757-3290 | 5 | 1 | REGTSTITR 6.15 K 1K , 12SW F TC $=0+100$ | 19731 |  |
| A14R42 | 0757-6200 | 7 | 1 |  | 24546 24546 | $\begin{array}{cc}C 4 & 1 / 8-T 0-56.21-F \\ C 4 & 1 / 8-73-1622-5\end{array}$ |
| A14R43 A1 14844 | $3757-0447$ $0757-0420$ | ${ }_{3}^{4}$ | 3 2 |  | 24546 24546 | C4 1/8-70-751-r |
| A1 AR 45 | 0698-3444 | 1 | 8 | aestisior 316 ix 12SU F IC=at-109 | 24546 | C4-1/8-T3-316R-F |
| A14R46 | 0698-3156 | 2 | 1 | RESISTOR $14.7 \mathrm{k} 1 \mathrm{~L}, 125 \mathrm{FF}$ TC=0+106 | 245.46 | C4 1/8-TE 1472-F |
| A14R47 | 9757-0346 | 2 |  |  | 24546 | C4 1/8-T0-10R3-F |
| A14R48 A1AR49 | $0.698-3150$ $3698-3132$ | 6 | $\stackrel{4}{1}$ |  | 24546 24546 |  |
| A14R50 | 0757-0279 | 0 | 4 | RESISTOP 3.16k $1 \mathrm{x}, 125 \mathrm{~F}$ Y $\mathrm{TC}=0.100$ | 24546 | C4 1/8-T0-31/1-F |
| A14R51 | 9757-0346 | 2 |  | RESISTRR $131 \%$. 225 W F $1 \mathrm{C}=0+-100$ | 24596 | C4-1/8-T0-10R3-F |
| A14RS2 | 0698-3444 | 1 |  |  | 24546 24546 |  |
| Al4R53 A1 AR54 | - $\begin{aligned} & \text { 9757-0444 } \\ & 0757-0444\end{aligned}$ | 1 | 6 |  | 24546 | C.4-1/8-TE-1212-F |
| A14R55 | 1757-3443 | ? | 3 |  | 24546 | C4-1/8-T0-7531-F |
| A1 4R5 6 | c757-0401 | 0 |  | RESISTOP 10.018 .125 W F TC=0+-100 | 24546 | C4-1/8-TR-161-F |
| A14RS5 | 0757-0280 | 3 |  |  | 24546 24546 | C4-1/8-T9-1391-F |
| A14R58 A14R59 | $8757-0346$ $0698-3150$ | 2 |  |  | 24546 24546 | C4-1/8-T3-2371-F |
| ${ }_{\text {AI ARGO }}$ | 06990-3444 |  |  |  | 24546 | C4 1/8-TC-31/R-F |
| A14R61 | 0757-8280 | 3 |  | RESISTOR $1 \mathrm{~K} 1 \%$, 12SW F TC=0t-100 | 24546 | C4-1/8-T0-1931-F |
| A14862 | 0757-0444 | 1 |  |  | 24546 24546 |  |
| Al4R63 A1 1 R 64 | $0757-0444$ $0757-0440$ | 7 |  |  | 24546 24546 | C4-18-T0-1212-F |
| A14R65 | 1757-0431 | ${ }^{3}$ |  | RESTSTOR $1001 \mathrm{X}, 1254$ F TC=0 +103 | 24546 | C4 1/8-T0-131-F |
| A14R66 | 0757-0280 | 3 |  | RESISTRR ik iz , 125W F TC $=0+-100$ | 24546 | C4-1/8-T0-1661-F |
| A14R67 A1 1 R 68 | $0757-0346$ $0698-8958$ | 2 |  |  | 24546 <br> 28480 | $\begin{aligned} & \text { C4-1/8-T0-10R3-F } \\ & 0693-8953 \end{aligned}$ |
| A14R69 | 2100-2692 | 6 | 1 | RESISTOR-TRMR in $20 X C$ SIDE-ADJ 1 -TRN | 33983 | ET50x105 |
| A1 4R70 | 06,98-3444 | 1 |  | RESISTOR 316 1 X , 125 W F TC=0+-100 | 24546 24546 | C4-1/8-T0-316P-F |
| A14R71 | 0757-0279 | , |  | RESISTOR 3.16k 1 X . 125 SW F $\mathrm{TC}=0+-100$ | 24546 | C4-188-70-3161-F |
| A1 14872 A14R73 A1 | $0757-0444$ $0755-0444$ | 1 |  |  | 24546 24546 24546 | C4-1/8-T0-1212-F $\mathrm{C4-1/8-T9-1212-F}$ C |
| A14R74 | 0757-0440 | ? |  | RESISTOR 7.5X $12 \mathrm{X}, 1254$ F TC $=0+1100$ | 24546 | C4-1/8-T0-7501-F |
| Al $14 R 75$ A1 AR76 | 0757-0401 $0757-0280$ | ${ }^{0}$ |  |  | 24546 24546 | C. $4-1 / 8-\mathrm{TO-101-F}$ $\mathrm{C} 4-1 / 8-\mathrm{TO}-1001-\mathrm{F}$ |

TABLE 8-12. LOG AMPLIFIER ASSEMBLYA14, REPLACEABLEPARTS(4OF 4)

| Reference Designation | HP Part Number | C | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {A } 14877}$ | ${ }^{0} 78570346$ | 3 |  |  | 245:46 | C4-1/8-TG- 16.pr-F |
| (1)1R79 ${ }_{\text {A1 ARED }}$ | 365818444 $0757-8209$ | $\stackrel{1}{2}$ | 6 |  | 24546 19761 | C4-1/8-TJ-316R-F M-4C1/8-TP-1320 |
| Al 1801 | 3757.9:39 | 2 | 6 |  | 19731 | MFAC1;a-T9-1332-F |
| A1 4RAC | 1757-0446 | 7 |  | RESISTOR 7.5\% $1 \%$, 125w F TC=0+-160 | 24546 | C.4-1/8- Tf -7501-F |
| $\mathrm{Alaras}^{\text {a }}$ |  | 3 |  |  | 24546 | C4 1/8-T0-131 F |
| $\mathrm{Al}^{14884}$ | 8757-02.80 | 3 |  |  | 24546 34.46 | C4. 1/8-T0-160, |
| ${ }_{\text {Al }}$ ARB6 | 2157-3279 | 3 |  |  | 24546 | C4-1/8-13-3161- |
| ${ }_{\text {at ARG7 }}$ | 36503414 | 1 |  | RESTSTHR 316 1\% , 12:54 F ir $=3+-133$ | 24546 | C4-1/8-T3-31/R- ${ }^{\text {F }}$ |
| A 1 4RB6 | 2100-252e | 1 |  |  | 36933 | E158×103 |
|  | $0757-9449$ $0757-0463$ | $?$ |  |  | 39546 | C4 1/8-T0-7591-F |
|  | 0757-01633 $3757-3: 59$ | 3 | $?$ |  | 24546 19731 |  |
| A 1 AR92 | 8:757-02:89 | 2 |  |  | 17701 | ¢F AC1/8-T0-1332-F |
| n1 1R23* | 3650.31:3 | $?$ | : |  | 24546 | C4-1/8-T0-3831-F |
|  | $06.98-3156$ 3757 0.346 | ? |  |  | 24546 23546 |  |
| A1 4R96 | 86.98-3444 | 1 |  | PESISTR 316 12 , 125w F TC=0t-160 | 24546 | C4-1/8-Te-3168-F |
| A14897 | コサ5.7-3:69 | 2 |  |  | 17731 | MF4C1/8-T0-1332-F |
| A $14 \mathrm{R99}$ | 6757-0289 | $\stackrel{2}{7}$ |  |  | 19761 24546 | MFACL/8 TE-1332-F |
| - ${ }_{\text {A1 } 148 \mathrm{R} 100}$ | cols | 2 |  |  | 24546 24.946 |  |
| A14R131* | 0698-3153 | \% |  | arcistur 3.gas 18.1254 \% $16=3$ - 103 | 24546 | C4 1/8-70-3831.F |
| Al ARion | 0\%57-0344 | 2 |  | RTSISTOR 10 12 .1254 F TC=64-100 | 24546 | C4 1/8-T0-10FE-F |
|  | 3757-9431 | 3 |  |  | 24546 | C4-1/B-T0-191 F |
| A14R104 ATAR105 | $0757-046.1$ 36.884844 | 0 |  |  | 24546 24546 |  |
| A14R106 | 0757-0417 | 8 | , |  | 24546 | C4 1/8-T0-5 $6.2 \mathrm{Pr-F}$ |
| A1AR107* | 0757-179 | 3 | 1 |  | 24546 | C4 1/8-T0-2152 F |
| A 14R108 | c6,98-34.34 | \% | 1 | RESIGTAP 34.0 12.1254 F TC=0+106 | 24546 | $\mathrm{CA}_{4} 1 / 8 \mathrm{~B}$ - T0-34P8-F |
|  | $0757-0439$ $0757-0418$ | ? | $\frac{1}{2}$ |  | 24546 24546 | C4 1/8-T3-93R - C. $41 / 8-\mathrm{TO}-6192-\mathrm{F}$ |
| A14R111 | $3690 \cdot 344.3$ | 7 | 1 |  | 24546 | C4-1/3-T3-19CR-F |
| A14R112 | 8757-0286 | 3 |  | RESSETOR 1K 1\% .125w F TC=0 - 100 | 24546 | C4 1/8-T0-1001-F |
| Al 4 R 113 | a757 - а280 | 3 |  | RESTSTOR 1K $1 \%$, 1254 F TC $=0,133$ | 24546 | C4.1/8-T0-1001-F |
|  | $6698-3136$ 0757 0.593 | ${ }_{9}^{8}$ |  |  | 24546 24546 | C4-1/8-TE-1782-F CA 1/8-T0-131 |
| A 14 R 116 | c698-315s | 1 | 1 |  | 24546 | C4-1/8-T0-4641-F |
| AlAR116 | 175570418 | 9 |  | RESTSTGR 619 18 . 125 SW F $1 \mathrm{C}=0$ ¢ - 120 | 24546 | C4-1/3-T0-619R-F |
| A14R117 Al 14 R 11 B | 8757-0440 | 7 |  |  | 24546 24546 | C4-1/9-T0-7501-F |
| A14R119 | ${ }^{10698-3438}$ | 3 | 1 | RESTGTOR $1471 \% \quad 1254 \mathrm{~F}$ TC=0+-106 | 245.46 24546 | C4-1/8-T0-2611-F C4-1/8-T0 1 17P-F |
| Alariza | 9757.0439 | 4 | 1 |  | 24546 | $\mathrm{C} 4-1 / 8-\mathrm{T0} 0$-6811-F |
| A14R121 | 2100-2b33 | 5 |  | RESISTOR-TPMR 1 K 10 XC C SIdF-ADJ 1-TRN | 30983 | ETS0×102 |
| Al4R122 | 07570420 | 3 |  | RESTSITRR 750 1X 125 W F $\mathrm{TC}=00-130$ | 24546 | C4-1/8-T0-751 F |
| A14R123 A1 14124 | $0757-0440$ $0757-0447$ | 7 |  |  | 24546 24546 | C4-1/8-T0-7501-F C4-1/8-T0-1622-F |
| A14R125 | 0757-0447 | 4 |  | RESISTO $16.2 \mathrm{~K} 1 \mathrm{iz}, 1254 \mathrm{~F}^{\text {F }}$ T $=0+-16 \mathrm{C}$ | 24546 | C4 1/8-T0 If?? ${ }^{\text {c }}$ |
| A1AR126 | 3757-0465 | $b$ |  | Restition $103 \mathrm{~K} 1 \mathrm{X}, 125 \mathrm{~W}$ F $1 \mathrm{C}=0+-100$ | 24546 | C4 1/8 TO-1033 F |
| A14R127 | 0757-0465 | 6 |  | RESISTOR 100k 1 X . 125 SW F TC=0+100 | 24546 | C4-1/8-T0-103-F |
| A14R128 A 14 R 129 | $0757-0465$ $0699-0083$ |  |  |  | 24546 | C4 1/8-T0-1003-F |
| A14R129 A1 1413130 | $069 \mathrm{e}-0083$ $0757-0279$ | ${ }_{0}$ |  |  | 24546 24546 |  |
| A14R131 | 0757-0402 | 1 | 1 | RESISTOR 11018.125 FF TC $=0+\cdots 100$ | 24546 | C4-1/8-T0-111-F |
| A14R132 | 9757-0430 | 3 | ${ }_{2}^{1}$ | REEISTGR S. 11 K 1\% 12 LSW F TC=0,-100 | 24546 | C4 1/8-T0-5111-F |
| Al 148133 Al 14 R 134 | $6698-7212$ $0698-7<12$ | 9 |  |  | 24546 24546 | C3- $3 / 8-\mathrm{TO-100R-F}$ $\mathrm{C3-1/8}-\mathrm{TO-103R-F}$ |
| A14R785 | 0690-3150 | 6 |  | RFSIGTOR $2.37 \mathrm{~K} 1 \% .125 \mathrm{~F}$ F TC=0+-100 | 24546 | C4-1/8-T0-2371-F |
| A14TP1 A14TP2 | $0360-0535$ $0360-0535$ | 0 | 19 | TERMINGL TEST POINT PCE | 28880 | 0360.0535 0360535 |
| A14TP2 | $0360-0535$ $0360-0535$ | 0 |  | TFRMINAL TEST POINT PCB | 28480 28480 | 0360.0535 $0360-0535$ |
| A14TP4 | 0360-0535 | 0 |  | TERMINAL TEST POINT PCU | 28480 | 0360.0535 |
| A14TPS | 0360-0535 | 0 |  | terminal test point pch | 28480 | 0360-0535 |
| A14TP6 | 0360-0535 | 0 |  | TERMINAL TESS POINT PCR | 28480 | 0360.0535 |
| A14TP7 A14TP | $0360-0535$ $0360-0535$ | 0 |  | TERMSNAL TEST POINT PCB | 28480 28880 | 0360.0535 0360.0535 |
| A14TP9 | 0360-0535 | 0 |  | TERMINAL TEST PO NT PCE | ${ }_{28480}^{2880}$ | 0360.0535 |
| A14TP 10 | 0360-0535 | 0 |  | tFRminal test point pcb | 28480 | 0360.0535 |
| $\begin{aligned} & A 14 U 1 \\ & A_{1} 14 \mathrm{UL} \end{aligned}$ | $\begin{aligned} & 1026-0092 \\ & 1826-0092 \end{aligned}$ | 3 | 2 | IC CIP AMP GP DLAL TO 99 PKG IC OP AMP GF DUAL TO 99 PKG | $\begin{aligned} & 28480 \\ & 28486 \end{aligned}$ | $\begin{aligned} & 1826-0092 \\ & 1826-0092 \end{aligned}$ |
| A14UR1 | 1902-0901 | 5 | 1 | DIODE ZNR 5.4V 1\% DO-35 PD=.4W TC=*.046\% | 28480 | 1702-0901 |
|  | 08559-00027 | 7 | 1 | A 14 misceilanedus Parts COVER, LOG AMPLIFIER | 28480 | 08559-00027 |



FIGURE8-67. LOG AMPLIFIER ASSEMBLY A14, BLOCK DIAGRAM

LOG AMPLIFIER ASSEMBLY


FIGURE8-68. LOG AMPLIFIER ASSEMBLYA14, COMPONENTLOCATIONS



## VERTICAL DRIVING/BLANKING ASSEMBLY A15, CIRCUIT DESCRIPTION

The Vertical Driving/Blanking Assembly A15 contains a preamplifier to amplify the detected and filtered video received from the Log Amplifier Assembly A14. It also supplies the video signal needed to trigger the sweep generator in the video trigger mode. Following the preamplifier is the vertical driver, a differential amplifier that drives the vertical deflection plates in push-pull. Blanking, penlift, retrace, and sweep indicator signals are also supplied by the Vertical Driving/Blanking Assembly A15.

## Preamplifier (A)

The detected and filtered video ( 0 to 800 mV ) from the Log Amplifier Assembly A14 is applied to the gate of Q17a. Transistors Q17 (both sections), Q11, Q12, and Q18 form an FET input differential amplifier; the gate of Q17a is the noninverting input and the gate of Q17b is the inverting input. The amplifier's output, at the emitter of Q18, is fed back to the inverting input (Q17b) through a voltage divider (R11, R12, and R13). A simplified preamplifier circuit diagram is shown in Figure 8-70. The voltage gain can be expressed as a function of these resistor values: Gain $=1+\mathrm{R} 11 / \mathrm{R} 12+\mathrm{R} 13$. The circuit's gain is 10 . Since the limit to the input voltage is 800 mV , the maximum voltage at the output of Q18 (TP3) is 8 V . This voltage is coupled through R17 and becomes the trigger voltage for the video trigger mode (VIDEO position). Transistor array section U2d and transistor Q13 are temperature-compensated current sources. These bias the differential amplifier (U2a, U2b, and Q20) that provides isolation between the preamplifier and the vertical driver. The preamplifier output is sent via R40 to the rear panel (AUX VERT OUTPUT, P1 pin 14).


FIGURE 8-70. PREAMPLIFIER CIRCUIT, SIMPLIFIED SCHEMATIC

Since the vertical driver deflection sensitivity is 800 mV , for full-scale deflection, a divide-by-ten circuit and an offset circuit are used to obtain the correct signal amplitude. With the LOG/LIN switch (A2A1A2) in either the 10 dB per division or linear position, +15 V is applied to the EXPAND line. This reverse biases CR1 and turns Q19 on, dividing the preamplifier's output by 10 . Diode CR2 is forward biased and diode CR3 is reverse biased. Transistor Q19, R18, and R20 form the output divider network. When 1 dB per division is selected, the EXPAND line is open and Q19 is biased off by CR1 and R22, disabling the divide-by-ten circuit. The full preamplifier voltage is now available at the output of Q18 and must be offset $\mathbf{+ 7 . 2 \mathrm { V } \text { to display the } 8 0 0 \mathrm { mV }}$ signal peak. This in effect expands the display.

The offset of the signal is accomplished by a circuit comprised of U2c, CR3, CR4, and R18. Transistor array section U2c forms an adjustable current source that draws current through CR3 and R18. The 1 dB offset control is used to set the voltage drop across R18 at +7.2 V . This voltage shifts the signal negatively as it passes through R18. Diode CR4, becomes forward biased as the offset signal goes below -0.6 V and acts to clamp the minimum output at that level.

## Beamfinder

With 1 dB per division selected, the baseline is off-screen. Without a visible signal present, there is no displayed trace. This condition could be misinterpreted as a display malfunction. On an HP 180 series mainframe, a visible trace can be produced by pressing the BEAMFINDER switch on the mainframe. This causes the -12.6 V on the beamfinder line to be removed, turns Q19 off, and disables the current source, U2c. The vertical display then reverts to the 10 dB per division mode while the horizontal display sweep is narrowed and the trace is intensified by the mainframe. The HP 853A mainframe does not require a BEAMFINDER, therefore the mainframe always supplies -12.6 V to the beamfinder line.

## - 5.5V Temperature CompensatingSupply (B)

The - 5.5V Temperature Compensating Supply controls four current sources: U2c, U2d, Q13, and Q15. The temperature sensing element, U 2 e , is connected as a diode and tracks the base-emitter temperature changes of the current-source transistors. Approximately -0.6 V is provided by the voltage regulator (zener) diode, VR1, and transistor U2e.

## Vertical Driver (E)

The Vertical Driver is a differential amplifier that consists of Q2, Q3, Q6, Q7, and Q14. Transistor Q15 is a temperature compensating current source (see Figure 8-71). The vertical signal from the preamplifier (0 to 800 mV ) is converted to the push-pull signal needed to drive the vertical deflection plates. Dual transistor Q14 is used as the input stage of the driver circuit. Its base voltage is adjusted from the front panel with the vertical position (VERT POSN) control A2A1R6. This establishes the input reference voltage.


FIGURE 8-71. VERTICALDRIVER. SIMPLIFIED SCHEMATIC

The gain of the vertical driver is set by a voltage divider consisting of R39, R42, and vertical gain control (VERT GAIN) A2A1R7. This gain control adjusts the ratio of the voltage divider. Transistor pairs Q2/Q6 and Q3/Q7 are current-to-voltage amplifiers driven by the current from the collectors of Q14a and Q14b, respectively. Diodes CR5 through CR8 prevent the bases of Q2, Q3, Q6, and Q7 from being driven negative more than 0.6 V . Resistors R44 and R52 decouple the capacitive load presented by the CRT plates from the emitter of Q2 and Q3. Decoupling is necessary to prevent overshoot and ringing in the Vertical Driver.

## Sweep Ramp High/Low Limit Comparator <br> (C)

Operational amplifiers Ula and Ulb are connected to form a comparator circuit. A voltage divider, comprising resistors R6, R7, and R8, establishes a high voltage reference at Ula pin 2 and a low voltage reference at Ulb pin 5. The switching limits are approximately +5 V and +0.7 V , respectively. The signal applied to other inputs of the comparator is the YIG tuning voltage, the same signal that drives the YIG main coil. It consists of the analog tuning voltage and the sweep ramp $(\mathrm{S}+\mathrm{T})$. The tuning voltage is proportional to the instantaneous frequency to which the analyzer is tuned; the ramp sweeps from +1.2 V to 4.8 V .
As the YIG tuning voltage at Ula pin 3 rises above the reference at Ula pin $2(+4.95 \mathrm{~V})$, the output of Ula rises to about +14 V . This turns on Q4 in the blanking driver and blanks the display. If the YIG tuning voltage goes below the lower reference limit $(+0.7 \mathrm{~V})$, the output of Ulb goes to about +14 V and again blanks the display. The upper and lower blanking limits correspond to 50 MHz below and 100 MHz above the ends of each band being swept.

## Vertical/Baseline Comparator (D)

The Vertical/Baseline Comparator consists of Q16 and Q8. The baseline clipping reference voltage is set by the BL CLIP control A2A1R2, which varies the base voltage of Q16. The Vertical Preamplifier output signal is applied to the base of Q8 and compared to the dc reference voltage at the base of Q16. If the signal becomes more negative than the reference, Q8 turns on. This turns Q4 on and blanks the display.

## Blanking Driver ( $\mathbf{F}$

The Blanking Driver comprises transistors Q4 and Q9 (see Figure 8-72). Normally, Q4 is off, placing a low level at the base of Q9 and causing Q9 to be turned on. For Q9 to be turned off and provide a positive going blanking


FIGURE8-72. BLANKING CIRCUIT, SIMPLIFIED SCHEMATIC
output to the mainframe, Q4 must receive a positive voltage. The Blanking Driver is driven by the Vertical/ Baseline Comparator and the Sweep Ramp High/Low Limit Comparator. Either of these circuits can produce the positive input needed by the Blanking Driver to produce a blanking output.

## Penlift Driver (G)

The display is blanked during retrace and during the dead time of the sweep ramp. Retrace blanking from the Sweep Generator/Bandwidth Control Assembly A9 is applied to the emitter of the buffer amplifier Q1. When the sweep ramp is turned off (dead time), the retrace blanking signal rises to +10 V . This voltage appears at the base of Q4, blanking the display. Simultaneously, the +10 V signal is applied to base of Q5, causing the collector of Q10 to rise to +15 Y Transistor Q10 provides the signal used to lift the pen of the $\mathbf{X}-\mathbf{Y}$ recorder during the analyzer's sweep retrace and dead time. Zener diodes VR2 and VR3 limit the output to 35V to protect Q10 from high voltage and inductive transits generated by the $\mathrm{X}-\mathrm{Y}$ recorder.

## Sweep Indicator Driver (H)

The front panel SWEEP indicator lights when the retrace blanking signal is low (OV). Transistor Q22 is turned on by the low retrace signal and switches on the SWEEP light-emitting diode.

## VERTICAL DRIVER/BLANKING ASSEMBLY A15, TROUBLESHOOTING

Display Held in Blanked Mode: When this occurs, it may be necessary to increase the display intensity (on HP 180 series mainframes) to make the trace visible. A bright dot appears at the beginning of the trace and the BL CLIP control does not work. Most common failures are Q8 and Q16 (always change both).

The S + T line from the Frequency Control Assembly A7 can cause the comparators (block C) to latch-up.
The Sweep Generator/Bandwidth Assembly A9 retrace line input line can lock-up retrace.
Display Offset in Linear: Most common failure is Q17.

TABLE 8－13．VERTICALDRIVER／BLANKING ASSEMBLY A15，REPLACEABLE PARTS（10F2）

| Reference Designation | HP Part <br> Number | $\begin{aligned} & \text { C } \\ & \text { D } \end{aligned}$ | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A15 | 36559 －630：9 | 5 | 1 | W：RTICAL DRIUER／RLANKING ASSEMDIY | 28983 | 385：39－60359 |
| A1SC1 | c180－0197 | 8 | 4 | CAPACSTOR－FXD 2．24\％＋－16\％2CUDC TA | 56：39 | 156T2asx70：6A： |
| A15CC | 3183－3197 | E |  | CAPAEITKR－XD 2．SUF－ 13 Z ZOULC TA | 56857 | 15172\％ $5 \times 9029 \mathrm{Aa}$ |
| A15c3 | 0186－0197 | 8 |  | CAPACITOR－FXD 2 ． 2 UF $+10 \%$ 2CUDC TA | şang cavai |  |
| A1SCA A1 SCS | $0160-2355$ $0160-0197$ | － | ？ |  | 58283 | 3163 2355 $1501225 \times 9$ 2．arat |
| A15C6 | 2160－2355 | $\%$ |  |  | こв4日 | 3163－2355 |
| A1SCR 1 A1ECR2 | 1901－6050 | 3 | 11 |  | 23488 $=8483$ | $\begin{aligned} & 120,1-6059 \\ & 1031-0350 \end{aligned}$ |
| A1SCR2 A1SCR3 | $1901-0350$ $1901-6050$ | $\frac{3}{3}$ |  |  | 29483 | $\begin{aligned} & 1031-0350 \\ & 1261-0050 \end{aligned}$ |
| A15CR4 | 1731－0535 | 5 | 1 | DTEDE SM SIG Sthotiky | 281830 | $1931-3535$ |
| A15CRS | 1701－8050 | 3 |  | DIOLE－SWITCHINE 000260 MA 2N：DO－35 | 28400 | 17610050 |
| A1ECRG | 1731－3053 | 3 |  | DTCDE ：WITCMING BJU 2a3ke ：WS Do 35 | －848） | 1291－3056 |
| A1SCR7 | 1961－6050 | 3 |  | DIODE SLITCHING BCU RECMA 2N：DA－35 | 28480 | 1901－0050 |
| A1SCRA | 19310050 | 3 |  | DTCOE SWITH，H1NG asu zaara ins eo 35 | （1380 | 1931－3950 |
| A15CR9 A15CR1？ | $1701-0650$ 1731.0050 | 3 <br> 3 |  |  | 28480 $\% 3480$ | $\begin{aligned} & 1701-0858 \\ & 1931-0350 \end{aligned}$ |
| A1 SCR 11 | 1961－0050 | 3 |  | DTODF－SUTTCHTNG BLU 26 EMA 2 N：DO－35 | 2：480 | 1761－0050 |
| A1SCR 12 | 1701． 3518 | E | 1 | DIDDE SM SIG SR 1017 KY | －8483 | 1931－0518 |
| A1SCR 13 | 1961－6058 | 3 |  | DTODE－SUITCHING：8LU 2CRMA $2 N: ~ D O-35 ~$ | ？${ }^{\text {ancon }}$ | 1761－0050 |
| A15CR14 | 1710－0316 | a | 1 | DICDE－EE bJU G3ria lis co 7 | 2898 | 1913－0316 |
| A $15 \mathrm{J1}$ | 1251－0660 | 0 | 12 |  | 2a480 | $1251-6600$ $1: 51-2630$ |
| A15J2 A15J3 | $1251-0690$ $1251-0660$ | 0 |  |  | － 2483 | $1: 51-56.30$ $12.51-0600$ |
| A15J4 | 1251－0633 | 3 |  | CONNFETIIR SEL RCONT PIN 1．14 M．M FSCC S\％SQ | 2e483 | 1：51－06．90 |
| A1sJs | 1251－0650 | 0 |  |  | 28480 | 1251－0666 |
| A15J6 | 1251－0603 | 0 |  | CONNECTUR－SGL CONT PIN 1.14 －mmercesz SQ | \％ 8983 | 1：51－0630 |
| A1537 | 1251－0660 | 0 |  | CONNECTOR SGL CONT PIN 1.14 MM－ESC－ 37 SR | 2．480 | 13．4－0660 |
| A1SL1 | 9140－0179 | 1 | $?$ |  | 284811 | 9140－3179 |
| A15L2 | 9140－0179 | 1 |  | INDUCTOP NF －CH－MLD 23UH $16 \%$ ，1665X，38\％LS | 23400 | 7146． 0179 |
| A1501 | 155，3－0037 | $\cdots$ | 4 |  | 34713 | $2 * 3: 51$ |
| A15Q2 A15 | $1854-0234$ $1854-3234$ | 4 4 | 4 |  | 3！ 595 | PN3440 2n 3443 |
| A15Q4 | 1854－0009 | 1 | 1 |  | 64713 | Pa\％c9 |
| A15Q5 | 1354．0404 | 3 | 1 |  | ？ 5463 | 1554－0404 |
| A1586 | 1054－0．034 | 4 |  | TRANSTSTOR NPN 2 M3440 SI TO－5 PD， 1 L | 31505 | 2N3440 |
| A1507 | 15554－0234 | 4 |  | TRANEISTOR NPN ENS449 ST $10-5 \mathrm{PD}=1 \mathrm{~W}$ | 31585 | 2N3440 |
| A1598 | 1853－0007 | 7 |  |  | 64713 | 2 N 3.51 |
| A1509 | 1554． 0319 | 3 | 1 | TRANGTGTRR URN SI Th－13 FD－3Gamid | 2e483 | 1654－0319 |
| A15810 | 1954－0039 | 7 | 1 | TRANGTSTOR NIN $2 N 30535$ St 10．39 PD iw | 31.595 | 2436535 |
| A15R12 | 1353 －0451 | 5 | $?$ | TRANSISTGR PNP ：N3799 SI 10.18 PDVIG，3ML | $31: 75$ | 2N3799 |
| A15Q12 A1SQ13 | $1853-0451$ $1854-0882$ | 5 | 4 |  | 01295 28480 | 2N． 3799 $1854-9882$ |
| A15Q14 | 1854－0475 | 5 | 1 | TRANSISTOP－DUAL NPN PD $=750 \mathrm{MW}$ | 28480 | 1054－0475 |
| A15Q15 | 1554－0682 | 8 |  | TRANSISTGR NPN PD＝303MW FT＝200M．HZ | 20480 | 1854－0ER2 |
| A15Q16 | 1853－0007 | 7 |  | TRANGTSTAR PNP 2N32S1 SI 10.18 PD＝36，0ML | 04713 | 2Nx25： |
| A15Q17 A15Q18 | $1855-0047$ $1854-0882$ | 1 8 | 1 |  | 28480 28480 | $1655-0049$ 1054 10851 |
| A15Q19 | 1055－0417 | 7 | 1 | IRANSISTGR J FET N CHAN D．WODE TO－111 OI | －8483 | 11．55－0417 |
| A15820 | 1854－0082 | E |  | TRANSISTOP NPN PD $=300 \mathrm{ML}$ F $\mathrm{T}=200 \mathrm{MHZ}$ | 28480 | 105．4－0802 |
| A15821 | 1555－0020 | ${ }^{8}$ | 1 | TRANGSSTGR J－FET N－CLIAN D－MGDE TO－18 SI | 28483 | 1055－0320 |
| A 15922 | 1953－0007 | 7 |  | TRANSISTOR PNP 2N32S：SI $10-18$ PD＝36GMU | 04713 | 2N3251 |
| A15R1 | 2100－3123 | g | 6 | RESISTER－TRMR $53010 \% \mathrm{C}$ SIDF－ADJ 17 IRN | 22111 | $43 P 501$ |
| A15R2 | 0757－0199 | 3 | 6 | RESISIOR $21.5 \times 1 \%$ ，125以 T TC＝0， 180 | 24546 | C4－1／8－T0 $2153-\mathrm{F}$ <br> $\mathrm{CA}-1 / 8-\mathrm{TO}$ <br> $51-\mathrm{F}$ |
| A15R3 A1584 | －3757－0420 | 3 3 | ${ }_{3}^{2}$ | RESISTGR RESISTOS R R R R | 24546 24546 | C． 4 1／8－T0－751－ C4 1／8－T0－1001－F |
| A15R5 | 0757－0279 | $\square$ | 3 |  | 24546 | C4－1／3－T0－3161－F |
| A15R6 | 0690－3155 | a | 4 | RESISTOR $14.7 \mathrm{~K} \quad 1 \%$ ． 125 S F $\mathrm{TC}=0+100$ | 24546 | C4－1／8－T0－1472－F |
| A15R7 | 1757－0290 | 5 | ， | RESTSTCR $6.19 \mathrm{~K} 1 \%$ ，12SW F IC $=3,-133$ | 17731 | MFAC1／B－T0－6191－F |
| A15R8 | 0757－0424 | 7 | 3 | RESISTOR $1.1 \mathrm{~K} 1 \mathrm{z}, 1254 \mathrm{~F}$ TC＝0＋－106 | 24546 | C4 $1 / 8$ TE－1181－F |
| A15R9 | 0690－3156 | $z$ |  | RESTSITIR 14， $7 \mathrm{~K} 1 \%, 125 \mathrm{~L}$ F TC $=0+100$ | 24546 | C． $1 / 8$－ $1 / 8$－1472－F |
| A15R10 | 0757－0199 | 3 |  | RESISTOR 21，5K 1x ，1254 F TC＝0＋ 100 | 24546 | 6．4－1／8－TE－2152－F |
| A15R11 | 0698－3155 | 1 | 3 | RESTSTOR $4.64 \mathrm{~K} \quad 1 \mathrm{X}, 1254$ F TS $=0+-103$ | 24546 | C4．1／8－70－4641－F |
| A15R12 | 0757－0416 | 7 | 3 | RESISTOR $5111 \%$ ． 125 W F TC $=0+100$ | 24546 | C4 1／8－TC－511R－F |
| A15R13 | 0683－0475 | 1 | ， | RESISTIR 4.752 ． 254 FC TC＝ $400 / 1500$ | 31121 | CE4765 |
| A15R14 | 0757－0424 | 7 |  | RESISTOR $1.1 \mathrm{~K} 1 \%, 125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4－1／8－TC 1101－F |
| A15R15 | 3757－0199 | 3 |  | RESTSTOR 21． 5 K 1\％，125W F TC＝34－100 | 24546 | C4－1／8－79－2152－F |
| A15R16 A15R 17 | $\begin{aligned} & 0757-0199 \\ & 0757-0280 \end{aligned}$ | 3 3 |  |  | 24546 24546 | $\begin{aligned} & \mathrm{C} 41 / 8-T 0-2152-F \\ & \mathrm{C} 4-1 / 8-\mathrm{T} 0-1091-\mathrm{F} \end{aligned}$ |
| A15R1B | 0698－3155 | 1 |  | RESISTOR 4.64 K i $\%$ ． 125 W F TC $=0+\cdots 100$ | 24546 | C．4－1／8－T0－4641－F |
| A15R19 | 0698－0084 | 9 | 1 | RESISTOR 2．1EK $1 \% .125 W$ F TC $=0+\cdots 100$ | 24546 | C．4－1／8－T0－2151－F |
| A15R20 | 0757－0416 | 7 |  | RESISTOR $5111 \% .125 \mathrm{~W} F$ TC $=0+-100$ | 24546 | C4－1／8－T0－5118－F |

TABLE 8-13. VERTICALDRIVERUBLANKING ASSEMBLY A15, REPLACEABLE PARTS (2OF2)



FIGURE 8-73. VERTICALDRIVER/BLANKING ASSEMBLY A15, BLOCK DIAGRAM


FIGURE 8-74. VERTICAL DRIVERIBLANKING ASSEMBLY A15,COMPONENTLOCATIONS


TABLE8-14. MOTHERBOARDASSEMBLY A16, REPLACEABLEPARTS (1 OF 2 )

| Reference Designation | HP Part Number | C | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A16 | 08559-63376 | 2 | 1 | KOTHERSGARD ASEEMRLY | 28490 | 06559-60376 |
| A16C1 | 6180-0197 | $\varepsilon$ | 1 | CAPACITOR-FXD 2.2UF+-16\% 2CUDC TA | 56289 | $150 \mathrm{P} 225 \times 902 \mathrm{CAR}$ |
| A16ce | 9180-2235 | 3 | 1 | CAPACTTOR - FXD , 33UF $+13 \%$ S5UCC TA | 56287 | $1500334 \times 9035 A 2$ |
| A1 6C3 | 0160-4C84 | a | 2 | CAPACITOR-FXD . $105+-2 C \%$ S0UDC CER | 23480 | 6160-4084 |
| ${ }^{\text {A1CCA }}$ | 0160-2955 | 8 | 16 | CAPAE,TTOR-FXD .011, $+30-20 \%$ 1JJULC CER | 28480 | 3163-2055 |
| A1 6C5 | 0160-2055 | 9 |  | CAPACITOR-FXD .C1UF + 6 C-20\% 10CUDC CLR | 28480 | C160-2055 |
| A1CC6 | 0160-3879 | 7 | 1 | CAPACITOR-FXD 01UF +-23X 1030 LCC CER | 28483 | 3160-3879 |
| A1 6C7 | 0160-2055 | 9 |  | CAPACITOR-FXD , C1UF +80-26\% 100UDC CER | 28480 | 01662655 |
| A16C8 | 0160-2355 | 5 |  | CAPACEITGR-FXD . 01115 183-2JX 1030 LC IER | 2 Can 3 | 3160-2355 |
| A16C9 A16C10 | $0160-2655$ $0160-2055$ | 9 |  |  | 23480 28480 | $6160-2055$ $3160-2355$ |
| A16C11 | 0160-2055 | 9 |  | CAPACITOR-FXD . C1UF + B6-20\% 100UDC CER | 28480 | 0160-2055 |
| A1sc12 | 3160-2355 | 5 |  | CAPACITGR-FXD .010F + 33-23\% 103VEC CER | 20485 | 3163-2355 |
| A16C13 | 0160-2055 | 9 |  | CAPACITOR-FXO .01UF + $30-2 E X$ 10CUDC CER | 28480 | ¢11.0 2055 |
| A16C14 | 0160-2355 | 5 |  | CAPACITGR-FXD .01UF 180 -23X 1J3VEC $C$ CR | 28480 | 3160-2355 |
| A1 6C15 | 0160-2055 | 9 |  | CAPACITRR-FXD .C1UF + 86-20\% 100UDC CER | 28480 | 6160-2055 |
| A1LC16 | 0169-2355 | 5 |  | CAPACEITGR-FXD . 31JF 1B3-2.3Z 1 IJJULC CER | 28483 | 3160-2055 |
| A16C17 | 0160-2655 | 9 |  |  | 29480 | 01602055 |
| A16C18 | 0160-2955 | 5 |  | CAPAR,ITGR-FXD .01UF +83-2.3\% 100 UDC CER | 29480 | 3160-2355 |
| A16C19 | 0160-2055 | 9 |  | CAPACITOR-FXD .01UF + $86-20 \%$ 100UDC CER | 28480 | 016.0-2055 |
| A16C23 | 0160-3456 | 6 | 1 | CAPAC:ITGR-FXD 1033 PF 1-10\% 1KVDC CER | CB480 | 3163-3456 |
| A16C21 | 0160-4084 | E |  | CAPACITOR-FXD .1UF +-20\% SOUDC CER | 28480 | 0160-4084 |
| A16C22 | 0180-2500 | 1 | 1 | CAPAC,ITOR-FXD $1530 \mathrm{UF}+50-13 \%$ 16UDC AL. | 37942 | 1T1520016G1C3P |
| A16C23 | 6160-2655 | 9 |  | CAPAC.ITOR-FXD C1UF +30-20\% 10CUDC CER | 28480 | ${ }^{6160.2055}$ |
| ${ }_{\text {A1 }}^{\text {Alc24 }}$ | $3160-3878$ $0160-3978$ | ${ }_{6}^{6}$ | 2 | CAPACITAR FXD 1330PF +-23\% 103VDC CER | 28480 | 3160-3878 |
| A16C25 | 0160-3978 | 6 |  | CAPACITRR-FXD $1000 \mathrm{PF}+-20 \% 100 \mathrm{UDC}$ CER | 28480 | 8160-3878 |
| A16E26 | 0160-3877 | 5 | 1 | CAPACITUR-FXD $133 P$ +-23X zajuCC LER | 58480 | 3160-3877 |
| A1 GCR 1 | 1901-0376 | 6 | 1 | DIODE-GEN PRP 354 SOMA DO-35 | 28486 | 1901-0376 |
| A16CR2 | 1901-0250 | 3 | 1 | DICDE-5WITCHING 3JV 20JMA ENS DO-35 | 23480 | 1731-0050 |
| A16J1 | 1251-3782 | 5 | 2 | CONNE CTOR 40 PIN M RECTANGIL AR | 2 2480 | 1251-3782 |
| A16.J2 | 1251-3782 | 5 |  | CONNECTIGR 43 PIN M RECTANTULAR | 28489 | 1251-3732 |
| A16J3 | 1250-0257 | 1 | 1 | CONNECTOR OF SME M PC 50 OHM | 23480 | 1250.0257 |
| A16J4 | 12500543 | E | 1 | CONNI CTITR XF 'M SNP M PC 50 OY:M | c8483 | 1250-0543 |
| A16J5 | 1251-8260 | 2 | 1 | CON FOST TYPE 100 PIN SPCO $9-T O N I$ | 28480 | 1251-8200 |
| A16L1 | 08411-6008 | 5 | 3 | CHiCKE FERRIIE | ¢3480 | 38411-6038 |
| A16L2 | 08411-6008 | 5 |  | CHOXE FERRITE | 28480 | 08411-6008 |
| A1613 | 03411-6098 | 5 |  | CHOKE FERRIIE | 28480 | 28411-6038 |
| A16L4 | 9100-2251 | 0 | 1 | INDUCTOR RF-CH-MLD 220NH $10 x .105 D X .26 L G$ | 28480 | 916c-2251 |
| A1601 | 18550417 | 7 | 1 | TRANSISTGR J-FET N CHAN D-MODE TE-18 SI | 28480 | 1355-0417 |
| A16R1 | 0757-0346 | 2 | 3 | RESIGTOA 10 12, 125w F TC $=01-100$ | 24546 | C4. 1/8-T0-10P0-F |
| A1/6R2 | 37570465 | ${ }_{4}^{4}$ | 1 | RESISTGR $133 \mathrm{~K} 1 \mathrm{1z}, 125 \mathrm{~W}$ F TC=31-130 | 24546 | C4-1/8-T9-1003 F |
| A1 GR3 | 0698-5368 | 2 | 1 |  | 28480 | 06925368 |
| A16R4 | 2100-1757 | 2 | 1 | RESTSTER-TRMR 500 5\% LiW Side-ADJ 1-TRN | 28483 | 2133-1757 |
| A16R5 | 6757-0444 | 1 | 1 | RESISTOR 12.1 K 12.1254 F $\mathrm{TC}=0+-106$ | 24546 | C4-1/8-TC-1212-F |
| A1GR6 A1 167 | $3698-3442$ $0757-0395$ | 5 | 1 |  | 24546 | C4-1/8-T3-237R-F |
| A16R7 A16R8 | -7757-0395 | $\frac{1}{2}$ | 1 |  | 24546 24546 | C4-1/8-T0-56R2-F CA-1/8-TJ-10Ra-F |
| A1 GR9 | 0757-0346 | 2 |  | RESISTOR $101 \%$, 12SW F TC $=0,-100$ | 24546 | C4 1/8-Tn-10PG-F |
| AlGR10 | 2690-3263 | 5 | 1 |  | 23480 | 0673-3260 |
| A16TP 1 | 1251-0600 | 0 | 1 | CONNECTOR-SGL CONT PJN 1.14 MM-BSC -SZ SQ | 28480 | 1251-0600 |
| A1CU1 | 1826-0122 | a | 1 | IC 7805 U RGLIR TO-2?0 | 37263 | 78050 C |
| At GUR 1 | 1962-0631 | 8 | 1 | DIODE ZNP 1N5351: $14 \mathrm{~V} 5 \%$ Pnz5W TC=- $75 \%$ | 04713 | 1 NS 351 B |
| A16UR2 | 1932-0632 | 9 | 1 |  | 04713 | 1 N5354B |
| A1GUR3 | 1962-318? | 0 | 1 | DIODF-ZNR 12.1U $5 \times$ DO-35 PD=,4W | 23480 | 1902-3182 |
| A16 61 A1 6 W 2 | $\begin{aligned} & 07559-60001 \\ & 08559-60061 \end{aligned}$ | 9 | 1 | CONNFCTOR ASSEMEIY, MAINHRAME CAFLE ASSEMEIY, YIG | $\begin{aligned} & 28489 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 28559-60081 \\ & 08559-60061 \end{aligned}$ |
| ${ }_{\text {A1 }} 1643$ | 00559-60059 | 7 | 1 | CAEIF ASSEMELY, MIXER | 28480 | -6559-60089 |
| A16 ${ }^{1} \times 7$ | 1251-1365 | 6 | 7 | CONNECTOR -FC [DGE 2 ? CONT/ROW 2 ROW.; | 28480 | 1251-1365 |
| A16XAB | 1251-1365 | 6 |  | CONNECTIR-PC FOGE 22-CONT/RDW 2 -ROWS | 28480 | 1251-1365 |
| A16XA9 | 1251-1365 | 6 |  | CONNECTOR-PC EDGE 22 -CONT/ROW 2 -ROW:; | 28480 | 1251-1365 |
| A16 XA1 OP 1 | 1251-1626 | 2 | 1 | CONACCTOR - PC FORE 12-CONT/RGW 2-RDWS | 28480 | 1251-1626 |
| A16 XA10P2 | 1251-2034 | 8 | 2 | CONNFCTOR-PC EDGC 10-CONT/ROW 2 -ROW: | 23480 | 1251-2034 |
| A16 $\times$ A11 | 1251-1365 | 6 |  | CONNECTOR PC EDSE 22-CONT/ROW ? ROWS | 28480 | 1251-1365 |
| A16 6 A12 | 1251-1365 | 6 |  | CONNFCTOR PC EDGE 22-CONT/RDW 2-ROWS | 28480 | 1251-1365 |
| A16 XA13 | 1251-1365 | 6 |  | CONNECTOR-PC EDSE $22-$ CONT/RUW 2 ROWS | 28480 | 1251-1365 |
| A16 ${ }^{\text {Pa1 }} 14$ | 1251-1365 | 6 |  | CONNECTOR -PC EDGE 22 CONT/ROW 2-ROWS | 28400 | 1251-1365 |
| A16 XA15 | 1251-2034 | - |  | CONNECTOR-PC EDGE 10-CONT/ROW 2-ROWS | 28480 | 1251-2034 |

TABLE814. MOTHERBOARDASSEMBLY A16, REPLACEABLEPARTS (2OF2)



FIGURE876. MOTHERBOARDASSEMBLY A16, COMPONENTLOCATIONS



Leftical opiver
BLAAKRING ASEEMELYA15




[^0]:    '<2 kHz p-p in 0.1 second in a 180 -series display mainframe with 220/240 line voltage.

[^1]:    '1nput level not to exceed maximum levels.

[^2]:    *Check function generator output frequency using a frequency counter. Frequency readout should be within $\pm 0.5 \%$ of desired audio frequency.

[^3]:    *Attenuations > dial settings are positive (+). Attenuations < dial settings are negative (-).

[^4]:    ${ }^{*}$ DVM Reading minus offset recorded in step 4.
    **All values in the Difference Between Adjacent Readings column must be less than or equal to $\pm 10 \mathrm{mV}$.

[^5]:    See introduction to this section for ordering information

