



**UNITED STATES DEPARTMENT OF COMMERCE**  
**National Institute of Standards and Technology**  
Gaithersburg, Maryland 20899

## **CERTIFICATE OF ANALYSIS**

MicroK Precision Thermometry Bridge  
Isotech MicroK-400  
Serial Number 27384/1

Tested for  
Isotech North America  
Colchester, Vermont

18 April 2008

Test Folder No.: 836/276547-08



UNITED STATES DEPARTMENT OF COMMERCE  
National Institute of Standards and Technology  
Gaithersburg, Maryland 20899

In reply refer to: 836/276547-08

Isotech North America  
Attn: Scott Sabourin  
158 Brentwood Drive  
Unit #4  
Colchester, VT 05446

Subject: Certification of an Isotech MicroK Bridge (Isotech Model MicroK-400, s/n 27384/1)

Purchase Order No.: 20302

Test Folder No.: 836/276547-08

Dear Mr. Sabourin:

The ratio accuracy and non-linearity of your precision thermometry bridge (Isotech Model MicroK-400, s/n 27384/1) was determined using a set of inter-related resistances and reciprocity techniques. Your Isotech MicroK-400 was tested using an AEONZ ratio bridge calibrator (Model RBC 100, s/n 36). The operating conditions of your Isotech MicroK-400 was with a sensing current of 1 mA, 4 sets of 9 readings, and an external reference resistor (100  $\Omega$  Tinsley model 5685A contained in a temperature controlled enclosure Tinsley model 5648). Using four base resistors, the RBC 100 yields 45 distinct ratios over the range from 0.17 to 1.29 and 70 distinctive ratios over the range from 0.17 to 5.94. A least-squares fit of the measurements is used to determine the non-linearity, ratio accuracy, and an expanded uncertainty ( $k=2$ ) for the tested bridge. No correction equation is applied to the results.

Figure 1 shows, for ratios up to 1.26, the standard deviation of the residuals is  $0.08 \times 10^{-6}$  with 40 degrees of freedom. This yields an expanded uncertainty (95 % confidence interval) of  $0.16 \times 10^{-6}$ . The uncertainty ( $k = 1$ ) for the non-linearity was calculated to be  $0.07 \times 10^{-6}$ . Additionally, the maximum compliments error of the 9 two-way combinations was found to be  $0.09 \times 10^{-6}$ . Table 1 gives the measurement results of the AEONZ RBC generated ratios and the residuals of the least-squares fit.

Figure 2 shows, for ratios up to 5.94, the standard deviation of the residuals is  $0.4 \times 10^{-6}$  with 64 degrees of freedom. This yields an expanded uncertainty ( $k=2$ ) of  $0.8 \times 10^{-6}$ . The maximum compliments error of the 34 two-way combinations was found to be  $0.09 \times 10^{-6}$ . Table 2 gives the measurement results of the AEONZ RBC generated ratios and the residuals of the least-squares fit.

Additionally, as shown in Figures 1 and 2, a two-way complements check using two 100  $\Omega$  reference resistors gave a ratio accuracy uncertainty ( $k = 1$ ) of  $0.12 \times 10^{-6}$ .

Test Folder No: 836/276547-08

Page 2 of 7

NIST

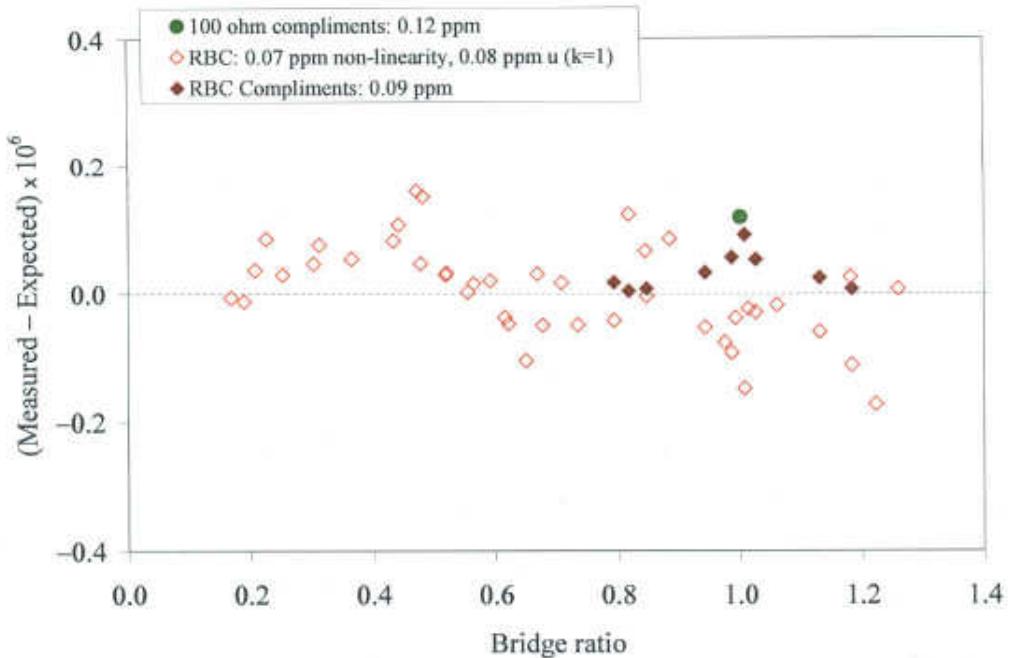


Figure 1. Isotech Model MicroK-400 (s/n 27384/1) results from the AEONZ RBC over a ratio from 0.17 to 1.26 and the two-way complements check measurements.

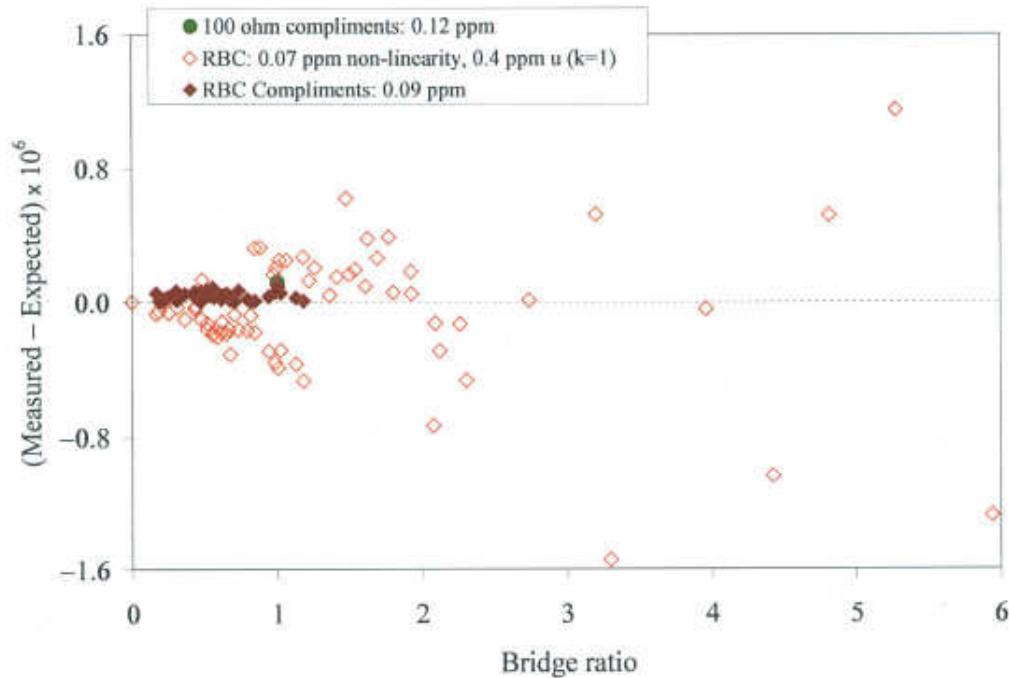
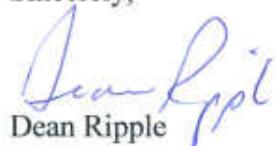


Figure 2. Isotech Model MicroK-400 (s/n 27384/1) results from the AEONZ RBC over a ratio from 0.17 to 5.94 and the two-way complements check measurements.

Table 3 gives expanded uncertainty ( $k=2$ ) results for various models of bridge error for the purpose of determining any possible source of problem. When bridge faults exist, the observed errors may depend on the measurement configuration. Consequently, we do not recommend the use of a correction equation. A description on the various models of bridge error are found in the following reference: D. R. White, "A Method for Calibrating Resistance Bridges", Proceedings of TEMPMEKO '96, 6<sup>th</sup> International Symposium on Temperature and Thermal Measurements in Industry and Science, pp. 129-134, 1997.

Sincerely,

  
Dean Ripple  
Leader, Thermometry Group  
Process Measurements Division

**Table 1. Isotech Model MicroK-400 (s/n 27384/1) AEONZ RBC measurement results for ratios from 0.17 to 1.26.**

Index	Combination	Reading	Fitted Value	Residual $\times 10^6$	Index	1 / Combination	Reading	Fitted Value	Residual $\times 10^6$
1	R1	0.81809357	0.81809369	0.12	36	R1	1.2223541	1.2223539	-0.17
2	R2	0.48172649	0.48172664	0.15	41	R1+R3	0.8451497	0.8451497	0.07
3	R3	0.36512856	0.36512861	0.05	42	R1+R4	0.8845915	0.8845916	0.09
4	R4	0.31237145	0.31237153	0.08	43	R2+R3	1.1808393	1.1808393	0.03
6	R1+R3	1.18322242	1.18322231	-0.11	44	R2+R4	1.2592901	1.2592901	0.01
7	R1+R4	1.13046528	1.13046522	-0.06	52	R1+R2//R3	0.9748546	0.9748545	-0.08
8	R2+R3	0.84685526	0.84685526	0.00	53	R1+R2//R4	0.9924684	0.9924684	-0.04
9	R2+R4	0.79409821	0.79409817	-0.04	54	R1+R3//R4	1.0137447	1.0137447	-0.02
10	R3+R4	0.67750019	0.67750014	-0.05	64	R1+R2//R3//R4	1.0606197	1.0606197	-0.02
11	R1//R2	0.30319380	0.30319385	0.05					
12	R1//R3	0.25245415	0.25245418	0.03					
13	R1//R4	0.22605656	0.22605665	0.09					
14	R2//R3	0.20770037	0.20770041	0.04					
15	R2//R4	0.18949508	0.18949507	-0.01					
16	R3//R4	0.16834799	0.16834798	-0.01					
17	R1+R2//R3	1.02579413	1.02579410	-0.03					
18	R1+R2//R4	1.00758891	1.00758876	-0.15					
19	R1+R3//R4	0.98644177	0.98644168	-0.09					
20	R2+R1//R3	0.73418087	0.73418082	-0.05					
21	R2+R1//R4	0.70778327	0.70778329	0.02					
22	R2+R3//R4	0.65007473	0.65007463	-0.10					
23	R3+R1//R2	0.66683243	0.666832246	0.03					
24	R3+R1//R4	0.59118524	0.59118526	0.02					
25	R3+R2//R4	0.55462368	0.55462368	0.00					
26	R4+R1//R2	0.61556541	0.61556537	-0.04					
27	R4+R1//R3	0.56482569	0.56482571	0.02					
28	R4+R2//R3	0.52007190	0.52007193	0.03					
29	R1+R2//R3//R4	0.94284513	0.94284508	-0.05					
30	R2+R1//R3//R4	0.62134409	0.62134404	-0.05					
31	R3+R1//R2//R4	0.51898572	0.51898575	0.03					
32	R4+R1//R2//R3	0.47801719	0.47801724	0.05					
33	R1//R2+R3//R4	0.47154167	0.47154183	0.16					
34	R1//R3+R2//R4	0.44194914	0.44194925	0.11					
35	R1//R4+R2//R3	0.43375697	0.43375705	0.08					

**Table 2.** Isotech Model MicroK-400 (s/n 27384/1) AEONZ RBC measurement results for ratios from 0.17 to 5.94.

Index	Combination	Reading	Fitted Value	Residual $\times 10^6$	Index	1 / Combination	Reading	Fitted Value	Residual $\times 10^6$
1	R1	0.81809357	0.81809349	-0.08	36	R1	1.2223541	1.2223542	0.13
2	R2	0.48172649	0.48172662	0.13	37	R2	2.0758669	2.0758662	-0.73
3	R3	0.36512856	0.36512846	-0.10	38	R3	2.7387621	2.7387621	0.01
4	R4	0.31237145	0.31237142	-0.03	39	R4	3.2013167	3.2013172	0.52
6	R1+R3	1.18322242	1.18322195	-0.47	41	R1+R3	0.8451497	0.8451500	0.32
7	R1+R4	1.13046528	1.13046491	-0.37	42	R1+R4	0.8845915	0.8845918	0.33
8	R2+R3	0.84685526	0.84685508	-0.18	43	R2+R3	1.1808393	1.1808396	0.27
9	R2+R4	0.79409821	0.79409804	-0.17	44	R2+R4	1.2592901	1.2592903	0.20
10	R3+R4	0.67775019	0.677749988	-0.31	45	R3+R4	1.4760144	1.4760150	0.62
11	R1//R2	0.30319380	0.30319381	0.01	46	R1//R2	3.2982219	3.2982203	-1.54
12	R1//R3	0.25245415	0.25245409	-0.06	47	R1//R3	3.9611164	3.9611163	-0.04
13	R1//R4	0.22605656	0.22605658	0.02	48	R1//R4	4.4236724	4.4236714	-1.04
14	R2//R3	0.20770037	0.20770035	-0.02	49	R2//R3	4.8146278	4.8146283	0.52
15	R2//R4	0.18949508	0.18949503	-0.05	50	R2//R4	5.2771822	5.2771834	1.15
16	R3//R4	0.16834799	0.16834792	-0.07	51	R3//R4	5.9400806	5.9400793	-1.27
17	R1+R2//R3	1.02579413	1.02579385	-0.28	52	R1+R2//R3	0.9748546	0.9748547	0.17
18	R1+R2//R4	1.00758891	1.00758852	-0.39	53	R1+R2//R4	0.9924684	0.9924686	0.20
19	R1+R3//R4	0.98644177	0.98644141	-0.36	54	R1+R3//R4	1.0137447	1.0137449	0.25
20	R2+R1//R3	0.73418087	0.73418071	-0.16	55	R2+R1//R3	1.3620624	1.3620625	0.04
21	R2+R1//R4	0.70778327	0.70778320	-0.07	56	R2+R1//R4	1.4128619	1.4128620	0.15
22	R2+R3//R4	0.65007473	0.65007454	-0.19	57	R2+R3//R4	1.5382849	1.5382851	0.19
23	R3+R1//R2	0.666832243	0.666832227	-0.16	58	R3+R1//R2	1.4962840	1.4962841	0.17
24	R3+R1//R4	0.59118524	0.59118504	-0.20	59	R3+R1//R4	1.6915175	1.6915178	0.26
25	R3+R2//R4	0.55462368	0.55462349	-0.19	60	R3+R2//R4	1.8030249	1.8030250	0.06
26	R4+R1//R2	0.61556541	0.61556523	-0.18	61	R4+R1//R2	1.6245228	1.6245232	0.38
27	R4+R1//R3	0.56482569	0.56482551	-0.18	62	R4+R1//R3	1.7704579	1.7704583	0.39
28	R4+R2//R3	0.52007190	0.52007177	-0.13	63	R4+R2//R3	1.9228113	1.9228115	0.18
29	R1+R2//R3//R4	0.94284513	0.94284484	-0.29	64	R1+R2//R3//R4	1.0606197	1.0606199	0.25
30	R2+R1//R3//R4	0.62134409	0.62134398	-0.11	65	R2+R1//R3//R4	1.6094144	1.6094145	0.09
31	R3+R1//R2//R4	0.51898572	0.51898556	-0.16	66	R3+R1//R2//R4	1.9268358	1.9268359	0.05
32	R4+R1//R2//R3	0.47801719	0.47801709	-0.10	67	R4+R1//R2//R3	2.0919755	2.0919754	-0.12
33	R1//R2+R3//R4	0.47154167	0.47154173	0.06	68	R1//R2+R3//R4	2.1207034	2.1207031	-0.29
34	R1//R3+R2//R4	0.44194914	0.44194911	-0.03	69	R1//R3+R2//R4	2.2627041	2.2627039	-0.13
35	R1//R4+R2//R3	0.43375697	0.43375693	-0.04	70	R1//R4+R2//R3	2.3054391	2.3054387	-0.46

Table 3. AEONZ RBC results for various models of bridge error for the purpose of determining any possible source of problem for the Isotech Model MicroK-400 (s/n 273841).

RBC Results for ratios from 0.17 to 1.26		
Model	$U(k=2)$ , residual $\times 10^6$	Degrees of Freedom
None	0.16	40
Offset	0.16	39
Offset + Linear	0.12	38

RBC Results for ratios from 0.17 to 5.94		
Model	$U(k=2)$ , residual $\times 10^6$	Degrees of Freedom
None	0.82	64
Offset	0.80	63
Offset + Linear	0.70	62