## Model 515A

 Megohm BridgeInstruction Manual

## WARRANTY

We warrant each of our products to be free from defects in material and workmanship. Our obligation under this warranty is to repair or replace any instrument or part thereof which, within a year after shipment, proves defective upon examination. We will pay domestic surface freight costs.

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# Model 515A Megohm Instruction Manual 

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## SPECIFICATIONS

RANGE: $10^{5}$ to $10^{15}$ ohms with a 7 -dial in-line readout.
ACCURACY: (when bridge is operated as described below):

| Range, ohms | Standard Deviation $(l \sigma) * *$ Bridge Voltage | Decade |  |
| :--- | :---: | :---: | :---: |
| $10^{5}$ to $10^{7}$ | $.012 \%$ | 10 v | $10^{5}$ to $10^{6}$ |
| $10^{7}$ to $10^{8}$ | $.02 \%$ | 10 v | $10^{7}$ |
| $10^{8}$ to $10^{9}$ | $.03 \%$ | 10 v | $10^{8}$ |
| $10^{9}$ to $10^{10}$ | $.06 \%$ | 10 v | $10^{10}$ |
| $10^{10}$ to $10^{11}$ | $.08 \%$ | 10 v | $10^{10}$ |
| $10^{11}$ to $10^{12}$ | $.16 \%$ | 10 v | $10^{11}$ |
| $10^{12}$ to $10^{13}$ | $.25 \%$ | 100 v | $10^{12}$ |
| $10^{13}$ to $10^{14}$ | $.3 \%$ | $500 \mathrm{v}^{*}$ | $10^{12}$ |
| $10^{14}$ to $10^{15}$ | $1.5 \%$ | $500 \mathrm{v}^{*}$ | $10^{12}$ |

INPUT: Built-in compartment or optional Remote Test Chamber with Teflon-insulated triaxial cable.

GROUNDING: One terminal of unknown is at ground potential.
NULL DETECTOR: Electrometer with sensitivity of 100 microvolts per division to 1 volt per division in five decade steps. Meter is non-linear past $1 / 3$ of full scale for ease in determining null.

BRIDGE POTENTIAL: Internal: From 0 to +110 volts dc in l-volt steps. External With Keithley Model 240 A or 241 High Voltage Supply, 1000 volts maximum, positive only.

INTERNAL CHECKS: Built-in zero check anc leakage (guard to ground) check. Test jacks for checking wirewound standard resistors. Bootstrap calibration from wirewound standards for the $10^{7}$ through $10^{12}$ decades.

ENVIRONMENT: Any $\pm 0.5^{\circ} \mathrm{C}$ span between 20 and $30^{\circ} \mathrm{C}, 20-50 \%$ relative humidity.
CONNECTORS: External Operate: Teflon-insulated triaxial panel jack, Gremar 5632A. External Bridge-Potential Input: UHF.

POWER: $105-125$ or $210-250$ volts, $50-60 \mathrm{~Hz}, 10$ watts.
DIMENSIONS, WEIGHT: Standard $19^{\prime \prime}$ wide $\times 14^{\prime \prime}$ high rack mounting, 11-1/2" behind front panel ( $483 \times 356 \times 292 \mathrm{~mm}$ ), total depth, $12-3 / 4^{\prime \prime}$ ( 324 mm ) ; net weight, 28 pounds (12,5 kg).

NOTES: *External supply requíred above $10^{13}$ ohms.
**Based on theoretical analysis of bridge errors. See Instruction Manual for details on obtaining specified performance.

## SECTION I. GENERAL DESCRIPTION

1-1. GENERAL. The Model 515A Megohm Bridge is an instrument for measuring resistance from $10^{4}$ ohms to 1015 ohms with a limit of error from . 05 to $1 \%$. It comprises a solid-state, guarded, electrometer null detector; an ultra-stable, highly-regulated dc voltage source, and a Wheatstone bridge.

## 1-2. FEATURES.

a. Accuracy Verification: Accuracy is traceable to the National Bureau of Standards by use of the Model 5155 resistance standards available as an optional accessory.
b. Selectable Bridge Voltage: An internal voltage
source spans a range from 1 to 110 volts in $1-v o l t$ steps.
c. Shielded Compartment: Connection to the bridge is made using a guarded terminal in the shielded compartment which minimizes noise pickup.
d. Standardize Mode: This mode can be selected for quick calibration of bridge elements to correct for slight changes in the standard high megohm resistors.
e. Guard Leakage Check: A quick self check of the guard to ground resistance can be made using test jacks on the front panel (inside the measuring compartment.


FIGURE 1. Front Pane1.

TABLE 1-1.
Front Panel Controls.

| Control | Functional Description | Paragraph |
| :---: | :---: | :---: |
| BRIDGE VOLTS |  |  |
| Power Switch (5311) | Controls power to bridge; Selects INT or EXT. | 2-2, al |
| X1 Switch (S203) | Sets voltage in 1 -volt steps. | 2-2, a2 |
| X10 Switch (S202) | Sets voltage in 10 -volt steps. | 2-2, a3 |
| NULL DETECTOR |  |  |
| Sensitivity Switch (S103) | Selects null detector sensitivity, . 1 to $1000 \mathrm{mV} / \mathrm{div}$. | 2-2, a4 |
| FINE 2ERO Control (Rl20) | Adjusts meter zero (inner knob). | 2-2, a5 |
| COARSE ZERO Control (S102) | Adjusts meter zero (outer knob). | 2-2, a6 |
| READ/ZERO CHECK (S201) | Selects READ or ZERO CHECK operation. | 2-2, a7 |
| FUNCTION Switch (S301) | Selects mode of operation; 4 positions. | 2-2, a8 |
| RESISTANCE |  |  |
| X100 (S304) | Adjusts bridge balance in steps of 100. | 2-2, a9 |
| $\mathrm{X10}$ (S305) | Adjusts bridge balance in steps of 10. | 2-2, al0 |
| XI (S306) | Adjusts bridge balance in steps of 1. | 2-2, al1 |
| X. 1 (S307) | Adjusts bridge balance in steps of . 1 . | 2-2, al2 |
| X. 01 (S308) | Adjusts bridge balance in steps of .01. | 2-2, al. 3 |
| X. 001 (S309) | Adjusts bridge balance in steps of . 001 . | 2-2, al4 |
| X. 0001 (S310) | Adjusts bridge balance in steps of . 0001 . | 2-2, al5 |
| Multiplier Switch (S302) | Sets multiplier ratio from $10^{5}$ to $10^{12}$. | 2-2, a16 |

TABLE 1-2.
Controls and Connections,
Front Panel Measuring Compartment.

| Control | Functional Description | Paragraph |
| :---: | :---: | :---: |
| CALIBRATE Controls | Adjusts bridge elements in CALIBRATE mode. | $2-2$, b1 |
| Safety Switch (S303) | Provides a safety interlock; removes bridge power when the compartment door is open. | 2-2, b2 |
| INPUT Terminal (J302) | Provides a guarded connection to INPUT high. | 2-1, a |
| EXT. INPUT Terminal (J303) | Provides a guarded connection using a triaxial cable for external inputs. | 2-1, a |
| Low Terminals | Provides a connection to INPUT low when using the guarded INPUT high terminal. | 2-1, a |
| Test Jacks J201-210 | Provide various circuit test points for checkout. | - |



FIGURE 2. Front Panel Controls


FIGURE 3. Shieided Measuring Compartment

## SECTION 2. OPERATION

## 2-1. MEASUREMENT CONSIDERATIONS.

## a. Connections.

1. Shielded Test Compartment. The Test Compartment shown in Figure 3 permits measurement of high resistance while minimizing noise pickup and the effects of leakage paths. Input connections can be made using a triaxial receptacle (EXTERNAL INPUT J303) or a guarded INPUT high receptacle (J302).
a.) High Megohm Resistors. Discrete resistors can be easily measured by connecting to the INPUT receptacle and any one of eight INPUT low receptacles. The receptacles are designed for use with test clips such as Grayhill 非2-1 which have a banana plug on one end and a spring clip on the other. The INPUT low receptacles are spaced one inch apart for resistors up to 8 inches long. A typical resistor connection is shown in Figure 3.
b.) External Connections. A teflon-insulated, guarded, triaxial receptacle (EXTERNAL INPUT J303) is provided for external connections. The receptacle is a Gremar Type 5632A triaxial connector which mates with a Gremar Type 7991-1 triaxial plug (Keithley CS-69). An optional accessory cable is available (Keithley Molel 5153) for external connections; a $60^{\prime \prime}$ triaxial cable with CS69 connector on one end. The Keithley Model 5152 Remote Test Chamber permits external shielded measurements (with a $60^{\prime \prime}$ triaxial cable and CS-69 connector).


FIGURE 4. Guarding
2. External Voltage Source. An external voltage source can be connected to the bridge using the rear panel UHF coaxial receptacle (J211). This connector is a Gremar Type 6804 UHF receptacle (Keithley CS-64) which mates with a Gremar Type 5127 plug (Keithley CS-49).
b. Guarding. A driven guard is used extensively in the bridge circuit to minimize the effects of spurious leakage currents.

1. Theory. In megohm bridge design, care must be taken to guard the high-resistance arm so that insulation leakage currents will not affect the balance point. Guarding in the Model 515A is shown in Figure 4. The guard enclosure is indicated by the dotted-line surrounding the high megohm STANDARD resistors, the electrometer null detector, and the guarded input terminal. The input high terminal utilizes a "guard ring" maintained approximately at the potential of the null detector low.
2. Circuitry. The guard potential is obtained from the null detector (electrometer) power supply common as illustrated in Figure 5. The potential of the "Driven Guard" is maintained at very nearly the Input High potential with the result that the High to Guard leakage is extremely small at bridge balance. The guard circuit is formed by a metal enclosure and plates which surround the STANDARD resistors, CALIBRATE resistors, the null detector, and the Input terminal.


FIGURE 5. Null Detector

## 3. Use of the Guard.

a.) Connections to guard. The INPUT terminal (J302) is a guarded receptacle (Gremar, Type 6804) with a center High contact and an outer Guard ring. The EXTERNAL INPUT terminal (J303) is a guarded triaxial receptacle (Gremar, Type 5632A) with a center High contact, an inner Guard contact and an outer Low contact. A drawing of the connector construction is shown in Figure 6.
b.) Applications. The driven guard can be used for external measurements when it is necessary to minimize the effects of spurious leakage currents across the insulation. A typical external measurement can be accomplished using Keithley Model 5152 Remote Test Chamber and teflon-insulated triaxial cable. The use of the Model 5152 is completely described in Section 4, Accessories.
c.) Guard to Ground Leakage. The design of the guard circuit in the Model 515A maintains the Guard to Low (ground) resistance greater than $10^{11}$ ohms. The Guard to Ground resistance should be high with respect to the resistance from floating low to ground so that the shunting effects across the Readout Resistance will not be significant. For example the worst-case condition would be a Readout Resistance of 10 megohms or $10^{7}$ ohms with a $0.02 \%$ tolerance. If the Guard to Ground resistance were $10^{11}$ ohms, an additional error of 0.01 \% would result.

c. Leakage. The Input terminals of the Model 515A have been designed using teflon insulation between High and Guard and Guard and Ground. In order to maintain the high insulation resistance, the terminals must be kept clean and dry. Preferred cleaning materials include: Chemically pure alcohol, sterile cotton swabs (to prevent contamination of alcohol), and a drying agent such as nitrogen. Leakage paths across the terminal can create intermittant errors or difficult bridge balance. The user should also take care to insure that the unknown resistor, holding fixtures and case are insulated properly. Glass envelopes (high megohm resistors) can be contaminated by oil and salts from improper handling. Paper base bakelite insulation can be degraded by improper handling and exposure to moisture. The humidity of the laboratory environment can also affect the measurement of very high resistances. See Specifications.
d. Noise. Noise pickup from ac electric and magnetic fields is minimized by the unit construction of the chassis and the use of a closed, shielded measuring compartment. When using an external unknown resistance, care should be taken to:

1. Use shielded cables such as Keithley Model 5153 triaxial cable.
2. Fasten down the cables so that flexure noise is minimized.
3. Maintain Guard to Ground insulation using tefion insulation.
4. Use an external shielded test box such as Keithley Model 5152 Remote Test Chamber.
e. Accuracy.
5. Specification. The specified accuracy for measurements on various ranges is valid for the following conditions.
a.) Minimum Bridge Potential. This potential is the minimum voltage required for resolution.
b.) Environment. The ambient temperature and relative humidity must be controlled within limits stated.
c.) Standardization. The Standardization procedure should be performed prior to very critical measurements.
d.) Proper Operating Technique. Care must be taken when connecting the unknown (See Measurement Considerations, Paragraph 2-1) and balancing the bridge (See Accuracy Considerations, Paragraph 2-7).
6. Verification. The Model 515A accuracy can be verified using the Model 5155 Megohm resistance standards.
7. Technique for Measuring $10^{10}$ to $10^{15}$ Ohm Resistances.

Set Controls as Indicated:
BRIDGE VOLTS: 0
FUNCTION SWITCH: OPERATE OR EXTERNAL OPERATE
MULTIPLIER:
RESISTANCE DECADE DIAL X100: 10
READ/ZERO SWITCH: ZERO
Insert unknown resistor. Set READ/ZERO Switch to READ and note offset of null detector with MULTIPLIER setting to be used in measurement. Allow approximately 15 minutes for reading to stabilize. The offset of the null detector is due to offset current from the null detector and from stressing of Teflon insulation surrounding the Hi terminal of the bridge. Use the offset reading as null for measuring the unknown.

Set READ/ZERO Switch to ZERO. Select the Bridge potential for the measurement based on desired accuracy as described in detail in the OPERATION section of the manual. Set READ/ZERO Switch to READ and balance bridge using Resistance decade dials.

METER NOISE: In balancing the bridge when measuring resistances greater than $10^{10}$ ohms there is meter noise present due to $1 / \mathrm{f}$ noise, alpha particle noise, etc. It may be noted that the meter indication has a base-line from which meter fluctuations diverge. The actual null detector reading is this base-line when balancing the bridge.

## NOTE

Care should be taken to allow enough time for bridge to stabilize tc a reading. This time will vary from one measurement to another however, a minimum time of 15 minutes is advisable to determine final null reading.
2-2. CONTROLS AND SWITCHES.
a. Front Pane 1.

1. Power Switch (S311). This switch controls the power to the bridge including the bridge potential and null detector supplies. The INT position permits a setting of the bridge potential from 1 to 110 volts using the Xl and XlO BRIDGE VOLTS switches. The EXT position connects the external voltage input (J211) so that a bridge potential up to 1000 V can be applied using an external voltage supply such as Keithley Model 241.
2. Xl Switch (S203). This switch permits a setting of the bridge potential in 1 -volt increments up to 10 volts.
3. X10 Switch (S202). This switch permits a setting of the bridge potential in 10 -volt increments up to 100 volts.
4. Sensitivity Switch (S103). This switch selects the null detector sensitivity from .1 to 1000 millivolts per division.
5. FINE Control (Rl20). This control is the inner knob of a dual-concentric control. The FINE Control permits adjustment of the meter zero.
6. COARSE ZERO Switch (S102). This switch is the outer knob of a dual-concentric control. The COARSE Switch permits adjustment of the meter zero in 10 steps.
7. READ/ZERO CHECK Switch (S201). This switch selects READ or ZERO CHECK operation for the meter circuit. In ZERO CHECK position the null detector High and Low are shorted together.
8. FUNCTION Switch (S301). This switch selects the mode of operation in 4 position, OPERATE, STANDARDIZE, CALIBRATE, and EXTERNAL OPERATE. A complete discussion of these modes is given in paragraph 2-3.
9. X100 Resistance Switch (S304). This switch adjusts the "Readout" arm of the bridge in steps of 100 .
10. X10 Resistance Switch (S305). This switch adjusts the "Readout" arm of the bridge in steps of 10 .
11. X1 Resistance Switch (S306). This switch adjusts the "Readout" arm of the bridge in steps of 1 .
12. X.l Resistance Switch (S307). This switch adjusts the "Readout" arm of the bridge in steps of .1 .
13. X. 01 Resistance Switch (S308). This switch adjusts the "Readout" arm of the bridge in steps of .01 .
14. X. 001 Resistance Switch (S309). This switch adjusts the "Readout" arm of the bridge in steps of . 001 .
15. X. 0001 Resistance Switch ( $\$ 310$ ). This switch adjusts the "Reađout" arm of the bridge in steps of .0001 .
16. Multiplier Switch (S302). This switch sets the multiplier ratio from $10^{5}$ to $10^{12}$.

## b. Measuring Compartment.

1. CALIBRATE Controls. These controls are used to adjust the bridge when the FUNCTION Switch is set to CALIBRATE. The use of these controls is described in paragraph 2-4, d (Standardization procedure).
2. Safety Switch (S303). This switch is a nor-mally-open interlock which removes bridge power when the compartment door is open. The safety interlock is defeated when the FUNCTION switch is set to EXTERNAL OPERATE.
c. Rear Panel. 117-234V Line Switch (S312). This switch sets the Model 515A for either 117V or 234 V rms line power, $50-60 \mathrm{~Hz}$.

## 2-3. MODES OF OPERATION.

a. Operate. This mode of operation permits measurements of high megohm resistances when connected to the INPUT receptacle. To select this mode, set the FUNCTION switch to OPERATE. Either the internal voltage source (bridge potential) or an external voltage source up to 1000 volts can be used. The safety interlock switch prevents operation of the bridge whenever the compartment door is open. If the unknown resistance must be measured externally, use the External Operate mode.
b. External Operate. This mode of operation permits resistance measurements the same as for the Operate mode. To select this mode set the FUNCTION switch to EXTERNAL OPERATE.

## WARNING

When the FUNCTION Switch is set to EXTERNAL OPERATE the safety interlock feature is defeated. Therefore the bridge voltage (up to 1000 volts) is present at the Guard circuit at receptacle J303. The user should be cautious when using very high bridge voltages. For maximum safety, the Power Switch (S311) should be set to INT when not making a measurement.
c. Standardize/Calibrate. These modes of operation permit adjustment of the bridge elements to compensate for slight variations of the standard high megohm resistors. To select either mode set the FUNCTION Switch to STANDARDIZE or CALIBRATE as described in paragraph 2-4, d.

## 2-4. PRELIMINARY PROCEDURES.

a. Power.

1. Line Voltage. This instrument can be connected to 117 volt, $50-60 \mathrm{~Hz}$ line power when the line Voltage Switch (on the rear panel) is set to 117 V . The fuse should be a type $3 \mathrm{AG}, 1 / 4 \mathrm{~A}, \mathrm{SLO}-\mathrm{BLO}$. When using 234 V power, set the Line Voltage Switch to 234 V and replace fuse with a type $3 \mathrm{AG}, \mathrm{I} / 8 \mathrm{~A}, \mathrm{SLO}-\mathrm{BLO}$.
2. Accessory Outlet. A three terminal power outlet (J3O1) is provided on the rear panel for operation of an accessory such as an external power supply. This outlet is wired to the line power cord and is not controlled by the Power Switch.
3. Power Cord. A three wire power cord is supplied ( 6 feet long). A third prong is used for earth ground connection for the chassis. An adapter is supplied for converting to a two prong outlet, but should only be used when a solid, earth-connection is made by some other means.
b. Meter Zero. The meter circuit can be zeroed by adjustment of COARSE ZERO and FINE ZERO Controls. The READ/METER ZERO Switch (S201) should be ret to METER ZERO.
4. COARSE 2ERO Switch (S102) (Outer Knob). This switch has eleven positions for adjustment of meter zero.
5. FINE ZERO Control (R120). This control provides fine (potentiometer) adjustment of the meter zero.
c. Warmup. The instrument should be allowed to stabilize with power on (at least 30 minutes). If the instrument has been exposed to an extreme ambient temperature change the warmup time should be extended to 24 hours or more.
d. Standardize Procedure. For critical measurements the instrument should be standardized prior to each measurement to compensate for slight changes of the standard high megohm resistors due to temperature variations and aging with time. The Standardize procedure should be performed as described in Table 2-1. A complete discussion of the Standardization technique is given in paragraph 2-5.

## 2-5. MEASUREMENT PROCEDURE.

a. Connect Unknown Resistance. Determine the method of connection to the unknown as discussed in paragraph 2-1.
b. Select the Bridge Potential. The minimum Bridge Potential should be determined for rated accuracy as stated in the specifications. The voltage can be applied internally (with Power Switch set to INT) or externally as described in paragraph 2-1.
c. Standardize Bridge. For measurements where the effects of variations of the bridge elements must be minimized, the Standardization procedure should be performed as described in paragraph 2-3, d.
d. Meter Zero. Adjust meter zero as necessary.
e. Bridge Balance. With the FUNCTION Switch set to OPERATE, proceed to balance the bridge (set the READ/ZERO Switch to READ). Increase the null sensitivity as necessary to obtain a precise bridge balance.
f. External Operate. If the unknown resistance is connected externaliy the FUNCTION Switch should be set to EXTERNAL OPERATE before bridge balance is attempted.

2-6. STANDARDIZE.
a. Purpose of Standardization Technique. Wirewound resistors have the greatest accuracy and keep their calibrations over long periods of time. Values greater than about one megohm, however, are too large and too expensive to be widely used. Film type resistors provide values up to $10^{12}$ ohms and higher with reasonable success and this type resistor is used in the Model 515A. But the value of these resistors changes with time, sometimes one percent per year. The Keithley Model 515A Megohm Bridge has been designed so that frequent compensations can be made for variations of its high-megohm standard resistors. This process is called Standardization and is carried out as in paragraph 2-4, d.


## b. Description of circuit and technique.

1. A simplified bridge circuit with FUNCTION switch in STANDARDIZE is shown in Figure 9.
2. With Resistance Multiplier Switch set at $10^{6}$, then the bridge null is obtained for the condition $S_{6} / S_{7}=B_{6} / A$, where $" S_{6}$ ", " $S_{7}$ ", " $B_{6}$ ", and "A" are defined as follows:
" $S_{6}$ " $=$ Standard resistor ( $10^{6}$ ohm, . $02 \%$ ) selected by resistance multiplier switch set at $10^{6}$.
" $S_{7}{ }^{\prime \prime}=$ Standard resistor ( $10^{7}$ ohm, $1.0 \%$ ).
" $\mathrm{B}_{6}$ " $=10^{5} \mathrm{ohm}, .02 \%$.
" $A$ " $=$ Resistance decade potentiometer adjusted for null ( $10^{6}$ ohms).

NOTE
This technique is used to determine the ratio of " $S_{6}$ " to " $\mathrm{S}_{7}$ " accurately as read by resistance decade dials.
3. A simplified bridge circuit with FUNCTION switch in CALIBRATE is shown in Figure 10
4. In the CALIBRATE position, a resistance ratio network of $1: 10$ is connected in place of " 56 " and " $\mathrm{S}_{7}$ ". The bridge null is obtained for the condition $R=B_{7} / A$, where $" R$ ", " $B_{7}$ ", and " $A$ " are defined as follows:
"R" = Ratio network of 1:10 with . $005 \%$ accuracy.
" $B_{7}$ " $=$ Calibrate potentiometer.
"A" = Resistance decade potentiometer adjusted previously in b2.

NOTE
This technique is used to set the calibrate potentiometer " $B_{7}$ " such that error in " $S_{7}$ " is compensated.
5. A simplified bridge circuit with FUNCTION switch in OPERATE is shown in Figure 11.
6. In the OPERATE position, the bridge null is obtained for the condition $\mathrm{S}_{7} / \mathrm{X}=\mathrm{B}_{7} / \mathrm{A}$, when resistance decade potentiometer " A " is properly adjusted.
7. A simplified bridge circuit with FUNCTION switch in OPERATE and resistance multiplier $10^{6}$ is shown in Figure 8.


FIGURE 7. Test Jack Identification.

## 2-7. THEORY OF OPERATION.

a. Bridge Theory. The Megohm Bridge has been designed to measure very high resistances using a Wheatstone Bridge and a sensitive null detector. The Wheatstone Bridge circuit basically consists of four arms, identified as $A, B, S$, and $X$ as shown in Figure 11. (A thorough discussion of bridge measurement is available in Electrical Measurement, F. K. Harris, Wiley, New York, 1952). The equation for the bridge at balance can be described by the equation:

$$
X=S \times A / B
$$

b. Null Detector Sensitivity. The sensitivity of the bridge can be described by the equation:

$$
e=\frac{S d}{(S+X)^{2}} \times E
$$

$\mathrm{e}=$ sensitivity in volts
$\mathrm{d}=$ incremental unbalance (in terms of the unknown)
$\mathrm{E}=$ bridge potential
$\mathrm{S}=$ standard resistance
$\mathrm{X}=$ unknown resistance.
c. Voltage Across the Unknown. The Voltage across the unknown resistance can be determined for a given set of conditions where:
$\mathrm{E}=$ bridge potential (bridge volts setting)
$S=$ standard resistance (multiplier setting)
$\mathrm{X}=$ unknown resistance (approximate value of the unknown)
$V_{X}=$ voltage across $X=E \frac{X}{X+S}$
2-8. GUARD LEAKAGE CHECK.
The following procedure should be used to verify the guard to ground resistance. The test jacks are identified in Figure 7.

## Procedure:

1. Connect power cord to line voltage.
2. Place jumpers between the following test jacks. J203 and J204 J205 and J206
3. Set 515A controls as follows.
BRIDGE POWER - EXT
MILLIVOLT PER DIVISION - 1000
FUNCTION - OPERATE

MULTIPLIER - $10^{5}$
READ/ZERO CHECK - ZERO CHECK
X100 DIAL - 1
DOOR - CLOSED
4. Connect Keithley Model 240A Power Supply to EXTERNAL INPUT on the rear panel.
5. Set Model 240A to 1000 volts with OUTPUT to +.
6. Set READ/ZERO CHECK switch to READ.
7. Allow five minutes for the Model 515A reading to stabilize. Reading shall be less than 1000 mV . NOTE; The meter indicates the voltage drop across a $10^{8}$ resistor in series with the leakage path. Leakage resistance from GUARD to GROUND is determined as follows.

Leakage current $=$ (Voltage drop $\div 10^{8}$ ohms) Leakage resistance $=(1000 \mathrm{~V} \div$ leakage current $)$ Typical GUARD to GROUND resistance is greater than $10^{11}$ ohms.


FIGURE 8.
Operate Position, $10^{6} \mathrm{Multiplier}$.

BALANCE
EQUATION
$S_{6} / S_{7}=B_{6} / A$


ERIDGE IN STANDAROIZE POSITION, MULTIPLIER AT 106

FIGURE 9.
Standardize Position, $10^{6}$ Multiplier.


FIGURE 10.
Calibrate Position, $10^{6}$ Multiplier.

BALANCE
EQUATION
$S_{7} / X=B_{7} / A$

MULTIPLIER $=10^{7}$


SIMPLIFIED SCHEMATIC OF BRIDGE IN OPERATE POSITION

FIGURE 11.
Operate Position, $10^{7}$ Multiplier.

## 2-9. ACCURACY CONSIDERATIONS.

a. Standard Deviation. The overall accuracy of the bridge given in the Specifications is defined as the "standard deviation" or lo-level. In a system where several components of error make up the total error, it is grossly unfair (when specifying the system) to use worst-case limits in describing accuracy. In many cases, the error so described may have a probability of less than one in a billion while human error (usually neglected in such an analysis) can easily contribute gross errors on the order of one in a thousand. It is far more reasonable to use a limit between one in a thousand ( $99.9 \%$ or 3.3 ) and one in ten thousand (99.99\% or 3.9 ) as a specification of system accuracy. If the $3 \sigma$ limits of two or more normally distributed ( ) randomly occurring components of error are summed in quadrature $\left(\sqrt{e_{1}}+\right.$ $\frac{e_{2}}{2}--\infty$ ) the sum is the 3 o error for the group. If three uniformly distributed ( $\sim \sim$ ) randomly occurring components of error have equal limits, the arithmetic sum of these limits will closely represent the 30 points of the near normal error distribution generated by the interaction of these error components. These
$3 \sigma$ limits may then be used to sum in quadrature with the $3 \boldsymbol{\sigma}$ limits of other normally distributed error components. The effect of error components which are not randomly distributed but are fixed or have a fixed rate of change (systematic errors) must be added directly to the random errors. If one component of error occurs more than once and does not have random change to have changed, it must be summed directly for the number of times occurred before being added in quadrature to other errors.
b. Error Analysis. The various factors which can be identified as sources of error include the following.

1. Bridge Arm. The errors pertaining to the bridge arm consist of the decade dial errors and the fixed arm to decade arm ratio.
a.) Decade Dial. The decade dial errors include the worst case dial setting within the decade span used, the inherent resistor error, the temperature and time stability of the resistors, and the effect of leakage resistance.

TABLE 2-2.
$3 \sigma$ Error Computation.
(All numbers in $\%$ of Reading with minimum bridge potential specified and dials between 1 and 10 ).

| Range ohms | Zero Check | Null | Temp. Coef. | Laddering |  |  |  | Bridge <br> Arms | Leakage | Total <br> Error <br> \% | $\begin{gathered} \text { Minimum } \\ \text { Bridge } \\ \text { Potential } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Volt Coef. | Temp. Coef. | Null | $\mathrm{R}_{\mathrm{a}} / \mathrm{R}_{\mathrm{b}}$ |  |  |  |  |
| $20^{5}-10^{7}$ | . 006 | . 006 | - | - | - | - | - | . 03 | . 001 | . 031 | 10 |
| $10^{7}-10^{8}$ | . 006 | . 006 | . 02 | . 04 | . 002 | . 009 | . 005 | . 03 | . 001 | . 056 | 10 |
| $10^{8}-10^{9}$ | . 006 | . 006 | . 03 | . 08 | . 004 | . 012 | . 010 | . 03 | . 001 | . 085 | 10 |
| $10^{9}-10^{10}$ | . 006 | . 012 | . 03 | . 16 | . 006 | . 015 | . 015 | . 03 | . 001 | . 17 | 10 |
| $10^{10}-10^{11}$ | . 006 | . 012 | . 04 | . 24 | . 010 | . 020 | . 020 | . 03 | . 001 | . 25 | 10 |
| $10^{11}-10^{12}$ | . 006 | . 03 | . 05 | . 48 | . 022 | . 024 | . 025 | . 03 | . 001 | . 49 | 10 |
| $10^{12} \cdot 10^{13}$ | . 006 | . 12 | . 07 | . 72 | . 064 | . 04 | . 030 | . 03 | . 001 | . 74 | 100 |
| $10^{13}-10^{14}$ | . 006 | . 24 | . 07 | . 72 | . 064 | . 04 | . 030 | . 03 | . 01 | . 77 | 500 * |
| $10^{14}-10^{15}$ | . 06 | 0.6 | . 07 | . 72 | . 064 | . 04 | . 030 | . 03 | 0.1 | 1.1 | 500 * |

[^0]b.) Fixed arm to decade arm ratio. The errors associated with the ratio accuracy include the basic Standard resistance error, the accumulative laddering error and the temperature and voltage coefficient of the Standard resistor.
2. Null Uncertainty. The errors pertaining to null uncertainty include the null detector sensitivity, the bridge voltage, the bridge ratio, and the $1 / f$ noise.
c. Error Computation.

The computation of total error at the $3 \sigma$-level is shown in Table 2-2 for each range.

## d. Error Factors.

1. Worst Case Dial Setting. For the "optimumuse range" between 1.0000 to 9.9999 , the worst case dial setting would be 1.0999 . Since each dial setting of 9 represents 3 resistors, the total contribution of dial settings .0999 would be:
$3 \sigma$ error $=\sqrt{(.005)^{2}+(.0025)^{2}+(.001)^{2} \doteq} \pm .006 \%$.
If this error is added to the base tolerance of . $01 \%$ and divided by the higher resistor value (1.0999), the result is:

$$
\% \text { error }=\frac{.016}{1.0999} \doteq .015 \%
$$

If this error is separated into components, then the uniformiy distributed error $=.01 \%$ while the normally distributed error $=.005 \%$.
2. Resistor Accuracy. The resistor accuracy for the various dials is given in Table 2-3.

TABLE 2-3.
Dial Resjstor Accuracy.

| Dial <br> Resistance | $\times 100$ | 10 | 1 | .1 | .01 | .001 | .0001 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Tolerance | $.5 \%$ | $.01 \%$ | $.01 \%$ | $.01 \%$ | $.05 \%$ | $.25 \%$ | $1 \%$ |

3. Temperature Coefficient. The temperature coefficients for the Standard resistors are given in Table $2-4$ (assuming a $\pm .5^{\circ} \mathrm{C}$ temperature).

TABLE 2-4.
Temperature Coefficient for Resistors ( $\pm \%$ ).

| Resistance $10^{5}$ | $10^{6}$ | $10^{7}$ | $10^{8}$ | $10^{9}$ | $10^{10}$ | $10^{11}$ | $10^{12}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Coefficient .00 | .00 | .02 | .03 | .03 | .04 | .05 | .07 |

4. Leakage Resistance. Leakage causes an error since the Readout Dials are shunted by approximately $10^{l l}$ ohms. The error should be added directly since it is a relatively fixed systematic error.
5. Voltage Coefficient. The voltage coefficient for each Standard resistor is given in Table 2-5.

TABLE 2-5.
Voltage Coefficient (1~10V)/V. in \%.

| Resistance | $10^{7}$ | $10^{8}$ | $10^{9}$ | $10^{10}$ | $10^{11}$ | $10^{12}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Coefficient | -.005 | -.005 | -.01 | -.01 | -.03 | -.03 |

6. Null Resolution. Null uncertainty is approximately the ratio of the smallest voltage drop across the bridge arm to the null resolution. As the bridge ratio departs from $1: 1$ the null uncertainty becomes more significant.

$$
\text { Error }=\frac{\text { Null Resolution }}{\text { Bridge Voltage }} \times\left[2+\left(\frac{1}{\text { Ratio }}\right)+\text { (Ratio) }\right]
$$

Table 2-6 gives the null uncertainty for the case where the ratio is $10: 1$ and the bridge voltage is 10V. (100:1 @ 100 V for $10^{14}$ range and 1000:1 @ 500 V for $10^{15}$ range).
7. Laddering. Laddering is the process of using the bridge to calibrate itself. Several errors compound during this process to increase the error of the bridge at higher resistances. The process consists of two modes: STANDARDIZE and CALIBRATE.

In CALIBRATE Mode: $\frac{\mathrm{R}^{6}}{\mathrm{R}^{7}}=\frac{\mathrm{B}^{6}}{\mathrm{D}}$
where $R^{6}$ is the $10^{6}$ miltiplier ( $+0.01 \%$ ) and $R^{7}$ is the 107 multiplier resistor ( $\pm 0 . \overline{0} 1 \%$ ), $B^{6}$ is the "fixed" arm associated with the $10^{6}$ multiplier and $D$ is the dial setting.
In STANDARDIZE Mode: $\frac{\mathrm{R}_{\mathrm{a}}}{\mathrm{R}_{\mathrm{b}}}=\frac{\mathrm{B}^{7}}{\mathrm{D}}$
where $R_{a} / R_{b}$ is the $1: 10$ ratio pair ( $\pm 0.005 \%$ ) and $B^{7}$ is the "fixed" arm associated with the $10^{7}$ multiplier (adjusted for proper ratio).
Thus, $B^{7}=\frac{B^{6}}{R^{6}}\left(\frac{R_{a}}{R_{b}}\right)$ at the end of the first
laddering. The dial accuracy drops from consideration and only 3 resistive error factors are included, $B^{6}, R^{6}$ and $R_{a} / R_{b}$. In addition, a nulling uncertainty at $10^{6}$ and a nulling uncertainty at low impedance (use $0.006 \%$ ) must be included.

It can be shown that further nullings give

$$
\frac{B^{8}}{R^{8}}=\frac{B^{6}}{R^{6}}\left(\frac{R_{a}}{R_{b}}\right)\left(\frac{R_{a}}{R_{b}}\right)
$$

thus adding one more $R_{a} / R_{b}$ uncertainty, one more low impedance null uncertainty and an aditional null uncertainty at $10^{7}$ ohms. The voltage across

TABLE 2-6.
Null Uncertainty-Null Detector Resolution.

| Range | $\begin{aligned} & 10^{5} \\ & \text { to } \\ & 10^{6} \end{aligned}$ | $\begin{aligned} & 10^{6} \\ & \text { to } \\ & 10^{7} \end{aligned}$ | $\begin{aligned} & 10^{7} \\ & \text { to } \\ & 10^{8} \end{aligned}$ | $\begin{aligned} & 10^{8} \\ & \text { to } \\ & 10^{9} \end{aligned}$ | $\begin{aligned} & 10^{9} \\ & \text { to } \\ & 10^{10} \end{aligned}$ | $\begin{aligned} & 10^{10} \\ & \text { to } \\ & 10^{11} \end{aligned}$ | $\begin{aligned} & 10^{11} \\ & \text { to } \\ & 10^{12} \end{aligned}$ | $\begin{aligned} & 10^{12} \\ & \text { to } \\ & 10^{13} \end{aligned}$ | $\begin{aligned} & 10^{13} \\ & \text { to } \\ & 10^{14} \end{aligned}$ | $\begin{aligned} & 10^{14} \\ & \text { to } \\ & 10^{15} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% Error | . 006 | . 006 | . 006 | . 006 | . 012 | . 012 | . 03 | . 12 | . 24 | . 6 |
| $\begin{aligned} & \text { N.D. Resolution } \\ & \pm \mathrm{mV} * \end{aligned}$ | . 05 | . 05 | . 05 | . 05 | . 10 | . 10 | . 25 | 1.0 | - | - |

[^1]the hi-meg changes from about 10 volts in "STANDARDIZE" position to about 1 volt in the next "CALIBRATE" position. Since the voltage coefficient is always negative, these errors must be added together prior to the summing procedure in quadrature with other random variable. The effect of voltage co-
efficient need only be accounted for one time. Table 2-7 shows the sum of the voltage coefficient errors on each range during laddering. For laddering the measurement time can be assumed short with respect to internal temperature changes. (The thermal time constant for the Model 515A is about 10 minutes). Table $2-8$ shows the total error for temperature changes.

TABLE 2-7.
Voltage Coefficient Errors.

| Range | $\mathrm{VC} / \mathrm{V}$ | V | VC Error |  |
| :---: | :---: | :---: | :---: | :---: |
| $10^{7}-10^{8}$ | .005 | 8 V | .04 |  |
| $10^{8}-10^{9}$ | .005 | 8 V | .04 | .04 |
| $10^{9}-10^{10}$ | .01 | 8 V | .08 |  |
| $10^{10}-10^{11}$ | .01 | 8 V | .08 |  |
| $10^{12}-10^{12}$ | .03 | 8 V | .24 | .24 |
| $10^{12}-10^{13}$ | .03 | 8 V | .24 |  |

TABLE 2-8.
Temperature Errors During Laddering.

| Range | Time to Calibrate | Temp. Change | TC | Total Error | TC * |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $10^{7}$ | 1 min | $0.05{ }^{\circ} \mathrm{C}$ | . 04 | .002\% | . 002 |
| $10^{8}$ | 1 min | $0.05^{\circ} \mathrm{C}$ | . 06 | .003\% | . 004 |
| $10^{9}$ | 1 min | $0.05^{\circ} \mathrm{C}$ | . 07 | . $0035 \%$ | . 006 |
| $10^{10}$ | 2 min | $0.1{ }^{\circ} \mathrm{C}$ | . 08 | . $008 \%$ | . 010 |
| 1011 | 5 min | $0.2{ }^{\circ} \mathrm{C}$ | . 10 | . $02 \%$ | . 022 |
| $10^{12}$ | 10 min | $0.4{ }^{\circ} \mathrm{C}$ | . 15 | .06\% | . 064 |

* TC represents the "root square sum" or total error for each range due to temperature coefficient errors during laddering.

TABLE 2-9.
Total Laddering Error

| Range | $\begin{array}{r} \text { VC } \\ \text { (a) } \end{array}$ | $\begin{gathered} \mathrm{TC} \\ \hline \end{gathered}$ | Lo 2 nulls | Hi 2 nulls | nulls <br> (a) | $B^{6} / R^{6}$ <br> (b) | $R_{a} / R_{b}$ | $\begin{aligned} & R_{a} / R_{b} \\ & (a)(c) \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $10^{7}$ | . 04 | . 002 | 2x.006\% | . 006 | $=.009$ | 2x.01 | 1x. 005 | $=.005$ |
| $10^{8}$ | . 08 | . 004 | 2x.006 | 2x.006 | $=.012$ | 2x. 01 | 2x. 005 | $=.010$ |
| $10^{9}$ | . 16 | . 006 | 3 x .006 | $3 \mathrm{x.006}$ | $=.015$ | 2 x .01 | 3 x .005 | $=.015$ |
| $1010$ | . 24 | . 010 | $4 \times .006$ | $3 \mathrm{x.006} \div .012$ | $=.020$ | 2 x .01 | 4x.005 | $=.020$ |
| $1011$ | . 48 | . 022 | $5 \times .006$ | 3x.006-2x.012 | $=.024$ | $2 \mathrm{x.01}$ | $5 x .005$ | $=.025$ |
|  | . 72 | . 064 |  | $3 \mathrm{x} .006-2 \mathrm{x} .012-.03$ | $=.040$ | 2x.01 |  |  |

(a) Normal Distribution.
(b) Uniform Distribution.
(c) $R_{a} / R_{b}$ will not change so addition of subsequent errors is direct, not in quadrature.

## SECTION 3. CIRCUIT DESCRIPTION

3-1. GENERAL. The Model 515A comprises a solid-state, guarded, electrometer null detector; an ultra-stable, highly-regulated dc voltage source, and a Wheatstone Bridge.

3-2. NULL DETECTOR. A simplified diagram of the null detector circuit is shown in Figure 12. The null detector utilizes a Keithley Model 302 Electrometer Amplifier and a $3 \mathrm{~A} / \mathrm{division} \mathrm{meter} \mathrm{(M101)}$. supplied by +12 volt regulated supplies. (See paragraph 3-4.) The Sensitivity Switch (S103) has five positions which provide sensitivity from $1000 \mathrm{mV} /$ division to $0.1 \mathrm{mV} / \mathrm{division}$. a center scale (zero) if there is no potential across the Sensitivity Switch resistors. With switch S201 set to ZERO CHECK, any offset indicated by the meter is due to the Model 302 offset voltage. By use of the COARSE (S102) and FINE (R120) zero controls the meter can be adjusted for center scale indication (thus the zero controls can be used to compensate for amplifier offset). With switch S201 set to READ, the potential difference between High and Low causes a current flow through the meter. A voltage is developed across the sensitivity resistor such that $I_{M}=e / R_{S}$, where $I_{M}=$ meter current, $R_{S}=$ sensitivity resistor and $e=u n-$ balance potential. Resistor. R102, in series with the meter, and diodes D103 and D104 are used to obtain a non-linear meter response beyond five divisions. The voltage developed across R102 will forward bias either diode so that diode so that diode conduction occurs. The current is shunted around meter thus giving a logarithmic meter sensitivity. The null de-
tector "Driven Guard" is the Common of the $\pm 12$ volt supplies. The ac potential of the "Driven Guard" follows the ac potential of the input High so that guarding of the input High can be used.

3-3. WHEATSTONE BRIDGE. The bridge circuit utilizes four resistance arms identified as Standard Resistor Arm "S", Unknown Resistor Arm 'X", Calibrated Resistance Arm "C"', and Read-out Resistance Arm "A".
a. Standard Resistor Arm. The Standard resistors R304 through R311 are connected to the Multiplier Switch S302. Resistors R304 and R305 are $0.01 \%$ wirewound types; resistors R306 and R307 are $1 \%$ deposited carbon types; resistors R308 through R311 are specially selected High-Meg types. A $10: 1$ (.005\%) ratio divider composed of R301 and R302 is used in the Standardization procedure. (See paragraph 2-4).
b. Unknown Resistor Arm. The unknown resistance " X " is connected at the Input connector (J302 or J303).
c. Calibrated Resistance Arm. The calibrated resistance arm consists of a $94.5 \mathrm{kilohm}, 1 \%$ deposited carbon type in series with a 10 kilohm , wirewound variable resistor. Resistors R313 through R318 and potentiometers R319 through R324 are connected to the Multiplier Switch S302. The Calibration potentiometers can be adjusted during the Standardization procedure and are accessible on the front panel (inside the shielded enclosure).
d. Readout Resistance Arm. The Readout Arm is composed of Resistance Dials S304 through S310.


FIGURE 12. Null Detector.

3-4. POWER SUPPLY. The poyer supply consists of a series regulated supply for Bridge Voltage and a floating $\pm 12 \mathrm{~V}$ supply for the null detector circuitry. T201 is the power transformer operating from power line, switch selectable for $117 \mathrm{~V}-234 \mathrm{~V}$ operation. One secondary is center-tapped and supplies a floating plus and minus voltage for the regulator amplifier. This secondary also drives the isolation transformer T101. The other secondary is full wave rectified to supply the unregulated voltage to series pass transistor Q206. Q201 and Q202 form a difference amplifier which compares the regulated output voltage to a reference voltage supplied by $D 203$ in a resistance programmable power supply with the Bridge volts Adjustment setting a lma current thru the reference divider string. Q203 and Q204 are used as amplifier and driver for Q206, correcting for any change in load current or line voltage. The secondary of Tlll is center-tapped and full-wave rectified to supply unregulated plus and minus voltage to Q101 and Q102 respectively which supply a constant load current. Zener diodes D103 and D104 set the null detector supply voltages to a nominal $\pm 12$ volts respectively. Tlol is especially well insulated to provide the necessary insulation of guard to ground in the bridge circuit.

3-5. OVER-VOLTAGE PROTECTION CIRCUIT. The Model 515A utilizes a zener diode (D301) to prevent damage to the readout resistors ( Xl and lower) from excessive bridge voltage from an external voltage source. The diode is connected (through auxiliary contacts on the X100 and Xlo dials) across the bridge voltage terminals when in

External Voltage mode only. Thus if both dials are set to zero the diode is directly across the bridge. For an external voltage greater than 100 volts, the zener will conduct. When using a current-limited voltage supply (such as Keithley Models 240A or 241) the diode will limit the voltage to 100 volts and prevent over-heating of the Dial resistors.

## WARNING

If the voltage supply used does not have current limiting ( 10 mA approximately), the zener protection diode could be overheated causing possible damage to the Dial resistors.


FIGURE 13. Null Detector, PC-233.


FIGURE 14. Bridge Voltage Supply, PC-244.

## SECTION 4. ACCESSORIES

4-1, GENERAL. The following Keithley accessories can be used with the Model 515A to provide additional convenience and versatility.

4-2. OPERATING INSTRUCTIONS. A separate Instruction Manual is supplied with each accessory giving complete operating information.

## Model 5151 End Frames

Description:
The Model 5151 is a bench mounting kit. The end frames provide convenience when carrying the instrument.


Model 5153 Triaxial Cable

Description:
The Model 5153 is a triaxial cable $60^{\prime \prime}$ long which mates with the EXT. INPUT connector on the Model 515A.

## Application:

The Model 5153 can be used for external measurements which require a shielded and guarded cable.

Model 5152 Remote Test Chamber

Description:
The Model 5152 is a shielded test chamber for remote resistance measurements. A 60 inch triaxial cable is provided.

Application:

The Model 5152 can be used for resistance measurements when the self-contained test compartment on the Model 515A is not useable. A separate GUARD terminal is provided on the Test Chamber.


Model 241 Regulated High Voltage Supply
Description:
The Model 241 is a very stable, accurate high voltage power supply especially useful as a laboratory reference.

Application:
The Model 241 can be used as an external voltage supply for the Model 515 A when applications require a bridge potential from 110 V to 1000 V . The Model 241 can be easily rack mounted with the Model 515 A by use of the Model 5154 Cabinet.

## Specifications:

OUTPUT:
Voltage: 0 to 1000 volts dc in 0.01 -volt steps.
Current: 20 milliamperes $d c$ maximum.
Polarity: Positive or negative.
Floating: 50 volts maximum off chassis ground.
ACCURACY: $\pm 0.05 \%$ of dial setting or $\pm 1$ millivolt, whichever is greater.
RESOLUTION: A "Trim" potentiometer permits interpolation between steps with a resolution of better than 100 microvolts.
RESETABILITY: $+0.025 \%$.
STABILITY: $\pm 0 . \overline{0} 05 \%$ per hour with constant load, line and ambient temperature.
TEMPERATURE COEFFICIENT OF REFERENCE: $\pm 10 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$.
LINE REGULATION: $\pm 0.005 \%$ or 1 millivolt for $10 \%$ line change.
LOAD REGULATION: $\pm 0.005 \%$ from no load to full load.
RIPPLE AND NOISE: Less than 1 millivolt rms above 5 Hz .
OUTPUT IMPEDANCE: Less than 0.05 ohm at dc.
RECOVERY TIME: No load to full load, less than 1 sec ond to rated accuracy.
OVERLOAD PROTECTION: Output is disconnected within 50 milliseconds if current exceeds approximately 24 mili iamperes.
CONNECTORS: Output: Teflon-insulated type UHF type.
POWER: $105-125$ or $210-250$ volts, $50-60 \mathrm{~Hz}, 105$ watts. DIMENSIONS, WEIGHT: $7^{\prime \prime}$ high $\times 19^{\prime \prime}$ wide $\times 12^{\prime \prime}$ deep, net weight, 26 pounds.
ACCESSORIES SUPPLIED: Mating connectors.


## Model 5154 Cabinet

Description:
The Model 5154 is a rack style cabinet with dimensions $25^{\prime \prime}$ high $x 21^{\prime \prime}$ wide $x$ 16-1/2" deep.

Application:
The Model 5154 can be used to rack mount the Model 515A with an auxilliary power supply such as the Keithley Model 241.


## Parts List:

Item
No.
Description
Part No.

| 1 | Cabinet | 14343 C |
| :--- | :--- | :--- |
| 2 | Panel, Blank | 14203 B |
| 3 | Cable, UHF-UHF | 16639 B |

Description:
The Model 5155 has been developed to verify the calibration of the Keithley 515A Megohm Bridge with traceability to the National Bureau of Standards. These units are convenient to use, since they plug directly into the 515A. The 5155 consists of six individually encased high megohm resistors with values of $10^{8}$ through $10^{13}$ ohms in decade steps. A certificate is included showing the actual value of each resistor with an accuracy limited by the maximum accuracy certified by National Bureau of Standards. Each resistor's temperature coefficient, voltage coefficient and history of measured values is also given.

Specifications:
RESISTOR VALUES: Six resistors $10^{8}, 10^{9}, 10^{10}, 10^{11}$, $10^{12}, 10^{13}$ ohms $+15 \%$.
ACCUPACY: $\pm 0.2 \%$ of certified value except $10^{13}$ ohms which is $\pm 0.5 \%$ (relative to N.B.S. certified standards).
STABILITY: Less than $\pm 0.1 \%$ change in value per thousand hours.
VOLTAGE COEFEICIENT: $-.03 \%$ per volt, nominal.
TEMPERATURE COEFFICIENT: $-0.1 \%$ per ${ }^{\circ} \mathrm{C}$, nominal.
GUARDING: Case is at guard potential when the resistor Standard is used in a Keithley Model 5l5A Megohm Bridge.
INSULATION: Teflon.

DIMENSIONS: Each resistor standard is $4^{\prime \prime}$ long x $2^{\prime \prime}$ deep $x 1^{\prime \prime}$ wide.
WEIGHT: Each resistor Standard is approximately 6 ounces. Six Standards in carrying case, 3-1/2 1bs.
SERVICE AVAILABLE: Recertification traceable to National Bureau of Standards.


Resistor Installation:


## SECTION 5. REPLACEABLE PARTS

5-1. REPLACEABLE PARTS LIST: This section contains a list of componenets used in this instrument for user reference. The Replaceable Parts List describes the individual parts giving Circuit Designation, Description, Suggested Manufacturer (Code Number),

Manufacturer's Part Number, and the Keithley Part Number. Also included is a Figure Reference Number where applicable. The complete name and address of each Manufacturer is listed in the CODE~TO-NAME Listing following the parts list.

TABLE 5-1.
Abbreviations and Symbols


5-2. ELECTRICAL SCHEMATICS AND DIAGRAMS. Schematics and diagrams are included to describe the electrical circuits as discussed in Section 3. Table 5-2 identifies all schematic part numbers included.

5-3. HOW TO USE THE REPLACEABLE PARTS LIST. This Parts List is arranged such that the individual types of components are listed in alphabetical order. Main Chassis parts are listed followed by printed circuit boards and other subassemblies.

## 5-4. HOW TO ORDER PARTS.

a. Replaceable parts may be ordered through the

Sales Service Department, Keithley Instruments, Inc. or your nearest Keithley representative.
b. When ordering parts, include the following information.

1. Instrument Model Number.
2. Instrument Serial Number.
3. Part Description.
4. Schematic Circuit Designation.
5. Keithley Part Number,
c. All parts listed are maintained in Keithley Spare Parts Stock. Any part not listed can be made available upon request. Parts identified by the Keithley Manufacturing Code Number 80164 should be ordered directly from Keithley Instruments, Inc.

TABLE 5-2.

| Description | Circuit Designation | Schematic |
| :---: | :---: | :---: |
| Megohm Bridge | PC-233, PC-244 | 24820 E |

NULL DETECTOR PARTS LIST
(PC-233)
CAPACITORS

| Circuit Desig. | Value | Rating | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{array}{r} \text { Fig. } \\ \text { Ref. } \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{ClO1}$ | . $02 \mu \mathrm{~F}$ | 1000 V | CerD | 56289 | 10ss-S20 | C64-.02M | - |
| C102 | Not Used | -- | -- | -- | -- | -- |  |
| C103 | $100 \mu \mathrm{~F}$ | 40 | EAL | 73445 | C437AR/G100 | C150-100M | 13 |
| C104 | 100 感 | 40 | EAL | 73445 | C437AR/G100 | C150-100M | 13 |

diodes

| Circuit Desig. | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. | $\begin{aligned} & \text { Fi.g. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D101 | Transistor, NPN, Case To-106 | 07263 | 2N3565 | TG-39 | - |
| D102 | Transistor, NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | - |
| D103 | Silicon | 01295 | 1 N 645 | RF-14 | 13 |
| D104 | Silicon | 01295 | 1N645 | RF-14 | 13 |
| D105 | Zener | 12954 | 1N706 | D2-1 | 13 |
| D106 | Zener | 12954 | 1N706 | DZ-1 | 13 |
| D107 | Silicon | 01295 | 1N645 | $\mathrm{RF}-14$ | 13 |
| D108 | Silicon | 01295 | 1N645 | RF-14 | 13 |
| D109 | Silicon | 01295 | 1N645 | RF-14 | 13 |
| D110 | Silicon | 01295 | 1N645 | RF-14 | 13 |
| D111 | (TG-39*) Transistor, NPN, Case T0-106 | 07263 | 2N3565 | 24220A* | - |
| D112 | (TG-39*) Transistor, NPN, Case T0-106 | 07263 | 2N3565 | 24220A* | - |

*Selected. Order from factory.
MISCELLANEOUS PARTS

| Circuit Desig. | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| T101 | Transformer | 801.64 | --- | TR-121 | 14 |
| M101 | Meter | 80164 | --- | ME-86 | - |
| S102 | Rotary Switch, COARSE ZERO | -... | -.- | SW-294 | - |
| S103 | Rotary Switch, Null Detector Sensivity | --- | --- | SW-292 | - |
| Plol | Connector, Male, 15 Pins | 27264 | 1625-15P | CS-227 | - |
| J101 | Connector, Female, 15 Pins | 27264 | 1625-15R | CS-228 | - |
| J102 | Connector, Female, 15 Pins | 27264 | 1625-15R | CS-228 | - |
| P102 | Connector, Male, 15 Pins | 27264 | 1625-15P | CS-227 | - |

RESISTORS

| Circuit <br> Desig. | Value | Rating | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. <br> Ref. |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  |  | M $\Omega$ | $10 \%, 1 / 2 \mathrm{~W}$ | Comp | 01121 | EB-10M |

## RESISTORS (cont ${ }^{\prime} \mathrm{d}$ )

| $\begin{aligned} & \text { Circuit } \\ & \text { Desig. } \\ & \hline \end{aligned}$ | Value |  | Rating |  | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R106 | 33.3 | $\Omega$ | 1\%, 1/2 | w | MtF | 07716 | CEC-33.3k | R94-33.3K | - |
| R107 | 33.3 | $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC- $33.3 \mathrm{k} \Omega$ | R94-33.3K | - |
| R108 | 2.7 | ks* | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-2.7k | R12-2.7K | 13 |
| R109 | 1 | k $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k ${ }^{\text {d }}$ | R94-1K | - |
| R110 | 1 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k $\Omega$ | R94-1K |  |
| R111 | 1 | $k \Omega$ | 1\%, 1/2 | w | MtF | 07716 | CEC-1k 8 | R94-1K | - |
| R112 | 1 | $k \Omega$ | 1\%, 1/2 | w | MtF | 07716 | CEC-1k | R94-1K | - |
| R113 | 1 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k 2 | R94-1K | - |
| R114 | 1 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k $\Omega$ | R94-1K | - |
| R115 | 1 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k ${ }^{\text {d }}$ | R94-1K | - |
| $R 116$ | 1 | k $\Omega$ | 1\%, 1/2 | w | MtF | 07716 | CEC-1k $\Omega$ | R94-1K | - |
| R117 | 1 | k ת | 1\%, 1/2 | W | MtF | 07716 | CEC-1k $\Omega$ | R94-1K | - |
| $R 118$ | 1 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k $\Omega$ | R94-1K | - |
| R119 | 1 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k 2 | R94-1K | - |
| R120 | 10 | $k \Omega$ | 5\%, 2 | W | WWVar | 12697 | $62 \mathrm{JA}-10 \mathrm{k} \Omega$ | RP42-10K | - |
| R121 | 4.7 | $k \Omega$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-4.7k | R12-4.7K | - |
| R122 | 2.7 | $k \Omega *$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-2.7k $\Omega$ | R12-2.7K | 13 |
| R123 | 700 | $\Omega$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-700 | R12-700 | 13 |
| R124 | 4.99 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-4.99k | R94-4.99K | 13 |
| R125 | 4.99 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-4.99k $\Omega$ | R94-4.99K | 13 |
| R126 | 700 | $\Omega$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-700 | R12-700 | 13 |
| R127 | 15k | $\Omega$ | 1\%, 1/8 | W | MtF | 07716 | CEA-15k-1\% | R88-15K | - |
| *Nomin | lue, | selec | in final | tes |  |  |  |  |  |

TRANSISTORS

| Circuit <br> Desig. | Type | Mfr. <br> Code | Mfr. <br> Part | Noithley <br> Part No. | Fig. <br> Ref. |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Q101 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 13 |
| Q102 | NPN, Case T0-106 | 07263 | 2N3565 | TG-39 | 13 |

BRIDGE VOLTAGE SUPPLY PARTS LIST
(PC-244)
CAPACITORS

| Circuit Desig. | Value | Rating | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C201 | $0.5 \mu \mathrm{~F}$ | 400 V | My | 13050 | SM1A-0.5 F F | C117-. 5M | 14 |
| C202 | . $0015 \mu \mathrm{~F}$ | 600 V | CerD | 72982 | ED-. 0015 | C22~.0015M | 14 |
| C203 | 0.1 HF | 400 V | My | 13050 | SM1A-0.14F | C73-.1M | 14 |
| C204 |  | 40 V | EAL | 73445 | C437AR/G100 | C150-100M | 14 |
| C205 | 100 F | 40 V | EAL | 73445 | C437AR/G100 | C150-100M | 14 |
| C206 | 100 MF | 40 V | EAL | 73445 | C437AR/G100 | C150-100M | 14 |
| C207 | 100 HF | 40 V | EAL | 73445 | C437AR/G100 | C150-100M | 14 |
| C208 | Not Used |  |  |  |  |  |  |
| C209 | $20 \quad \mu \mathrm{~F}$ | 450 V | EMC | 37942 | FP144-20 ${ }^{\text {F }}$ | C36-20M | 14 |
| C210 | 100 HF | 40 V | EAL | 73445 | C437AR/G100 | C150-100M | 14 |
| C211 | $0.047 \mu \mathrm{~F}$ | 100 V | Poly | - | MW9410473 | C67-0.047M | - |


| Circuit Desig. | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| D201 | Silicon | 02735 | 1N3255 | RF-17 | 14 |
| D202 | Silicon | 02735 | 1N3255 | RF-17 | 14 |
| D203 | Zener | 04713 | 1 N936 | D2-5 | 14 |
| D204 | Zener | 12954 | 1N718 | D2-18 | 14 |
| D205 | Zener | 12954 | 1N706 | DZ-1 | 14 |
| D206 | Zener | 12954 | 1N718 | D2-18 | 14 |
| D207 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D208 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D209 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D210 | Silicon | 01295 | 1N645 | RF-14 | 1.4 |
| D211 | Not Used | -- | -- | -- | - |
| D212 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D213 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D214 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D215 | Zener | 12954 | 1N723 | D2-17 | 14 |
| D216 | Zener | 12954 | 1N723 | D2-17 | 14 |
| D217 | Silicon | 02735 | 1N3255 | RF-17 | 14 |
| D218 | Silicon | 02735 | 1N3255 | RF-17 | 14 |
| D219 | Silicon | 02735 | 1N3255 | RF-17 | 14 |
| D220 | Silicon | 02735 | 1N3255 | RF-17 | 14 |
| D221 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D222 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D223 | Silicon | 01295 | 1N645 | RF-14 | 14 |
| D224 | Silicon | 01295 | 1N645 | RF-14 | 14 |

MISCELLANEOUS PARTS

| Circuit Desig. | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. | $\begin{aligned} & \text { Fig. } \\ & \text { Ref. } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| J211 | Receptacle, UHF | 91737 | 6804 | CS-64 | - |
| S201 | Toggle Switch, ZERO CHECK | 80164 | --- | SW-236 | 2 |
| J201 | Test. Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J202 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J203 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J204 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J205 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J206 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J207 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J208 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J209 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| J210 | Test Jack | 71279 | 4352-1-0319 | TJ-9 | 3 |
| SL201 | Shorting Link | 71279 | 3771-20310 | TJ-10 | 3 |
| SL201 | Shorting Link | 71279 | 3771-20310 | TJ-10 | 3 |
| S203 | Rotary Switch, X1 BRIDGE VOLTS | 80164 | --- | SW-291 | 2 |
| S202 | Rotary Switch, Xl0 BRIDGE VOLTS | 80164 | --- | SW-291 | 2 |
| K201a | Solenoid, ZERO CHECK | --- | E155 | SOL-2 |  |
| K201b | Reed Relay, SPST | 95348 | MR406 | RL-25B | - |
| T201 | Transformer | 80164 | TR-120 | TR-120 | 14 |
| K202 | Relay, INTERLOCK | --- | KA11DY | RL-36 | - |


| Circuit Desig. | Value |  | Rating |  | Type | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R201 | 56 | $\Omega$ | 10\%, 1/2 | W | Corap | 01121 | EB-56 ${ }^{\text {d }}$ | R1-56 | 14 |
| R202 | 20 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-20k $\Omega$ | R94-20K | 14 |
| R203 | 10 | k $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-10k | R94-10K | 14 |
| R204 | 40.2 | k $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-40.2k $\Omega$ | R94-40.2K | 14 |
| R205 | 40.2 | k $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-40.2k $\Omega$ | R94-2K | 14 |
| R206 | 2 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-2k | R94-2K | 14 |
| R207 | 1 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-1k | R94-1K | 14 |
| R208 | 4.02 | $k \Omega$ | 1\%, $1 / 2$ | W | MtF | 07716 | CEC-4.02k $\Omega$ | R94-4.02K | 14 |
| R209 | 4.02 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-4.02k $\mathrm{S}_{8}$ | R94-4.02K | 14 |
| R210 | 8.06 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-8.06k $\Omega$ | R94-8.06K | 14 |
| R211 | 2 | $k \Omega$ | 20\%, 2 | W | WWVar | 71450 | 1NS-115-2k8 | RP-50-2K | 14 |
| R212 | 10 | $k \Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-10k | R1-10 | 14 |
| R213 | 40.2 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-40.2k $\Omega$ | R94-40.2K | 14 |
| R214 | 40.2 | k $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-40.2k $\Omega$ | R94-40.2K | 14 |
| R215 | 1 | $k \Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-1k ? | R1-1K | 14 |
| R216 | 47 | $k \Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-47k $\Omega$ | R1-47K | 14 |
| R217 | 10 | $k \Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-10k $\Omega$ | R1-10K | 14 |
| R218 | 47 | $\mathrm{k} \Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-47k $\Omega$ | R1-47K | 14 |
| R219 | 2 | $k \Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-2k8 | R94-2K | 14 |
| R220 | 47 | $k \Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-47k ${ }^{\text {d }}$ | R1-47 | 14 |
| R221 | 6 | $k \Omega$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-6k8 | R12-6K | 14 |
| R222 | 500 | $\Omega$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-500 | R12-500 | 14 |
| R223 | 6 | $k \Omega$ | 1\%, 1/2 | w | DCb | 91637 | DCF-1/2-6k $\Omega$ | R12-6K | 14 |
| R224 | 100 | $\Omega$ | 1\%, 1/2 | W | DCb | 91637 | DCF-1/2-100 | R2-100 | 14 |
| R225 | 15 | $\Omega$ | 10\%, 1/2 | W | Comp | 01121 | EB-158 | R1-15 | 14 |
| R226 | 68 k | $\mathrm{k} \Omega$ | 1\%, 1/2 W |  | DCb | 91637 | DCF-1/2-68k $\Omega$ | R12-68K | 14 |
| R227 | 4.7 | $\mathrm{k} \Omega$ | 1\%, 1/2 |  | DCb | 91637 | DCF-1/2-4.7k | R12-4.7K | 14 |
| R228 | 1 k | $\mathrm{k} \Omega$ | 1\%, 1/2 W |  | DCb | 91637 | DCF-1/2-1k | R12-1K | 14 |
| R229 | 1 k | $k \Omega$ | 1\%, 1/2 |  | DCb | 91637 | DCF-1/2-1k | R12-1K | 14 |
| R230 | 700 | $\Omega$ | 1\%, 1/2 W |  | DCb | 91637 | DCF-1/2-700: | R12-700 | 14 |

TRANSISTORS

| Circuit <br> Desig. | Type | Mfr. Code | Mf. <br> Part No | Keithley <br> Part No. | Fig. Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Q201 | NPN, Case TO-18 | 73445 | A1380 | TG-32 | 14 |
| Q202 | NPN, Case T0-18 | 73445 | A1380 | TG-32 | 14 |
| Q203 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 14 |
| Q204 | NPN, Case T0-106 | 07263 | 2N: 65 | TG-39 | 14 |
| Q205 | NPN, Case T0-106 | 07263 | 2N:565 | TG-39 | 14 |
| Q206 | NPN, Case T0-5 | 02735 | 40327 | TG-63 | 14 |
| Q207 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 14 |
| Q208 | PNP, Case R-110 | 07263 | S17638 | TG-33 | 14 |
| Q209 | PNP, Case TO-5 | 02734 | 40319 | TG-50 | 14 |
| Q210 | PNP, Case T0-5 | 02734 | 40319 | TG-50 | 14 |
| Q211 | NPN, Case TO-5 | 0.2 .734 | 40317 | TG-43 | 14 |

SWITCHING ASSEMBLIES
MISCELLANEOUS PARTS

| Circuit <br> Desig. | Type | Mfr. <br> Code | Mfr. <br> Part | No. <br> Part |
| :--- | :--- | :--- | :--- | :--- |
| D301 | Diode, Zener, loov, 5W |  |  |  |

RESISTORS

| Circuit Desig. | Value |  | Rating |  | Type |  | Mfr. <br> Code | Mfr. <br> Part No. | Keithley Part No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R301 | 10 k | $k \Omega\}$ | 10:1 Div | ider | Network, | .005\% | 80164 | -- | 23685 |
| R302 | 100 k | $k \Omega$ |  |  |  |  |  |  |  |
| R303 | 10 | k? | 1\%, 1/2 | W | MtF |  | 07716 | CEC-10k $\Omega$ | R94-10K |
| R304 | 100 k | $k \Omega$ | . $01 \%, 1$ | W | WW |  | 15909 | 1252-100ks | R154-100K |
| R305 | M | M $\Omega$ | . $01 \%, 1$ | W | Ww |  | 15909 | 1252-1M 8 | R154-1M |
| R306 | 10 | M $\Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-10M 8 | R12-10M |
| R307 | 100 M | $\mathrm{M} \Omega$ | 1\%, 2 | W | DCb |  | 91637 | DC-2-100M | R14-100M |
| R308 | $10^{9}$ | $\Omega$ | Selected |  | --- |  | 80164 | --- | 24159A |
| R309 | $10^{10}$ | $\Omega$ | Selected |  | --- |  | 80164 | --- | 24160A |
| R310 | 1011 | $\Omega$ | Selected |  | --- |  |  | --- | 24161A |
| R311 | $10^{12}$ | $\Omega$ | Selected |  | --- |  | 80164 | --- | 24162A |
| R312 | 100 | $\mathrm{k} \Omega$ | .01\%, 1 | W | WW |  | 15909 | 1252-100k $\Omega$ | R154-100K |
| R313 | 94.5 | k $\Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-94.5k $\Omega$ | R12-94.5K |
| R314 | 94.5 k | k $\Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-94.5k $\Omega$ | R12-94.5K |
| R315 | 94.5 | $k \Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-94.5k 2 | R12-94.5K |
| R316 | 94.5 | $k \Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-94.5k 8 | R12-94.5K |
| R317 | 94.5 | k $\Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-94.5k $\Omega$ | R12-94.5K |
| R318 | 94.5 | $\mathrm{k} \Omega$ | 1\%, 1/2 | W | DCb |  | 91637 | DCF-1/2-94.5k 8 | R12-94.5K |
| R319 | 10 | $\mathrm{k} \Omega$ | 20\%, 1/4 | W | DCb |  | 71450 | $45-10 \mathrm{k} \Omega$ | RP81-10K |
| R320 | 10 | $k \Omega$ | 20\%, 1/4 | W | DCb |  | 71450 | $45-10 \mathrm{k} \Omega$ | RP81-10K |
| R321 | 10 | k $\Omega$ | 20\%, 1/4 | W | DCb |  | 71450 | $45-10 \mathrm{ks}$ | RP81-10K |
| R322 | 10 | $k \Omega$ | 20\%, 1/4 | W | DCb |  | 71450 | $45-10 \mathrm{k} \Omega$ | RP81-10K |
| R323 | 10 | $\mathrm{k} \Omega$ | 20\%, 1/4 | W | DCb |  | 71450 | $45-10 \mathrm{k} \Omega$ | RP81-10K |
| R324 | 10 | k $\Omega$ | 20\%, 1/4 | W | DCb |  | 71450 | 45-10k8 | RP81-10K |
| R325 | 20 | $\mathrm{M} \Omega$ | . $5 \%, 2$ | W | DCb |  | 03888 | PT2000-20M | R52~20M |
| R326 | 10 | $\mathrm{M} \Omega$ | . $5 \%, 2$ | W | DCb |  | 03888 | PT2000-10M ${ }^{\text {a }}$ | R52-10M |
| R327 | 40 | $\mathrm{M} \Omega$ | . $5 \%, 2$ | W | DCb |  | 03888 | PT2000-40M | R52-40M |
| R328 | 40 | M $\Omega$ | . $5 \%, 2$ | W | DCb |  | 03888 | PT2000-40M | R52-40M |
| R329 | 2 | $\mathrm{M} \Omega$ | .01\%, 2 | W | WW |  | 15909 | 1179-2M | R155-2M |
| R330 | 1 | $\mathrm{M} \Omega$ | .01\%, 2 | W | WW |  | 15909 | 1179-1M8 | R155-1M |
| R331 | 4 | $\mathrm{M} \Omega$ | . $01 \%, 2$ | W | WW |  | 15909 | 1179-4M | R155-4M |
| R332 | 4 | M $\Omega$ | .01\%, 2 | W | WW |  | 15909 | 1179-4M | R155-4M |
| R333 | 200 | $k \Omega$ | .01\%, 1 | W | WW |  | 15909 | 1252-200ks | R154-200K |
| R334 | 100 | $k \Omega$ | . $01 \%$, 1 | W | WW |  | 15909 | 1252-100k | R154-100K |
| R335 | 400 | $k \Omega$ | .01\%, 1 | W | WW |  | 15909 | 1252-400k $\Omega$ | R154-400K |

## RESISTORS (cont'd)

| Circuit <br> Desig. | Value |  | Rating |  | Type | Mfr. Code | Mfr. <br> Part No. | Keithley <br> Part No. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R336 | 400 | $k \Omega$ | . $01 \%, 1 \mathrm{~W}$ |  | WW | 15909 | 1252-400k $\Omega$ | R154-400K |
| R337 | 20 | $k \Omega$ | .01\%, 1 W |  | WW | 15909 | 1252-20k $\Omega$ | R154-20K |
| R338 | 10 | $k \Omega$ | . $01 \%$, 1 W |  | WW | 15909 | 1252-10k $\Omega$ | R154-10K |
| R339 | 40 | $k \Omega$ | . $01 \%, 1 \mathrm{~W}$ |  | WW | 15909 | 1252-40k $\Omega$ | R154-40K |
| R340 | 40 | $k \Omega$ | . $01 \%, 1 \mathrm{~W}$ |  | WW | 15909 | $1252-40 \mathrm{k} \Omega$ | R154-40K |
| R341 | 2 | k $\Omega$ | .04\%, 1/2 | W | WW | 01686 | 1142-2k $\Omega$ | R99-2K |
| R342 | 1 | $k \Omega$ | . $04 \%, 1 / 2$ | W | WW | 01686 | 1142-1k $\Omega$ | R99-1K |
| R343 | 4 | k $\Omega$ | . $04 \%$, 1/2 | w | WW | 01686 | $1142-4 \mathrm{k} \Omega$ | R99-4K |
| R344 |  | $k \Omega$ | . $04 \%, 1 / 2$ | W | WW | 01686 | $1142-4 \mathrm{k} \Omega$ | R99-4K |
| R345 | 200 | $\Omega$ | . $1 \%, 1 / 2$ | W | MtF | 07716 | CECT1-2008 | R135-200 |
| R346 | 100 | $\Omega$ | . $1 \%, 1 / 2$ | W | MtF | 07716 | CECT1-1008 | R135-100 |
| R347 | 400 | $\Omega$ | . $1 \%, 1 / 2$ | W | MtF | 07716 | CECT1-4008 | R135-400 |
| R348 | 400 | $\Omega$ | . $1 \%, 1 / 2$ | w | MtF | 07716 | CECT1-400』 | R135~400 |
| R349 | 20 | $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-208 | R94-20 |
| R350 | 10 | $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-10 | R94-10 |
| R351 | 40 | $\Omega$ | 1\%, $1 / 2$ | W | MtF | 07716 | CEC-40л | R94-40 |
| R352 | 40 | $\Omega$ | 1\%, 1/2 | W | MtF | 07716 | CEC-40л | R94-40 |
| R353 | 100 | M $\Omega$ | 1\%, 2 | W | DCb | 91637 | DC2-100M $\Omega$ | R14-100M |
| SWITCHES |  |  |  |  |  |  |  |  |
| Circuit Desig. | Type |  |  |  |  | Mfr. Code | $\begin{aligned} & \text { Mfr. } \\ & \text { Part } \\ & \hline \end{aligned}$ | Keithley <br> Part No. |
| S301 | Rotary Switch, function |  |  |  |  | 80164 | --- | SW-293 |
| S302 | Rotary Switch, MULTIPLIER |  |  |  |  | 80164 | $\cdots$ | SW-335 |
|  | Knob Assembly, MULTIPLIER |  |  |  |  | 80164 | --" |  |
| S303 | Safety Interlock |  |  |  |  |  |  | SW-94 |
| S304 | Rotary Switch, X100 |  |  |  |  | 80164 | --- | SW-295 |
| --. | Knob Assembly, X100 |  |  |  |  | 80164 | --- | 14829A |
| S305 | Rotary Switch, X10 |  |  |  |  | 80164 | --- | SW-295 |
|  | Knob Assembly, Xlo |  |  |  |  | 80164 | --- | 14829A |
| S306 | Rotary Switch, Xl |  |  |  |  | 80164 | --- | SW-296 |
|  | Knob Assembly, X1 |  |  |  |  | 80164 | -- | 14829A |
| S307 | Rotary Switch, X. 1 |  |  |  |  | 80164 | --- | SW-296 |
|  | Knob Assembly, X. 1 |  |  |  |  | 80164 | --- | 14829A |
| S308 | Rotary Switch, X. 01 |  |  |  |  | 801.64 | --- | SW-296 |
|  | Knob Assembly, X. 01 |  |  |  |  | 80164 | --- | 14829A |
| S309 | Rotary Switch, X. 001 |  |  |  |  | 80164 | --- | SW-296 |
|  | Knob Assembly, X. 001 |  |  |  |  | 80164 | --- | 14829A |
| S310 | Rotary Switch, X. 0001Knob Assembly, X. 0001 |  |  |  |  | 80164 | --- | SW-296 |
|  |  |  |  |  |  | 80164 | --- | 14829A |
| S311 | Knob Assembly, X. 0001Rotary Switch, BRIDGE VOLTS |  |  |  |  | 80164 | -~ | 5W-297 |
|  | Knob Assembly, BRIDGE VOLTSSlide Switch, 117-234V |  |  |  |  | 80164 | --- | 14838A |
| S312 |  |  |  |  |  | 80164 | -~- | SW-151 |

## CODE-TO-NAME LIST

CODE TO NAME List of Suggested Manufacturers
Reference: Federal Supply Code for Manufacturers, Cataloging Handbook h4-2.

| 00656 | Aerovox Corp. <br> 740 Belleville Ave. <br> New Bedford, Mass. 02741 | 07137 | Transistor Electronics Corp. Hwy. 169 - Co. Rd. 18 Minneapolis, Minn. 55424 | 14659 | Sprague Electric Co. P.O. Box 1509 <br> Visalia, Calif. 93278 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 00686 | Film Capacitors, Inc. 100 Eighth St. Passaic, N.J. | 07263 | Fairchild Camera \& Inst. Corp. 313 Frontage Road Mountain View, Calif. | 15238 | ITT Semiconductors Div. of ITT Corp. Lawrence, Mass. 01841 |
| 01121 | Allen-Bradley Corp. 1201 South 2nd St. Milwaukee, Wisc. 53204 | 07716 | IRC, Inc. <br> 2850 Mt. Pleasant <br> Burlington, Lowa 52601 | 15909 | Daven Div, of T,A. Edison Ind. McGraw Edison Co. Livingston, N.J. |
| 01295 | Texas Instruments, Inc. <br> Semiconductor-Components Div. <br> Dallas, Texas 75231 | 0881.1 | GL Electronics Div. of GL Industries, Inc. Westville, N.J. 08093 | 16170 | Teledyne Systems Co. Communications Div. Los Angeles, Calif. 90066 |
| 01686 | RCL Electronics, Inc. 195 McGregor St. <br> Manchester, N.H. 03102 | 09052 | Gulton Industries, Inc. Alkaline Battery Div. Metuchen, N.J. | 175.54 | Components, Inc. <br> Smith St. <br> Biddeford, Ma. 04005 |
| 02101 | Varo Inc. <br> Electrokinetics Div. <br> Santa Barbara, Calif. 93102 | 09823 | Burgess Battery Co. Div. of Servel Inc. Freeport, Ill. | 23020 | General Reed Co. 174 Main St. <br> Metuchen, N.J. 08840 |
| 02660 | Amphenol Corp. 2801 South 25th Ave. Broadview, Ill. 60153 | 09922 | Burndy Corp. <br> Richards Ave. <br> Norwalk, Conn. 06852 | 24655 | General Radio Co. 22 Baker Ave. West Concord, Mass. 01781 |
| 02734 | Radio Corp. of America Defense Electronic Products Camden, N.J. | 10582 | CTS of Asheville Inc. Mills Gap Road Skyland, N.C. | 27682 | Hathaway Instruments, Inc. 5800 E. Jewe 11 Ave. <br> Denver, Colorado 80222 |
| 02735 | Radio Corp, of America Receiving Tube Div. Somerville, N.J. | 11502 | IRC Inc. <br> Greenway Road Boone, N.C. 28607 | 28520 | Heyman Mfg. Co. 147 N. Michigan Ave. Kenilworth, N.J. |
| 02777 | Hopkins Engineering Co. 12900 Foothill Blvd. <br> San Fernando, Calif. 91342 | 11837 | Electro Scientific Indus., Inc. 13645 NW Science Park Dr. <br> Portland, Or. 97229 | 29309 | Richey Electronics Inc. 1307 Dickerson Rd. Nashvilie, Tenn, 37213 |
| 02985 | Tepro Electric Corp. 5 St. Paul St. <br> Rochester, N.Y. 14604 | 12040 | National Semiconductor Corp. Commerce Drive <br> Danbury, Conn. 06813 | 35529 | Leeds and Northrup 4901 Stenton Ave. Philadelphia, Pa. 19144 |
| 03508 | General Electric Co. Semiconductor Products Dept. Syracuse, N.Y. 13201 | i2065 | Transitron Electronic Corp. 144 Addison St. <br> East Boston, Mass. | 37942 | Mallory, P. R. and Co., Inc. 3029 E. Washington St. Indianapolis, Ind. 46206 |
| 04009 | Arrow-Hart \& Hegeman Electric Co. 103 Hawthorne St. <br> Hartford, Conn. 06106 | 12697 | Clarostat Mfg. Co., Inc. Lower Washington St. <br> Dover, N.H. 03820 | 44655 | Ohmite Mfg. Co. 3601 Howard St. Skokie, Ill. 60076 |
| 04713 | Motorola Semiconductor Prod. Inc. 5005 E. McDowell Rd. <br> Phoenix, Ariz. 85008 | 12954 | Dickson Electronics Corp. 302 S. Wells Fargo Ave. Scottsdale, Ariz. | 53201 | Sangamo Electric Co. 1301 North lith <br> Springfield, I11. 62705 |
| 05079 | Tansistor Electronics, Inc. 1000 West Road Bennington, Vt. 05201 | 13050 | Potter Co. <br> Highway 51 N . <br> Wesson, Miss. 39191 | 54294 | Shalicross Mfg. Co. 24 Preston St. Selma, N.C. |
| 05397 | Union Carbide Corp. Electronics Div. New York, N.Y. 10017 | 13327 | Solitron Devices, Inc. 256 Oak Tree Road Tappan, N.Y. 10983 | 56289 | Sprague Electric Co. North Adams, Massachusetts |
| 06751 | Components, Inc. <br> Arizona Div. <br> Phoenix, Ariz. 85019 | 13934 | Midwec Corp. <br> 602 Main <br> Oshkosh, Nebr. 69154 | 58474 | Superior Electric Co., The 383 Middle St. <br> Bristol, Conn. 06012 |
| 06980 | Varian Assoc. EIMAC Div. 301 Industrial Way San Carlos, Calif. 94070 | 14655 | ```Cornell-Dubilier Electric Corp. 50 Paris Street Newark, N.J.``` | 61637 | Union Carbide Corp. 270 Park Ave. New York, N.Y. 10017 |


| 63060 | Victoreen Instrument Co. 5806 Hough Ave. <br> Cleveland, Ohio 44103 | 75042 | IRC Inc. <br> 401 North Broad St. <br> Philade1phia, Pa. 19108 | 86684 | Radio Corp. of America <br> Electronic Components \& Devices Harrison, N.J. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 70309 | Allied Control Co., Inc. 2 East End Ave. New York, N.Y. | 75915 | Littlefuse, Inc. 800 E. Northwest Hwy. Des Plaines, Ill. 60016 | 87216 | Philco Corp. <br> Lansdale Div., Church Rd. <br> Lansdale, Pa. 19446 |
| 70903 | Belden Mfg. Co. 415 So. Kilpatrick Chicago, Ill. 60644 | 76055 | Mallory Controls, Div. of Mallory P. R, \& Co., Inc. Frankfort, Ind. | 90201 | Mallory Capacitor 3029 East Washington Indianapolis, Ind. 46206 |
| 71002 | Birnbach Radio Co., Inc. 147 Hudson St. New York, N.Y. | 76493 | ```Miller, J. W. Co. 5915 S. Main St. Los Angeles, Calif. }9000``` | 90303 | Mallory Battery Co. Tarrytown, New York |
| 71279 | Cambridge Thermionic Corp. 430 Concord Avenue Cambridge, Mass. | 76545 | Mueller Electric Co. 1583 E . 31st St. Cleveland, Ohio 44114 | 91637 | $\begin{aligned} & \text { Dale Electronics, Inc. } \\ & \text { P.O. Box } 609 \\ & \text { Columbus, Nebr. } 68601 \end{aligned}$ |
| 71400 | Bussmann Mfg. <br> Div. of McGraw-Edison Co. <br> St. Louis, Mo. | 77764 | Resistance Products Co. 914 S. 13th St. <br> Harrisburgh, Pa. 17104 | 91662 | Elco Corp. Willow Grove, Pennsylvania |
| 71450 | CTS Corp. <br> 1142 W. Beardsley Ave. <br> Elkhart, Ind. | 79727 | Continental-Wirt Electronics Corp. Philadelphia, Pa. | 91737 | Gremar Mfg. Co., Inc. 7 North Ave. Wakefield, Mass. |
| 71468 | ITT Cannon Electric, Inc. 3208 Humbolt St. <br> Los Angeles, Calif. 90031 | 80164 | Keithley Instruments, Inc. 28775 Aurora Road Cleveland, Ohio 44139 | 91802 | Industrial Devices Inc. 982 River Rd. <br> Edgewater, N.J. 07020 |
| 71590 | Centralab Div. of Globe-Union, Inc. Milwaukee, Wisc. 53212 | 80294 | Bourns, Inc. <br> 6135 Magnolia Ave. <br> Riverside, Calif. 92506 | 91929 | Honeywell Inc. <br> Micro Switch Div. <br> Freeport, I11. 61032 |
| 71785 | Cinch Mfg. Co. and Howard B. Jones Div. Chicago, Ill. 60624 | 81073 | Grayhill, Inc. 561 Hillgrove Ave. La Grange, Ill. 60525 | 93332 | Sylvania Electric Products, Inc. Semiconductor Products Div. Woburn, Mass. |
| 72619 | Dialight Corp. 60 Stewart Ave. Brooklyn, N.Y. 11237 | 81483 | International Rectifier Corp. 1523 East Grand Ave. El Segundo, Calif. | 93656 | Electric Cord Co. 1275 Bloomfield Ave. Caldwell, N.J. |
| 72653 | G-C Electronics Co. 400 S . Wyman Rockford, Ill. 61101 | 82389 | Switchcraft, Inc. 5527 N . Elston Ave. Chicago, Ill. 60630 | 94144 | Raytheon Co., Industrial Operation Components Div. Quincy, Mass. |
| 72699 | General Instrument Corp. Capacitor Division Newark, N.J. 07104 | 83125 | General Instrument Corp. Capacitor Division Darlington, S.C. 29532 | 94154 | Tung-Sol Electric, Inc. Newark, <br> New Jersey |
| 72982 | Erie Technological Prods Inc. 644 W. 12th St. <br> Erie, Pa. 16512 | 83330 | Smith, Herman H., Inc. 812 Snediker Ave. Brooklyn, N.Y. 11207 | 94310 | Tru-Ohm products <br> Memcor Components Div. <br> Huntington, Ind. 46750 |
| 731.38 | Beckman Instruments, Inc. Helipot Division <br> Fullerton, Calif. 92634 | 83594 | Burroughs Corp. Electronic Components Div. Plainfield, N.J. 07061 | 94696 | Magnecraft Electric Co. 5579 North Lynch Chicago, I11. |
| 73445 | Amperex Electronic Co., Div. of North American Philips Co., Inc. Hicksville, N.Y. | 83701 | Electronic Devices, Inc. <br> Brooklyn, <br> New York | 95348 | Gordos Corp. <br> 250 Glenwood Ave. <br> Bloomfield, N.J. 07003 |
| 73690 | Elco Resistor Co. 1158 Broadway New York, N.Y. | 84171 | Arco Electronics, Inc. Community Drive Great Neck, N.Y. 11022 | 95712 | Dage Electric Co., Inc. Hurricane Road Franklin, Ind. |
| 74276 | Signalite Inc. 1933 Heck Ave. Neptune, N.J. 07753 | 84411 | TRW Capacitor Div. 112 W. First St. Ogallala, Nebr. | 97933 | Raytheon Co. Components Div. Semiconductor Operation Mountain View, Calif. |
| 74970 | Johnson, E. F., Co. 297 Tenth Ave. S.W. Waseca, Minn. 56093 | 84970 | Sarkes Tarzian, Inc. <br> E. Hillside Dr. <br> Bloomington, Ind. | 99120 | Plastic Capacitors, Inc. 2620 N. Clybourn Ave. Chicago, Ill. |

## APPENDIX

RESISTANCE DIAL ACCURACY CHECK.
The following procedure should be used to verify the accuracy of the various resistors of the decade dials. The test jacks are identified in Figure 7.

Procedure:

1. Set the Model 515A controls as follows: FUNCTION - OPERATE MULTIPLIER - $10^{5}$ DECADE DIALS - ALL 0
2. Connect ESI Model 242 Resistance Bridge between test jack J202 and GROUND.
3. Measure the resistance of the DECADE DIAL resistors for dial positions $0,1,2,4$, and 8 as in the table
X. 0001 through X10
4. Connect ESI Model 242 between test jacks J201 and J203.
5. Measure the resistance of the X100 DIAL resistors for dial positions $1,2,4$, and 8 .
6. Measure the resistance of the remaining resistors by connecting ESI Model 242 between the test jacks specified in the table

CONNECT TO J202 AND CHASSIS

|  | DIAL | NOMTNAL | TOLERANCE | R\% |
| :---: | :---: | :---: | :---: | :---: |
| ZERO R | ALL 0 | 0.130 | 1 OHM |  |
| X. 0001 | 1 | 10 | $\pm 1 \%$ |  |
|  | 2 | 20 | $\pm 1 \%$ |  |
|  | 4 | 40 | $\pm 1 \%$ |  |
|  | 8 | 80 | $\pm 1 \%$ |  |
| X. 001 | 1 | 100 | $\pm 0.1 \%$ |  |
|  | 2 | 200 | $\pm 0.1 \%$ |  |
|  | 4 | 400 | +0.1\% |  |
|  | 8 | 800 | $\pm 0.1 \%$ |  |
| X. 01 | 1 | 1K | +0.04\% |  |
|  | 2 | 2K | +0.04\% |  |
|  | 4 | 4K | $\pm 0.04 \%$ |  |
|  | 8 | 8K | $\pm 0.04 \%$ |  |
| X. 1 | 1 | 10K | $\pm 0.01 \%$ |  |
|  | 2 | 20K | $\pm 0.01 \%$ |  |
|  | 4 | 40K | $\pm 0.01 \%$ |  |
|  | 8 | 80K | $\pm 0.01 \%$ |  |
| X 1 | 1 | 100K | +0.01\% |  |
|  | 2 | 200K | $\pm 0.01 \%$ |  |
|  | 4 | 400K | $\pm 0.01 \%$ |  |
|  | 8 | 800K | $\pm 0.01 \%$ |  |
| X 10 | 1 | 1M | $\pm 0.01 \%$ |  |
|  | 2 | 2M | $\pm 0.01 \%$ |  |
|  | 4 | 4M | $\pm 0.01 \%$ |  |
|  | 8 | 8M | $\pm 0.01 \%$ |  |
| CONNECT TO J203 AND J201 |  |  |  |  |
|  |  |  |  |  |
| X 100 | 2 | 20M | $\pm 0.5 \%$ |  |
|  | 4 | 40M | $\pm 0.5 \%$ |  |
|  | 8 | 80M | $\pm 0.5 \%$ |  |
| CONNECT TO J205 AND J201 |  |  |  |  |
| R353 | - | 100M | $\pm 0.01 \%$ |  |
| CONNECT TO J207 AND J201 |  |  |  |  |
| R312 | $\sim$ | 100 K | + $0.01 \%$ |  |
| CONNECT J208 AND CHASSIS |  |  |  |  |
| R 305 | - | 1 M | +0.01\% |  |
| CONNECT J209 AND CHASSIS |  |  |  |  |
| * R302 | - | 100K | $\pm 0.01 \%$ |  |
| CONNECT TO J210 AND J209 |  |  |  |  |
| * R301 | - | 10K | $\pm 0.01 \%$ |  |




$$
v_{L_{1}} 1_{6}{ }_{19 q_{1}}
$$

MODEL NO.
SERIAL NO.
SHIP INSTRUMENT \& FORM TO:
SALES SERVICE DEPT.
KEITHLEY INSTRUMENTS, INC.

## 28775 AURORA ROAD

CLEVELAND, OHIO 44139

DATE $\qquad$ FROM:

USER'S NAME
RETURN ADDRESS
CITY
STATE
TELEPHONE

1. REASON FOR RETURN. Check appropriate box.
$\square$ Repair and Recalibration
$\square$ Recalibration only. (If repairs are required to meet specifications, an additional repair charge will be added to recalibration cost.)
2. CALIBRATION REPORT. Specify report desired. (See reverse side of form for details.)
$\square$ Calibration Report (Certified Traceable to N.B.S.)
$\square$ Calibration Report (Production Calibration Equipment at the factory)
$\square$ Certificate of Compliance
3. DESCRIPTION OF PROBLEM. (Include a block diagram of instruments connected in system. Recorder charts or other data would be helpful.)

Is problem constant or intermittent? $\qquad$
4. OPERATING CONDITIONS.

Control setting (range, multiplier, etc.)
Line voltage used $\qquad$ Line frequency used
Temperature $\quad{ }^{\circ} \mathrm{F}$ Temperature variation $\pm \ldots{ }^{\circ} \mathrm{F}$
Humidity (high, medium, low)
Other (please specify, such as line transients, etc.)
5. EQUIPMENT USED.

Signal source
Readout device
Cables used
$\qquad$ Source impedance
(Recorder, oscilloscope, etc.) Length
6. ADDITIONAL INFORMATION. Please indicate any other pertinent information which may help the Keithley Repair and Calibration Department. (If repairs or modifications have been made to instrument by other than Keithley personnel, please specify below.)

Listed and defined below are the four types of calibrations and the ir associated report formats which are presently available at Keithley Instruments. They fall into the following categories:

## 1. Report of Calibration Certified Traceable to the National Bureau of Standards <br> 2. Calibration Report <br> 3. Certificate of Compliance <br> 4. Recalibration

All calibration and certification performed by Keithley Instruments is in accord with MIL-C-45662A.

Prices shown below are in addition to repair charges for any work necessary to place a customer's unit into first class condition prior to the calibration.

1. Report of Calibration Certified Traceable to the National Bureau of Standards.

This is a completely documented report, including all basic errors or deviations from nominal settings on appropriate ranges, terminals, dials, etc. Work is performed using the primary standards of the company with secondary transfers kept to a minimum. The NBS test numbers for the latest recalibration of the primary standards are furnished.

By definition, the above is performed in our Standards Laboratory so that random operator induced error is minimized and maximum protection to the equipment used is maintained.

This type of calibration is not recommended for instruments with a basic inaccuracy of $1 \%$ or greater. The precision involved in this report makes it uneconomical for such instruments. The Calibration Report listed below (No. 2) would be better suited in this case.

The Report of Calibration Certified Traceable to the National Bureau of Standards is available on the following instrments at the prices listed:

| Model 140 . . . . . . . . . . . $\mathbf{2}^{\text {275 }}$ | Model 5155-10 ${ }^{8}$ | . $\$ 50$ |
| :---: | :---: | :---: |
| Model 260 . . . . . . . . . . . $\$ 225$ | Model 5155-10 ${ }^{9}$ | . $\$ 50$ |
| Model 261 . . . . . . . . . . . $\$ 375$ | Model 5155-1010. | . \$ 50 |
| Model 662 . . . . . . . . . . $\$ 275$ | Model 5155-10 ${ }^{11}$. | . $\$ 60$ |
| Model 5155 (Complete Set) . . . 295 | Model Model 5155-10 512 ${ }^{12}$. | . . . $\$ 60$ |

2. Calibration Report.

This report shows only the cardinal range, terminal, dial, etc. errors as determined by production calibration equipment and personnel. The production equipment is maintained traceable by transfer techniques against the primary standards maintained by the company. We attest to this fact and list basic deriations from nominal but the conditions of calibration are not as precisely controlled as the previous report nor are NBS test numbers supplied.

This report is available for any instrument in our line. The sollowing price has been established for this report:

Model 261 . . . . . . . . . . . $\$ 60$
Prices for other units can be estimated upon request.
3. Certificate of Compliance.

This is merely a restatement of the basic guarantee that the instrument was calibrated on equipment that is maintained by our standards personnel against primary standards. No report is issued.

This Certificate of Compliance is available at no charge for any instrument with the exception of the Model 261.

A newly purchased Mooel 261 or one returned for repair or recalibration is automatically supplied with a Crilibration Report (as described in (2) above). The nature of this instrument makes it necessary to complete this report to ascertain specified accuracy. This Calibration Report is forwarded to the customer with the instrument. The $\$ 60$ charge is incorporated as part of the normal calibration charge of the Model 261.
4. Recalibration.

This is a recalibration of the instrument according to our factory calibration procedures.

| Model 260 . . . . . . . . . . $\$ 90$ | (No report supplied. A Certificate of Com- <br> pliance can be had at no charge if requested). |
| ---: | :--- |
| Model 261 . . . . . . . . . $\$ 60$ | (Calibration Report as described in (2) above <br> is supplied. See (3) for explanation). |

All other instriments are on a time and material basis for the particular unit involved.

All prices subject to change without prior notification.

## KEITHLEYINSTRUMENTS. INC.

## INSTRUCTION MANUAL

CHANGE NOTICE
MODEL 515A MEGOHM BRIDGE

INTRODUCTION: Since Keithley Instruments is continually improving product performance and reliability, it is often necessary to make changes to Instruction Manuals to reflect these improvements. Also, errors in Instruction Manuals occasionally occur that require changes. Sometimes, due to printing lead time and shipping requirements, we can't get these changes immediately into printed Manuals. The following new change information is supplied as a supplement to this Manual in order to provide the user with the latest improvements and corrections in the shortest possible time. Many users will transfer this change information directly to a Manual to minimize user error. All changes or additions are underlined.

## CHANGES:

(1) Page 26, Replaceable Parts, Resistors, Add the following resistor as follows:
B354, $100 \Omega, 10 \%, 1 / 2 W$, Comp, 01121, EB- $100 \Omega$, Rl-100
(2) Page 21, Replaceable Parts, Diodes, Change D105, D106, D111, D112, D113, and D114 to read as follows:
D105, Not Used.
D106, Not Used.
D111, Not Used.
D112, Not Used.
D113, Zener, 15V, 1/4W, 12954, IN718, DZ-18
D114, Zener, $15 \mathrm{~V}, 1 / 4 \mathrm{~W}, 12954$, IN718, DZ-18
(3) Page 22, Replaceable Parts, Resistors, Change R123, R124, R125, and R126 to read as follows:
R123, $845 \Omega, 1 \%, 1 / 2 \mathrm{~W}, \mathrm{MHF}, 07716$, CEC-845 2 , R94-845
R124, Not Used
R125, Not Used
R126, $845 \Omega, 1 \%, 1 / 2 \mathrm{~W}, \mathrm{MtF}, 07716$, CEC-845, $\mathrm{R} 94-845$
(4) Page 22, Replaceable Parts, Transistors, Change Q101 and Q102 to read as follows:
Q101, Not Used
Q102, Not Used

MODEL 515A
م
Distribution:

| All Officers | Herron |
| :--- | :--- |
| Nichols | Streetz |
| Sheridan | Kifer |
|  | Sutphin |
|  | Butler |

Kaplan
Allen
Cech
Nowac
Kronenwetter
Bartos

Sarkisian Naylor Angeline Peabody Engrq. File Seifert

The following change has been approved by an executive committee and will be implemented according to the following schedule:

Change: Model 515A $\triangle$ CCURACY specifications are changed from:
ACCURACY: (when bridge is operated as described below)
Range,
ohms

Standard
Bridge
Deviation (1 10 )** Voltage
Decade

| $10^{5}$ to $10^{7}$ | $.012 \%$ | 10 v | $10^{5}-10^{6}$ |
| :--- | :--- | :--- | :--- |
| $10^{7}$ to $10^{8}$ | $.02 \%$ | 10 v | $10^{7}$ |
| $10^{8}$ to $10^{9}$ | $.03 \%$ | 10 v | $10^{8}$ |
| $10^{9}$ to $10^{10}$ | $.06 \%$ | 10 v | $10^{9}$ |
| $10^{10}$ to $10^{11}$ | $.08 \%$ | 10 v | $10^{10}$ |
| $10^{11}$ to $10^{12}$ | $.16 \%$ | 10 v | $10^{11}$ |
| $10^{12}$ to $10^{13}$ | $.25 \%$ | 10 v | $10^{12}$ |
| $10^{13}$ to $10^{14}$ | $.3 \%$ | 100 v | $10^{12}$ |
| $10^{14}$ to $10^{15}$ | $.5 \%$ | $500 \mathrm{v} *$ | $10^{12}$ |

* External supply required above $10^{14}$ ohms.
** Based on theoretical analysis of bridge errors, see instruction manual for details on obtaining specified performance.
to:

| Range, <br> ohms | Standard <br> Deviation ( $1 \sigma$ )** | Briage Voltage | Decade |
| :---: | :---: | :---: | :---: |
| $10^{5}$ to $10^{7}$ | . $012 \%$ | 10 v | $10^{5}-10^{6}$ |
| $10^{7}$ to $10^{8}$ | . $02 \%$ | 10 v | 10.7 |
| $10^{8}$ to $10^{9}$ | . $03 \%$ | 10 v | $10^{8}$ |
| $10^{9}$ to $10^{10}$ | . $06 \%$ | 10 v | $10^{9}$ |
| $10^{10}$ to $10^{11}$ | . $08 \%$ | 10 v | $10^{10}$ |
| $10^{11}$ to $10^{12}$ | . $16 \%$ | 10 v | $10^{11}$ |
| $10^{12}$ to $10^{13}$ | . $25 \%$ | 100 v | 1012 |
| $10^{13}$ to $10^{14}$. | . 3 \% | 500 v * | 1012 |
| $10^{14}$ to $10^{15}$ | $1.5 \%$ | 500 v* | $10^{12}$ |

* bixtermal :apply recpurad above $10^{13}$ ohms.
** Based on theoretical analysis of bridge errors, see instruction manual for details on obtaining specified performance.


## ACTION

| Manufacturing: | Sct up manufacturing procedures as necessary to <br> achieve the revised specification. Give notice <br> of the change to applicable personnel in tech <br> check-out and repair. |
| :--- | :--- |
| Engineering: $\quad$Note revision and change any applicable drawings <br> for instrument or its parts. |  |
| $\quad$Issue notice of change to entire world-wide sales <br> organization, applications engineers, etc. |  |
| Change $515 A$ manual and any other applicable manuals <br> to reflect revision. |  | to reflect revision.

MODEL 515A

## MEGOHM BRIDGE


#### Abstract

This Preliminary Instruction Manual is supplied to permit earliest possible delivery of your instrument.

It contains Specifications, Operation Instructions, Circuit Description, Replaceable Parts List and Schematics. The Final Edition will contain Servicing and Calibration information to maintain the instrument.

Please detach, fill out and return the Warranty Card attached to the instrument so that the Final Edition Instruction Manual can be sent to your attention. If you have further questions, please contact your Keithley Representative or the Sales Service Department.


Product Literature Department

To receive future information on product upgrades and enhancements, complete this card and mail, or FAX to 440/248-6168.

MODEL $\qquad$ SERIAL NO. $\qquad$ DATE $\qquad$
COMPANY

$\overline{\text { ADDRESS }}$| $\overline{\text { CITY }}$ |
| :--- |
| $\overline{\text { PHONE }}$ |

## E-MAIL

For FREE additional information, check below:

Application Notes
$\square$ Low Level Measurements
$\square$ Semiconductor Measurements

- General Purpose Measurements
- Component Test Applications

Reference Publications

- Low Level Handbook

Switching Handbook

- Gas Sensors Handbook


## Catalogs

$\square$ Keithley Instruments
$\square$ Channel K / Kcithley Metrabyte

Job Function (Check One)

| $\square$ | 4 | Calibration/Metrology |
| :--- | :--- | :--- |
| $\square$ | 6 | Component Test |
| $\square$ | C | Consulting |
| $\square$ | $G$ | Corp./General Mgmt. |
| $\square$ | 7 | Education |
| $\square$ | 3 | Engineering Design |
| $\square$ | 1 | Engineering Management |
| $\square$ | 5 | Mfg. Production Test |
| $\square$ | 0 | Purchasing |
| $\square$ | 8 | Quality Assurance/Control |
| $\square$ | 2 | Research \& Development |
| $\square$ | $S$ | Safety Manager |
| $\square$ | 9 | Service/Repair |
| $\square$ | E | System Enginecring/mtegration |
| $\square$ | $T$ | Test Technician |
| $\square$ | $X$ | Other |

## Product Interest(s)

| $\square$ | G | Commumications Test |
| :---: | :---: | :---: |
| $\square$ | 7 | Current/Voltage Source |
| $\square$ | V | C-V Measurements |
| $\square$ | 2 | Digital Multimeters |
| $\square$ | 4 | Electroncters/Picoammeters |
| $\square$ | A | Flat Panel Display Test |
| $\square$ | F | Function Generators |
| $\square$ | 3 | High Rexistance Mcters |
| $\square$ | C | Industrial Gas Sensors |
| $\square$ | 1 | I-V Characterization |
| $\square$ | N | LCZ Meters |
| $\square$ | 5 | Nanovoltmeters |
| $\square$ | 6 | Ohmmeters |
| $\square$ | 8 | Precision Power Supplies |
| $\square$ | U | Source/Measure Instruments |
| $\square$ | S | Switching Systems/Scanners |
| $\square$ | 0 | Temperature Measurements |
| $\square$ | X |  |

## Facility (Check One)

```
\ K Aerospace/Dcfense
\square S Automotive/Parts Mfg.
Q Q Chemical/Petroleum Processing
\square H Components Mfg. (Non-Semi)
\square N Computer/Peripherals
\square T Consumer Electronics
L Digital ICs
\square U Discrete Components
\square D Displays
V Distributors/Resellers/Rental
\square F Education/University
\square 3 Health Services
\square] Industrial Controls Mfg.
Z M Medical Equip. and Services
[] Mixed-Signal Components
Z Z Office Equipment Mfg.
[] O Optoelectronic Components
5 Other Discrete Manufacturing
I Process Control Industries
C Regulatory
[] E Research Laboratories
\square J Semi. Components - Other
\square 1 Semiconductor Mfg.
\square] Semi. Pkg. Part Testing
| Telecommunications Equip.
G G Tes//Measurement Equipment Mfg.
M Utility
\square] 4 VAR/System Integrator/Consultant
\square X Other
```

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1. What other Keithley products do you currently use?
2. What effects, devices or phenomena do you measure with this instrument?
3. What was the main reason a Keithley unit was purchased?
4. Do you have any design suggestions concerning this unit?

[^0]:    * To obtain this accuracy specification an external voltage supply is required. Accuracy (3 o) for $10^{15}$ range would be $\pm 6 \%$ at a bridge potential of 110 V .

[^1]:    * With a loV bridge potential.

