HEADQUARTERS
DEPARTMENT OF THE ARMY
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OPERATOR'S, ORGANIZATIONAL, DIRECT SUPPORT, AND GENERAL SUPPORT MAINTENANCE MANUAL
(INCLUDING REPAIR PARTS AND SPECIAL TOOLS LISTS) FOR
DIFFERENTIAL AMPLIFIER AM-6786/U (TEKTRONIX TYPE 7A22, VERTICAL PLUG-IN UNIT) NSN 6625-00-478-0597)

Current as of 20 March 1979

## REPORTING OF ERRORS

You can improve this manual by recommending improvements using DA Form 2028-2 located in the back of the manual. Simply tear out the self-addressed form, fill it out as shown on the sample, fold it where shown, and drop it in the mail.

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In either case, a reply will be furnished direct to you.

This manual is an authentication of the manufacturer's commercial literature which, through usage, has been found to cover the data required to operate and maintain this equipment. Since the manual was not prepared in accordance with military specifications, the format has not been structured to consider levels of maintenance.
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Fig. 1-1. Type 7A22 Differential Amplifier.

## SECTI ON 0

## I NTRODUCTI ON

## 0-1. SCOPE

This manual describes Vertical Plug-In Unit, Differential Amplifier AM6786/U and provi des instructions for oper ation and mai ntenance. Throughout this manual, the AM 6786/U is referred to as Tektronix Type 7A22 Differential Amplifier. The maintenance allocation chart appears ir appendix D. Al so, included is a repair parts list.

## 0-2. I NDEXES OF PUBLI CATI ONS

a. DA Pam 310-4. Ref er to the latest issue of DA Pam 310-4 to determine whet her there are new editions, changes, or additional publications pertaining to the equi pment.
b. DA Pam 310-7. Refer to DA Pam 310-7 to determine whether there are modification work orders ( $M 1 O^{\prime} S$ ) pertaining to the equi prent.

## 0-3. FORMS AND RECORDS

Reports of Mai ntenance and Unsatisfactory Equi prent. Mai nt enance forms, records, and reports which are to be used by mai ntenance personnel at all maintenance levels are listed in and prescribed by TM 38-750.
b. Report of Packaging and Handling Deficiencies. Fill out and forward DD Form 6 (Packaging I mprovement Report) as prescribed in AR 700-58/ NAVSUPI NST 4030. 29/ AFR 71-13/ MCO P4030. 29A and DLAR 4145. 8.

Di screpancy in Shi pment Report (DI SREP) (SF 361). Fill out and forward Discrepancy in Shi pment Report (DISREP) (SF 361) as prescribed in AR 55-38/ NAVSUPI NST 4610. 33B/ AFR 75-18/ MCO P4610. 19C and DLAR 4500. 15.

## 0-4. REPORTI NG EQUI PMENT I MPROVEMENT RECOMMENDATI ONS (EI R)

El R's will be prepared using DA Form 2407, Mai ntenance Request. I nstructions for preparing ElR's are provided in TM 38-750, The Army Maintenance Management System ElR's should be mailed direct to Commander, US Army Communi cations and El ectroni cs Materi el Readi ness Command; ATTN: DRSEL-ME-MQ, Fort Mbnmouth, NJ 07703. A reply will be furni shed di rectly to you.

## $0-5$. ADM NI STRATI VE STORAGE

Admini strative storage of equi pment issued to and used by Army activities shall be in accordance with TM 750-244-2.

## $0-6$. DESTRUCTI ON OF ARMY ELECTRONI CS MATERI EL

Destruction of Army el ectronics materiel to prevent enemy use shall be in accordance with TM 750-244-2.

## SECTION 1 SPECIFICATION

## Introduction

The Type 7A22 Vertical Plug-in is a DC coupled differential amplifier with excellent common-mode rejection characteristics and high gain for low level applications.

The DC Offset capability of the Type 7A22 allows the display of the very small low-frequency signals containing a large DC component, at deflection factors not possible with AC coupling. The vertical deflection factor range of the Type $7 A 22$ is from $10 \mu \mathrm{~V}$ to 10 V . The high and low frequency -3 dB points can be selected at the front panel, to set the bandwidth of the instrument. Thus, for low frequency applications the signal-to-noise ratio can be improved by restricting the bandwidth of the Type 7A22. The bandwidth selection and excellent drift-with-time characteristics provide measurement capabilities in the biomedical, transducer, and other areas which require stable, low deflection factor, low noise measurements.

The Type 7A22 is designed for use in Tektronix 7000 Series oscilloscopes.

The electrical characteristics described in this section are valid over the stated environmental range for instruments calibrated at an ambient temperature of $+20^{\circ} \mathrm{C}$ to $+30^{\circ} \mathrm{C}$ and after a 5 minute warmup unless otherwise noted.

ELECTRICAL CHARACTERISTICS

| Characteristic | Performance Requirements |
| :--- | :--- |
| Deflection Factor <br> (VOLTS/DIV) <br> Gain Ratio Accuracy | Within $2 \%$ with GAIN adjusted at <br> $1 \mathrm{mV} /$ div |
| VAR (CAL IN) Range |  |
| Continuously variable; extends de- |  |
| flection factor to at least 25 V/div |  |


| ```DC OFFSET COARSE Range from Electrical Zero \(10 \mu\) V/Div to \(10 \mathrm{mV} / \mathrm{Div}\)``` | At least +1 V to -1 V |
| :---: | :---: |
| $\begin{aligned} & 20 \mathrm{mV} \text { to } 0.1 \\ & \text { V/Div } \end{aligned}$ | At least +10 V to -10 V |
| 0.2 V to $\mathrm{IV} / \mathrm{Div}$ 2 V to $10 \mathrm{~V} /$ Div | At least +100 V to -100 V <br> At least +1000 V to -1000 V |
| Frequency Response (8 div Reference) <br> Overall Frequency Response DC (Direct) Coupled Input | DC to within $10 \%$ of 1 MHz at $-3 \mathrm{~dB}$ |
| AC (Capacitive) Cou pled Input Lower Bandwidth Frequenc: | 2 Hz or less |
| Bandwidth Limit Accuracy |  |
| Accuracy <br> $\mathrm{HF}-3 \mathrm{~dB}$ POINT 100 Hz to 1 MHz | 9 steps in a 1-3 sequence |
| Accuracy | Within $10 \%$ of selected frequency |
| LF - 3 dB POINT <br> 0.1 Hz to 10 kHz | 6 steps in a 1-10 sequence |
| Accuracy | Within $12 \%$ of selected frequency |
| Recovery Time | $10 \mu$ s or less to recover to within $0.5 \%$ of zero level after the removal of $a+$ or - test input applied for 1 s . Test signal not to exceed Differential Signal Range. Specified aberration ( $0.5 \%$ ) based on test signal amplitude |
| $\begin{aligned} & \text { Common Mode Signal } \\ & 10 \mu V / D i v \text { to } \\ & 10 \mathrm{mV} / \text { Div } \end{aligned}$ | At least +10 V and -10 V |
| $20 \mathrm{mV} /$ Div to $0.1 \mathrm{~V} / \mathrm{Div}$ | At least +100 V and -100 V |
| $0.2 \mathrm{~V} / \mathrm{Div}$ to $10 \mathrm{~V} / \mathrm{Div}$ | At least +500 V and -500 V |
| Common-Mode |  |
| Rejection Ratio DC (Direct) Coupled | See Verification Points on graph, fig. 1-2 |
| AC (Capacitive) Coupled | See Verification Points on graph, fig. $1-2$ |



ELECTRICAL CHARACTERISTICS (cont)

| Characteristic | Performance Requirements |
| :---: | :---: |
| Maximum Input Voltage leach input) <br> DC (Direct) Coupled, DC + Peak AC, AC Component 1 MHz or less |  |
| $10 \mu \mathrm{~V} / \mathrm{Div}$ to 10 mV/Div | $\pm 15 \mathrm{~V}$ |
| $\begin{aligned} & 20 \mathrm{mV} / \mathrm{Div} \text { to } 0.1 \\ & \mathrm{~V} / \mathrm{Div} \end{aligned}$ | $\pm 200 \mathrm{~V}$ |
| . $2 \mathrm{~V} /$ Div to $10 \mathrm{~V} /$ Div | $\pm 500 \mathrm{~V}$ |
| AC (Capacitive) Coupled Input DC Voltage | $\pm 500 \mathrm{~V}$, each input |
| AC (Capacitive) Coupled Input DC Rejection | At least $4 \times 0{ }^{5}$ : 1 |
| Input $R$ and $C$ Resistance | $1 \mathrm{M} \Omega \pm 1 \%$ |
| Capacitance | Approximatel 47.0 pF |
| R \& C Produc $\ddagger$ | Within $\pm 1 \%$ between all deflection factors |
| Maximum Input Gate | $+25^{\circ} \mathrm{C} \quad+50^{\circ} \mathrm{C}$ |
| Current <br> $10 \mu \mathrm{~V} /$ Div to $10 \mathrm{mV} /$ Div | $\pm 20 \mathrm{pA} \pm 100 \mathrm{pA}$ each input $\pm 40 \mathrm{pA} \pm 200 \mathrm{pA}$ Differentially |
| $20 \mathrm{mV} / \text { Div to } 10 \mathrm{~V}$ $\operatorname{Div}$ | $\pm 10 \mathrm{pA} \pm 20 \mathrm{pA}$ |
| Display Shift at $10 \mu \mathrm{~V}$ /Dir (AC Coupled) | $\pm 4 \mathrm{div} \pm 20 \mathrm{div}$ |
| Variable Balance | 0.2 div or less shift with VARIABLE control turned from fully cw to fully caw position |
| Displayed Noise (Tangetially Measured) | $16 \mu \mathrm{~V}$ or 0.1 Div (whichever is greater), $1 \mathrm{MHz} \mathrm{HF}-3 \mathrm{~dB}$ POINT, source resistance $25 \Omega$ or less |

DC Drift
Drift with Time (Ambient Temperature and Line Voltage Constant) Short Term

Long Term

Drift with Ambient
Temperature (Line
Voltage Constant)
Isolation between + and

- Inputs (+ INPUT to an Open - INPUT, INPUT to an Open + INPUT)
$5 \mu \mathrm{~V}$ (P-P) or 0.1 div (whichever is greater) in any minute after 1 hour warmup
$10 \mu \mathrm{~V}(\mathrm{P}-\mathrm{P})$ or $0.1 \operatorname{div}$ (whichever is greater) in any hour after 1 hour warmup
$50 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}$ or less

At least 200:1, DC to 1 MHz

## ENVIRONMENTAL

PLUG-IN TESTED OUT OF INDICATOR OSCILLOSCOPE

| ITEM | CHARACTERISTIC |
| :--- | :--- |
| Altitude | To 50,000 feet and $-55^{\circ} \mathrm{C}$ |
| Non-operating | Qualified under National Safe <br> Transportation Committee test procedure |
|  | 1A, Category II |

PHYSICAL

| ITEM | CHARACTERISTIC |
| :--- | :--- |
| Finish | Front panel is anodized aluminum |
| Dimensions | $\widetilde{\widetilde{47 / 8} \text { inch } \mathrm{H}} \mathrm{L} \times 25 / 8$ inch $\mathrm{W} \times$ |
| Weight | $\simeq 25 / 8 \mathrm{lbs}$ |

## SECTION 2

## OPERATING INSTRUCTIONS

## Introduction

This section opens with a brief functional description of the front-panel controls, input overdrive lamp, and input connectors. Following the front-panel description is a familiarization procedure and finally a general discussion of the operation of the Type 7A22.

## CONTROLS AND CONNECTORS

INPUT OVERDRIVE

VOLTS/DIV

VARIABLE
(CAL IN]
VOLTS/DIV

Input overdrive indicator lamp tums on to indicate excessive differential drive to the input amplifier stage. Lights when the differential dynamic range between input connectors is exceeded.

Volts per displayed division. Nineteen position switch used to select the calibrated deflection factors.

Two-position switch activated by the VARIABLE knob to select calibrated or uncalibrated deflection factors. At the IN position, the VARIABLE control is inoperative and the deflection factor is calibrated. When pressed and released, the knob moves outward to activate the VARIABLE control for uncalibrated deflection factors. The uncalibrated position provides continuously variable uncalibrated attenuation between the calibrated deflection factors and extends the deflection factor to at leost 25 VOLTS/DIV.

Screwdriver adjust control to set the CRT display scale factor to agree with the VOLTS/DIV switch indication. Adjusted for proper deflection with the VOLTS/ DIV switch set to the 1 mV position.

The control that vertically positions the trace or display.

Momentary contact, push-button switch, concentric with POSITION. Will cause the trace, representing the output of the Type 7A22, to move a small amount when pressed. Aids in identifying the Type 7A22 trace when multiple traces are displayed.

Nine position switch to select the approximate high frequency -3 dB point. The switch positions are: $100 \mathrm{~Hz}, 300 \mathrm{~Hz}$, $1 \mathrm{kHz}, 3 \mathrm{kHz}, 10 \mathrm{kHz}, 30 \mathrm{kHz}, 100 \mathrm{kHz}$, 300 kHz , and 1 MHz .

LO W FREQ UENCY -3 dB POINT

+ INPUT
- INPUT

Eight position switch to select DC coupling or the approximate low frequency -3 dB points. The switch positions are: DC OFFSET, DC, . $1 \mathrm{~Hz}, 1 \mathrm{~Hz}, 10 \mathrm{~Hz}$, $100 \mathrm{~Hz}, 1 \mathrm{kHz}$, and 10 kHz .

Signal input connector. Positive input produces deflection upward (see Fig. 2-I).

Signal input connector. Positive input produces deflection downward (see Fig. 21,


Fig. 2-1. Signals applied to the + INPUT connector produces an upright display, while signals applied to the - INPUT are inverted.

+ AC-GND-DC A miniature illuminated push-button type switch. The buttons are interlocked so that only one button may be depressed at one time. When the ' $A C$ ' button is depressed the signal is coupled through $0.1 \mu \mathrm{~F}$ to the Input Amplifier and only the varying component of the input signal is amplified.

When the 'DC' button is depressed the signal is coupled directly to the Input Amplifier and the entire input signal, both AC and DC, is amplified. When the 'GND' button (or none of the buttons) is depressed, the signal is coupled through $0.1 \mu \mathrm{~F}$ and through $1 \mathrm{M} \Omega$ to ground. The Amplifier Input is grounded in this condition.

Each push-button is illuminated from behind when the button is depressed.

- AC-GND-DC

Same function as the + AC-GND-DC
switch but applied to the - INPUT.

## IMPORTANT

The following two controls are operative only when the LOW FREQUENCY -3 dB POINT switch is set to DC or DC OFFSET.

STEP ATTEN DC BAL (DC MODE ONLY)

DC OFFSET
(DC OFFSET mode only)

RELEASE LATCH

Front panel control for DC balancing the amplifier input stage. With no signals applied to the input connectors, the control is adjusted for no trace shift as the VOLTS/DIV switch is moved from the 10 mV position to the $10 \mu \mathrm{~V}$ position.

Coarse and fine controls to provide internal offset bias while maintaining the differential capability. Available range of the offset bias depends upon the settings of the VOLTS/DIV switch, and is indicated by shaded gray bands (OFFSET RANGE) around the VOLTS/ DIV switch.

Gray rectangular knob near the bottom left of the front panel. Pull out to remove Plug-In from Plug-In compartment.

## OPERATING INSTRUCTIONS

## First-Time Operation

Steps 1 through 5 in the following procedure are intended to help place the trace on the screen quickly and prepare the unit for immediate use. Steps 6 through 8 are used to check the GAIN adjustment. These steps along with those remaining are intended to demonstrate some of the basic functions of the Type 7A22.

1. Insert the unit into the oscilloscope plug-in compartment.
2. Set the Type 7A22 front-panel controls as follows:

| VOLTS/DIV | 1 mV |
| :--- | :--- |
| VARIABLE | IN (CAL) |
| POSITION | Midrange |
| HIGH FREQUENCY | 1 MHz |
| $\quad-3 \mathrm{~dB}$ POINT |  |
| LOW FREQ -3 dB POINT | DC |
| AC-GND-DC (+ INPUT) | GND |
| AC-GND-DC (- INPUT) | GND |
| STEP ATTEN DC BAL | Midrange |

3. Turn the oscilloscope Intensity control fully counterclockwise and furn the oscilloscope Power ON. Preset the time-base and triggering controls for a .5 ms sweep rate and automatic triggering.
4. Wait about five minutes for the Type 7A22 and the oscilloscope to warm up.

## NOTE

About five minutes is sufficient time for warmup when using the Type 7A22 for short-term DC measurements. For long-term DC measurements using the lower deflection factors, allow at least one hour.
5. Adjust the Intensity control for normal viewing of the trace. The trace should appear near the graticule center.
6. Using the POSITION control, position the trace 2 divisions below graticule center.

## CAUTION

If the maximum input voltage rating in the $10, \mathrm{~V}$ to 10 mV range of the VOLTS/DIV switch is exceeded, the inputs are diode-clamped to fixed voltages of approximately +16.5 volts and/or -16.5 volts and damage to the signal source is possible. If the signal source can supply more than 1/16 A of current, the input protective fuse (s) will open. An open input fuse is indicated by the lighting of the INPUT OVERDRIVE indicator with the input coupling switches set to GND.
7. Apply a 4 mV peak-to-peak calibrator signal through a coaxial cable to the + INPUT connector on the Type 7A22.
8. For DC coupled, single-ended operation, set the + INPUT AC-GND-DC coupling switch to DC. The display should be square waves 4 divisions in amplitude with the bottom of the display at the reference established in step 6.
9. For AC coupled, single-ended operation, reposition the display with the Type 7A22 POSITION control to place the bottom of the display at the graticule center line.
10. Set the + INPUT AC-GND-DC coupling switch to AC and note that the display shifts downward about 2 divisions to its average leve!.
11. Disconnect the coaxial cable from the + INPUT connector. Connect a dual input connector to the + INPUT and - INPUT connectors. Connect the coaxial cable from the Calibrator to the dual input connector.
12. For $A C$ coupled differential operation, set the -INPUT AC-GND-DC coupling switch to AC. The calibrator signal is now coupled to both inputs as a commonmode signal. A straight line display should be observed, since the common-mode is being rejected.

Operational Adjustments
NOTE
Most of the following checks and adjustments may be made after a 5 minute warmup; however due to the DC drift of the amplifier during subsequent warmup, the STEP ATTEN DC BAL should be readjusted for each check or adjustment, and a warmup of at least one hour should be allowed before a final adjustment of the STEP ATTEN DC BAL is attempted. Insure that the oscilloscope used in conjunction with the Type 7A22 is correctly calibrated (refer to the oscilloscope manual) and that the calibrated output voltage is correct.

1. AC ATTEN BAL (internaladjustmentl. When the LOW FREQ -3 dB POINT switch is used to limit the low frequency response of the Type 7A22, the unit employs $A C$ stabilization. This means that when the switch is set to any position except DC or DC OFFSET, the STEP ATTEN DC BAL and DC OFFSET controls become inoperative. VOLTS/DIV balance is then controlled with the AC ATTEN BAL, an internal adjustment (seefig.2-2).


Fig. 2-2. Location of AC ATTEN BAL control.

When transferring the Type 7A22 from one oscilloscope to another, it may be necessary to perform a minor readjustment of this control, due to normal power supply vari= ations between oscilloscopes.

NOTE
An unbalance of up to $30 \mu \mathrm{~V}$ is normal and cannot be reduced by adjusting the AC ATTEN BAL control.
a. With the Type 7A22 inserted into the oscilloscope, remove the left side panel of the oscilloscope and set the Type 7A22 controls as follows:

| VOLTS/DIV | 1 mV |
| :--- | :---: |
| AC-GND-DC $(+$ INPUT $)$ | GND |
| AC-GND-DC $(-I N P U T)$ | GND |
| LOW FREQ -3 dB POINT 10 Hz |  |
| HIGH FREQ -3 dB POINT 100 Hz |  |

b. Using the POSITION control, position the trace to graticule center.
c. Set the VOLTS/DIV switch to $20 \mu \mathrm{~V}$.
d. Adjust the AC ATTEN BAL control, R505, to position the frace to within 1.5 divisions of graicule center. (See note in step 1).

INTERACTION: If this adjustment is made out of sequence, steps 2 and 3 must also be performed.
2. VAR BAL R425. (internaladjustment).
a. Set the Type 7A22 controls as in step 1 -a.
b. Position the trace to graticule center with the POSITION control.
c. With the VAR (CAL $I N$ ) in the out position, rotate the VARIABLE control from stop to stop. Check for no movement of trace.
d. Adjust R425 for no movement of trace as the VARIABLE control is rotated from stop to stop. (Seefrig. 2-2 for location of adjustment.)
3. STEP ATTEN DC BAL. With zero input voltage and the LF -3 dB POINT selector at DC, if the STEP ATTEN DC BAL is not properly adjusted the CRT trace will shifi vertically as the VOLTS/DIV switch is rotated throughout its range. The shift is more noticeable at the most sensitive positions.
a. Set the Type 7A22 front-panel controls as follows:

| VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE (CAL IN) | CAL |
| POSITION | Midrange |
| HIGH FREQ -3 dB POIN | 1 MHz |
| LOW FREQ -3 dB POINT | DC |
| AC-GND-DC $(+\mathrm{INPUT)}$ | GND |
| AC-GND-DC (-INPUT) | GND |
| STEP ATTEN DC BAL | Midrange |

b. Using the Type 7A22 POSITION control, position the CRT trace to the center of the graticule.
c. Set the VOLTS/DIV switch to $10 \mu \mathrm{~V}$.
d. Return the trace to graticule center by adjusting the STEP ATTEN DC BAL control.
N O TE

The adiustment of the STEP ATTEN DC BAL control should be checked periodically during the use of the instrument. If the Type 7A22 is used DC coupled or in significantly varying ambient temperatures in the $10 \mu \mathrm{~V} /$ DIV to $.1 \mathrm{mV} /$ DIV ranges, the STEP ATTEN DC BAL should be checked quite frequently. It is good practice to check this control and readjust, if necessary, before any critical measurement is made under the above conditions.

## 4. GAIN

a. Perform steps 1 through 8 in the First-Time Operation Procedure.
b. Adjust the GAIN control for exactly 4 divisions of display.

## NOTE

Accuracy of this adjustment is dependent upon the voltage accuracy of the calibration source.

## GENERAL OPERATING INFORMATION

## Trace Drift

The environment in which the Type 7A22 is operated and the inherent characteristics of the Type 7A22 influence trace drift. Therefore, to determine trace drift for a specific environment refer to the Specification Section. In environment in which the ambient temperature does not vary much (such as an air-conditioned building) the trace drift generally will not exceed $10 \mu \mathrm{~V}$ in one hour.

## Input Gate Current

When using the $.1 \mathrm{mV} /$ DIV to $10 \mu \mathrm{~V} /$ DIV ranges for measurement with an AC coupled input, for DC measurements where the source impedance is high (in excess of $1 M \Omega$ ) the input gate current should be checked and allowed for, or adjusted to zero. This is particularly desired at high temperatures (above $40^{\circ} \mathrm{C}$ ). Steps 7 and 8 in the Performance Check/Calibration Procedure describe the check and adjust procedures for setting the gate current to zero.

## Voltage Measurement

To obtain accurate DC measurements at maximum sensitivity, it is necessary to ground the input and DC balance the amplifier just before making the measurement. This is accomplished by adjusting the STEP ATTEN DC BAL as described under operational adjustment number 3 .

When measuring DC voltages, use the largest deflection factor ( $10 \mathrm{~V} / \mathrm{DIV}$ ) when first connecting the Type 7A22 to an unknown voltage source. Then, if the deflection is too small to make the measurement, switch to a lower deflection factor. If the input stage is overdriven, a large amount of current might flow into the input. See CAUTION after item 6 of First Time Operation.

Where only the $A C$ component of a signal having both $A C$ and $D C$ components is to be measured, use the $A C$ -GND-DC switches to take advantage of the pre-charging circuit incorporated in the unit. The pre-charging circuit permits the coupling capacitor to charge to the DC source voltage when the AC-GND-DC switch is set to GND. Procedure for using this circuit is as follows:
a. Before connecting the Type 7A22 to a signal containing a DC component, set the AC-GND-DC input coupling switch to GND. Then connect the input to the circuit under test.
b. Allow about one second for the coupling capacitor to charge.
b. Set the input coupling switch to AC. The display will remain on the screen and the $A C$ component can be measured in the usual manner.
d. On completion of the measurement, set the AC-GNDDC switch to GND and short the input connector to ground.
The above procedure should be followed whenever another signal with a different $D C$ level is connected.

## CAUTION

If the Type 7A22 is connected to a large DC voltage source without using the pre-charge provision, the peak charging current (into $0.1 \mu \mathrm{~F}$
capacitor) will be limited only by the signal source, and this source may be damaged or destroyed.

When a large DC voltage has been applied to the Type 7A22 with the input AC coupled, the input coupling capacitor acquires a charge due to dielectric polarization and acts as a low voltage, high impedance voltage source with a very slowly decaying output voltage. This can offset subsequent $A C$ coupled measurements at other DC voltages and drive the trace off-screen. A period of at least 10 min utes, with input set to GND, should be allowed to assure reasonable recovery from polarization, and a longer period may be necessary for critical measurements. If the input connectors are shorted to ground the depolarization process will require less time.

Signal Input Connectors
When connecting signals to the +INPUT and --INPUT connectors on the Type 7A22, consider the method of cou pling that will be used. Ordinary unshielded test leads can sometimes be used to connect the Type 7A22 to a signal source, particularly when a high level, low-frequency signal is monitored at a low impedance point. However when any of these factors are missing, it becomes increasingly important to use shielded signal cables. In all cases, the signaltransporting leads should be kept as short as practical.

When making single-ended input measurements, be sure to establish a common ground between the device under test and the Type 7A22. The shield of a coaxial cable is normally used for this purpose.

In some cases differential measurements require no common ground ${ }^{1}$, and therefore are less susceptible to interference by ground loop currents. Some problems with stray magnetic coupling into the signal transporting leads can also be minimized by using a differential rather than single-ended measurement. These considerations are discussed later in this section under Differential Operation.

It is always important to consider the signal-source loading and resulting change in the source operating characteristics due to the signal-transporting leads and the input circuit of the Type 7A22. The circuit at the input connectors can normally be represented by a 1 megohm resistance to ground paralled by 47 pF . A few feet of shielded cable may increase the parallel capacitance to 100 pF or more. In many cases, the effects of these resistive and capacitive loads may be too great and it may be desirable to minimize them through the use of an attenuator probe.

Attenuator probes not only decrease the resistive and capacitive loading of a signal source, but also extend the measurement range of the Type 7A22 to include substantially higher voltages. Passive attenuator probes having attenuation factors of $10 \times, 100 \times$, and $1000 \times$, as well as other special-purpose types are available through your Tektronix Field Engineer or Field Office.

Some measurement situations require a high-resistance input to the Type 7A22 with very little source loading or sig-

[^0]nal attenuation. In such a situation a passive attenuator probe cannot be used. However, this problem may be solved by using an active probe or the high input impedance provision of the Type 7A22.

## High Input Impedance

The high input impedance provision applies only to DC coupled signals which permit the use of 10 mV through 10 $\mu \mathrm{V}$ positions of the VOLTS/DIV switch, (DC coupled). Since no input attenuator is used at these switch positions, the internal gate return resistor alone establishes the 1 megohm input resistance.
The high input impedance is obtained by unsoldering the wire strap (seefig. 2-3) between the input line and the internal gate return resistance. The signal source must then provide a DC path for the FET gate current.


Fig. 2-3. Location of wire strop between inpul line and infernal gate return resistor.

The uncompensated gate current is typically less than 100 picoamperes, but may be several times higher depending upon the operating temperature. The signal-source impedance is therefore an important factor since gate current will produce a DC offset. For example, a 100 picoampere gate current through 10 megohms produces a 1 mV offset; this may result in a significant error where small voltages are of concern.

## NOTE

When the wire straps are removed, R111 and R211 are disconnected. The deflection factor in the $20 \mathrm{mV} /$ DIV to $10 \mathrm{~V} / \mathrm{DIV}$ range will be incorrect.

The high-frequency response will also depend upon the signal-source impedance, since various shunt capacitances between the source and the 7A22 input as well as the 47 pF input capacitance, must charge and discharge through that impedance (see Fig. 2-4).

## Display Polarity

Single-ended signals can be applied to either the +INPUT or -INPUT connector. If the + INPUT is chosen, positivegoing changes in the input signal will cause the trace to be deflected upward, and negative-going changes will cause the trace to be deflected downward. If the -INPUT is chosen, input-to-display polarity relationship will be reversed as shown previously infig. 2-i.

## Deflection Factor

The amount of trace deflection produced by a signal is determined by the signal amplitude, the attenuation factor of the probe, the setting of the VOLTS/DIV switch and the setting of the VARIABLE control. The calibrated deflection factors indicated by the VOLTS/DIV switch apply only when the VARIABLE control is pushed "in" to the CAL IN position.

The range of the VARIABLE control is at least 2.5:1. It provides uncalibrated deflection factors covering the full range between the fixed settings of the VOLTS/DIV switch. The control can be set to extend the deflection factor to at least 25 volts/div.

## Noise

To reduce noise and obtain a more usable display when the VOLTS/DIV switch is operated in the $10 \mu \mathrm{~V}, 20 \mu \mathrm{~V}$, and $50 \mu \mathrm{~V}$ positions or when the signal source is noisy, it is suggested that the HIGH FREQ - 3 dB POINT selector be sel to use the lowest bandwidth setting which does not appreciably distort the desired features of the signal under observation. Refer torig. 2-an for the high frequency rolloff for each setting of the HIGH FREQ -3 dB POINT selector.

## Bandwidth Selection

In addition to the differential rejection of unwanted signals, many times an undesired signal can be attenuated by varying the bandwidth of the unit. The LOW FREQ - 3 dB POINT and HIGH FREQ -3 dB POINT selectors on the front panel of the 7A22 control the low-frequency and high-frequency -3 dB points of the amplifier. The LOW FREQ - 3 dB POINT selector provides low-frequency response to $D C$ or to approximate -3 dB points at $.1 \mathrm{~Hz}, 1 \mathrm{~Hz}, 10 \mathrm{~Hz}, 100 \mathrm{~Hz}, 1 \mathrm{kHz}$, and 10 kHz . Refer tofig. 2.5 The HIGH FREQ -3 dB POINT selector controls the high-frequency rolloff from 1 MHz to 100 Hz in a 1-3-10 sequence. Beyond the -3 dB points the frequency response falls off at a 6 dB per octave rate. Refer torfig. 2-6.

Varying the bandwidth of the Type 7A22 is useful, for example, when displaying a low-frequency signal. By reducing the high-frequency response the noise can, in many cases, be considerably reduced without distorting the desired signal (seefig.2-7). Likewise, undesired line-frequency signals can be filtered out by restricting the low-frequency response of the unit. When using the LOW FREQ -3 dB POINT and HIGH FREQ - 3 dB POINT selectors, care must be taken not to distort non-sinusoidal waveforms by overly restricting the amplifier bandwidth.





Fig. 2-7. Improving signal-to-noise ratio by setfing bandwidth. (A) Lower - 3 dB FREQUENCY selector to DC, UPPER - 3 dB FREQUENCY 1 MHz . (B) Lower - 3 dB FREQUENCY selector to DC, UPPER - $\mathbf{3} \mathrm{dB}$ FREQUENCY, 10 kHz .

## Voltage Comparison Measurements

Some applications require a set of deflection factors other than the fixed values provided by the VOLTS/DIV switch. One such application is comparison of signal amplitudes by ratio rather than by absolute voltage.

To accomplish this, apply a reference signal to either input of the Type 7A22. Set the VOLTS/DIV switch and VARIABLE control throughout the subsequent comparisons. The settings of the VOLTS/DIV switch can be changed, however, to accommodate large ratios. In doing so, regard the numbers which designate the switch position as ratio factors rather than voltages.

## Differential Operation

Differential voltage measurements are made by applying the signals to the +INPUT and -INPUT connectors. Then, both AC-GND-DC switches should be set to the same positions: $A C$ or $D C$, depending on the method of signal

The Type 7A22 differential input provision may be used to eliminate interfering signals such as $A C$ line-frequency hum. Single-ended measurements often yield unsatisfactory information because of interference resulting from groundloop currents between the oscilloscope and the device under test. In other cases, it may be desirable to eliminate a DC voltage by means other than the use of a DC-blocking capacitor which would limif low-frequency response. These limitations of single-ended measurements are virtually eliminated in differential measurements.

A differential measurement is made by connecting each of the two inputs to selected points in the test circuit. The input to the amplifier will then be the difference in voltage of the two selected points (seefig. 2-9).

The ability of the Type 7A22 to reject common-mode signals is indicated by the common-mode rejection ratio (CMRR). This ratio is at least $100,000: 1$ at the input connectors for the lower deflection factors ( $10 \mu \mathrm{~V}$ to 10 mV per division) when signals between DC and 100 kHz are DC-coupled to the in puts. To show the significance of this characteristic, assume that a single-ended input signal consists of an unwanted 60 Hz signal at 1 volt $\mathrm{P}-\mathrm{P}$ plus a desired signal at $1 \mathrm{mV} \mathrm{P}-\mathrm{P}$. If an attempt is made to display the desired signal with the VOLTS/DIV switch set to .2 mV , the 60 Hz signal would produce a deflection equivalent to 5000 div, and thus little useful information about the 1 mV signal could be obtained.

If, however, the same 1 mV signal is monitored differentially so that the 60 Hz signal is common-mode at the inputs, no greater than one part in one hundred thousand of the common-mode signal will appear in the display. Thus, the desired signal produces a display amplitude of 5 div with only .05 div of interference due to the common-mode signal.

There are a number of factors which can degrade commonmode rejection. The principal requirement for maximum rejection is for the common-mode signal to arrive at the input FET gates in presicely the same form. A difference of only $0.01 \%$ in the attenuation factors of the input attenuators may reduce the rejection ratio to $10,000: 1$. Likewise, any difference in source impedance at the two points in the source under test will degrade the rejection ratio. Attenuator probes which do not have an adjustable resistance may reduce the rejection ratio to $100: 1$ or less.

Outside influences such as electrostatic and magnetic fields can also degrade the performance, particularly when low level signals are involved. Electrostatic interference can be minimized by using shielded signal transporting leads of the same type to the two inputs, and by twisting the leads together throughout most of their length.

Care should be taken to minimize the movement of the signal transporting leads, as any movement of a lead, in the presence of a maanetic field, will tend to induce a sianal into that lead. Where an interfering magnetic field cannot be avoided, the pickup loop formed by the two leads should be minimized by taping or twisting them together throughout most of their length. Low-frequency measurements can be similarly protected by using a shielded cable which contains a twisted pair of conductors.

(B) Signal applied to - INPUT.

Fig. 2-8. Waveforms showing differential reiection of a common-mode signal. Resultant waveform (c) shows the difference between the two signals.

## DC Offset Operation

By using the DC OFFSET controls, it is possible to use the Type 7A22 differentially in a slide-back mode, to observe small signal whose DC potential difference may be considerable. The offset is continuously adjustable from +1 V to -1 V when the VOLTS/DIV switch is in the $10 \mu \mathrm{~V}$ to 10 mV positions. In the $20 \mathrm{mV}, 50 \mathrm{mV}$ and .1 V positions of the VOLTS/DIV switch, the 1 V offset is effectively multiplied by the input attenuator to a range of E1O V. Iable 2-1 summarizes the effective DC offset voltages internally available for all the VOLTS/DIV switch positions. The table also lists the input attenuator that is switched into the amplifier circuit for the various VOLTS/DIV switch positions.

TABLE 2-1

| VOLTS/DIV setting | OFFSET RANGE | ATTENUATOR in |
| :---: | :---: | :---: |
| $10 \mu \mathrm{~V}$ to 10 mV | $\pm 1 \mathrm{~V}$ | $1 \times$ |
| 20 mV to 0.1 V | $\pm 10 \mathrm{~V}$ | $10 \times$ |
| 0.2 V to 1 V | $\pm 100 \mathrm{~V}$ | $100 \times$ |
| 2 V to 10 V | $\pm 1000 \mathrm{~V}$ | $1000 \times$ |

${ }^{2}$ CAUTION- $\pm \mathbf{5 0 0}$ valis is the maximum allowable signal voliage of each inpul.

Using the DC OFFSET functions:
Set the Type 7A22 controls as follows:

| VOLTS/DIV | loV |
| :--- | :--- |
| VARIABLE (CAL IN) | CAL |
| POSITION | Midrange |
| AC-GND-DC <br> ( + and - INPUT) | GND |
| HF -3 dB POINT | 1 MHz |
| LF -3 dB POINT | DC |
| STEP ATTEN DC BAL | Adjusted for DC balance |

1. Position the trace to graticule center (or some other convenient reference line) using the POSITION control.
2. Connect a coaxial cable from the signal source to the +INPUT.
3. Set the + INPUT AC-G ND-DC switch to $D C$ and measure the DC level to be offset.
4. Set the VOLTS/DIV to the largest deflection factor in an offset range which will encompass the DC level measured in step 3. Se Table 2-1 and front panel color bands.
5. Set the LF -3 dB POINT selector to DC OFFSET,


Fig. 2-9. Connecting a differential amplifier across a circuit.
6. Use the COARSE and FINE controls to move the portion of the signal to be observed to the reference line established in step 1.
7. If a different size display is needed, the deflection factor may be changed in the same offset range.

## NOTE

If switching into another offset range, the OFFSET controls will need to be readjusted. If switching into a smaller offset range, check that the available range is sufficient to encompass the DC level present (see steps 3 and 4 above).

## Input Overdrive Indicator

The INPUT OVERDRIVE indicator turns on when the signal to the input FETs approaches the differential dynamic range of the amplifier. The 7A22 should not be left connected to a circuit if this light is on, as this may mean that a damaging voltage is present.

The INPUT OVERDRIVE indicator serves another important function. If the amplifier is direct-coupled at the input, a DC differential signal could overdrive the input stage and cause a reduction in gain. The small voltages to be measured will not be distorted, but will be reduced in amplitude. As a result, amplitude measurements made under such conditions will not be accurate. The Type 7A22 INPUT OVERDRIVE indicafor provides an indication that such a signal is present by lighting before the gain calibration changes by $1 \%$.

If the INPUT OVERDRIVE lamp turns on, there are two pos sible ways to continue:

1. Switch the LF -3 dB POINT selector to DC OFFSET. DC differential sianals may then be balanced out as indicated in Table 2-1.
2. Switch the AC-GND-DC switch to AC. DC differential signals up to 1000 V (either input not to exceed 500 V ) may be removed by using $A C$ coupling at the input. This necessarily limits the low frequency response to 1.6 Hz (or 0.16 Hz with a $10 \times$ probe).

The INPUT OVERDRIVE lamp is insensitive to commonmode overdrives, and it is possible to overload the Type 7A22 without lighting the input overdrive light.

In summary the overdrive indicator will turn on under the following conditions:
a. The input signal exceeds the differential dynamic range of the amplifier (seesectiondfor table of dynamic ranges).
b. An input protective fuse is blown. In this case, the light will remain on even if the AC-G ND-DC switches are set to GND.
c. There is a circuit malfunction.

## Readout

If the Type 7A22 is to be used in an oscilloscope having readout capabilities, special probes which correct the readout deflection factor for probe attenuation may be used. Divider probes not having the sensing capability may be used with the instrument, but they will not operate the sensing system, and the deflection factor of the plug-in only (as read on the VOLTS/DIV knob) will be displayed.

The +INPUT and -INPUT connectors have an outer ring which is connected to the readout probe sensing device. This allows the main-frame readout to display the correct deflection factor from the probe tip for any probe attenuation. For
example: if a 10X probe is used it will increase the deflection factor, in the readout display, by a factor of 10 . Then the actual deflection factor at the probe tip is displayed (see Table 2-2).

## NOTE

If only one divider probe (or two probes with equal divider ratios) is connected, the deflection factor at the probe tip will displayed; if probes with different divider ratios are connected (e.g., IOX and 100X), the readout will display the deflection factor at the tip of the probe with the larger division ratio (100X).

TABLE 2-2

| TYPE 7A22 <br> Plug In | Main-Frame Displayed Readout |  |  |
| :---: | :---: | :---: | :---: |
| VOITS/DIV <br> Setting | Probe Atten <br> used 1 X | Probe Atten <br> used 10X | Probe Atten <br> used 100X |
| .5 mV | $500 \mu \mathrm{~V}$ | 5 mV | 50 mV |
| 50 mV | 50 mV | 500 mV | 5 V |

Trace Identify. With the oscilloscope turned on and a sweep displayed on the CRT, check for approximately 0.2 div of vertical movement of the trace when the IDENTIFY pushbutton is depressed. The vertical scale factor readout associated with the 7A22 will change to the ward IDENTIFY.

NOTE

An incorrect CRT readout will occur in the $10 \mathrm{~V} / \mathrm{div}$ position when using the 100X Readout coded probe (P6009, Tektronix Part No. 010-0264-01). When used in $10 \mathrm{~V} /$ div setting, reading will show IV instead of 1 KV .

## introduction

A block diagram description covering the general configuration of each circuit in the Type 7A22 is included in this section. Following the block diagram description is a detailed description of each circuit and the functions of specific components.

Simplified drawings are provided where necessary for easier circuit understanding. Complete schematic diagrams are included in the Diagrams section. These should be referred to throughout the detailed circuit descripttion.

The values of resistors on the schematics are in ohms unless otherwise specified. Capacitor values are indicated in the following manner unless otherwise specified: whole numbers indicate that the value is in pF , decimal numbers indicate that the value is in $\mu \mathrm{F}$. For example, 33 pF and 0.1 $\mu \mathrm{F}$.

## BLOCK DIAGRAM DESCRIPTION (see Block Diagram Pullout preceding schematics)

## Input coupling

A signal applied to the + or -Input connector passes through the input coupling selector switch to the input attenuator circuit. The signals can be AC coupled, DC coupled or disconnected internally. (See Schematic Diagram Number 1].

## Input Attenuators

The input attenuators for the + and -inputs are identical and are conventional RC type attenuators. Common resistive elements are adjustable to facilitate matching the - and + attenuators to obtain optimum DC common-mode signal rejection.

The attenuators (Schematic Diagram number 3) are fre-quency-compensated voltage dividers which provide constant aftenuation at all frequencies within the passband of the instrument, while maintaining a constant input time con-

## Preamp

From the input attenuators, the signal is coupled to the preamp. The preamp consists of two identical feedback amplifiers connected in a differential configuration. The overall differential gain is approximately 15.

The supply voltages for the two amplifiers are obtained from a common power supply which is bootstrapped to the input to improve the common-mode rejection ratio of the preamp.

Each input is equipped with an overdrive protection circuit consiting of fuses and clamping diodes. For deflection factors from $10 \mu \mathrm{~V} / \mathrm{DIV}$ through $10 \mathrm{mV} / \mathrm{DIV}$ the fuse will open if the current exceeds $1 / 16$ A (approximately 16.5 volts at the input), preventing damage to the input circuitry.

## CAUTION

The input protection circuit clamps the input to a fixed voltage when too large an input signal is applied. In the $10 \mu \mathrm{~V}$ to 10 mV positions there is no resistance through the ATTENUATOR switch. There is a possibility of damage to the signal source, since a very large current surge can flow before the fuse opens.

When the LOW FREQ -3 dB POINT selector is in any position other than DC or DC OFFSET and the Input Coupling switch is in DC, there is no on-screen indication of the DC conditions in the preamp. If the differential dynamic range of the amplifier is exceeded and the amplifier is driven into non-linearity or overdrive, an erronerous display is likely.

An overdrive detector circuit is provided to indicate when the preamp is approaching the limits of its differential dynamic range. A front-panel indicating lamp lights when overdrive occurs.

An offset generator is provided to balance out any current in the preamp resulting from signals containing differential components. Offset (variable) allows the varying component to be amplified, and at the same time maintains the amplifier differential capabilities.

## Low Frequency - 3 dB Point

The push-pull output of the preamp is coupled through a LOW FREQ - 3 dB POINT selector. The selector switches the components of the coupling network in each half of the preamp to select the low frequency -3 dB points $(.1 \mathrm{~Hz}, 1 \mathrm{~Hz}$, $10 \mathrm{~Hz}, 100 \mathrm{~Hz}, 1 \mathrm{kHz}$ and 10 kHz ). The DC position of the selector bypasses the low frequency selection circuitry and direct-couples the preamp to the Output Amplifier.

## Output Amplifier

The signal from the LF -3dB POINT selector is coupled to the gain-switching section of the Output Amplifier. This section of the Output Amplifier is a pair of feedback amplifiers similar to 'that of the prearnp. The VOLTS/DIV switch changes the amplifier gain.


Fig, 3-1. Generalized feedback system showing the relation between input and output.

## High Frequency -3 dB Point

The HF -3dB POINT selector switches capacitance across the output of the Gain Switching Amplifier to set the high frequency -3 dB point at any of 9 frequencies; $100 \mathrm{~Hz}, 300$ $\mathrm{Hz},{ }^{\prime} 1 \mathrm{kHz}, 3 \mathrm{kHz}, 10 \mathrm{kHz}, 30 \mathrm{kHz}, 100 \mathrm{kHz}, 300 \mathrm{kHz}$, and 1 MHz . The capacitance used in the 1 MHz position is adjustable to set the bandwidth to normal value.
Positioning of the trace, and VARIABLE VOLTS/DIV, are provided in the stage following the HF -3 dB POINT selector.

Overall amplifier gain is adjusted in the signal output stage of the Output Amplifier by adjusting the common emitter resistance.

## GENERAL INFORMATION

## Feedback Amplifiers

Since the Type 7A22 utilizes several multi-stage feedback amplifiers, a brief review of feedback systems in general is given.

Fig. 3-1 represents a generalized feedback system in which it is desired to produce an output signal accurately and stably related to the input. The arrangement of Fig. 3-1 causes the modified output to be nearly equal to the input. Any difference between these is detected by the comparator, which produces an error signal equal to the difference, and applies this error to the amplifier, which amplifies the error and feeds back a correction to' reduce the 'original error


Fig. 3-2. Feedback amplifier (Single-ended version)

The input to the modifier (the system output) is also accurately related to the system input, provided the modifier is constructed of stable components.

Another way of looking at the system is to start at the output and work backward. Specifically, assume an amplifier gain of 10,000 and a feedback modifier which is a $10 \times$ divider. Assume a 10 volt output. The modifier output is 1 volt, and the error signal (output $\div$ gain) is 1 mV , so that the input is 1.001 volts. In this case, the error between the desired output ( $10 \times$ input) of 10.01 volts and the actual output of 10.00 volts is only 10 mV , or 1 part in 1,000 .

In practice the comparator and error amplifier are often combined in a differential amplifier. A single-ended version of the basic configuration used in the Type 7A22 is illustrated in fig. 3-2 with the basic blocks offig. 3-1 identified. The comparator is $F E T Q_{1}$. Any change in the gate-to-source bias voltage Idictated by the standing current established by $R_{4}$ and the supply voltages) will cause a change in drain current, the change being applied as an error signal to the input of the error amplifier.

The error amplifier consists of grounded emitter stage $Q_{2}$ driving emitter follower $Q_{3}$. The internal output appears at the emifter of $Q_{3}$ and is fed back to the comparator input via modifier (voltage divider) $\mathbf{R}_{2}, \mathbf{R}_{\mathbf{1}}$. For this amplifier, the system output, $V_{o s,}$ can be determined by:

$$
V_{o s}=\left(1+\frac{R_{2}}{R_{1}}\right) V_{o m} .
$$

Since $V_{o m}$ is approximately equal to the input voltage $V_{i}$, then the system gain, $\frac{V_{i}}{V_{o s}}$, is approximately equal to $1+$ $\mathbf{R}_{\mathbf{g}}$ $\mathrm{R}_{1}$

The useful output of the amplifier is the $Q_{3}$ collector signal current $i_{0}$, which flows through $R_{11}$ (in addition to the relatively small error current from $Q_{1}$ ). $V_{\text {om }}=i_{0} R_{1}$ and since $V_{o m}$ is approximately equal to $V_{i}$, and $i_{0}$ is approximately equal to $i_{0}$ o then $i_{0}$ is approximately equal to $\frac{V_{i}}{R_{1}}$. Thus the output current vs, the input voltage depends primarily on the gainsetting resisfor, $\mathrm{R}_{1}$.

An output voltage can also be obtained by passing $i_{0}$ through the load resistor, $R_{3}$. The overall voltage gain is then $\frac{V_{0}}{V_{i}}$, which is approximately equal to $\frac{R_{0}}{R_{1}}$.

## Differential Configuration

If the lower end of $R_{1}$ is connected to the same point in another identical circuit instead of being returned to ground, the result is a differential feedback amplifier with push-pull output, which is the configuration in the Type 7A22. A differential feedback amplifier, such as is used in the $15 \times$ preamp, is shown infig. 3-3.

From the previous description, the $Q_{1 a}$ and $Q_{1 b}$ source voltages $V_{a m}(a$ and $b)$ follow the input voltages $V_{i a}$ and $V_{i b}$ respectively, hence any differential input voltage, $V_{i}$ will result in a nearly equal source to source voltage $V_{\text {om, }}$, which in turn is due to an output signal current $i_{o}^{\prime}=\frac{V_{o m}}{R_{1 \mathrm{a}}+R_{\mathrm{tb}}}$


Fig. 3-3. Feedback amplifier (Differential configuration).
$=\frac{V_{i}}{R_{1 \mathrm{a}}+R_{1 \mathrm{~b}}}$.
Note that FETs have been used in $\mathrm{Q}_{3}$, rather than NPN bipolars as in Fig. $3-2$ to avoid loss of signal current from the base lead. The operation of the amplifier remains unchanged.

## DETAILED CIRCUIT DESCRIPTION

## Input Coupling (See Schematic 1)

Input signals applied to the +input connector can be AC coupled or internally disconnected. When the input coupling switch, S101 (see $\times 15$ preamp diagram), is in the DC position, the input signal is coupled directly to the input attenuator. In the $A C$ position, the $A C$ signal is coupled through coupling capacitor Cl 01 , and the DC component is blocked from the input amplifier. The GND position internally connects the gate of the input amplifier to ground. This provides a ground reference for the amplifier without removing the input leads or otherwise disconnecting the input signal.

Resistor R103 allows C101 to be precharged in the GND position so that when S101 is switched to the AC position with a high DC level applied, there is no charging current surge into the input of the amplifier. Excessive loading is also avoided for the circuit under test, since the normal im-
pedance of $1 M \Omega-47 \mathrm{pF}$ is still seen by the signal source. The -input switch, S201, functions in the same manner as the +input.

## Input Attenuators

## See Schematic

To produce the vertical deflection factor indicated on the front panel by the VOLTS/DIV switch, the gain of the feedback amplifier in the gain switched amplifier circuit is changed by switching the source resistor (R407) of Q404 A and B (See Schematic 2 ) for switch positions $10 \mu \mathrm{~V}$ to 10 mV . For switch positions above 10 mV , input attenuators are switched by S108 into the input circuit of the Type 7A22, in conjunction with the gain switching resistors, R407, to produce the selected deflection factors.

These attenuators are frequency-compensated voltage dividers. For DC and low frequency signals, they are primarily resistive dividers (e. g., R108C, R108D) and the voltage attenuation is determined by the resistance ratio in the circuit. The reactance of the capacitors in the circuit is so high at the lower frequencies that their effect is negligible. However, at higher frequencies, the reactance of the capacitors decreases and the attenuator becomes primarily a capacitive voltage divider (e.g., C108C, C108D).

In addition to providing constant attenuation at all frequencies within the bandwidth of the instrument, the input attenuators are designed to maintain the same input RC characteristics ( 1 megohm in parallel with 47 pF ) for each setting of the VOLTS/DIV switch. Each attenuator contains an adjustable capacitor (e.g. C108C) to provide correct attenuation at high frequencies, and an adjustable shunt capacitor to provide correct input capacitance.

## Gate Current Compensation

The leakage current associated with the gates of the input FETs may be as high as 100 pA . This 100 pA of leakage current (through 1 megohm to ground, R111 or R211) will produce an offset of $100 \mu \mathrm{~V}$, which at high input sensitivities is not acceptable. To compensate this effect, the gates of the input FETs may be adjusted to zero volts by returning R111, R211 through variable controls R115 and R215 to a slightly negative supply voltage (see Fia. 3-4).

Leakage current associated with the gates of the input FETs and the overdrive protection diodes increases rapidly with temperature, approximately doubling for every 10 " C . To compensate this increase, a temperature sensitive input current balancing network is included, using thermistors as the sensing elements.

As the voltage across R111 and R211 increases due to increasing FET gate current at increased temperatures, an equal voltage change is produced in the thermistor compensating circuit, maintaining the FET gate level at zero volts.

The gate current compensation becomes inoperative if the straps are removed for high input impedance operation.

## Input Amplifier

The input amplifier circuit in the Type 7A22 is made up of two identical feedback amplifiers connected in a differ-


Fig. 3-4. Gate Current Compensation.
ential configuration with a push-pull output. The power supply voltages (except at the output) for each feedback amplifier are obtained from a power supply that is bootstrapped to the common-mode input signal. This improves the CMRR of the amplifier, Input overdrive protection is provided in the input circuit to prevent damage to the semiconductors if a large overdrive is inadvertently applied to the input.

Any amplifier of this type, in which the feedback is taken to the input element, is likely to exhibit a negative resistance component of impedance at higher frequencies. If the input signal source impedance is inductive with a sufficiently high "Q", the amplifier could oscillate. C115, R116, R117 and C215, C 217 compensate for this negative input resistance.

X 15 Preamp. The feedback amplifiers in the + and inputs are identical except for circuit numbers, and operate in a coupled differential mode as described previously underfeedback amplifiers.

In the actual circuit (see Schematic 1 ) the + feedback amplifier consists of the comparator Q133A, error amplifier Q144A, Q153, feedback modifier R151, R153 and output load resistor R159. R151 is the gain setting resistor for the amplifier, and the approximate gain of the amplifier can be determined by dividing R159 by R151, ( $\left.\begin{array}{l}R_{0} \\ R_{i}\end{array}\right)$.

Diode CR131 is used for temperature compensation of the base-emitter junctions of Q144A and Q144B. This keeps the total voltage across the input stage current-setting resistors R133, R233 constant with temperature, Diode CR144 connected between base-emitter of Q1 44A, protects the transistor against reverse base-emitter breakdown. CI 44 and C244 stabilize the circuit at the higher frequencies.

DC Balance. The DC level at the output of $Q 153, Q 253$ is balanced by R258, STEP ATTEN DC BAL. The STEP ATTEN


Fig 3-5. Common-mode Rejection using floating power supply.

DC BAL control changes the current through R257, R259, thereby changing the DC balance. It is used to adjust the difference in potential across the output of the $\times 15$ Preamp (pins Z and W) to zero with the input coupling switches at GND and the LOW FREQ - 3 dB POINT switch set to DC.

With high frequency common-mode signals the wiring stray capacitance of the $\times 15$ preamp can inject undesirable current into the two output lines at high frequencies. C330 is adjusted to equalize these currents, thus extending the frequency range over which useful CMRR can be obtained.

Floating Power Supply. The supply voltages for the $\times 15$ preamp are obtained from a chain of Zener diode shunt regulators, VR305, VR320 and VR325 connected in series. Cuprent is supplied by two current sources, Q304 and Q324.

C307, C317 and C325 filter out the Zener noise. C315 increases the bootstrap stability at higher frequencies.
Any common-mode changes that occur in the input amplifier, except at the output, are coupled to the power supply through Q314. Q314 is an emitter follower whose gain is maintained very close to unity by the minimum loading presented to its output by the high collector impedance of Q304 and Q324, thus achieving good bootstrap efficiency.

Common Mode Rejection. One of the primary functions of the $\times 15$ preamp is to reject any common-mode component in the input signals, and amplify only the difference. In the extreme case of the inputs tied together and a common voltage applied, the output of the amplifier is ideally zero, and would actually be zero provided that the characteristics


Fig. 3-6. Input cross neutralization.
of all corresponding elements on the two sides of the amplifier (seefig. 3-5) were exactly matched. In practice any mismatch will cause a differential output. Even with perfect matching, there is still a common-mode output current resulting in an undersirable common-mode signal applied to the subsequent stages of the amplifier (common mode gain).

The floating power supply eliminates these difficulties and improve the CMR. Suppose the input to the bootstrap amplifier is connected to the junction of R151 and R251 (seefig $3-5)$. It can be seen that now the entire power supply and amplifier moves an amount equal to Vcm (ie: follows Vcm ) and that no changes in voltage or current levels occur anywhere within the amplifier as a result of Vcm , except for Q153 and Q253 drain to gate voltage. Thus the only mismatch of importance is that of Q153, Q253 amplification
factors, and being in the third stage of the amplifier at a point of relatively large differential signal level, this causes only a small degradation in CMR.
At higher frequencies the inevitable stray capacitances from various points in the $\times 15$ preamp to ground begin to inject significant current into the amplifier as a result of common mode signals. The differential capacitor C330, (Fig. $3-5$ or Schematic $\langle\downarrow$ ) connected from a point in the floating power supply to the two output lines, is used to inject adjustable currents into the output. It can be adjusted to equalize the net output currents resulting from high frequency common mode signals and so extend the range of frequencies over which useful CMRR can be obtained.

Cross Neutralization. The use of a common bootstrap power supply results in an undesirable capacitive coupling
between the two inputs. Consider the effect of applying +1 volt to the + input while keeping the - input at 0 volts (see fig. 3-6).

The results are (a) an output current of 4 mA , as shown, and (b) a shift of all supply voltages and several other voltage levels by +0.5 V due to the divider action of R151, R251 operating into the bootstrapped power supply system. Specifically, the drain of Q133B also rises +0.5 V and injects a current $i_{1 b}$ through the drain to gate capacitance of Q133B and into the -input. If there is any impedance between the -input and ground, $i_{1 b}$ will develop a voltage across it which, being applied to the -input subtracts from the original + input and causes an erroneous output (see fig. 377).

Note that the output current flowing through R253 causes its output end (Q253 source) to go to -0.6 V. A capacitor, C241, connected from this point to the -input can be adjust to divert $i_{1 b}$ away from the input line $\left(i_{1 b}\right)$ and so neutralize the effect of $C_{d g}$ and reduce the -input current to zero. R141 and Cl 41 perform a similar function for the tinput.

Input Overdrive Protection. Since the input FETs Q133A and $B$, being semiconductors can be destroyed by sufficiently large overdrive applied directly to them, some input protection is a necessity. The important components of the protection system used in the Type 7A22 are shown infig. 3-8A.

There are two different kinds of overdrive associated with the Type 7A22, (a) single-ended overdrive, with one inpuit grounded, and (b) common-mode overdrive, with approximately equal input voltages.
(a) Assume the -input grounded and a steadily increasing voltage on the + input. The chart infig 3-8B indicates the sequence of events: Fl 19 will open if the + signal source can supply $1 / 16 \mathrm{amp}$ of current. If this much current is not present, the +input remains at +16.5 V , with the overdrive current flowing to ground as shown inrig. 3-9.

Now assume the +input grounded and a steadily increasing - voltage on the -input. The sequence of events is shown infrig. 3-8C.


Fig. 3-7. Effects of high impedance to ground in the - INPUT.
(b) For common-mode overdrives the clamping sequence is essentially similar, except the $\times 15$ amplifier does not overload, and the current $i_{2}$ does not flow until the input reaches approximately -13 V . The fuse opening current paths are shown infig. 3-8ิA.

For differential overdrive the action is a combination of the + and - single-ended sequences, with the -input supplying $\mathrm{i}_{2}$. (In effect a $5 \mathrm{k} \Omega$ resistor is connected across the inputs when the differential voltage reaches 3 V ). The fuses will not open until one or both inputs reach +16.5 V or -16.5 V .

DCOffset. The purpose of the DC offset system is to allow a differential slideback measurement, i.e.: to buck out small DC components of input signals and allow the amplifier to amplify only the varying components, while keeping the differential capability. This means that when a DC voltage is applied across the inputs, some means must be found to balance out the resultant output current. rig. 3-9 illustrates how this is done.
frig. 3-9A shows the standing currents for zero inputrig, [3-98 shows the currents with a 0.25 V DC input applied to the +input. This would cause an $i_{0}^{\prime}$ of 1 mA to flow through R151, R251. However, if this 1 mA is supplied as shown by the offset generator, then no net output current results. Both the Q1 33A and Q133B source currents and the output standing currents, $i_{0}{ }^{\prime}$, remain at their zero signal value, 2 mA and 5 mA respectively.

Offset Generator. The offset generator produces the adjustable balanced offset current for use in the $\times 15$ preamp. Due to the wide range of the offset system ( 200,000 div at $10 \mu \mathrm{~V}$ per div) stable components are used and circuit techniques which minimize drift and noise are employed in the offset generator. A 10 turn coarse and 1 turn fine OFFSET control is used to obtain adequate resolution at low deflection factors.

The functional arrangement of the offset generator is shown in Fig. 3-10. In the reference voltage generator the OFFSET control, R270, taps an adjustable portion ( $\mathrm{V}_{1 \mathrm{~b}}$ ) of the voltage across the reference Zener VR270, and a fixed voltage $\left(V_{1 a}\right)$ is taken from the voltage divider formed by R271, R279 (approximately $50 \%$ of the reference voltage); thus, the difference voltage $\left(\mathrm{V}_{1 \mathrm{~b}}-\mathrm{V}_{1 \mathrm{a}}\right)$ is adjustable over the range of at least -4 V to +4 V .

This adustable difference voltage is applied to the inputs of a balanced feedback amplifier conceptually similar to that described previously under differential configuration. In amplifier " $A$ ", the feedback action forces the -input voltage (also the output voltage) $\mathrm{V}_{2 \mathrm{~d}}$ to follow the + input $\mathrm{V}_{1 \mathrm{a}}$. In a similar manner, $\mathrm{V}_{2 \mathrm{~b}}$ follows $\mathrm{V}_{1 \mathrm{~b}}$ in amplifier " B ". The differential input $\left(V_{1 b}-V_{1 a}\right)$ is therefore reproduced across resistors R287, R289. The resultant current, $\frac{V_{2 b}-V_{2 a}}{R 287+R 289^{\circ}}$, which is "ioffset", flows through the FET (Q273, Q283) output stages of the amplifier and out their drains to the $\times 15$ preamp.

When the offset is not in use $V_{1 b}$ is switched to the fixed divider (R273, R277) by the OFFSET ON/OFF switch (part of the LF -3 dB POINT switch). $\mathrm{V}_{1 \mathrm{a}}$ is adjustable over a small range with respect to $\mathrm{V}_{1 \mathrm{~b}}$ by the COARSE DC BAL control, whose purpose is to adjust out any initial DC unbalance in the $\times 15$ preamp, and to bring its output to zero with zero input.


Fig. 3-8. (A) Overdrive Protection System showing current paths. (B, C) Sequence of events leading to excessive overdrive.

In the actual circuit, the reference voltage generator is modified by the addition of a FINE OFFSET control (R265), which changes the effective range of the 10 turn COARSE potentiometer by means of two voltage dividers, one connected to each end of the COARSE control. A capacitor filters out Zener noise from the reference voltage.
The feedback amplifiers A and B are composed of Q264A, Q273 and Q264B, Q283 respectively, with the reference input applied to the emitters of dual transistor Q264 and the feedback to its bases. Current source Q284 supplies operating current for the amplifiers.

Input overdrive Indicator. When the LF - 3 dBPOINT selector is in a position other than DC, there is no on-screen indication of the DC conditions in the $\times 15$ preamp, and it may be driven into non-linearity or overload by a DC component, leading to erroneous displays. The input overdrive indicator detects this condition and indicates by means of a warning light that the $\times 15$ preamp is approaching the limits of its dynamic range.
The indicator consists of a threshold detector (CR341, CR343, Q344) and a monostable lamp driver (Q334, Q354). In the quiescent state, while no overdrive exists, CR341,


Fig. 3-9. Offsei system showing (A) Conditions with zero offset, (B) 0.25 V DC offset.

CR343, Q344, Q334 and Q354 are all cut off. R341 and R343 form a voltage divider to set the emitter of the threshold detector, Q344, at approximately +32 V .

Now suppose one of the $\times 15$ preamp output lines exceeds $+33.4 \mathrm{~V}_{i}$ CR341 (or CR343) and Q344 collector current turns on Q334 via R347. Q334 collector current turns on Q354 via R333, and the resulting negative going step at Q354 collector furns on the lamp. This causes current in R349 to turn Q334 on harder. If the overdrive is removed immediately, Q344 turns off. However, the current through C349, R349 keeps Q334, Q354 and the lamp on until C349 is charged to its new voltage (approximately 1 second) and the current through R337 exceeds that in R349, R337. This keeps Q334 off for approximately 1 second, even if Q344 receives another overdrive signal.. Thus for repetitive overdrives, (up to about 10 kHz ), the monostable free-runs and the lamp flashes at approximately a 2 second rate. (Above 10 kHz the high speed $A C$ effectively charges up the stray capacitance and makes the circuit act as if it had a DC overload.) If, however, a DC overload keeps Q344 on, the end of C349 discharge does not turn Q334 off since it is kept on by current through R347. Thus, the lamp stays on until the overdrive is removed.

LF - 3 dB POINT Selector. This switch selects the low frequency -3 dB point of the amplifier and has a range of 0.1 Hz to 10 kHz in decade steps. Selection is done by switching the resistor and capacitor of a pair of capacitor couplings in each leg of the amplifier. fig. 3-it shows half of the selector, with the switch split up into its functional elements.

For the 100 Hz to 10 kHz positions, Cl 56 is used and resistors R353C, R353B and R353A are switched to the output in the following combinations:

| -3 dB frequency | 100 Hz | 1 kHz | 10 kHz |
| :---: | :---: | :---: | :---: |
| output resistors | R353C | R353 \& R353B | R353C \& R353A |

Whenever R353A or R353B is not on the output side of Cl 56, it is placed across the input, to keep the high frequency load resistance seen by Vin constant.

C353A is switched across Cl 56 for the lower 3 ranges, $(0.1 \mathrm{~Hz}, 1 \mathrm{~Hz}$ and 10 Hz ) and C156 is shorted out for DC coupling. Resistor R157 adds a small increment in gain when C156 is used to compensate for the loss of gain through the capacitive divider formed by Cl 56 and stray capacitance $\mathrm{C}_{\mathrm{s}}$.

When the 0.1 Hz to 10 Hz positions are in use, C353A may be rapidly pre-charged by switching to the 10 Hz position momentarily.

## OUTPUT AMPLIFIER (See Schematic)

## Gain Switching Amplifier

The gain switching amplifier (Q404, Q414, Q424, Q524) is a balanced differential configuration very similar to the $\times 15$ preamp but with a fixed power supply. Gain switching is accomplished by switching R407.


Fig. 3-10. Functional orrangement of the offset generator.

Diodes CR413, CR513 prevent base-emitter reverse breakdown in Q414 under overdrive conditions: CR419, CR519 limit the output current that can flow through Q424, Q524. CR415, CR417 and CR515, CR517 prevent the bases of Q424, Q524 from swinging too far from the emitter, preventing breakdown and ensuring a fast, clean overdrive recovery. The AC STEP ATTEN BAL adjustment (R505) in series with the source of Q404B, develops a small adjustable voltage which removes any initial unbalance in the gate-to-source voltages of Q404 $A \& B$. The AC STEP ATTEN BAL also sets the voltage across
gain-setting resistor R407 to zero when the differential input (gate-to-gate) voltage is zero.

VAR BAL (R425) is used to balance the output currents of Q424 and Q524 with zero input to the amplifier.

The gain switched amplifier has excellent overdrive characteristics so that the full dynamic range of the input amplifier can be used. It is gain-switched over a range of about $1,000: 1$ with no significant change in bandwidth or any other characteristics.

HF - $\mathbf{3} \mathrm{dB}$ POINT Selector. The HF -3dB POINT selector simply switches different values of capacitance across the output of the gain-switched stage to set the high frequency -3 dB point of the amplifier. The -3 dB point is adjusted in the 1 MHz position by C 425 .

## Variable Output Stage

The variable output stage (Q434, Q534) does not contribute much voltage gain, but it performs a number of other functions. The configuration is a collector loaded, common emitter amplifier with emitter degeneration, the gain (collector signal current vs. input voltage) being determined by the total emitter to emitter resistance. This resistance is adjusted over a 2.5:1 range by the VAR control, R535, which provides a fine control of gain in the uncalibrated position, and interpolates between the steps of the VOLTS/DIV switch.

POSITION control is obtained by feeding adjustable currents into the emitters of Q434, Q534, via resistors R431, R531. This current adds to or subtracts from the signal current developed in the emitter resistors R432, R535, R532, and flows out of the collectors into the signal and trigger output amplifiers.

## Signal Output Amplifier

The signal output amplifier (Q444, Q544) is a push-pull common ernitter configuration with emitter degeneration to improve the stability and linearity of the circuit. The gain of the stage is determined by the total emitter-to-emitter resistance, which is adjustable by GAIN control (R540) to facilitate calibration of the instrument. The gain of the amplifier is set in the 1 mV position of the VOLTS/DIV switch.

R443, R543 equalize the power in Q444, Q544 under dy.namic conditions, thereby eliminating thermal distortion. C443, C543 are high-frequency by-pass capacitors.

## Trigger Output Amplifier

The trigger output stage (Q454, Q554) is almost identical to the signal output stage, except the stage gain is not adjustable, so that the output, while nominally the same as the signal output level, can in fact have quite a wide tolerance.

## INDICATOR OSCILLOSCOPE READOUT

## General

The readout block consists of switching resistors and a probe sensing device. The switching resistors are used to signal to the Indicator Oscilloscope the setting of the VOLTS/ DIV switch. R618A, R618B, and R618G select the number 1, 2, or 5 depending upon the combination that is switched in. R618C, R618D, R618L, and the output of the probe sensing device (Q614) select the decimal point (number of zeroes) again depending on the switched-in resistor combination. R618E, R618F, and R618N select the Volts sub-unit, either m (milli), $\mu$ (micro), or no sub-unit. R618H and R618K select


Fig. 3-11. Partial Low Frequency $\mathbf{- 3} \mathbf{d B}$ Point selector for $\boldsymbol{+}$ Input amplifier.
the symbol V (volts). R618J and R618M select the symbol $>$ when the VARIABLE VOLTS/DIV knob is in the uncalibrated position. Refer to the Schematic Diagram of the VOLTS/DIV Switch to find the resistors associated with a particular setting of the VOLTS/DIV switch.

## Probe Sensing

The probe sensing device (Q614) identifies the attenuation of the probe connected to the front panel connector, by sensing the amount of current flowing from the current sink through the probe coding resistance, and adjusts the readout display so that the actual probe tip deflection factor is displayed.

The probe connected to the + (or - ) INPUT connector forms a voltage divider with R610 (R620) through CR615 to the -15 V supply. This forward biases CR610 (CR620) allowing current to flow through R630, reducing the bias on Q614. The bias voltage, applied to the base of Q614, is set by the probe coding resistance of the divider probe.

When the -15 V clock pulse is applied to interface connector B33, Q674 is interrogated and its collector currents (detrmined by the base voltage and emitter resistor, R614) is added to the column current through interface connector A37.

With a $1 \times$ probe (or no probe) connected, Q614 is tumed off, and the deflection factor, in the readout display, is determined by the setting of the Readout Switch, S407, (part of the VOLTS/DIV switch) only.

With a 10X probe connected to the input ( + or -), the bias on Q614 will allow $100 \mu \mathrm{~A}$ of collector current to flow. This increases the deflection factor (in the readout display) by a factor of 10.

When different-attenuation divider probes are connected to the + and - INPUT connectors, the displayed readout will be the probe tip deflection factor of the larger divider. For example: if a 10 X probe is connected to the +INPUT and a 100X probe is connected to the -INPUT the readout will display the deflection factor at the tip of the 100X probe. The 100X probe will set the bias on Q 614 to allow $200 \mu \mathrm{~A}$ of collector curent which will increase the deflection factor (in the readout display) by a factor of 100.

This means that the Indicator Oscilloscope displayed readout will give the correct deflection factor from the probe tip, for o single probe or two probes having the same attenuation factor, whereas the VOLTS/DIV knob on the plug-in will display only the plug-in deflection factor.

## Trace Identify

The TRACE IDENTIFY button, when pressed, does two things:

1. It causes the troce, representing the output of the Type 7A22, to move a small amount by inserting a $2 \mathrm{k} \Omega$ resistor, R622, from ground through CR630 to the junction of R632 and R634. This shunts a small amount of the output current causing the trace to move.
2. Forms a voltage divider from the -15 V supply through R630 and R622, placing the base of Q614 at approximately -1.5 V . This low value of bias will cause Q 614 to turn on hard (1 ,000 $\mu \mathrm{A}$ collector current) when interface connector B33 is interrogated, erasing the readout display and causing the word "IDENTIFY" to appear.

These two actions aid in identifying the Type 7A22 trace when multiple traces are displayed. When the IDENTIFY button is released, the readout is restored to its previous display.

For more specific information on the operation of the system, refer to the appropriate Indicator Oscilloscope manual.

# SECTION 4 <br> MAINTENANCE 

## Introduction

Information which will aid in keeping the Type 7A22 operating at its peak performance is contained in this section. Cleaning, lubricating and visual inspection hints are included under preventative maintenance. The section on corrective mainienance includes troubleshooting and corrective procedures. Parts identification and soldering techniques are included where necessary.

## preventive MAINTENANCE

## General

The instrument should be cleaned, inspected and recalibrated at regular intervals. The recommended interval for average operating conditions is every 6 months or every 1000 hours of operation, whichever occurs first.

## Cleaning the Front Panel

Loose dust may be removed with cloth and a dry paint brush. Water and mild detergents such as Kelite or Spray White may be used.

## CAUTION

Avoid the use of chemical agents which might damage the plastics used in this unit. Avoid chemicals such as benzene, toluene, xylene, acetone or similar solvents.

## Cleaning the Interior

Cleaning of the interior of the unit should precede calibration, since the cleaning process might alter the settings of the calibration adjustments.

To clean the interior, use low-velocity compressed air to blow off the accumulated dust. High velocity air streams should be avoided to prevent damage to components.

## WARNING

Use an eye-shield when cleaning with pressurized air. Hardened dirt can be removed with a paint brush, cotton tipped swab or cloth dampened with a water and mild detergent solution. Avoid the use of chemical cleaning agents that might damage the plastic parts.

## Visual Inspection

The unit should be inspected occasionally for such defects as poor connections, broken or damaged circuit boards, improperly seated transistors and heat-damaged parts. The remedy for most visible defects is obvious. However, damage from overheating is usually a symptom of less obvious trouble; and unless the cause is determined before parts are replaced the damage may be repeated.

## Transistor Checks

Periodic preventive maintenance checks on the transistors used in the unit are not recommended. The circuits within the unit generally provide the most satisfactory means of checking transistors usability. Performance of the circuits is thoroughly checked during recalibration, and substandard transistors will usually be detected at that time.

## Calibration

To insure accurate measurements, the Type 7A22 calibration should be checked after each 1000 hours of operation or every six months if used intermittently. Complete calibration instructions are contained in Section 5.

The calibrated procedure can be helpful in isolating major troubles in the unit. Moreover, minor troubles not apparent during regular operation may be revealed and corrected during calibration.

## CORRECTIVE MAINTENANCE

## General

Replacement of some parts in the unit should be done by following a definite procedure. Some procedures, such as soldering and replacing components on the circuit boards, are outlined in this portion of the manual.

Many electrical components are mounted in a particular way to reduce or control stray capacitance and inductance. When selecting replacement parts, it is important to remember that the physical size and shape of a component may affect its performance at high frequencies. When a repair is made, calibration and performance of the relevant portions of the circuit should be checked. Refer to Tabie 4-i and to the Performance Check/Calibration procedure in Section 5 and perform the applicable steps.

TABLE 4-1

| Areas of Repair | Checks and Adjustments Affected | Section 5 Calibration Step Step |
| :---: | :---: | :---: |
| Input Coupling switches and cables <br> Input Aftenuators | Input $R$ and $C$, Attenuator compensation, CMRR, LF response, Gain | $\begin{aligned} & 6,13,14,15,16, \\ & 17,18,19,20, \\ & 21,22 \end{aligned}$ |
| Preamp | $1 \times$ input C, Cross <br> Neutralization, DC BAL, CMRR Com-non-Mode dynamic range, Differential dynamic range, Offset range, <br> Noise, Input protection system Gain, 1 MHz freq. response, Overdrive indicator | $\begin{aligned} & 3,6,10,11,12 \\ & 13,14,20,22 \\ & 23,24 \end{aligned}$ |
| $\overline{L F-3} \mathrm{~dB}$ POINT | Gain, LF freq. response, 1 MHz freq. response | 6, 20, 21 |
| Overdrive Indicator | Dynamic range | 23, 24 |
| Gain Switched Amp | Gain, Deflection factor tracking, AC Atten Bal, HF - 3 dB POINT, 1 MHz freq. response, Overdrive recovery Variable Balance | $\begin{aligned} & 1,2,6,8 \\ & 20,26 \end{aligned}$ |
| $\overline{\text { Offset Generator }}$ | Offset Range, DC Bal, CMRR | 3, 10, 22 |
| Output Amplifier | $\mathrm{HF}-3 \mathrm{~dB}$ POINTS, Var balance, Variable range, Gain | 2, 6, 7, 20 |

## Obtaining Replacement Parts

Standard Parts. All electrical and mechanical part replacements for the Type 7A22 can be obtoined through your local Tektronix Field Office or representative. However, many of the standard electronic components can be obtained locally in less time than is required to order them from Tektronix, Inc. Before purchasing or ordering replacement parts, check the parts lists for value, tolerance, rating and description.

NOTE
When selecting replacement parts, it is important to remember that the physical size and shape of the component may affect its performance in the instrument, particularly at high frequencies. All replacement parts should be direct replacements unless it is known that a different component will not adversely affect instrument performance.

Special Parts. Some parts are manufactured or selected by Tektronix to satisfy particular requirements, or are manufactured for Tektronix to our specifications. These and most
mechanical parts should be ordered through your Tektronix Field Engineer or Field Office. See Parts Ordering Information and Special Notes and Symbols on the page immediately preceding Section 6.

Soldering Techniques
Circuit Boards. Use ordinary $60 / 40$ solder and a 35 to 40 -watt pencil type soldering iron on the circuit boards. The tip of the iron should be clean and properly tinned for best heat transfer to the solder joint. A higher wattage soldering iron may separate the etched wiring from the base material.

The following technique should be used to replace a component on the circuit board. Most components can be replaced without removing the board from the unit.

1. Grip the component lead with long-nosed pliers. Touch the soidering iron to the lead at the solder connection. Do not touch the soldering iron tip directly on the board, as it may damage the board.
2. When the solder begins to melt, pull the lead out gently. This should leave a clean hole in the board. If not, the hole can be cleaned by reheating the solder and placing a sharp object, such as a toothpick or pointed tool, into the hole to clean it out.
3. Bend the leads of the new component to fit the holes in the board. Cut the leads of the new component to the same length as those of the old component. Insert the leads into the board until the component is firmly seated against the board, or as positioned originally. If it does not seat properly, heat the joint, and gently press the component into place.
4. Apply the iron and a small amont of solder to the connection to make a firm solder joint. To protect heat-sensitive components, hold the lead between the component body and the solder joint with a pair of long-nose pliers or other tieat sink (seerity 4-in).
5. Clip the excess lead that protrudes through the board.
6. Clean the area around the soldered connection with flux-remover solvent to maintain good environmental characteristics and appearance. Be careful not to remove information printed on the board.


Fig. 4-1. Removing or replacing component on circuif board.

## CAUTION

Silk-screen lettering dissolves when contacted by flux-remover.

Metal Terminals. When soldering metal terminals (interconnecting plug pins, switch terminals, potentiometers, etc.) ordinary $60 / 40$ solder can be used. The soldering iron should have a 40 - to 75 -watt rating with a $1 / 8$ inch wide chisel-shaped tip.

Observe the following precautions when soldering to metal terminals:

1. Apply heat only long enough to make the solder flow freely.
2. Apply only enough solder to form a solid connection; excess solder may impair the function of the part.
3. If a wire extends beyond the solder joint, clip the excess close to the joint.
4. Clean the flux from the solder joint with a flux-remover solvent to maintain good environmental characteristics and appearance.

## Specific Component Replacement Information

 WARNINGDisconnect the instrument from the power source before removing or replacing components.
The pushbutton switches are not repairable and should be replaced if defective. Components which are mounted on the circuit board associated with the pushbutton switch can be replaced using the normal replacement procedure. See the information under Light-Bulb Replacement for bulb replacement. Use the following procedures to replace the +INPUT and -INPUT pushbutton switches.

## 1. AC-GND-DC ( + INPUT) Switch

a. Set the front panel controls as follows:

| POSITION | Midrange |
| :--- | :--- |
| STEP ATTEN DC BAL | Midrange |
| VOLTS/DIV | 10 V |
| HF -3 dB POINT | 1 MHz |
| LF -3 dB POINT | DC OFFSET |
| DC OFFSET (FINE) | Midrange |
| DC OFFSET (COARSE) | 5 turns from either extreme |

b. Remove all front panel knobs.
c. Remove the GND binding post assembly.
d. Remove the nut and washer from the POSITION and DC OFFSET shafts.
e. Remove the plastic bushing from the VOLTS/DIV shaft.
f. Remove the front panel overlay.
g. Without unsoldering any leads, carefully push the dual DC OFFSET potentiometers out of the front panel and lift them out of the way.
$h$. Unsolder and unplug the connecting leads from the AC.GND-DC switch.
i. Remove four corner screws and remove the front subpanel.
i. Remove the two screws securing the AC-GND-DC switch to the front sub-panel and remove the switch.
k. Replace by reversing the above procedure.

## 2. AC-GND-DC ( - INPUT) Switch

a. Perform step 1, parts a through f, of Specific Component Replacement.
b. Loosen the setscrew on the collar connecting the GAIN shaft to the pot coupler and pull the shaft out of the front panel.
c. Unsolder and unplug the connecting leads from the AC-GND-DC switch.
d. Remove the four corner screws and remove the front sub-panel.
e. Remove the two screws securing the switch to the front panel.
f. Remove the switch.
g. Replace by reversing the above procedure.
3. Light-Bulb Replacement, + INPUT and -INPUT

Push-Button Switches
Two types of pushbutton switches which have different light designs are in use. One switch design uses a metal cover over the light bulb(s) on the back of the switch; the other type does not. Either or both types of switches may be used in the 7A22.

To replace light bulbs in the pushbutton switches, use the following procedure:
a. Remove the applicable INPUT switch as described in steps 1 and 2.
b. On switches with the metal cover, remove the screw holding the cover and remove the cover.
c. Clip off the bulb leads near the bulb body.
d. Remove the leads from the circuit board.
e. Remove the excess solder from the circuit board with a vacuum-type desoldering tool.
f. Solder the new bulb to the circuit board (replace cover).
g. Replace the switch in the instrument.

## 4. Bandwidth Circuit Board

a. Set the LF and HF -3 dB POINT Selectors to either extreme.
b. Loosen the setscrews securing the LF -3 dB POINT shaft to the collar on the cam switch. Pull the shaft forward until it clears the collar.
c. Loosen the setscrews securing the HF -3 dB POINT shaft to the collar on the cam switch. Pull the shaft forward until it clears the bandwidth board.
d. Loosen the setscrew securing the GAIN shaft to the collar on R540. Pull the shaft forward until it clears the bandwidth circuit board. Loosen the setscrew securing the collar to R540 and remove the collar.
e. Loosen the four circuit board retaining screws and lift out the Bandwidth Circuit Board.
f. Unclip the leads from solderless connectors A, AN, AP, AO, and D.
g. Replace by reversing the above procedure.

## CAUTION

Repair of cam-type switches should be undertaken only by experienced personnel. Switch alignment and spring tension of the contacts must be carefully maintained for proper operation of the switch. Far assistance in maintenance of the cam-type switches, contact your local Tektronix Field Office or representative.

## 5. Cam-Type Switches

## NOTE

A cam-type switch repair kit including necessary teals, instructions and replacement contacts is available from Tektronix, Inc. Order Tektronix Part No. 040-0541-00.

The cam-type switch consists of a rotating cam, which is rotated by a front-panel knob, and a set of contacts mounted on the adjacent circuit board. These switch contacts are actuated by lobes on the cam. The VOLTS/DIV, LF -3 dB POINT and HF -3 dB POINT cam-type switches can be disassembled for inspection, cleaning, repair or replacement, as follows:

## A. LF -3 dB POINT and HF -3 dB POINT Switches

1. Remove the Bandwidth board as described in step 4.
2. Remove the two screws which hold the metal covers in place. (The front switch on the Bandwidth board is the LF -3 dB POINT Selector and the rear switch is the HF -3 dB POINT Selector). The switches are now open for cleaning or inspection.
3. To completely remove either of the two switches from the board, remove the four screws (from the back side of the board) which hold the cam assembly to the circuit board.
4. To remove the cam from the front support block, remove the retaining ring from the shaft on the front of the switch and slide the cam out of the support block. Be careful not to lose the small detent roller (between detent and detent spring).
5. To replace defective switch contacts, unsolder the damaged contact and clean solder from the hole in the circuit board. Position the new contact in the hole in proper alignment relative to the other switch contacts and with the mating area on the circuit board (alignment tool provided in switch repair kit). Solder the new contact into place; be sure that the spring end of the contact has adequate clearance from the circuit board.
6. To re-install the switch assembly, reverse the above procedure.

## B. VOLTS/DIV Switch

1. Remove the Bandwidth board as described in step 4.
2. Remove the two screws which hold each of the metal switch covers in place.
3. Push the VARIABLE (CAL $I N$ ) to the ' $I N$ ' position.
4. Loosen the set screw which secures the VARIABLE shaft to the VARIABLE control assembly.
5. Pull the VARIABLE shaft through the front of the instrument.
6. Remove the 4 screws (from the rear side of the board) which hold the rear cam assembly to the circuit board.
7. Remove the rear cam assembly.

To remove the front cam switch assembly, perform the preceding steps and then proceed as follows:

1. Remove the VOLTS/DIV knob.
2. Loosen the $1 / 2$-inch hex bushing nut which secures the front support block.
3. Remove the plastic bushing from front of panel.
4. Remove the retaining ring from the shaft at the front of the switch.
5. Remove the 4 screws which secure the support blocks to the board.
6. Loosen the 2 set screws in the half of the flexible coupling and remove coupling.
7. Remove the rear support block by carefully lifting the block away from the circuit board far enough to clear the alignment prelection on the bottom of the block. Carefully slide the rear block toward the rear (off the shaft).
8. Slide the cam shaft carefully (keep cam lobes clear of contacts] out of the front support block and bushing a ssembly.
9. To re-assemble, reverse the above procedure.

## 6. Interconnecting Pins

Interconnecting pins are used on the Type 7A22 to interconnect circuit boards. When interconnection is made at a circuit board, the pin is soldered into the board. Two types of mating connectors are used for these interconnecting pins. If the mating conector is mounted on a plug-on circuit board, a special socket is soldered into the board. If the mating connector is on the end of a lead, an end-lead pin connector (which mates with the interconnecting pin) is used. The following information provides the replacement procedures for the types of interconnecting methods.

## A. CIRC UIT-BOARD PINS

## N O TE

A pin replacement kit including necessary tools, instructions and replacement pins is available from Tektronix, Inc. Order Tektronix Part No. 040-0542-00.

To replace a pin which is mounted on a circuit board, first disconnect any pin connectors. Then unsolder the damaged pin and pull it out of the circuit board with a pair of pliers. Be careful not to damage the wiring on the board with too much heat. Ream out the hole in the circuit board with a 0,031 -inch drill. Then remove the femule from the new interconnecting pin and press the new pin into the hale in
the circ uit board. Position the pin in the same manner as the old pin. Then, solder the pin on both sides of the circuit board. If the old pin was bent at an angle to mate with a connector, bend the new pin to match the associated pins.

## B. CIRCUIT-BOARD PIN SOCKETS

The pin sockets on the circuit boards are soldered to the rear of the board. To replace one of these sockets, first unsolder the pin (use a vacuum-type resoldering tool to remove excess solder]. Then straighten the tabs on the socket and remove it from the hole in the circuit board. Place the new socket in the circuit board hole and press the tabs down against the board. Solder the tabs of the socket to the circuit board; be careful not to get solder into the socket.

## NOTE

The spring tension of the pin sockets ensures a good connection between the circuit board and the pin. This spring tension can be destroyed by using the pin sockets as connecting points for spring-loaded probe tips, alligator clips, etc.

## C. END-LEAD PIN CONNECTORS

The pin connectors used to connect the wires to the interconnecting pins are clamped to the ends of the associated leads. To replace damaged end-lead pin connectors, remove the old pin connector from the end of the lead and clamp the replacement connector to the lead.

Some of the pin connectors are grouped together and mounted in a plastic holder; the overall result is that these connectors are removed and re-installed as a multi-pin connector when it is replaced. An arrow is stamped on the circuit board and a matching a rrow is molded into the plastic housing of the multi-pin connector. Be sure these arrows are aligned as the multi-pin connector is replaced. If the individual end-lead pinconnectorsare removed from the plastic holder, note the color of the individual wires for replacement.

## TROUBLESHOOTING

## Introduction

The following information is provided to facilitate troubleshooting of the Type 7A22. Information contained in other sections of this manual should be used along with the following information to aid in locating the defective component. An understanding of the circuit operation is very helpful in locating troubles. See the Circuit Description Section for complete information.

## General

If trouble occurs in the Type 7A22, the following procedure is recommended to accomplish rapid and effective repairs.

1. Check that the plug-in unit and the oscilloscope connectors are not damaged, and that the plug-in unit is properly inserted.
2. Inspect the front panels of the Type 7A22 and indicator oscilloscope to be sure that the trouble is not from an incorrect control setting.
3. Insure that the indicator oscilloscope is not at fault by inserting a known-good plug-in unit and checking its operation.
4. Detemine all trouble symptoms.
5. Perform a visual inspection of the Type 7A22.
6. Repair or replace obviously defective parts.
7. Troubleshoot the Type 7A22 as necessary.
8. Recalibrate the Type 7A22.

## Indicator Oscilloscope

The quickest check of the oscilloscope is to use it with a good plug-in unit, or check the questionable plug-in with another oscilloscope. Refer to the oscilloscope manual to verify proper operation of the oscilloscope.

## Operating Procedures and Control Settings

Refer to the Operating Instructions Section of this manual to verify operating procedures and front panel control settings of the Type 7A22.

## Trouble Symptoms

The Type 7A22 response to all front panel controls should be observed. The first-time operation in Section 2 or the Performance Check in Section 5 may be used for this purpose. All trouble symptoms should be evaluated and compared against each other. A casualty will often create a combination of symptoms that, when considered together, will pinpoint the trouble.

## Visual Inspection

In physically examining the Type 7A22, take special note of the area indicated by evaluation of symptoms. Look for loose or broken connections, improperly seated transistors and bumed or otherwise damaged parts. Repair or replace all obviously defective components.

## Calibration Check

Troubles can frequently be located and corrected by recalibrating the instrument. Unless the casualty has definitely been isolated to a specific circuit, it is recommended that the calibration procedure contained in Section 5 be performed to provide a logicalcircuit troubleshooting sequence.

## DETAILED TROUBLESHOOTING

## General

If the casualty has not been disclosed and corrected through the procedure outlined, a detailed troubleshooting
analysis will have to be performed. The Circuit Description Section, the Schematic Diagrams, and the troubleshooting aids contained in this section are designed to expedite troubleshooting.

The Circuit Description Section provides a fundamental understanding of circuit operation and is referred to the Schematic Diagrams. The Schematic Diagrams contain voltage and resistance values and signal waveforms. The specified operating conditions should be duplicated before making voltage or waveform comparisons.

## NOTE

Voltages and waveforms may vary slightly between instruments. Those given in the schematics should be checked against each instrument while it is operating properly. Deviations should be noted on the schematics for later reference.

## Test Equipment Recommended for Troubleshooting

The test equipment listed here should suffice for most troubleshooting jobs. Test equipment required for calibration is listed in the Calibration Section.

High Impedance Voltmeter ( $20,000 \Omega / V$ DC or greater) Ohmmeter ( 2 mA or less current on the $\times 1 \mathrm{k} \Omega$ scale)
Test Oscilloscope and Probes
Flexible Plug-in Extension Cable
Dynamic Transistor Tester

## DC Balance Check

A properly operating oscilloscope will have its trace centered vertically on the CRT only when the Type 7A22 has a balanced output. The Type 7A22 is a balanced amplifier connected in a differential configuration, with the +INPUT circuit being electrically identical to the-INPUT circuit. With no signal or comparison voltage applied to the FET gates, any point in the +INPUT circuit should have a potential equal to an identical point in the -INPUT circuit.
If the CRT trace is deflected as a result of a Type 7A22 problem, unbalances will exist between the two circuits. The unbalance can be detected by connecting a high impedance voltmeter between identical points in the two circuits.

An aid to this process is to short together the inputs of the stage being checked as shown in this example.

| Stage | Devices | Short Together |
| :--- | :--- | :--- |
| Signal Output | Q444, Q544 | Q444, Q544 bases |
| Trigger Output | Q454, Q554 | Q454, Q554 bases |
| Variable Stage | Q434, Q534 | Q434, Q534 bases |
| Gain Switching <br> Amplifier | Q404A, Q404B, <br> Q414A, Q414B، <br> Q424, Q524 | Front ends of R401 and <br> R501 |
| Input Amplifier | AC-GND-DC switches <br> to GND |  |

If the output balance is checked first and is in error, work toward the front unfil an unbalance no longer exists. This localizes the trouble to the circuitry between the points which


Fig. 4-2, Transistor junction-voltage measurements.
are balanced and the points which are unbalanced. The individual components must then be checked.

## Troubleshooting by Direct Replacement

Semi-conductor failures account for the majority of electronic equipment troubles. The ea ie of replacing transistors often makes substitution the most practical means of repair. If this method is used, these guide lines should be followed:

Determine that the circuit is safe for the substitute component.

Use only substitute components that are known to be good.
Remove the plug-in from the oscilloscope before substituting components, to protect both you and the equipment.

Be sure components are inserted properly.
Check operation after each component is replaced.
Return good components to their original sockets.
Check calibration after a bad component has been replaced (see Table 4-1).

## Component Checks

## Transistors

The best means of checking a transistor is by using a transistor curve display instrument such as the Tektronix Type 576. If a transistor checker is not readily available, a defective transistor can be located by signal tracing, by making in-circuit voltage checks, by measuring the transistor resistances or by the substitution method previously described.

When troubleshooting using a voltmeter, measure the emitter-to-base and emitter-to-collector voltages to determine whether the voltages are consisent with normal circuit voltages. Voltages across a transistor vary with the device and its circuit function. Some of these voltages are predictable. The base-emitter voltage of a conducting germanium transistor will normally be approximately 0.2 V and that of a silicon transistor will normally be approximately 0.6 V . The col -

# SECTION 5 <br> PERFORMANCE CHECK/ CALIBRATION PROCEDURE 

## Introduction

Complete information for performing a Performance Check or Calibration of the Type 7A22 is contained in this section of the manual. The Equipment Required list is needed both for a Performance Check and for calibrating the Type 7A22. All waveform photographs, equipment setup pictures, and control settings apply whether the instrument is being calibrated or checked for performance.

To conduct a Performance Check complete all parts of each step in the following procedure, except the part subpifled ADJUST. To check the performance of the Type 7A22, it is not necessary to remove the oscilloscope side panel or make any internal adjustments. Adjustments located on the front panel of the Type 7A22 can be performed when checking the performance of the instrument. If the instrument does not meet the performance requirements given in this procedure, the complete procedure including adjustments should be done. All performance requirements given in this section correspond to the Specifications given in Section I). For convenience in calibrating the Type 7A22, steps containing internal adjustments are marked with the symbol (1).

Calibration of the Type 7A22 requires completion of all ; larts of each step in the following procedure. Completion of every step in this procedure returns the Type 7A22 to its original performance standards. To assure accurate measurements and correct operation, the calibration of the Type 7 A22 should be checked after each 1000 hours of operation; or every six months if used infrequently. Before performing a complete calibration, thoroughly clean and inspect this instrument as outlined in the Maintenance section.

## TEST EQUIPMENT REQUIRED

## General

The following test equipment and accessories for their equivalent) are required for a complete performance check or calibration of the Type 7A22. Specifications given are the minimum necessary for accurate performance of this instrument. All test equipment is assumed to be correctly cali= brated and operating within the given specifications. If equipment is substituted, it must meet or exceed the specifications of the recommended equipment.

For the quickest and most accurate calibration or performance check, special Tektronix calibration fixtures are used where necessary. These special calibration fixtures are
available through your local Tektronix Field Office or representative.

1. 7000 Series Oscilloscope, referred to as "oscilloscope" in this procedure. For this procedure a Type 7504 with a 7B50 Time Base is used.
2. Constant Amplitude Sine-Wave Generator. Output frequency range of 10 Hz through 1.0 MHz ; output amplitude range from 2 V to 20 V peak to peak. General Radio Type 1310A is recommended.
3. Standard Amplitude Calibrator. Amplitude accuracy, within $0.25 \%$; signal amplitude 0.5 mV to 100 V ; output signal 1 kHz square wave and DC. Tektronix Calibration Fixture 067-0502-01 recommended.
4. Reed Pulse Generator. Tektronix Calibration Fixture 067-0608-00 is recommended.
5. Coaxial Cable. Impedance, 50 ohms; length, 42 inches; connectors, BNC. Two required. Tektronix Part Number 012-0057-01.
6. Dual Input BNC connector. Provides matched signal paths to both Type 7A22 input connectors. Tektronix Part Number 067-0525-00.
7. Variable Attenuator. A variable attenuator which has the end terminals of a 100 ohm potentiometer connected from input to ground and the potentimeter divider arm connected to the attenvator output. Tektronix Calibration Fixture 067. 0511-00 is recommended.
8. 1000:1 Divider. Tektronix Part Number 067-0529-00 is recommended.
9. Input RC Normalizer. RC time constant, 1 megohm $X$ 47 pF; connectors, BNC. Tektronix Part Number 067-0541-00 is recommended.
10. Attenuator. Impedance, $50 \Omega$; Ratio, 10:1; connectors, BNC. Two each, Tektronix Part Number 011-0059-02.
11. Plug-in extender. Tektronix Calibration Fixture 067 -0589-00.
12. Termination. Impedance, $50 \Omega$. Tektronix Part Number 011-0049-01.
13. BNC T Connector. Tektronix Part Number 103-0030-00.
14. Adapter, GR to BNC Female. Tektronix Part Number 017-0063-00.
15. Adapter, GR to BNC Male. Tektronix Part Number 017-0064-00.
16. Banana plug-jack to banana plug-jack patch cord. Tektronix Part Number 012-0031-00 (red) or 012-0034-00 (black). Three needed.

## SHORT-FORM PERFORMANCE CHECK/CALIBRATION PROCEDURE

This short-form procedure is provided to aid in checking the performance or calibration of the Type 7A22. It may be used as a guide by the experienced operator or calibrator, or it may be reproduced and used as a permanent record of calibration. Since the step numbers and titles used here correspond to those used in the complete procedure, this procedure also serves as an index to locate a step in the complete procedure. Performance requirements listed here correspond to those given insectiond.

Type 7A22, Serial No.
Calibration Date
Calibrated By

1. Check or Adjust AC Atten Bal (R505) Page 5-4 Trace within 1.5 Div of graticule center as VOLTS/ DIV switch is changed from 10 mV to $20 \mu \mathrm{~V}$.
$\square$ 2. Check or Adjust Variable Bal (R425) Page. 5-4 Maximum trace shift $\pm 0.2$ Div as the VARIABLE (VOLTS/DIV) is rotated stop-to-stop.
2. Check or Adjust Coarse DC Bal (R275) P尸age 5-4 Trace within 0.1 Div of graticule center as $L F-3 \mathrm{~dB}$ POINT selector is changed from 10 kHz to DC.
3. Check or Adjust + INPUT Zero (R115) Page 5-5 Maximum trace shift $\pm 2$ Div as the + INPUT AC. GND-DC switch is switched from GND to AC.
4. Check or Adjust - INPUT Zero (R215) proge 5-5 Maximum trace shift $\pm 2$ Div as the - INPUT AC-GND-DC switch is switched from GND to AC.
5. Check or Adjust GAIN (R540)

Page 5-5
Correct vertical deflection in the 1 mV position of the VOLTS/DIV switch (front panel adjustment).
7. Check VARIABLE (VOLTS/DIV) control fage $5-5$ Ratio
Display amplitude decreases by a ratio of 2.5:1 when the VARIABLE control (in the out position) is rotated fully counterclockwise.
8. Check VOLTS/DIV Gain Switching

Page 5.5 Correct vertical deflection from $10 \mu \vee$ through 10 mV .
9. Check Isolation Between + and - INPUTGPage 5-7 Trace deflection of 0.5 Div or less.
10. Check Total DC OFFSET Range

Page 5-7 Check for minimum offset range of + and -l volt.11 Check or Adjust C241-Cross Neutralization Page 5-7 With signal connected to + INPUT, switch the -

INPUT AC-GND-DC from GND to DC; aberration should not exceed $\pm 1 \%$.12. Check or Adjust Cl41-Cross Neutralizatio Page 5-8 With sianal connected to - INPUT. switch the + INPUT AC-G ND-DC from GND to DC; aberration should not exceed $+1 \%$.13. Check or Adjust C115 $\times 1+$ INPUT Roge 5-9 Attenuator
Time Constant
Optimum square wave response
14. Check or Adjust C215 $\times 1$-INPUT Page 5-8 Attenuator
Time Constant
Optimum square wave response.15. Check Input Attenuator Accuracy Proge-5-9 Correct vertical deflection from 10 mV through 10 V .16. Check or Adjust Attenuator Differential Page 5-9 Balance (R108E, R109E, R110E)
Optimum differential balance.17. Check or Adjust + Input Attenuator Page 5-10 Compensation
(C108C, C109C, C110C, Cl08A, C109A, C1 10A) Optimum square wave response.
18. Check or Adjust - Input Attenuator Series Poge 5-in Compensation to match + Input (C208C, C209C, (210C) Best common-mode sianal rejection (minimum spike amplitude).
19. Check or Adjust - Input Attenuator Shuntrage 5-iit Compensation (C208A, C209A, C21 0A)
Optimum flat bottom display.20. Check or Adjust HF -3 dB POINT (C425 Fage $5-10$ HIGH FREQ - 3 dB POINT bandwidth limit.21. Check LF -3 dB POINT P尸age 5-12 LOW FREQ -3 dB POINT bandwidth limit.22. Check or Adjust CMRR (C330)
fage 5-13 CMRR must be equal to or better than the specified requirements at the verification points show in Sec. tion fig. ${ }^{1}-2$ - p the manual.

## 23. Check OVERDRIVE Indicator <br> Page 5-13

 Indicator turns on at approximately 1 volt.24. Check Differential Signal Range Range 5-14 No change in sine-wave amplitude when + or - 1 volt DC is applied.25. Check Overall Noise Level Tangentially FPage 5-15 Less than $16 \mu \mathrm{~V}$ of displayed noise, measured tangentally.26. Check Overdrive Recovery

Page 5.15 $10 \mu \mathrm{~s}$ or less to recover to within $0.5 \%$ of zero level.
lector-emitter voltage will vary with the circuit and circuit conditions but it should always exceed 0.5 V . The best way of checking these devices is by connecting a voltmeter across the junction, using a sensitive voltmeter setting (seefig. 4-2).

An ohmmeter can be used to check a transistor if the ohmmeter's voltage source and current are kept within safe limits. 1.5 V and 2 mA are generally acceptable. Selecting the $X 1$ $k \Omega$ scale on most ohmmeters will provide voltage and current below these values.

Table 4-2 contains the normal values of resistance to expect when making an ohmmeter check of an otherwise unconnected transistor.
rrig. 4-3 shows the transistor base and socket arrangements used in this instrument.

TABLE 4-2

## Transistor Resistance Checks

| Ohmmeter <br> Connections | Resistance Reading That Can be <br> Expected Using the $R \times 1 \mathrm{k}$ Range |
| :---: | :---: |
| Emitter-Collector | Hiah readinas both ways |
| Emitter-Base | High reading one way, low read- <br> ing the other way |
| Base-Collector | High reading one way, low read- <br> ing the other way |

${ }^{1}$ Test prods from the ohmmeter are first connected to the transistor leads and then the test lead connections are reversed. Thus, the effects of the polarity reversal of the voltage applied from the ohmmeter to the transistor can be observed.


Plastic Case Transistor


Metal Case Transistors


0133
0404


Plastic Case Transistors

Fig. 4-3. Transistor base pin and socket arrangement.


Fig. 4-4. Diode polarity and color code.

## Diodes

A diode can rechecked for an open or for a short circuit by measuring the resistance between terminals with an ohmmeter set to the $R \times 1 \mathrm{k}$ scale. The diode resistance should be very high in one direction and very low when the meter leads are reversed. Do not check tunnel diodes or back diodes with an ohmmeter.

Some diodes used in the Type 7A22 are color coded to identify the diode type. The" cathode end of each glassencased diode is indicated by a stripe, a series of stripes or o dot. For most diodes with a series of stripes, the first stripe (either pink or blue) indicates a Tektronix part and the next three stripes indicate the three significant figures of the Tektronix Part Number. Example: a diode color coded blue-brown-gray-green indicates a diode with Tektronix Part No. 152-0185-00. The cathode and anode of a metal-encased diode can be identified by the diode symbol marked on the body. Se Fig. 4-4, DIODE POLARITY AND COLOR CODES.

## Resistors

The types and accuracies of resistors found in this instrument vary in accordance with the circuit needs, Replacement resistors should be of the same type and must be at least as accurate as those originally contained in the circuit, to maintain the high common-mode rejection ratio. The size, location and lead length are often critical because of frequency considerations.


Fig. 4-5. Color code for resistors and ceramic capacitors.

Composition, wire-wound and metal film resistors are used in this unit. The stable metal film resistors may be identified by their light blue or gray body color. If a metal film resistor has a value indicated by three significant figures and a multiplier, it will be color coded according to the EIA standard pesistor color code. If it has a value of more than three significant figures and a multiplier, the value will be printed

## Capacitors

A leaky or shorted capacitor can be detected by checking resistance with an ohmmeter using the highest scale that does not exceed the voltage rating of the capacitor. The resistance reading should be high after the initial charge of the capacitor. An open capacitor can be detected with a capacitance meter or by checking whether the capacitor passes AC signals.

The capacitance values of common disc capacitors and small electrolytics are marked in microfarads on the side of the component body. The white ceramic capacitors used in the Type 7A22 are color coded in picofarads using a modified EIA code (seefig $4=5$ ).

## Repackaging for Shipment

If the Tektronix instrument is to be shipped to a Tektronix Service Center for service or repair, attach a tag showing: owner (with address) and the name of an individual at your firm that can be contacted, complete instrument serial number and a description of the service required.

Save and re-use the package in which your instrument was shipped. If the original packaging is unfit for use or not available, repackage the instrument as follows:

Surround the instrument with polyethylene sheeting to protect the finish of the instrument. Obtain a carton of corrugated cardboard of the correct carton strength and having inside dimensions of no less than six inches more than the instrument dimensions. Cushion the instrument by tightly packing three inches of dunnage or urethane foam between carton and instrument, on all sides. Seal carton with shipping tape or industrial stapler.

The carton test strength for your instrument is $\mathbf{2 0 0}$ pounds.


Fig. 4-6. Main circuit board (components)


Fig. 4-7. Main circuit board [wire color code)


Fig. 4-8. Bandwidth circuit board (components and wire color code)

## PERFORMANCE CHECK/CALIBRATION PROCEDURE

## General

The following procedure is arranged in a sequence which allows the Type 7A22 to be calibrated with the least interaction of adjustments and reconnection of equipment. The steps in which adjustments are made are identified by the symbol following the title. Instrument performance is checked in the "CHECK" part of the step before an adjustment is made. The "ADJUST" part of the step identifies the point at which the actual adjustment is made. Steps listed in the "INTERACTION" part of the step may be affected by the adjustment just performed. This is particularly helpful when only a partial calibration procedure is performed.

## NOTE

To prevent recalibration of other parts of the instrument when performing a partial calibration, readjust only if the tolerances given in the "CHECK" part of the step are not met. However, when performing a complete calibration, best overall performance is obtained if each adjustment is made to the exact setting even if the "CHECK" is within the allowable tolerance.

In the following procedure, a test-equipment setup picture is shown for each major group of checks and adjustments. Each step continues from the equipment setup preceding the desired portion. External controls or adjustments of the Type 7A22 referred to in this procedure are capitalized (e.g., POSITION). Internal adjustment names are initial capitalized only (e.g., Variable Bal).

All waveforms shown in this procedure are actual waveform photographs taken with a Tektronix Oscilloscope Camera System. The following procedure uses the equipment listed under Test Equipment Required. If equipment is substituted, control settings or test equipment setup may need to be altered to meet the requirements of the equipment used. Detailed operating instructions for the test equipment are not given in this procedure. If an doubt as to the correct operation of any of the test equipment, refer to the instruction manual for that unit.

## NOTE

It is assumed that performance is checked within a temperature range of $0^{\circ} \mathrm{C}$ to $+50^{\circ} \mathrm{C}$ and calibration $+25^{\circ} \mathrm{C}, \pm 5^{\circ} \mathrm{C}$; the tolerances given in this procedure are for this temperature range. However, if the procedure is performed at some other temperature, check the applicable tolerances for that temperature range.

Preliminary Procedure

1. If the Type 7A22 is to be calibrated, insert the plugin extender into the oscilloscope and plug the Type 7A22 into the plug-in extender. If this procedure is a Performance Check only, insert the Type 7A22 into the oscilloscope plugin compartment.
2. Connect the oscilloscope power cord to the design center operating voltage for which the oscilloscope is wired.
3. Turn on the oscilloscope POWER switch. Allow at least 20 minutes warmup for checking the instrument to the given accuracy.
4. Preset the Type 7A22 front panel controls as follows:

| VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| POSITION | Midrange |
| HIGH FREQ -3 dB POINT | 100 Hz |
| LOW FREQ -3 dB POINT | 10 kHz |
| AC-GND-DC $(+\mathbb{I N P U T})$ | GND |
| AC-GND-DC (-INPUT) | GND |
| STEP ATTEN DC BAL | Midrange |
| DC OFFSET COARSE | 5 turns from either extreme |
| DC OFFSET FINE | Midrange |

5. Preset the Time Base front panel controls to these settings:

| Time/Div | .5 ms |
| :--- | :--- |
| Variable | In (Calibrated) |
| Triggering | Auto, AC, Int |

6. Set the oscilloscope Focus and Intensity for best viewing.


Fig. 5-1. Left side of the 7A22 showing adjustment locations

## NOTE

Calibration of the Type 7A22 must be performed with the side covers in place. All internal adjustments can be made using the access holes provided in the side covers.

1. Check or Adjust AC Step Atten Bal
a. Center the trace on the CRT with the POSITION control.
b. Rotate the VOLTS/DIV switch from 10 mV to the 20 $\mu \mathrm{V}$ position.
c. CHECK-The trace should remain within 1.5 div of graticule center.
d. ADJUST-AC Step Atten Bal control, R505, (see figh 5-1 to position the trace within 1.5 div of graticule center.

## 2. Check or Adjust Variable Bal

a. Set the Type 7A22 VOLTS/DIV switch to 10 mV .
b. Position the trace to graticule center with the POSITION control.
c. Rotate the VARIABLE VOLTS/DIV (in the out position) from stop to stop.
d. CHECK-For maximum trace shift not to exceed $\pm 0.2$ div while rotating the VARIABLE control throughout its range.
e. ADJUST-Variable Bal control, R425, (seerig_il) for no trace shift while rotating the VARIABLE control.

## 3. Check or Adjust Coarse DC Bal

a. Set the VARIABLE VOLTS/DIV to the CAL IN position.
b. Position the LOW FREQ -3 dB POINT switch to the $D C$ position.
c. CHECK - The trace should be within 0.1 div of graticule center.
d. ADJUST-Coarse DC Bal, R275, (see $\sqrt{\text { fig. 51) }}$ ) to posifion the trace to graticule center.
e. Set the VOLTS/DIV switch to $50 \mu \mathrm{~V}$.
f. CHECK - The trace should be on screen.
g. ADJUST-If the trace is not on screen, start at the position of the VOLTS/DIV switch where an on screen display is obtained and readjust the Coarse DC Bal, working down to the $50 \mu \mathrm{~V}$ position so the end result is an on-screen trace at $50 \mu \mathrm{~V}$.

Type 7A22 Controls

| VOLTS/DIV | $10 \mu \mathrm{~V}$ |
| :--- | :--- |
| VARIABLE | $C A L ~ I N$ |
| POSITION | Midrange |
| HIGH FREQ -3 dB <br> POINT  | 100 Hz |

AC-GND.DC (-INPUT) GND

```
AC-GND-DC (+ INPUT) DC
AC-GND-DC (-INPUT)
STEP ATTEN DC BAL
GND
Adjust for proper DC bal-
ance.
```

| Time/Div | .5 ms |
| :--- | :--- |
| Variable (Time/Div) | Cal |
| Triggering | Auto, AC, Int |

4. Check or Adiust + Gate Current Zero (I)
b. Using the POSITION control, position the trace to graticule center.
c. Set the + INPUT AC-GND-DC switch to AC.
d. CHECK-For maximum trace shift within $\pm 2$ div.
e. ADJUST--The + Gate Current Zero control, R1 15, (see fig. 5-1 ), to position the trace to graticule center.
f. CH ECK-(only if adjustment has been made). Switch the + INPUT AC-GND-DC switch to GND and back to AC. There should be no movement of the trace.
g. Set the + INPUT AC-GND-DC switch to GND.
5. Check or Adjust - Gate Current Zero
a. Remove the $50 \Omega$ termination from the + INPUT and connect it to the -INPUT connector.
b. Position the trace to graticule center with the POSITION control.
c. Set the -INPUT AC-GND-DC switch to AC.
d. CHECK-For maximum trace shift within $\pm 2$ div.
e. ADJUST-The -Gate Current Zero control, R215, (see Ffig. 5-1) , to return the trace to graticule center.
f. CHECK-fonly if adjustment has been made). Return the -INPUT AC-GND-DC switch to GND and back to $A C$. There should be no trace shift.
g. Disconnect the $50 \Omega$ termination.
h. Set the -INPUT AC-GND-DC switch to GND.

Type 7A22 controls

| VOLTS/DIV | 1 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| POITION | Midrange |
| HIGH FREQ -3 dB | 1 MHz |
| POINT <br> LOW FREQ <br> POINT | DC |

6. CheckorAdjust GAIN
(1)
a. Test equipment setup is shown infig. 5-2.
b. Connect a 5 mV peak-to-peak square wave signal from a standard amplitude calibrator through a 1000:1 divider and a coaxial cable to the + INPUT connector.
c. Set the $1000: 1$ divider to $\times 1$.
d. Align the display with the graticule lines using the POSITION control.
e. CHECK-The display for a vertical amplitude of exactly 5 div.
f. ADJUST-The GAIN control front panel adjustment R540) for exactly 5 div of display amplitude.
7. Check Variable control Ratio
a. With the VARIABLE in the OUT position, rotate the control fully counterclockwise.
b. CHECK-The display amplitude should be 2 div or less to meet the $2.5: 1$ ratio requirement.
8. Check VOLTS/DIV G ain Switching
a. Set the HIGH FREQ -3 dB POINT switch to 3 kHz .
b. Set the LOW FREQ -3 dB POINT switch to 1 Hz .
c. Set the standard amplitude calibrator output to 10 mV .
d. Using the VARIABLE VOLTS/DIV control, adjust the display amplitude to exactly 5 div.
e. Set the Time Base Triggering Source to Line.
f. Position the Time/ Div switch to $.1 \mu \mathrm{~s}$
g. Switch the $1000: 1$ divider to $\times 1000$.
h. CHECK-The vertical deflection factor from $10 \mu \mathrm{~V}$ through $50 \mu \mathrm{~V}$. fable 5 -itis provided as a guide.

TABLE 5-1

| VOLTS/DIV switch position | Standard Amplitude Calibrator Output Amplitude | Divisions of Deflection | Accuracy |
| :---: | :---: | :---: | :---: |
| $10 \mu \mathrm{~V}$ | . 1 V | 5 | $\pm 2 \%$ |
| $20 \mu \mathrm{~V}$ | . 2 V | 5 | $\pm 2 \%$ |
| $50 \mu \mathrm{~V}$ | . 5 V | 5 | $\pm 2 \%$ |



Fig. 5-2. Equipment required for steps 6 through 19.
i. Return the VARIABLE to the CAL IN position.
i. Switch the $1000: 1$ divider to the XI position.
k. CHECK—The vertical deflection factor from . 1 mV through 10 mV using table 5-2 ds a guide.

TABLE 5-2

| VOLTS/ DIV <br> switch <br> position | Standard <br> Amplitude <br> Calibrator <br> Output <br> Amplitude | Divisions <br> of <br> Deflection | Accuracy |
| :---: | :---: | :---: | :---: |
| .1 mV | .5 mV | 5 | $\pm 2 \%$ |
| .2 mV | 1 mV | 5 | $\pm 2 \%$ |
| .5 mV | 2 mV | 4 | $\pm 2 \%$ |
| 1 mV | 5 mV | 5 | $\pm 2 \%$ |
| 2 mV | 10 mV | 5 | $\pm 2 \%$ |
| 5 mV | 20 mV | 4 | $\pm 2 \%$ |
| 10 mV | 50 mV | 5 | $\pm 2 \%$ |

1. Remove the $1000: 1$ divider from the Standard Amplitude Calibrator.

Type 7A22 Controls

| VOLTS/DIV | 1 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| POSITION | Midrange |
| HIGH FREQ -3 dB | 1 MHz |
| POINT |  |
| LOW FREQ -3 dB | DC OFFSET |
| POINT |  |
| AC-GND-DC (+ INPUT) | DC |
| AC-GND-DC (-INPUT) | GND |
| STEP ATTEN DC BAL | Adjusted for DC balance |

Time Base Controls

| Time/Div | 1 ms |
| :--- | :--- |
| Variable | Calibrated |
| Slope | + |
| Coupling | AC |
| Source | Int |
| Mode | Auto |

9. Check Isolation Between + and -Inputs
a. Set the Standard Amplitude Calibrator to .1 V square wave.
b. Adjust the DC OFFSET COARSE and FINE controls to position the top of the square wave to the graticule center line.
c. Switch the -AC-GND-DC switch to DC.
d. CHECK - Trace deflection must be 0.5 division or less.
e. Repeat the above procedure for the -INPUT, checking for trace deflection when switching the +AC-GND-DC switch to DC.
10. Check Total DC OFFSET Range
a. Set the Type 7A22 confrols as follows:

| VOLTS/DIV | 10 mV |
| :--- | :--- |
| AC-GND-DC $\quad$ (+INPUT) | DC |
| AC-GND-DC $\{$-INPUT $)$ | GND |

b. Set the Standard Amplitude Colibrator to 1 V and Mode selector to $+D C$.
c. Connect a coaxial cable from the Standard Amplitude Calibrator oufput to the Type 7A22 + INPUT connector.
d. Turn the COARSE and FINE OFFSET controls fully counterclockwise.
e. CH ECK-The trace can be returned to graticule center. (1 V minimum DC offset).
i. Set the + NPUT AC-GND-DC switch to GND.
i. Rotate the FINE and COARSE OFFSET controls clockwise to return the trace to graticule center lapproximately 5 turns of the COARSE OFFSET controi).

NOTE
The $\times 10, \times 100$, and $\times 1000$ input attenuators will be checked in step 15. Consequently, the remainder of the DC OFFSET ranges stated in Section 1 will be verified by that step.
Type 7A22 Controls

| VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| POSITION | Midrange |
| HIGH FREQ -3 dB | 1 MHz |
| POINT |  |
| LOW FREQ -3 dB <br> POINT | DC |
|  | DC |
|  | GND |

## Time Base Controls

$$
\begin{aligned}
& .5 \mathrm{~ms} \\
& \text { In } \\
& \text { Norm, +Slope, AC, Int }
\end{aligned}
$$



Fig. 5-3. Typical waveform showing (A) Cross neutralization properly cadjusted, (B) incorrectly adjusied.
11. Check or Adjust C241 + Cross Neutralization
a. Set the Standard Amplitude Calibrator for a 50 mV square-wave output.

## NOTE

The Type 7A22 POSITION control and the Time Base horizontal positioning control may not always be mentioned. Use these controls as necessary to position the display for easy viewing.
b. CHECK-The upper leading corner of the waveform, and note any aberration that occurs while switching the -INPUT AC-GND-DC switch from GND to DC. The waveform should appear similar to the oneinfigs 5-3. The aberration should not exceed $\pm 1 \%$.
c. Set the -INPUT AC-GND-DC switch to DC.
d. ADJUST-C241 (see rig. 5-1) for best square upper leading corner.
e. INTERACTION-C241 affects the $\times 1$ input capacitance and all other input attenuator adjustments. If C241 is adjusted out of sequence, steps 13,14 and 16 through 18 must also be performed.

## 12. Check or Adiust $\mathrm{Cl} 41+$ Cross Neutralization

a. Disconnect the signal from the $+\mathbb{N}$ PUT connector and connect it to the -INPUT connector.
b. Set the +INPUT AC-GND-DC switch to GND.
c. CHECK-The lower leading corner of the second cycle of the display and note any aberration that occurs while switching the +INPUT AC-GND-DC switch from GND to DC. The bottom leading corner of the waveform should appear similar to the one shown infig. 5-3, The aberration should not exceed $\pm 1 \%$.
d. Set the +INPUT AC-GND-DC switch to DC.
e. ADJUST- Cl 41 (seefrig.5-5) for best square corner.
f. INTERACTION-C141 affects the $X 1$ input capacitance and all other input atfenvator adjustments. If Cl 41 is adjusted out of sequence, steps 13,14 and 16 through 18 must be performed.
g. Disconnect the coaxial cable from the -INPUT.

## 13. Check or Adiust CI 15-x 1 +HNPUT O

 Attenuator Time Constant> N O TE

It is important that C141 and C241 be properly adjusted before performing this adjustment. If you have not performed steps 11 and 12, do so at this point.
a. Connect a 47 pF input RC Normalizer to the + INPUT.
b. Connect a coaxial cable from the Standard Amplifude Calibrator to the RC Normalizer.
c. Set the -INPUT AC-G ND-DC switch to GND.
d. Set the + INPUT AC-GND-DC switch to DC.
e. Set the Standard Amplitude Calibrator output to 0.1 V square wave.
f. CHECK-The square wave display for flat tops (see Fig. 5-4).
g. ADJUST-Cl 15 (see rig. $5-1$ ) to obtain best squarewave response.
h. INTERACTION-If Cl 15 is adjusted out of sequence, steps 14 and 16 through 19 must also be performed.

## 14. Check or Adiust C21 5—)(x1 -INPUT O

 Attenuator Time Constanta. Disconnect the RC Normalizer from the +INPUT and connect it to the -INPUT.
b. Set the + INPUT AC-GND-DC switch to GND.

(A)

(B)

(C)

Fig. 5-4. Typical waveform showing (A) Correct cdjustment of Input Attenuator Time Constant. (B) and (C) incorrect adjustment.
c. Set the -INPUT AC-G ND-DC switch to DC.
d. CHECK-Each square wave for a flat bottom, using fig. 5-4 as a guide.
e. ADJUST-C215 (see fig. 5-7) for best flat bottom square-wave display, as in fig. 5-4A.
f. INTERACTION-If C215 is adjusted out of sequence, steps 13 and 16 through 19 must also be performed.
g. Disconnect the signal and the RC Normalizer.

## 15. Check Input Attenuator Accuracy

a. Connect a 50 mV peak-to-peak square wave signal from the Standard Amplitude Calibrator through a coaxial cable to the +INPUT.
b. Set the + INPUT AC-GND-DC switch to DC.
c. CHECK - The input attenuators using Gable $5-3$ as a guide.

TABLE 5-3

| VOLTS/DIV <br> Switch <br> Position | CALIBRATOR <br> Output <br> Peak to Peak | VERTICAL DEFLECTION <br> (Accuracy $\pm 2 \%$ ) |
| :---: | :---: | :---: |
| 10 mV | 50 mV | $5 \operatorname{div} \pm .1 \operatorname{div}$ |
| 20 mV | .1 V | $5 \operatorname{div} \pm .1 \operatorname{div}$ |
| 50 mV | .2 V | $4 \operatorname{div} \pm .08 \operatorname{div}$ |
| .1 V | .5 V | $5 \operatorname{div} \pm .1 \operatorname{div}$ |
| .2 V | 1 V | $5 \operatorname{div} \pm .1 \operatorname{div}$ |
| .5 V | 2 V | $4 \operatorname{div} \pm .08 \operatorname{div}$ |
| 1 V | 5 V | $5 \operatorname{div} \pm .1 \operatorname{div}$ |
| 2 V | 10 V | $5 \operatorname{div} \pm .1 \operatorname{div}$ |
| 5 V | 20 V | $4 \operatorname{div} \pm .08 \operatorname{div}$ |
| 10 V | 50 V | $5 \operatorname{div} \pm .1 \operatorname{div}$ |

d. Disconnect the signal from the Type 7A22.

## NOTE

(Applies to calibration only)
If there is a spike or fast rolloff of the leading corner of the square wave when checking from 20 mV to 10 V , ignore these, as they will be corrected in step 17.
16. Check or Adjust Input Attenuator Differential Balance
a. Connect a T connector to the Output connector of the Standard Amplitude Calibrator and a dual connector to the + INPUT and -INPUT connectors of the Type 7A22.
b. Connect a coaxial cable from the $T$ connector to the dual input connector. Connect a coaxial cable from the $T$ connector to the Ext In connector on the oscilloscope.
c. Set the Type 7A22 controls as follows:

VOLTS/DIV
AC-GND-DC $(+\mathbb{N} P U T)$
AC-GND-DC (-INPUT)
d. Set the oscilloscope Triggering Source switch to Ext.
e. Set the Standard Amplitude Calibrator output to 50 V .
f. CHECK-For optimum differential balance according to the information given in fable $5-4$. When properly ad-

$$
50 \mathrm{mV}
$$

DC
DC
(1)


Fig. 5-5. Typical display obtained when Input Attenuators are adjusted for optimum differential balance.
justed, the waveform should appear as shown in rig. 5-5, Disregard any spikes on the waveform.
g. ADJUST-R108E, R109E and R1 10E (see Fig. 5-1) for minimum amplitude as shown in rig. 5-5, usingrable 5-4 as a guide.

TABLE 5-4

| VOLTS/DIV <br> Switch <br> Position | Calibrator <br> Output <br> (peak to <br> peak) | Check and <br> Adjust <br> for Null | Input <br> Attenuator |
| :---: | :---: | :---: | :---: |
| 50 mV | 50 V | Check/Adjust R108E |  |
| 20 mV | 50 V | Check | $\times 10$ |
| .1 V | 50 V | Check |  |
| .5 V | 100 V | Check/Adjust R109E |  |
| .2 V | 100 V | Check | $\times 100$ |
| 1 V | 100 V | Check |  |
| 5 V | 100 V | Check/Adjust R110E |  |
| 2 V | 100 V | Check | $\times 1000$ |
| 10 V | 100 V | Check |  |

h. Set the Standard Amplitude Calibrator for 0.2 V peak-to-peak output.
i. Disconnect the dual input connector from the Type 7A22.

Set the Type 7A22 Controls:

| VOLTS/DIV | 50 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| HIGH FREQ -3dB | 1 MHz |
| POINT | DC |
| LOW FREQ -3 dB <br> POINT | DC |
| AC-GND-DC (+INPUT) | DC-GND-DC (-INPUT) | | GND |
| :--- |
| Adjusted for proper DC Bal- |
| ance |

Set the Time Base Controls.

| Time/Div | .5 ms |
| :--- | :--- |
| Variable | In (Cal) |
| Triggering | Auto, Ac, Int |

## 17. Check or Adjust + Input Attenuator O Compensation

a. Connect a 0.2 V peak-to-peak signal from the Standard Amplitude Calibrator through a coaxial cable to the +INPUT of the Type 7A22.
b. CHECK—The +INPUT Attenuator compensation for good square wave response.
c. ADJUST-The +INPUT Attenuator compensation for best square wave response using Table 5-5 as a guide Fiq. 5-1 shows the locations of the adjustments.

TABLE 5-5

| Calibrator Output P-P | VOLTS/DIV Switch Position | Check/Adjust for Optimum |  | $+ \text { Input }$ Attenuator |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Upper Leading Corner | Flat Top |  |
| . 2 V | 50 mV | C108C |  | $\times 10$ |
| . 1 V | 20 mV | Check |  |  |
| . 5 V | . 1 V | Check |  |  |
| 2 V | . 5 V | C109C |  | $\times 100$ |
| 1 V | . 2 V | Check |  |  |
| 5 V | 1 V | Check |  |  |
| 20 V | 5 V | C110C |  | $\times 1000$ |
| 10 V | 2 V | Check |  |  |
| 50 V | 10 V | Check |  |  |

Connect the 47 pF input RC normalizer between the $+\mathbb{I N}$ PUT and the coaxial cable.

| 50 V | 5 V |  | Cl10A | $\times 1000$ |
| :---: | :---: | :---: | :---: | :---: |
| 20 V | 2 V |  | Check |  |
| 100 V | 10 V |  | Check |  |
| 5 V | .5 V |  | Cl09A | $\times 100$ |
| 2 V | .2 V |  | Check |  |
| 10 V | 1 V |  | Check |  |
| .5 V | 50 mV |  | Cl08A | $\times 10$ |
| .2 V | 20 mV |  | Check |  |
| 1 V | .1 V |  | Check |  |

c. INTERACTION--If this step is performed out of sequence, steps 18 and 19 must be performed.
d. Disconnect the RC nomalize, and coaxial cable from the Type 7A22 and the Standard Amplitude Calibrator.

## 18. Check or Adjust - Input Attenuator O Series Compensation

o. Connect a T connector to the Standard Amplitude Calibrator output connector and a dual input connector to the


Fig. 5-6. Typical display obtained with - Input attenuator ad. ijusted for optimum Common-Mode signal rejection. (AI C208C adjusted properly (B) C209C adjusted properly.

Type 7A22 +INPUT and -INPUT connectors. Connect a coaxial cable from the T connector to the dual input connector. Connect a coaxial cable from the T connector to the oscilloscope Ext In connector.
b. Set the oscilloscope Triggering Source switch to Ext.
c. Set the Standard Amplitude Calibrator output to 50 V square wave.
d. Set the Type 7A22 controls os follows:

$$
\begin{array}{lll}
\text { VOLTS/DIV } & 50 \mathrm{mV} \\
\text { AC-GND-DC } & \text { (-INPUT) } & \text { DC }
\end{array}
$$

e. CHECK-The displayed waveform for good com-mon-mode signal rejection (minimum spike amplitude).
f. ADJUST-The - Input attenuator series compensation for best common-mode signal rejection (minimum spike amplitude) using the information given in Table 5-6. Fig. 5-6 illustrates the typical displays obtained and Fig. 5-1] shows the adjustment locations.


Fig. 5-7. Equipment required for steps 20 through 24.

TABLE 5-6

| Calibrator Output P-P | VOLTS/DIV <br> Switch Position | Check or Adjust for Min. Spike Amplitude | - Input <br> Attenuator |
| :---: | :---: | :---: | :---: |
| 50 Volts | $\begin{aligned} & \hline 50 \mathrm{mV} \\ & 20 \mathrm{mV} \\ & .1 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \hline \hline \text { C208C } \\ & \text { Check } \\ & \text { Check } \end{aligned}$ | $\times 10$ |
| 100 Volts | $\begin{aligned} & .5 \mathrm{~V} \\ & .2 \mathrm{~V} \\ & 1 \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \text { C209C } \\ & \text { Check } \\ & \text { Check } \end{aligned}$ | $\times 100$ |
|  | $\begin{array}{r} 5 \mathrm{~V} \\ 2 \mathrm{~V} \\ 10 \mathrm{~V} \end{array}$ | C210C Check Check | $\times 1000$ |

g. Disconnect all signal leads.
h. Return the oscilloscope Triggering Source switch to Int.
19. Check or Adjust -Input Attenuator O Shunt Compensation
a. Connect a 47 pF RC Normalizer to the -INPUT of the Type 7A22. Connect a coaxial cable from the Standard Amplitude Calibrator output connector to the RC Normalizer.
b. Set the Standard Amplitude Calibrator output to . 5 V square wave.
c. Set the Type 7 A22 controls as follows:

VOLTSIDIV 50 mV
AC-GND-DC (+- INPUT) GND
d. CHECK—Using Table 5-7 as a guide, check the display for a square wave response similar to the display illustrated in Fia. 5-4
e. ADJUST-C208A, C209A, and C210A (see FLD. 5-1] for best flat bottom on the display, according to the information given in able 5-7.

TABLE 5-7

| Standard Amplitude Calibrator Output P-P | VOLTS/DIV Switch Position | Check or Adjust for Optimum Flat Bottom | - Input Attenuator |
| :---: | :---: | :---: | :---: |
| . 5 Volt | 50 mV | C208A | $\times 10$ |
| . 2 Volt | 20 mV | Check |  |
| 1 Volt | . 1 V | Check |  |
| 5 Volts | . 5 V | C209A | $\times 100$ |
| 2 Volts | . 2 V | Check |  |
| 10 Volts | 1 V | Check |  |
| 50 Volts | 5 V | C210A | $\times 1000$ |
| 20 Volts | 2 V | Check |  |
| 100 Volts | 10 V | Check |  |

f. Disconnect the RC normalizer and all coaxial cables. Type 7A22 controls:

| POSITION | Midrange |
| :--- | :--- |
| VOLTS/DIV | 1 V |
| VARIABLE | CAL IN |
| AC-GND-DC (+ INPUT) | GND |
| AC-GND-DC (-INPUT) | GND |
| LOW FREQ -3 dB POINT | DC |
| HIGH FREQ -3 dB POINT | 1 MHz |
| STEP ATTEN DC BAL | Adjusted for DC balance |

## 20. Check or Adiust HIGH FREQ -3dB POINT

a. Test equipment setup is shown in Frig. 5-7,
b. Set theType 7A22 + INPUT AC-GND-DC switch to DC and use the oscilloscope controls as necessary for easy viewing of display.
c. Connect a coaxial cable from the constant Amplitude Sine-Wave Generator to the Type 7A22 + INPUT.
d. Set the output frequency of the Sine Wave Generator to 1 kHz and adjust for a 6 div display on the oscilloscope.
e. Set the Sine Wave Generator output frequency to 1 MHz .
f. CHECK-The amplitude of the oscilloscope display should be 4.2 div (this is the -3 dB point at 1 MHz ). The 4.2 div display requirement must be met af $1 \mathrm{MHz}+$ or $-10 \%$ (. 9 MHz to 1.1 MHz ).
g. ADJUST-With the frequency set to 1 MHz , adjust C 425 for 4.2 div of display amplitude. Se fig. 5-8 for location of adjustment.
h. CHECK - The remaining positions of the HIGH FREQ
-3 dB POINT selector in the same manner as in step $h$ using Table 5-9as a guide.

TABLE 5-9

| Sine Wave <br> Generator <br> Output <br> Frequency | HIGH FREQ <br> -3 dB <br> POINT <br> Selector <br> Position | Oscilloscope <br> Display <br> Amplitude | Bandwidth <br> Tolerance <br> $\pm \quad 12 \%$ of <br> Input Freq |
| :---: | :---: | :---: | :---: |
| 300 kHz | 300 kHz | 4.2 div | $\pm 30 \mathrm{kHz}$ |
| 100 kHz | 100 kHz | 4.2 div | $\pm 10 \mathrm{kHz}$ |
| 30 kHz | 30 kHz | 4.2 div | $\pm 3 \mathrm{kHz}$ |
| 10 kHz | 10 kHz | 4.2 div | $\pm 1 \mathrm{kHz}$ |
| 3 kHz | 3 kHz | 4.2 div | $\pm .3 \mathrm{kHz}$ |
| 1 kHz | 1 kHz | 4.2 div | $\pm .1 \mathrm{kHz}$ |
| 300 Hz | 300 Hz | 4.2 div | $\pm 30 \mathrm{~Hz}$ |
| 100 Hz | 100 Hz | 4.2 div | $\pm 10 \mathrm{~Hz}$ |



Fig. 5-8. Right side of Type 7 A22 showing location of adjustments.
i. Sei the HIGH FREQ - 3 dB POINT selector to 1 MHz .

## 21. Check LOW FREQ -3 dB POINT

a. CHECK-UsingTable 5-10 as a guide, check the LOW FREQ -3 dB POINT in the same manner that was used to check the HIGH FREQ -3 dB POINT.

TABLE 5-10

| Sine Wave | LOW FREQ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Generator | -3 dB | Oscilloscope <br> Display | Bandwidth <br> Tolerance |  |  |
| Output | POINT | Amplitude | $\pm 12 \%$ of |  |  |
| Freq | Selector <br> Position |  | Input Freq |  |  |
|  | 10 Hz | 4.2 div | $\pm 1.2 \mathrm{~Hz}$ |  |  |
| 10 Hz | 100 Hz | 4.2 div | $\pm 12 \mathrm{~Hz}$ |  |  |
| 100 Hz | 1 kHz | 4.2 div | $\pm 120 \mathrm{~Hz}$ |  |  |
| 1 kHz | 10 kHz | 4.2 div | $\pm 1.2 \mathrm{kHz}$ |  |  |
| 10 kHz | NOTE |  |  |  |  |

The components that are used in the 0.1 Hz and 1 Hz positions of the LOW FREQ -3 dB POINT selector are also used in the other positions of the selector; therefore, the tolerance of the 0.1 Hz and 1 Hz positions are checked.

Type 7A22 controls:

| VOLTS/DIV | 5 V |
| :--- | :--- |
| VARIABLE | CAL IN |
| HIGH FREQ -3 dB | 1 MHz |
| POINT |  |
| LOW FREQ -3 dB <br> POINT | DC |
| AC-GND-DC(+INPUT) | DC |
| AC-GND-DC (-INPUT) | GND |
| STEP ATTEN DC | Adjusted for proper DC |
| BAL | balance |

Time-Base controls:
Time/Div

Variable
Triggering

$$
\begin{aligned}
& \text { CAL IN } \\
& 1 \mathrm{MHz} \\
& \text { DC } \\
& \text { DC } \\
& \text { GND } \\
& \text { Adjusted fo } \\
& \text { balance }
\end{aligned}
$$

As necessary for easy viewing of display In (Cal)
Auto, AC, Ext

## 22. Check or Adjust Attenuator Common Mode Rejection

a. Attach a BNC $T$ connector to the 7850 EXT in connector. Connect a coaxial cable from the Constant Amplitude Sine-Wave Generator output to the BNC T connector. Connect another coaxial cable from the BNC T connector to the dual input connector.
b. Connect the Dual-Input connector to the Type 7A22 + and - INPUTS.
c. Set the 7B50 SOURCE to EXT X10, and DISPLAY MODE to AMPLIFIER. Adjust the Constant Amplitude SineWave Generator Level control for 20 V P-P at 100 kHz . Use the VARIABLE on the 7B50 to adjust for a suitable display of 4 to 6 horizontal divisions.

## N O TE

The Sine-Wave Generator output must be maintained at a constant 20 V p-p for all of the CMRR checks.
d. Switch the Type 7A22 AC-GND-DC (+INPUT) to GND.
e. Switch the Type 7A22 VOLTS/DIV to .1 mV .
f. Simultaneously switch the Type 7A22 + and - AC-GND-DC switches to DC.
g. CHECK-The vertical deflection should not exceed 2 div. The 2 div requirement at $0.1 \mathrm{mV} /$ DIV is equivalent to a CMRR of 100,000:1 (2 div at $.1 \mathrm{mV} /$ DIV $=.2 \mathrm{mV} ; 20 \mathrm{~V} \div .2 \mathrm{mV}=$ 100,000 ).
h. Adjust C330 (and C144 SN B080000 and up) for minimum vertical deflection. Seefig. 5-8 for C330 location. C144 is under the plastic cover near Q153 on the left side of the 7A22 (see שg-4-6 page 4-10.

## NOTE

These adjustments interact, and a slight readjustment of C330 will be necessary after the cover is replaced over C144.

1. Set the Sine Wave Generator frequency to 100 kHz .
2. Set the Type 7A22 VOLTS/DIV to 20 mV .
3. Adjust-C1 08C for minimum vertical deflection.
4. ADJUST-R1 16 for minimum vertical deflection.
i. CHECK-Using Table 5-11 as a guide, check the CMRR at the remaining attenuator positions.
j. Disconnect all test leads and connectors.

Type 7A22 Controls:

| VOLTS/DIV | 10 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| POSITION | Midrange |
| HIGH FREO -3 dB | 1 MHz |
| POINT |  |
| LOW FREO -3 dB <br> POINT | DC |
| AC-GND-DC (+INPUT) | GND |
| AC-GND-DC (-INPUT) | GND |
| STEP ATTEN DC |  |
| BAL | Adjusted for DC balance |

Time Base Controls:

| Time/Div | 1 ms |
| :--- | :--- |
| Triggering | + , Auto, AC, Int |

## 23. Check Input OVERDRIVE Indicator

a. Connect a coaxial cable between the Sine-Wave Generator output and the Type 7A22 +INPUT.
b. Set the Sine-Wave Generator amplitude to minimum and frequency to 1 kHz .
c. Increase the Sine-Wave Generator amplitude until the Type 7A22 Input OVERDRIVE indicator lights.
d. CHECK-The sine-wave amplitude, peak to peak, and divide by 2 to find the + or - driving signal amplitude. The overdrive signal should be approximately 1 volt.
e. Disconnect coaxial cable from +Input.

Type 7A22 Controls:

| VOLTS/DIV | 1 mV |
| :--- | :--- |
| VARIABLE | CAL IN |
| POSITION | Midrange |
| HF -3 dB POINT | 1 MHz |
| LF-3 dB POINT | 10 Hz |
| AC-GND-DC (+ INPUT) | GND |


| Sine-Wave Gen. |  | Type 7A22 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Amplitude | Frequency | VOLTS/DIV <br> switch | + and <br> INPUT <br> switches | Vertical <br> Deflection <br> (max) | CMRR <br> (min) |
| 20 V p-p | 100 kHz | 1 mV | AC | 1 div | $20,000: 1$ |
|  | 100 kHz | 20 mV | AC | 2.2 div | $450: 1$ |
|  | 100 kHz | 20 mV | DC | 2 div | $500: 1$ |
|  | 1 kHz | 20 mV | DC | 1 div | $1,000: 1$ |
|  | 1 kHz | 20 mV | AC | 1.1 div | $900: 1$ |
|  | 60 Hz | 2 mV | AC | 5 div | $2,000: 1$ |

```
AC-GND-DC (-INPUT)
STEP ATTEN DC BAL
```

Time Base Controls:

| Time/Div | 1 ms |
| :--- | :---: |
| Variable | Calibrated |
| Slope | + |
| Coupling | AC |
| Source | Int |
| Mode | Auto |

b. Set the Standard Amplitude Calibrator amplitude to $1 V$, $+D C$.
c. Connect a coaxial cable between the Sine-Wave Generator output and the Type 7 A 22 -INPUT.
d. Switch the -AC-GND-DC switch to $D C$
e. Adjust the Sine-Wave Generator amplitude control to give 5 div of 1 kHz display on the CRT graticule (if the SineWave Generator minimum amplitude is too large, insert an attenuator between the coaxial cable and the -INPUT).
f. Switch the $+A C-G N D-D C$ switch to $D C$.
g. CHECK-Sine wave amplitude should not change when DC level from Standard Amplitude Calibrator is applied.
tude Calibrator output connector and the Type $7 A 22+I N P U T$. $\quad$. Switch the $+A C-G N D-D C$ switch to GND.

$$
\text { h. Switch the }+A C-G N D-D C \text { switch to GND. }
$$

-1_


Fig. 5-9. Equipment required for step 25.
i. Switch the Standard Amplitude Calibrator mode to -DC.

1. Switch the + AC-GND-DC switch to DC.
k. CHECK-Sine wave amplitude should not change when DC level from Standard Amplitude Calibrator is applied.
2. Disconnect all test equipment and test leads.
3. Check Overall Noise Level Tangentially
a. Equipment sefup is shown infrig. 5-9.
b. Connect a $50 \Omega$ termination to the + INPUT connector of the Type 7A22. Connect two $10 \times$ attenuators to the $50 \Omega$ termination.
c. Connect a GR to BNC adapter to the Oscilloscope Calibrator + Volts connector and connect the Varibale Attenuator to the GR connector. Connect a GR to BNC adapter to the Variable Attenuator. Connect a coaxial cable from the $10 \times$ attenuators to the Variable Attenuator.
d. Set the Oscilloscope Calibrator to 4 mV and 1 kHz .
e. Set the 7A22 VOLTS/ DIV switch to $10 \mu \mathrm{~V}$.
f. Turn the Variable Attenuator fully clockwise.
g. Set the Time Base Triggering Mode to Auto and Time/ Div to 10 f es.
h. Turn the Variable Attenuator counterclockwise until the darker band between the two noise bands just disappears (secfig_5.10).
i. Set the Type 7A22 VOLTS/DIV switch to 1 mV and the Time Base Time/Div switch to 1 ms .
$j$. Remove the two $10 \times$ attenuators and connect the coaxial cable to the $50 \Omega$ termination.
k. Measure the square wave amplitude. Calculate the tangentially measured display noise as follows:
sauare wave amblitude
100
The tangentially measured noise should not exceed $16 \mu \mathrm{~V}$.
Type 7A22 controls:

VOLTS/DIV
VARIABLE /VOLTS/DIV POSITION

HF-3dB POINT
LF -3 dB POINT
AC-GND-DC +INPUT
AC-GND-DC -INPUT
STEP ATTEN DC BAL Adjusted for Dc Balance

CAL IN
1 division below graticule center
1 MHz
DC
DC
GND

(A)

(B)

Fig. 5-10. Typical display showing $[A)$ two noise bands and (B) merging noise bands,

Time Base controls:

| Time/Div | $2 \mu \mathrm{~s}$ |
| :--- | :--- |
| Variable | Cal In |
| Level/Slope | - |
| Coupling | DC |
| Source | Int |
| Mode | Auto |

26. Check Overdrive Recovery Time
a. Test equipment setup is shown infig. 5-id.
b. Connect the Reed Pulse Generator Output to the Type $7 A 22+$ INPUT.
c. Connect the Reed Pulse Generator Power Cable to the Oscilloscope Probe Power connector (rear panel).
d. Switch the Reed Pulse Generator Polarity switch to + .


Fig. 5-11. Equipment required for step 26.
e. Hold down the Reed Pulse Generator Man switch and adjust the Level control to position the trace to the top graticule line ( 1 volt).
f. Release the Man switch and switch the Time Base Mode to Norm.
g. Set the Type 7A22 VOLTS/DIV switch to 1 mV .
h. Increase sweep Intensity to maximum (clockwise).
i. Depress the Reed Pulse Generator Man switch for 1 second.
i. CHECK-The waveform as the Reed Pulse Generator Man switch is released. Readjust the Time Base Level-Slope as necessary for proper triggering. The trace should return to within 5 mV of the reference ( 1 division below the graticule center) within 10 /us ( 5 divisions). See fig. 5 - 12 for photograph of typical recovery waveform.
k. Switch the Reed Pulse Generator Polarity switch to -
I. Set the Time Base Level/Slope to + .
m. Decrease sweep Intensity for normal viewing.
n. Reset the Time Base Mode to Auto.
o. Position the trace (7A22 POSITION control) to 1 division above graticule center.
p. Reset the Time Base Mode to Norm.
q. Repeat parts h through i (waveform will be inverted from that in step il.
r. Connect Reed Pulse Generator Output to the 7A22 -INPUT and repeat above procedure.


Fig. 5-12. Typical waveform showing overdrive recovery time.

# REPLACEABLE ELECTRICAL PARTS 

PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. FieldOffice or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or representative will contact you concerning any change in part number.

## SPECIAL NOTES AND SYMBOLS

X000 Part first added at this serial number
00X Part removed after this serial number

ITEM NAME
In the Parts List, an Item Name is separated from the description by a colon (:). Because of space limitations, an Item Name may sometimes appear as incomplete. For further Item Name identification, the U.S. Federal Cataloging Handbook H6-1 can be utilized where possible

## ABBREVIATIONS

| ACTR | ACTUATOR | PLSTC | PLASTIC |
| :--- | :--- | :--- | :--- |
| ASSY | ASSEMBLY | QTZ | QUARTZ |
| CAP | CAPACITOR | RECP | RECEPTACLE |
| CER | CERAMIC | RES | RESISTOR |
| CKT | CIRCUIT | RF | RADIO FREQUENCY |
| COMP | COMPOSITION | SEL | SELECTED |
| CONN | CONNECTOR | SEMICOND | SEMICONDUCTOR |
| ELCTLT | ELECTROLYTIC | SENS | SENSITIVE |
| ELEC | ELECTRICAL | VAR | VARIABLE |
| INCAND | INCANDESCENT | WW | WIREWOUND |
| LED | LIGHT EMITTING DIODE | XFMR | TRANSFORMER |
| NONWIR | NON WIREWOUND | XTAL | CRYSTAL |


| Mfr. Code | Manufacturer | Address | City, State, Zlip |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & 00853 \\ & 01002 \end{aligned}$ | SANGAMO ELECTRIC CO., S. CAROLINA DIV. | Р О box 128 | PICKENS, SC 29671 |
|  | GENERAL ELECTRIC COMPANY, INDUSTRIAL |  |  |
|  | AND POWER CAPACITOR PRODUCTS DEPARTMENT | John Street | HUDSON FALLS, NY 12839 |
| 01121 | ALLEN-BRADLEY COMPANY | 1201 2ND STREET SOUTH | MILWAUKEE, WI 53204 |
| 02111 | SPECTROL ELECTRONICS CORPORATION | 17070 EAST GALE AVENUE | CITY OF INDUSTRY, CA 91745 |
| 03508 | GENERAL ELECTRIC COMPANY, SEMI-CONDUCTOR |  |  |
|  | PRODUCTS DEPARTMENT | ELECTRONLCS PARK | SYRACUSE, NY 13201 |
| 04713 | MOTOROLA, INC. , SEMICONDUCTOR PROD. DIV. | 5005 E MCDOWELL RD,PO BOX 20923 | phoenix, Az 85036 |
| 08806 | GENERAL ELECTRIC CO., MINIATURE |  |  |
|  | LAMP PRODUCTS DEPARTMENT | NELA PARK | CLEVELAND, OH 44112 |
| 11237 | CTS KEENE, INC. | 3230 RIVERSIDE AVE. | PASO ROBLES, CA 93446 |
| 12697 | CLAROSTAT MFG. CO, , INC. | LOWER WASHINGTON STREET | DOVER, NH 03820 |
| 15454 | RODAN INDUSTRIES, INC. | 2905 BLUE STAR ST. | ANAHEIM, CA 92806 |
| 15818 | TELEDYNE SEMICONDUCTOR | 1300 terra bella ave. | MOUNTAIN VIEW, CA 94043 |
| 24931 | SPECIALTY CONNECTOR CO., INC. | 3560 MADISON AVE. | INDIANAPOLIS, IN 46227 |
| 27014 | NATIONAL SEMICONDUCTOR CORP. | 2900 SEMICONDUCTOR DR. | SANTA CLARA, CA 95051 |
| 32997 | BOURNS, INC., TRIMPOT PRODUCTS DIV. | 1200 Columbia AVE. | RIVERSIDE, CA 92507 |
| 56289 | Sprague electric Co. |  | NORTH ADAMS, MA 01247 |
| 71400 | BUSSMAN MFG., division of mcgraw- |  |  |
|  | EDISON CO. | 2536 W. UNIVERSITY ST. | ST. LOUIS, MO 63107 |
| 71744 | CHICAGO MINIATURE LAMP WORKS | 4433 RAVENSWOOD AVE. | Chicago, Il 60640 |
| 72982 | ERIE TECHNOLOGICAL PRODUCTS, INC. | 644 W .12 TH ST . | ERIE, PA 16512 |
| 73138 | BECKMAN INSTRUMENTS, INC., HELIPOT DIV. | 2500 HARBOR BLVD. | FULLERTON, CA 92634 |
| 74970 | JOHNSON, E. F., CO. | 299 10Th Ave. S. W. | WASECA, MN 56093 |
| 75042 | TRW ELECTRONIC COMPONENTS, IRC FIXED |  |  |
|  | RESISTORS, PHILADELPHIA DIVISION | $401 \mathrm{~N} . \mathrm{BROAD}$ ST. | Philadelphia, PA 19108 |
| 80009 | TEKTRONIX, INC. | P O box 500 | BEAVERTON, OR 97077 |
| 80294 | BOURNS, INC., INSTRUMENT DIV. | 6135 MAGNOLIA AVE. | RIVERSIDE, CA 92506 |
| 80740 | BECKMAN INSTRUMENTS, INC. | 2500 HARBOR BLVD. | FULLerton, CA 92634 |
| 81483 | INTERNATIONAL RECTIFIER CORP. | 9220 SUNSET BLVD. | LOS ANGELES, CA 90069 |
| 87034 | ILLUMINATED PRODUCTS INC., A SUB OF |  |  |
|  | OAK INDUSTRIES, INC. | 2620 SUSAN ST, PO BOX 11930 | SANTA ANA, CA 92711 |
| 91637 | DALE ELECTRONICS, INC. | P. O. BOX 609 | COLUMBUS, NE 68601 |


| Ckt N | Tektronix Part No. | Serial/Model Eff | No. Dscont | Name \& Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 670-1013-00 |  |  | CKT BOARD ASSY:BANDWIDTH | 80009 | 670-1013-00 |
|  | 670-1014-00 | B010100 | B029999 | CKT Board Assy main | 80009 | 670-1014-00 |
|  | 670-1014-01 | в030000 | в059999 | CKT Board Assy :MAIN | 80009 | 670-1014-01 |
|  | 670-1014-03 | B060000 | B069999 | CKT board assy main | 80009 | 670-1014-03 |
|  | 670-1014-04 | B070000 | в079999 | CKT Board Assy main | 80009 | 670-1014-04 |
|  | 670-1014-05 | B080000 | B115479 | CKT board assy main | 80009 | 670-1014-05 |
|  | 670-1014-06 | B115480 |  | CKT Board Assy main | 80009 | 670-1014-06 |
|  | 670-1050-00 | B010100 | B059999 | CKT BOAR ASSY :AC-GND-DC | 80009 | 670-1050-00 |
|  | 670-1050-01 | B060000 |  | CKT BOARD ASSY :AC-GND-DC | 80009 | 670-1050-01 |
|  | 670-1051-00 | B010100 | B059999 | CKT BOARD ASSY: $+\mathrm{AC}-\mathrm{GND}-\mathrm{DC}$ | 80009 | 670-1051-00 |
|  | 670-1051-01 |  |  | CKT BOARD ASSY: +AC-GND-DC | 80009 | 670-1051-01 |
| ${ }^{C 1011}$ | 295-0117-00 |  |  | CAP. ,SET, MTCHD: (2) 0.1 UVF , MATCHED 0.19 | 80009 | 295-0117-00 |
| C103 | 283-0636-00 |  |  | CAP.,FXD, MICA D: $36 \mathrm{PF}, 1.48$, 100 V | 00853 | D155F360G0 |
| C108A | 281-0092-00 | B010100 | B059999 | CAP.,VAR, CER DI:9-35PF,200V | 72982 | 538-011 D9-35 |
| C108A | 281-0131-00 | 8060000 |  | CAP., VAR,AIR DI $: 2.4$-24.5PF,250V | 74970 | 189-509-5 |
| C108C | 281-0131-00 |  |  | CAP.,VAR,AIR DI: $2.4-24.5 \mathrm{PF}, 250 \mathrm{~V}$ | 74970 | 189-509-5 |
| C108D | 283-0638-00 |  |  | CAP. ,FXD, MICA D: $130 \mathrm{PF}, 18,100 \mathrm{~V}$ | 00853 | D151F131F0 |
| C109A | 281-0092-00 | B010100 | B059999 | CAP., VAR, CER DI:9-35PF, 200V | 72982 | 538-011 D9-3 |
| C109A | 281-0131-00 | B060000 |  | CAP.,VAR,AIR DI : 2.4 -24.5PF, 250 V | 74970 | 189-509-5 |
| C109C | 281-0081-00 |  |  | CAP., VAR,AIR DI 1.8 8-13PF, 375VDC | 74970 | 189-6-5 |
| Cl09D | 283-0594-00 |  |  | CAP., FXD, MICA D: $0.001 \mathrm{~F}, 18,100 \mathrm{~V}$ | 00853 | D151F102F0 |
| C110A | 281-0092-00 | B010100 | B059999 | CAP. ,VAR, CER DI :9-35PF, 200 V | 72982 | 538-011 D9-35 |
| C110A | 281-0131-00 | в060000 |  | CAP., VAR, AIR DT : 2.4 -24.5PF, 250V | 74970 | 189-509-5 |
| C110C | 281-0079-00 |  |  | CAP. ,VAR, AIR DI :1.5-9.1PF, 800 V | 74970 | 189-4-5 |
| Cl10d | 283-0617-00 |  |  | CAP. ,FXD, MICA D: $4700 \mathrm{PF}, 10 \%$,300V | 00853 | D193F472k0 |
| C115 | 281-0092-00 | в010100 | B059999 | CAP.,VAR, CER DI:9-35PF, 200 V | 72982 | 538-011 D9-3 |
| C115 | 281-0131-00 | в060000 |  | CAP., VAR, AIR DI : 2.4 -24.5PF, 250V | 74970 | 189-509-5 |
| C141 | 281-0093-00 |  |  | CAP., VAR, CER DI: $5.5-18 \mathrm{PF}$ | 72982 | 538-01145.5-18 |
| C144 | 281-0544-00 | в010100 | B079999 | CAP. ,FXD, CER DI: $5.6 \mathrm{PF}, 108,500 \mathrm{~V}$ | 72982 | 301-000СОН0569D |
| C144 | 281-0122-00 | в080000 |  | CAP.,VAR, CER DI: $2.5-9 \mathrm{PF}, 100 \mathrm{~V}$ | 72982 | 518-000A2.5-9 |
| C156 | 283-0594-00 |  |  | CAP.,FXD,MICA D: $0.001 \mathrm{FF}, 18,100 \mathrm{~V}$ | 00853 | D151F102F0 |
| $\mathrm{c} 201{ }^{1}$ | 295-0117-00 |  |  | CAP. ,SET, MTCHD : (2) 0.1UF, MATCHED 0.18 | 80009 | 295-0117-00 |
| c203 | 283-0636-00 |  |  | CAP. ,FXD, MICA D: $36 \mathrm{PF}, 1.48$, 100 V | 00853 | D155F36060 |
| c208A | 281-0092-00 | B010100 | B059999 | CAP. ,VAR, CER DI :9-35PF,200V | 72982 | 538-011 D9-35 |
|  | 281-0131-00 | B060000 |  | CAP.,VAR,AIR DI $: 2.4$-24.5PF,250V | 74970 | 189-509-5 |
|  | 281-0131-00 |  |  | CAP.,VAR,AIR DI : 2.4 -24.5PF,250V | 74970 | 189-509-5 |
| C208D | 283-0638-00 |  |  | CAP.,FXD, MICA D:130PF, 18,100V | 00853 | D151F131F0 |
| c209A | 281-0092-00 | 8010100 | B059999 | CAP.,VAR,CER DI:9-35PF,200V | 72982 | 538-011 D9-35 |
| C209A | 281-0131-00 | B060000 |  | CAP.,VAR,AIR DI $=2.4$-24.5PF, 250 V | 74970 | 189-509-5 |
| C209C | 281-0081-00 |  |  | CAP.,VAR,AIR DI: 1.8 -13PF, 375 VDC | 74970 | 189-6-5 |
| C209D | 283-0594-00 |  |  | CAP.,FXD,MICA D: $0.0016 \mathrm{~F}, 18,100 \mathrm{~V}$ | 00853 | D151F102F0 |
| c210a | 281-0092-00 | B010100 | B059999 | CAP.,VAR, CER DI:9-35PF, 200V | 72982 | 538-011 D9-35 |
| C210A | 281-0131-00 | 8060000 |  | CAP, ,VAR,AIR DI: 2.4 -24.5PF,250V | 74970 | 189-509-5 |
| c210c | 281-0079-00 |  |  | CAP.,VAR,AIR DI: 1.509 .1 PF , 800 V | 74970 | 189-4-5 |
| C2100 | 283-0617-00 |  |  | CAP. , FXD,MICA D: $4700 \mathrm{PF}, 108,300 \mathrm{~V}$ | 00853 | D193F472k0 |
| C215 | 281-0092-00 | B010100 | B059999 | CAP.,VAR, CER DI:9-35PF,200V | 72982 | 538-011 D9-35 |
| C215 | 281-0131-00 | в060000 |  | CAP.,VAR,AIR DT : 2.4 -24.5PF, 250V | 74970 | 189-509-5 |
| C241 | 281-0093-00 |  |  | CAP.,VAR, CER DI: 5.5 -18PF | 72982 | 538-011A5.5-13 |
| C244 | 281-0544-00 |  |  | CAP. ,FXD, CER DI :5.6PF, 108,500V | 72982 | 301-000сон0569D |
| C256 | 283-0594-00 |  |  | CAP., FXD, MICA D: $0.001 \mathrm{FF}, 18,100 \mathrm{~V}$ | 00853 | D151F102F0 |
| C264 | 283-0059-00 |  |  | CAP., FXD, CER DI :IUF, +80-20\%, 25V | 72982 | 8141N037z500105z |
| C283 | 290-0284-00 |  |  | CAP., FXD, ELCTLT:4.7UF,108,35V | 56289 | 150D475×9035B2 |


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| :---: | :---: | :---: | :---: | :---: |
| C307 | 290-0297-00 | CAP.,FXD, ELCTLT: 39UF, 10\%,10V | 56289 | 15 0D396x9010B2 |
| C315 | 281-0613-00 | CAP., FXD, CER DI:10PF, $+/-1 \mathrm{PF}$, 200V | 72982 | 374-001C0G0100F |
| C317 | 290-0297-00 | CAP.,FXD, ELCTLT: 39UF, 10\%,10V | 56289 | 150D396x9010B2 |
| C325 | 290-0297-00 | CAP.,FXD, ELCTLT : 39UF, 10\%,10V | 56289 | 150D396x9010B2 |
| C329 | 283-0002-00 | CAP., FXD, CER DI:0.01UF, +80-208,500V | 72982 | 811-546E1032 |
| C330 | 281-0114-00 | CAP.,VAR, AIR DI:1.3-5.4PF,750V | 74970 | 189-0352-075 |
| C349 | 290-0177-00 | CAP.,FXD, ELCTLT:1UF,20\%,50V | 56289 | 162 D105x0050CD2 |
| C353A | 285-0809-00 | CAP., FXD, PLSTC : 1 UF,10\%,50V | 56289 | LP66A1A105K |
| C353D | 285-0809-00 | CAP.,FXD, PLSTC:IUF,10\%,50V | 56289 | LP66AlAl05K |
| C353G | 283-0058-00 | CAP.,FXD, CER DI:0.027UF,10\%,100V | 72982 | 8131N147X7R0273K |
| C413 | 281-0534-00 | CAP. , FXD, CER DI:3.3PF, + /-0.25PF,500V | 72982 | 301-000C0J0339C |
| C425 | 281-0093-00 | CAP.,VAR, CER DI:5.5-18PF | 72982 | 538-011A5.5-18 |
| C426A | 281-0528-00 | CAP.,FXD, CER DI:82PF, +/-8.2 PF, 500 V | 72982 | 301-000U2M0820K |
| -reat |  |  | W08, | $\bigcirc 1555551454$ |
| C4: | 283-0594. |  | 00 | 3 Dl51F10: |
| C4: | 285-0627. |  | 56: | 3 410P33: |
| C4: | 285-0598. | C.P.,FKD,PL TC:0.01UF 5\%,11 | 01 | ? 61Fl0ac. |
| C4: | 285-0702. | C.P.,F <D,PLi TC:0.033 JF 5\%,11 | 56: | 3 410P33: |
| C4: | 285-0703. |  | 56: | 3 410P10. |
| C4: | 285-0633. | CIP.,F KD, PLSTC:0.22UF, 20:5,11 | 56: | 7 410P22، |
| C. | 283-0000. |  | 72 | 831-516E1 |
| C. | 283-0092. | CP.,F KD, (3R DI:0.03 JF, +80-20\%,21 | 72 | $2845-534 \mathrm{E} 31$ |
| C | 283-0111. | CLP.,FXD, (ER DI:0.1UF,20\%, | 72 | ? 8.L21-N088Z5ult |
| C | 281-0534. |  | 72 | $2301-000 \mathrm{COJO3}$ |
| c | 283-0000. | C.P.,FXD, $\mathrm{CJR} \mathrm{DI:0.001UF,+100-08,51}$ | 72 | 831-516E1 |
| C | 283-0059. | CIP.,F KD, (SR DI: 1 JF, +80-208, | 72 | 8141N03725U014 |
| C | 283-0134. |  | 72 | 8.L41N077z5u04 |
| C | 283-0080. | CIP., F KD, (SR DI:0.022 JF, +80-20\%,: | 56: | 190 |
| 12 | 283-0080. | C.P.,FKD, 3 R DI :0.022 JF, $+80 \cdot-208$, | 56: | 1901 |
| C | 283-0080. |  | 56. | 3190 |
| CR: | 152-0323. | SEMIC (ND DEVI PE:SILICON, 35v,0 | 80 | 3 152-0323. |
| CR: | 152-0323. | SEMIC ND DEVI PE:SILICON, 35v,0 | 80 | 3 152-0323. |
| CR | 152-0141. | SEMIC ${ }^{\text {ND D D }}$ DVICE:SILICON,30V,151 | 801 | ) 152-0141. |
| CR: | 152-0141. | SEMIC ${ }^{\text {ND D D }}$ DVICE:SILICON,30V,15 | 801 | 3 152-0141 |
| CR: | 152-0323. | SEMIC ND DEVICE:SILICON, 35v,0 | 801 | 3 152-0323. |
| C. z | 152-0323. | SEMIC ND DEvICE:SILICON,35v,0 | 801 | 3 152-0323. |
| CR: | 152-0141. | SEMIC ND DEVICE:SILICON,30V,151 | 80 | 3 152-0141 |
| CR: | 152-0141. |  | 80 | 3 152-0141. |
| CR: | 152-0141. | SEMIC ${ }^{\text {JD }}$ DEV: CE:SILICON,30V,15 | 80 | 3 152-0141 |
| CR | 152-0141. | SEMIC ${ }^{\text {ND }}$ DEVICE:SILICON, 30V,151 | 801 | 3 152-0141 |
| CR | 152-0141. | SEMIC ND DEVICE:SILICON, 30V,151 | 80 | 3 152-0141. |
| CR | 152-0141. | SEMIC ${ }^{\text {SD D DEVI }}$ SE:SILICON, 30v,154 | 80 | 3 152-0141 |
| CR | 152-0141 | SEMIC ND DEVICE:SILICON,30V,151 | 801 | 3 152-0141 |
| CR | 152-0141 | SEMIC ND DEVICE:SILICON,30V,151 | 801 | 3 152-0141 |
| CR. | 152-0141. | SEMIC ${ }^{\text {ND }}$ DEVICE:SILICON, $30 \mathrm{~V}, 151$ | 801 | 3 152-0141 |
| CR | 152-0141. | SEMIC ${ }^{\text {ND }}$ DEVI TE :SILICON, $30 \mathrm{~V}, 151$ | 80 | 152-0141. |
| CR | 152-0141. | SEMIC ND DEVICE:SILICON, 30V,15 | 801 | 152-0141 |
| CR | 152-0141 | SEMIC ND DEVICE:SILICON,30V,15 | 801 | 152-0141. |
| CR: | 152-0141. | SEMIC ND DEVICE:SILICON,30v,154 | 801 | 152-0141 |
| CRI | 152-0141. | SEMIC ${ }^{\text {ND }}$ DEVICE:SILICON, $30 \mathrm{~V}, 151$ | 801 | ) 152-0141 |
| CR | 152-0141. | SEMIC ND DEVICE:SILICON,30V,151 | 80 | 3 152-0141. |
| CRI | 152-0141. | SEMIC ND DEVICE:SILICON,30v,154 | 80 | 3 152-0141 |
| C. 31 | 152-0141. | SEMIC ${ }^{\text {ND }}$ DEVICE:SILICON, 30V,151 | 801 | 152-0141 |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CR630 | 152-0141-02 |  |  | SEMICOND DEVICE:SILICON,30V,150MA | 80009 | 152-0141-02 |
| DS101 | 150-0093-00 | B010100 | B039999 | LAMP, INCAND:5.0V,0.06A | 71744 | 6833AS15 |
| DS101 | 150-0057-01 | B040000 | B059999 | LAMP, INCAND:5V,0.115A,WIRE LD, SEL | 87034 | $17 \mathrm{AS15}$ |
| DS101 | 150-0048-01 | 1 B060000 |  | LAMP, INCAND:5V,0.06A,SEL | 08806 | 683AS15 |
| DS301 | 150-0046-00 |  |  | LAMP, INCAND: $10 \mathrm{~V}, 0.04 \mathrm{~A}$ | 08806 | 2107D |
| F119 | 159-0024-00 |  |  | FUSE,CARTRIDGE:3AG, 0.06A, 250V,FAST BLOW | 71400 | AGC 1/16 |
| F219 | 159-0024-00 |  |  | FUSE,CARTRIDGE:3AG, 0.06A,250V,FAST BLOW | 71400 | AGC 1/16 |
| 5101 | 131-0679-00 | - B010100 | B093219 | CONNECTOR,RCPT, : BNC W/HARDWARE | 24931 | 28JR168-1 |
| J101 | 131-0679-02 | 2 B093220 |  | CONNECTOR, RCPT, : BNC W/HARDWARE | 24931 | 28JR270-1 |
| J201 | 131-0679-00 | - B010100 | B093219 | CONNECTOR,RCPT, : BNC W/HARDWARE | 24931 | 28JR168-1 |
| . $2 \Omega$ | 1.21- $-6.79-\Omega 2$ | 2 Rnq323 |  | SתNNESTSR, RCPTT, -RNC W/HAROWABF | 24921 | 2RTR2.78-1 |
| 2133 | 151-1027-00 | 3010100 | 3099999 | [RANSISTOR: 3 ILICON, JFE N-CHAN | 30009 | 151-1027-00 |
| 2133 | 151-1101-00 | 3100000 |  | [RANSISTOR: ${ }^{\text {SILICON, }}$, ET ,N NHANNEL | :7014 | ? N 5565 |
| 2144 | 151-0261-00 |  |  | [RANSISTOR: SILICON, ? ${ }^{\text {NP , }}$ JUAL | 30009 | L51-0261-00 |
| 2153 | .51-1028-00 |  |  | [RANSISTOR:SILICON,FET,N JHANNEL | L5818 | $J 1908$ |
| 2253 | .51-1028-00 |  |  | [RANSISTOR:SILICON,FET,N こHANNEL | L5818 | 11908 |
| 2264 | 151-0261-00 |  |  | [RANSISTOR ; IIICON . ${ }^{\text {NSP }}$. JUAL | 30009 | 151-0261-00 |
| 2273 | 151-0128-00 |  |  | CRANSISTOR:GE PNP | 34713 | ? N 2140 |
| 2283 | 151-0128-00 |  |  | [RANSISTOR: ${ }^{\text {EE }}$ ? ${ }^{\text {NP }}$ | 24713 | ? N 2140 |
| 2284 | 151-0195-00 |  |  | [RANSISTOR:SILICON NPN | 30009 | 151-0195-00 |
| 2304 | 151-0260-00 |  |  | [RANSISTOR:S: :LICON,NPN | 30009 | -51-0260-00 |
| 2314 | 151-0220-00 |  |  | [RANSISTOR:SILICON, PNP | 30009 | L51-0220-00 |
| 2324 | 151-0228-00 |  |  | [RANSISTOR:SILICON,PNP,SEL ?ROM 2 N 4888 | 30009 | 151-0228-00 |
| 2334 | 151-0228-00 |  |  |  | 30009 | L51-0228-00 |
| 2344 | 151-0195-00 |  |  | [RANSISTOR:SILICON, NPN | 30009 | 151-0195-00 |
| 2354 | .51-0195-00 |  |  | [RANSISTOR:SILICON NPN | 30009 | .51-0195-00 |
| 2404 | 151-1019-00 | 3010100 | 3069999 | CRANSISTOR ${ }^{\text {3 }}$ LLICON FET, N-CHANNEL | 30009 | L51-1019-00 |
| 2404 | 151-1050-00 | 3070000 |  | [RANSISTOR:S:CLICON,FET,N-CHANNEL DUAL | 30009 | L51-1050-00 |
| 2414 | 151-0261-00 |  |  | [RANSISTOR:SILICON, PNP,DUAL | 30009 | 1.51-0261-00 |
| 2424 | 151-0219-00 |  |  | [RANSISTOR: 3 ILICON, ${ }^{\text {PNP }}$ | 30009 | .51-0219-00 |
| 2434 | 151-0219-00 |  |  | [RANSISTOR:SILICON, PNP | 30009 | 151-0219-00 |
| 3444 | 151-0219-00 |  |  | [RANSISTOR:SILICON PNP | 30009 | 1.51-0219-00 |
| 2454 | 151-0219-00 |  |  | CRANSISTOR: ${ }^{\text {SILIICON, }}$, NP | 30009 | L.51-0219-00 |
| 2524 | 151-0219-00 |  |  | [RANS: SSTOR: iSILICON . ?NP | 30009 | 151-0219-00 |
| 2534 | 151-0219-00 |  |  | [RANSISTOR:SILICON PNP | 30009 | 151-0219-00 |
| 2544 | 151-0219-00 |  |  | [RANSISTOR:S:CLICON, PNP | 30009 | 151-0219-00 |
| 2554 | 151-0219-00 |  |  | CRANSISTOR:SILICON PNP | 30009 | 1.51-0219-00 |
| 2614 | 151-0254-00 | 3010100 | 3116609 | [RANSISTOR:SILICON,1NPN | 30009 | L51-0254-00 |
| 2614 | 151-0281-00 | - 3116610 |  | [RANSISTOR: isILICON NPN | 33508 | \{16P4039 |
| 2103 | 315-0105-00 |  |  | 2ES.,FXD,CMPSN:1M 3HM, 5\%,0.25W | 21121 | 2B1055 |
| 2108C | 323-0611-07 |  |  | RES. FXD,FILM:900K 3 HM, 0.1\%,0.5W | 31637 |  |
| 2108D | 121-0389-01 |  |  | 3ES. FXD,FILM:110K 3 HM,0.5\%,0.125W | 31637 | 4FF1816G11002D |
| 2108E | 111-0609-00 |  |  | 2ES. VAR,NONWIR:2K 3 HM, 10\%,0.50W | 13138 | 32-26-0 |
| 2109 C | 323-0614-07 |  |  | 2ES. FXD,FILM:990K JHM, 0.1\%,0.5W | 31637 | 4FF1226C99002B |
| 21090 | 121-0289-00 |  |  | 3ES. FXD, :ILM:10K JHM,1\%,0.125W | 31637 | 4FF1816G10001F |
| 2109E | 111-0605-00 |  |  | 2ES. VAR,NONWIR: 200 JHM, 10\%,0.50W | 30740 | 52-54-3 |
| 31100 | 123-0623-07 |  |  | EES. FXD, 7 ILM:999K JHM, ).1\%,0.5W | 31637 | 4FF1226C99902B |
| 21100 | 321-0197-00 |  |  | 2ES. FXD, ?ILM:1.1K JHM, 1\%, ).125W | 31637 | 4FF1816G11000F |
| 2110E | 111-0609-00 |  |  | 2ES. VAR, JONWIR: 2 K JHM, 10\%, J. 50W | 13138 | 32-26-0 |
| 2110 F | 321-0289-01 |  |  | 2ES. FXD, :ILM:10K HM, 0.5\%,0.125W | 31637 | 9FF1816G10001D |
| 2111 | 121-0481-07 |  |  | 2ES. FXD, :ILM:IM 3 HM, ).1\%,125W | 31637 | IMF188C10003B |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R115 | 311-0827-00 | B010100 | B069999 | RES., VAR,NONWIR:TRMR, 250 OHM, 0.5 W | 01121 | SV2511 |
| R115 | 311-1260-00 | B070000 |  | RES., VAR,NONWIR: 250 OHM, 10\%, 0.50W | 32997 | 3329 P-L58-251 |
| R116 | 311-0635-00 |  |  | RES., VAR, NONWIR: 1 K OHM, $10 \%, 0.50 \mathrm{~W}$ | 73138 | 82-32-0 |
| R117 | 321-0210-00 |  |  | RES.,FXD,FILM:1.5K OHM, 1\%,0.125W | 91637 | MFF1816G15000F |
| R119 | 315-0510-00 |  |  | RES. ,FXD, CMPSN:51 OHM, 5\%, 0.25 W | 01121 | CB5105 |
| R12I | 321-0344-00 |  |  | RES. FXX , FILM $: 37.4 \mathrm{~K}$ OHM, 1\%, 0.125 W | 91637 | MFFl816G37401F |
| R123 | 315-0151-00 |  |  | RES. ,FXD, CMPSN: 150 OHM, 5\%, 0.25W | 01121 | CB1515 |
| R133 | 308-0495-00 |  |  | RES.,FXD,WW:4.5K OHM, 0.1\% | 91637 | RS2B110-45000B |
| R141 | 315-0512-00 |  |  | RES.,FXD, CMPSN:5.1K OHM,5\%,0.25W | 01121 | CB5125 |
| R145 | 321-0289-00 |  |  | RES.,FXD,FILM:10K OHM, 1\%,0.125W | 91637 | MFF1816G10001F |
| R151 | 308-0546-00 |  |  | RES. ,FXD, WW:125 OHM, 0.1\%, 3W | 91637 | RS2Bll0-125ROB |
| R153 | 321-0114-00 |  |  | RES. ,FXD, FILM:150 OHM, 18,0.125W | 91637 | MFF1816G150ROF |
| R155 | 315-0101-00 |  |  | RES. ,FXD, CMPSN: 100 OHM, 5\%, 0.25W | 01121 | CB1015 |
| R157 | 321-0030-00 |  |  | RES. FXX, FILM:20 OHM, 18, 0.125W | 91637 | MFF1816G20R00F |
| R159 | 308-0436-00 |  |  | RES. ,FXD, WW : 2 K OHM, 0.1\%, 3 W | 91637 | RS2B-A20000B |
| R203 | 315-0105-00 |  |  | RES. ,FXD, CMPSN: 1 M OHM, 5\%, 0.25 W | 01121 | CB1055 |
| R208C | 323-0611-07 |  |  | RES. ,FXD,FILM:900K OHM, 0.1\%,0.5W | 91637 | MFF1226C90002B |
| R208D | 321-0389-01 |  |  | RES., FXD,FILM:110K OHM, 0.5\%,0.125W | 91637 | MFF1816Gl1002D |
| R209C | 323-0614-07 |  |  | RES. ,FXD,FILM:990K OHM, 0.18,0.5W | 91637 | MFF1226C99002B |
| R209D | 321-0289-00 |  |  | RES.,FXD,FILM:10K OHM, 1\%,0.125W | 91637 | MFFl816G10001F |
| R2 10C | 323-0623-07 |  |  | RES. FSX , FILM 999 K OHM, $0.1 \%, 0.5 \mathrm{~W}$ | 91637 | MFF1226C99902B |
| R2 100 | 321-0197-00 |  |  | RES.,FXD, FILM:1.1K OHM, 1\%,0.125W | 91637 | MFF1816G11000F |
| R210F | 321-0289-01 |  |  | RES.,FXD,FILM:10K OHM, 0.5\%,0.125W | 91637 | MFFl816G10001D |
| R211 | 323-0481-07 |  |  | RES. ,FXD, FILM:1M OHM, 0.1\%,0.50W | 75042 | CECT9-1004B |
| R215 | 311-0827-00 | B010100 | B069999 | RES., VAR, NONWIR:TRMR, 250 OHM, 0.5 W | 01121 | SV2511 |
| R215 | 311-1260-00 | B070000 |  | RES., VAR,NONWIR: 250 OHM, 10\%, 0.50W | 32997 | 3329P-L58-251 |
| R217 | 321-0222-00 |  |  | RES.,FXD,FILM: 2 K OHM, 1\%,0.125W | 91637 | MFF1816G20000F |
| R219 | 315-0510-00 |  |  | RES. ,FXD, CMPSN:51 OHM, 5\%, 0.25W | 01121 | CB5105 |
| R227 | 315-0562-00 |  |  | RES.,FXD, CMPSN:5.6K OHM, 5\%,0.25W | 01121 | CB5625 |
| R233 | 308-0495-00 |  |  | RES.,FXD, WW:4.5K OHM, 0.1\% | 91637 | RS2B110-45000B |
| R241 | 315-0512-00 |  |  | RES.,FXD, CMPSN:5.1K OHM, 5\%, 0.25W | 01121 | CB5125 |
| R245 | 321-0289-00 |  |  | RES.,FXD,FILM:10K OHM, 1\%,0.125W | 91637 | MFF1816G10001F |
| R251 | 308-0546-00 |  |  | RES. ,FXD,WW: $125 \mathrm{OHM}, 0.18,3 \mathrm{~W}$ | 91637 | RS2Bllo-125ROB |
| R253 | 321-0114-00 |  |  | RES. ,FXD,FILM:150 OHM, 1\%,0.125 | 91637 | MFFl816G150R0F |
| R255 | 315-0101-00 |  |  | RES. ,FXD, CMPSN: 100 OHM, 5\%, 0.25W | 01121 | CB1015 |
| R256 | 315-0185-00 |  |  | RES. ,FXD, CMPSN: 1.8 M OHM, 5\%, 0.25 W | 01121 | CB1855 |
| R257 | 321-0030-00 |  |  | RES.,FXD,FILM:20 OHM, 1\%, 0.125 W | 91637 | MFF1816G20R00F |
| R258 | 311-0467-00 |  |  | RES., VAR,NONWIR: 100 K OHM, 20\%,0.50W | 11237 | 300SF-41334 |
| R259 | 308-0436-00 |  |  | RES. ,FXD,WW:2K OHM, $0.18,3 \mathrm{~W}$ | 91637 | RS2B-A20000B |
| R261 | 321-0126-00 |  |  | RES. ,FXD,FILM:200 OHM, 1\%,0.125W | 91637 | MFF1816G200ROF |
| R263 | 321-0385-00 |  |  | RES. ,FXD, FILM: 100 K OHM, 1\%,0.125W | 91637 | MFFl816G10002F |
| R264 | 321-0414-00 |  |  | RES.,FXD,FILM:200K OHM, 1\%,0.125W | 91637 | MFF1816G20002F |
| R265 | 311-0887-00 |  |  | RES., VAR, NONWIR:50K OHM, 10\%, 0.50 W | 80009 | 311-0887-00 |
| R267 | 321-0385-00 |  |  | RES. ,FXD,FILM:100K OHM, 1\%,0.125W | 91637 | MFF1816G10002F |
| R269 | 321-0126-00 |  |  | RES.,FXD,FILM: $200 \mathrm{OHM}, 1 \%, 0.125 \mathrm{~W}$ | 91637 | MFF1816G200R0F |
| R270 | 311-0889-00 |  |  | RES. ,VAR,WW : PNL, 5K OHM, 1W | 02111 | 162-214 |
| R271 | 308-0436-00 |  |  | RES. ,FXD, WW : 2 K OHM, 0.1\%, 3 W | 91637 | RS2B-A20000B |
| R273 | 321-0114-00 |  |  | RES., FXD,FILM:150 OHM, 1\%,0.125W | 91637 | MFF1816G150ROF |
| R275 | 311-0532-00 |  |  | RES. ,VAR, WW :TRMR, 1.5K OHM, 1W | 80294 | 3345P-1-152 |
| R277 | 321-0114-00 |  |  | RES., FXD, FILM:150 OHM , 18, 0.125 W | 91637 | MFF1816G150R0F |
| R279 | 308-0436-00 |  |  | RES. , FXD, WW : 2 K OHM, $0.18,3 \mathrm{~W}$ | 91637 | RS2B-A20000B |
| R281 | 321-0126-00 |  |  | RES.,FXD,FILM:200 OHM, 18,0.125W | 91637 | MFF1816G200R0F |
| R283 | 323-0220-00 |  |  | RES.,FXD, FILM:1.91K OHM, $1 \%$, 0.50 W | 75042 | CECTO-1911F |



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| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ckt | Part No. |  | Dscont |  |  |  |
| R432 | 321-0164-00 |  |  | RES. ,FXD,FILM:499 OHM, 1\%,0.125W | 91637 | MFF1816G499ROF |
| R433 | 321-0335-00 |  |  | RES. ,FXD,FILM:30.1K OHM, 1\%,0.125W | 91637 | MFF1816G30101F |
| R434 | 321-0211-00 |  |  | RES. ,FXD,FILM:1.54K OHM, 1\%,0.125W | 91637 | MFF1816G15400F |
| R436 | 321-0197-00 |  |  | RES., FXD, FILM:I.1K OHM, 1\%,0.125w | 91637 | MFF1816G11000F |
| R437 | 321-0260-00 |  |  | RES. FSXD,FILM:4.99K OHM, 1\%,0.125 | 91637 | MFF1816G49900F |
| R440 | 321-0143-00 | B010100 | B029999 | RES. ,FXD,FILM:301 OHM, 1\%,0.125W | 91637 | MFF1816G301R0F |
| R440 | 321-0149-00 | B030000 |  | RES.,FXD, FILM: 348 OHM, 1\%, 0.125 W | 91637 | MFF1816G348R0F |
| R441 | 321-0222-00 | B010100 | B029999 | RES. ,FXD,FILM:2K OHM, 18,0.125W | 91637 | MFF1816G20000F |
| R441 | 321-0202-00 | B030000 |  | RES.,FXD, FILM: 1.24 K OHM, 1\%, 0.125W | 91637 | MFF1816Gl2400F |
| R443 | 317-0561-00 | B010100 | B029999 | RES., FXD, CMPSN: 560 OHM, 5\%,0.125W | 01121 | BB5615 |
| R443 | 317-0391-00 | B030000 | B089999 | RES. ,FXD, CMPSN: 390 OHM, 5\%, 0.125W | 01121 | BB3915 |
| R443 | 315-0391-00 |  |  | RES. ,FXD, CMPSN: 390 OHM, 5\%,0.25W | 01121 | CB3915 |
| R445 | 321-0251-00 | B010100 | B029999 | RES.,FXD, FILM:4.02K OHM, 1\%, 0.125 W | 91637 | MFF1816G40200F |
| R445 | 321-0231-00 | B030000 |  | RES.,FXD,FILM:2.49K OHM, 1\%,0.125 | 91637 | MFF1816G24900F |
| R450 | 321-0147-00 | B010100 | B029999 | RES. ,FXD, FILM 332 OHM, 1\%, 0.125 | 91637 | MFF1816G332ROF |
| R450 | 321-0149-00 | B030000 |  | RES., FXD, FILM $3488 \mathrm{OHM}, 1 \%, 0.125 \mathrm{~W}$ | 91637 | MFF1816G348ROF |
| R451 | 321-0222-00 | B010100 | B029999 | RES.,FXD, FILM : 2 K OHM, 1\%, 0.125 W | 91637 | MFF1816G20000F |
| R451 | 321-0202-00 | B030000 |  | RES.,FXD,FILM:1.24K OHM, 1\%,0.125W | 91637 | MFF1816Gl2400F |
| R453 | 321-0251-00 | B010100 | B029999 | RES. ,FXD,FILM:4.02K OHM, 1\%,0.125W | 91637 | MFFl816G40200F |
| R453 | 321-0231-00 | B030000 |  | RES.,FXD, FILM:2.49K OHM, 1\%,0.125W | 91637 | MFFl816G24900F |
| R457 | 317-0241-00 | B010100 | B089999 | RES. , FXD, CMPSN : 240 OHM , 5\%, 0.125W | 01121 | BB2415 |
| R457 | 315-0241-00 |  |  | RES. , FXD, CMPSN $: 240$ OHM, 5\%, 0.25 W | 01121 | CB2415 |
| R458 | 301-0470-00 |  |  | RES. , FXD, CMPSN : 47 OHM, 5\%,0.50W | 01121 | EB4705 |
| R459 | 315-0510-00 |  |  | RES., FXD, CMPSN:51 OHM , 5\% , 0.25W | 01121 | CB5105 |
| R501 | 315-0202-00 |  |  | RES.,FXD, CMPSN : 2 K OHM, 5\%,0.25W | 01121 | CB2025 |
| R503 | 321-0272-00 |  |  | RES. ,FXD,FILM:6.65K OHM, 1\%,0.125W | 91637 | MFF1816G66500F |
| R505 | 311-0839-00 | B010100 | B099999 | RES. ,VAR,WW:TRMR,50 OHM, 0.5 W | 80294 | 3305P-1-500 |
| R505 | 311-1258-00 | B100000 |  | RES., VAR,NONWIR:50 OHM, 10\%,0.50W | 32997 | 3326 P-T02-500 |
| R509 | 321-0343-00 |  |  | RES. ,FXD,FILM:36.5K OHM, 1\%,0.125W | 91637 | MFF1816G36501F |
| R513 | 321-0361-00 |  |  | RES.,FXD, FILM:56.2K OHM, 1\%,0.125W | 91637 | MFF1816G56201F |
| R521 | 321-0614-00 |  |  | RES.,FXD, FILM:10.1K OHM, 1\%,0.125W | 91637 | MFFI816G10101F |
| R523 | 315-0101-00 |  |  | RES.,FXD, CMPSN: 100 OHM, 5\%, 0.25W | 01121 | CB1015 |
| R527 | 321-0227-00 |  |  | RES.,FXD, FILM 2.26 K OHM, $18,0.125 \mathrm{~W}$ | 91637 | MFF1816G22600F |
| R531 | 321-0334-00 |  |  | RES.,FXD, FILM:29.4K OHM, 18,0.125W | 91637 | MFF1816G29401F |
| R532 | 321-0164-00 |  |  | RES.,FXD, FILM: 499 OHM, $18,0.125 \mathrm{~W}$ | 91637 | MFFl816G499ROF |
| R.533 | 321-0335-00 |  |  | RES.,FXD, FILM 30.1 K OHM, 1\%, 0.125 W | 91637 | MFF1816G30101F |
| R534 | 321-0211-00 |  |  | RES.,FXD, FILM:1.54K OHM, 1\%,0.125W | 91637 | MFFl816G15400F |
| R5351 | 311-0949-00 |  |  | RES., VAR,NONWIR:2K OHM,10\%,0.50W | 01121 | WAlG040S202UA |
| R540 | 311-0702-00 |  |  | RES.,VAR,NONWIR:250 OHM, 10\%,0.50W | 12697 | 382-CM39823 |
| R541 | 321-0222-00 | B010100 | B029999 | RES.,FXD, FILM : 2 K OHM, 18, 0.125 W | 91637 | MFF1816G20000F |
| R541 | 321-0202-00 | B030000 |  | RES.,FXD,FILM:1.24K OHM, 1\%,0.125W | 91637 | MFF1816G12400F |
| R543 | 317-0561-00 | B010100 | B029999 | RES. ,FXD, CMPSN:560 OHM, 5\%,0.125W | 01121 | BB5615 |
| R.543 | 317-0391-00 | B030000 | B089999 | RES. ,FXD, CMPSN : 390 OHM, 5\%,0.125W | 01121 | BB3915 |
| R543 | 315-0391-00 | B090000 |  | RES.,FXD, CMPSN: 390 OHM, 5\%,0.25W | 01121 | CB3915 |
| R545 | 321-0251-00 | B010100 | B029999 | RES.,FXD, FILM: 4.02K OHM, 1\%,0.125W | 91637 | MFFI816G40200F |
| R545 | 321-0231-00 | B030000 |  | RES.,FXD,FILM:2.49K OHM, 1\%,0.125W | 91637 | MFF1816G24900F |
| R551 | 321-0222-00 | B010100 | B029999 | RES. ,FXD,FILM : 2 K OHM, 1\%,0.125W | 91637 | MFF1816G20000F |
| R551 | 321-0202-00 | B030000 |  | RES.,FXD, FILM:1.24K OHM, 1\%,0.125W | 91637 | MFF1816G12400F |
| R553 | 321-0251-00 | B010100 | B029999 | RES.,FXD, FILM: 4.02 K OHM, $18,0.125 \mathrm{~W}$ | 91637 | MFF1816G40200F |
| R553 | 321-0231-00 | B030000 |  | RES.,FXD, FIIM $: 2.49 \mathrm{~K}$ OHM, 1\%, 0.125 W | 91637 | MFF1816G24900F |
| R557 | 317-0241-00 | B010100 | B089999 | RES. ,FXD, CMPSN: 240 OHM, 5\%,0.125W | 01121 | BB2415 |
| R557 | 315-0241-00 | B090000 |  | RES., FXD, CMPSN: 240 OHM, 5\%,0.25W | 01121 | CB2415 |
| R559 | 315-0510-00 |  |  | RES. ,FXD, CMPSN:51 OHM,5\%,0.25W | 01121 | CB5105 |

[^1]| Ckt No. | Tektronix Part No. | Serial/M <br> Eff | odel No. Dscont | Name \& Description | Mfr <br> Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R618C | 315-0154-00 |  |  | RES.,FXD, CMPSN:150K OHM, 5\%,0.25w | 01121 | CB1545 |
| R618D | 315-0753-00 |  |  | RES. ,FXD, CMPSN: 75 K OHM, 5\%,0.25W | 01121 | CB7535 |
| R618E | 315-0753-00 |  |  | RES. ,FXD, CMPSN: 75 K OHM, 5\%,0.25w | 01121 | CB7535 |
| R618F | 315-0154-00 |  |  | RES. ,FXD, CMPSN:150K OHM,5\%,0.25W | 01121 | CB1545 |
| R618G | 315-0753-00 |  |  | RES.,FXD, CMPSN:75K OHM,5\%,0.25W | 01121 | CB7535 |
| R618H | 325-0753-00 |  |  | RES. ,FXD, CMPSN:75K OHM, 5\%,0.25W | 01121 | CB7535 |
| R618J | 315-0123-00 |  |  | RES. ,FXD, CMPSN:12K OHM,5\%,0.25W | 01121 | CB1235 |
| R618K | 321-0344-00 |  |  | RES. ,FXD, FILM:37.4K OHM,1\%, 0.125W | 75042 | CEATO-3742F |
| R618L | 315-0753-00 |  |  | RES. ,FXD, CMPSN:75K OHM,5\%,0.25W | 01121 | CB7535 |
| R618M | 315-0154-00 |  |  | RES. ,FXD, CMPSN:150K OHM,5\%,0.25W | 01121 | CB1545 |
| R618N | 315-0513-00 |  |  | RES. ,FXD, CMPSN:51K OHM,5\%,0.25W | 01121 | CB5135 |
| R620 | 321-0223-00 |  |  | RES.,FXD, FILM:2.05K OHM,1\%, 0.125W | 75042 | CEATO-2051F |
| R622 | 315-0222-00 |  |  | RES. ,FXD, CMPSN:2.2K OHM, 5\%,0.25W | 01121 | CB2225 |
| R630 | 315-0104-00 |  |  | RES. ,FXD, CMPSN:100K OHM,5\%,0.25W | 01121 | CB1045 |
| R632 | 317-0223-00 | B030000 | B089999 | RES. ,FXD, CMPSN: 22 K OHM,5\%,0.125W | 01121 | BB2235 |
| R632 | 315-0223-00 | B090000 |  | RES. ,FXD, CMPSN: 22 K OHM, 5\%,0.25W | 01121 | CB2235 |
| R634 | 317-0203-00 | B010100 | B089999 | RES. ,FXD, CMPSN:20K OHM, 5\%,0.125w | 01121 | BB2035 |
| R634 | 315-0203-00 | B090000 |  | RES.,FXD, CMPSN: 20 K OHM, 5\%,0.25W | 01121 | CB2035 |
| RT221 | 307-0181-00 |  |  | RES. ,THERMAL:100K OHM, 10\%,4MW/DEG C | 50157 | JP-51J2 |
| RT223 | 307-0181-00 |  |  | RES. ,THERMAL:100K OHM, 10\%,4MW/DEG C | 50157 | JP-51J2 |
| S101A, ${ }^{1}$ | ------- | B010100 | B059999 | CKT BOARD ASSY: AC-GND-DC |  |  |
| S101A, ${ }^{\text {d }}$ | ---------- | B060000 |  | CKT BOARD ASSY: AC-GND-DC |  |  |
| S108 ${ }^{2}$ | 670-1014-00 | B010100 | B029999 | CKT BOARD ASSY:MAIN | 80009 | 670-1014-00 |
| \$108 ${ }^{2}$ | 670-1014-01 | B030000 | B059999 | CKI BOARD ASSY:MAIN | 80009 | 670-1014-01 |
| S108 ${ }^{2}$ | 670-1014-03 | B060000 | B069999 | CKT BOARD ASSY:MAIN | 80009 | 670-1014-03 |
| \$108 ${ }^{2}$ | 670-1014-04 | B070000 |  | CKT BOARD ASSY:MAIN | 80009 | 670-1014-04 |
| S201A, $\mathrm{B}^{3}$ | ----- ----- | B010100 | B059999 | CKT BOARD ASSY:+AC-GND-DC |  |  |
| \$201A, $\mathrm{B}^{3}$ | ---------- | B060000 |  | CKT BOARD ASSY:+AC-GND-DC |  |  |
| S353 ${ }^{2}$ | 670-1013-00 |  |  | CKT BOARD ASSY:BANDWIDTH | 80009 | 670-1013-00 |
| S407 ${ }^{2}$ | 670-1014-00 | B010100 | B029999 | CKT BOARD ASSY:MAIN | 80009 | 670-1014-00 |
| S407 ${ }^{2}$ | 670-1014-03 | B060000 | B069999 | CKT BOARD ASSY:MAIN | 80009 | 670-1014-03 |
| \$4072 | 670-1014-04 | 8070000 |  | CKI BOARD ASSY:MAIN | 80009 | 670-1014-04 |
| \$426 ${ }^{2}$ | 670-1013-00 |  |  | CKT BOARD ASSY:BANDWIDTH | 80009 | 670-1013-00 |
| S535 ${ }^{4}$ | 311-0949-00 |  |  | RES. ,VAR, NONWIR: 2 K OHM, 10\%, 0.50W | 01121 | WAlG040S202UA |
| $5622^{5}$ | 311-0888-00 | B010100 | B069999 | RES. ,VAR, NONWIR:PNL, 2X10K OHM, 0.5W | 12697 | 381-CM40098 |
| $5622^{5}$ | 311-0888-01 | B070000 |  | RES. ,VAR, NONWIR:PNL, 2X10K OHM, 0.5W | 12697 | D381S-CM40098 |
| VR270 | 152-0212-00 |  |  | SEMICOND DEVICE: ZENER, 0.5W, 9V, $5 \%$ | 04713 | SZ50646 |
| VR271 | 152-0405-00 |  |  | SEMICOND DEVICE: ZENER,1w,15v,5\% | 99942 | 1N5567B |
| VR305 | 152-0306-00 | B010100 | B029999 | SEMICOND DEVICE:ZENER, 0.4W,9.1V,5\% | 81483 | 1N960B |
| VR305 | 152-0168-00 | B030000 |  | SEMICOND DEVICE: ZENER, 0.4W, 12V,5\% | 04713 | 1N963B |
| VR320 | 152-02 80-00 |  |  | SEMICOND DEVICE: ZENER,0.4W,6 . $2 \mathrm{~V}, 5 \%$ | 04713 | 1N753A |
| VR325 | 152-0212-00 |  |  | SEMICOND DEVICE: ZENER, 0.5w, $9 \mathrm{~V}, 5 \%$ | 04713 | 5250646 |
| VR330 | 152-0280-00 |  |  | SEMICOND DEVICE: ZENER, 0.4W,6.2V,5\% | 04713 | 1N753A |

[^2]SECTION 7
DIAGRAMS

MECHANICAL PARTS ILLUSTRATIONS


## Waveforms show amplitude of signal at various points with -INPUT grounded and 25 mV peak to peak sine wave of approximately 1 kHz

 grounded and 25 mV peak to peak sine wave of apapplied to + INPUT. Front panel controls set as follows:
LF -3 dB Point
HF -3 dBPoint
VOLTS/DIV
DC
1 MHz
As sho
1 MHz
As shown at waveform
DC voltages measured with front panel controls set as follows:

VOLTS/DIV
POSITION
+INPUT AC-GND-DC
DC
1 mV
Trace

GND








# REPLACEABLE <br> MECHANICALPARTS 

## PARTS ORDERING INFORMATION

Replacement parts are available from or through your local Tektronix, Inc. Field Office or representative.

Changes to Tektronix instruments are sometimes made to accommodate improved components as they become available, and to give you the benefit of the latest circuit improvements developed in our engineering department. It is therefore important, when ordering parts, to include the following information in your order: Part number, instrument type or number, serial number, and modification number if applicable.

If a part you have ordered has been replaced with a new or improved part, your local Tektronix, Inc. Field Office or pepresentative will contact you concerning any change in part number.

## SPECIAL NOTES AND SYMBOLS

X000 Part first added at this serial number
00x Part removed after this serial number

FIGURE AND INDEX NUMBERS
Items in this section are referenced by figure and index numbers to the illustrations.

## INDENTATION SYSTEM

This mechanical parts list is indented to indicate item relationships. Following is an example of the indentation system used in the description column.

$$
12345
$$

Name \& Description
Assembly and/or Component
Attaching parts for Assembly and/or Component
-.. *-. .
Detail Part of Assembly and/or Component
Attaching parts for Detail Part
...*-..
Parts of Detail Part
Attaching parts for Parts of Detail Part
....*...

Attaching Parts always appear in the same indentation as the item it mounts, while the detail parts are indented to the right. Indented items are part of, and included with, the next higher indentation. The separation symbol-- * - - indicates the end of attaching parts.

Altaching parts musi be purchased separately, unless otherwise specified.

## ITEM NAME

In the Parts List, an Item Name is separated from the description by a colon (:). Because of space limitations, an Item Name may sometimes appear as incomplete. For further Item Name identification, the U.S. Federal Cataloging Handbook H6-1 can be utilized where possible.

| ABBREVIATIONS |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | INCH | ELCTRN | ELECTRON | IN | INCH | SE | SINGLE END |
| * | NUMBEA SIZE | ELEC | ELECTRICAL | INCAND | INCANDESCENT | SECT | SECTION |
| ACTR | ACTUATOR | ELCTLT | ELECTROLYTIC | INSUL | INSULATOR | SEMICOND | SEMICONDUCTOR |
| ADPTA | ADAPTEA | ELEM | ELEMENT | INTL | INTERNAL | SHLD | SHIELD |
| ALIGN | ALIGNMENT | EPL | ELECTRICAL PARTS LIST | LPHLDR | LAMPHOLDER | SHLDR | SHOULDERED |
| A | ALUMPNDM | EOPT | EQUIPMENT | MACH | MACHINE | SKT | SOCKET |
| ASSEN | ASSEMBLED | EXT | EXTERNAL | MECH | MECHANICAL | SL | SLIDE |
| ASSY | ASSEMELY | FIL | FILLISTEAHEAD | MTG | MOUNTING | SLFLKG | SELF-LOCKING |
| ATTEN | ATTENUATOR | FLEX | FLEXIBLE | NIP | NIPPLE | SLVG | SLEEVING |
| AWG | ANERICAN WUPE GAGE | FLH | FLAT HEAD | NON WIRE | NOT WIRE WOUND | SPR | SPRING |
| B0 | BOARD | FLTR | FILTER | OBD | ORDER BY DESCRIPTION | SQ | SQUARE |
| BRKT | BRACKET | FR | FRAME or FRONT | OD | OUTSIDE DIAMETER | SST | STAINLESS STEEL |
| EAS | BRASS | FSTNR | FASTENER | OVH | OVAL HEAD | STL | STEEL |
| BR2 | BRONZE | FI | FOOT | PHBRZ | PHOSPHOR BRONZE | SW | SWITCH |
| BSHG | BUSHING | FXD | FIXED | $P \mathrm{P}$ | PLAIN or PLATE | T | TUBE |
| CAB | CABUNET | GSKT | GASKET | PLSTC | PLASTIC | TERM | TERMINAL |
| CAP | CAPACITOA | HDL | HANDLE | PN | PART NUMBER | THD | THREAD |
| CEF | CERAMIC | HEX | HEXAGON | PNH | PAN HEAD | THK | THICK |
| CHAS | CHASSIS | HEXHD | HEXAGONAL HEAD | PWR | POWER | TNSN | TENSION |
| CKT | circuit | HEX SOC | HEXAGONAL SOCKET | RCPT | RECEPTACLE | TPG | TAPPING |
| COMP | COMPOSITBON | HLCPS | HELICAL COMPRESSION | RES | RESISTOA | TRH | TRUSS HEAD |
| CONN | CGNNECTOR | HLEXT | HELICAL EXTENSION | RGD | RIGID | $V$ | VOLTAGE |
| COV | COVEA | HV | HIGH VOLTAGE | RLF | RELIEF | VAR | VARIABLE |
| CPLG | COUPLING | IC | INTEGRATED CIRCUIT | RTNA | RETAINEA | W/ | WITH |
| CRT | CATHODE RAY TUBE | ID | INSIDE DIAMETER | SCH | SOCKET HEAD | WSHR | WASHER |
| DEG | DEGREE | IDENT | IDENTIFICATION | SCOPE | OSCILLOSCOPE | XFMR | TRANSFORMER |
| DWP | DRAWEA | IMPLR | IMPELLER | SCR | SCREW | XSTR | TRANSISTOR |

Manufacturer
Address
City, State, Zip

00779
13257
22526
24931
55210
70276
71785
73743
74445
76854
78189
79136
79807
80009
83385
86928
87308
STAUFFER SUPPLY
105 SE TAYLOR
P O BOX 3608
10 ESNA PARK DRIVE
youk expressway
3560 MADISON AVE.
po box 85, off ROUTE 45
P. O. DRAWER 570

1501 MORSE AVENUE
446 MORGAN ST.
31 BROOK ST. WEST
S. MAIN ST.

St. CHARLES ROAD
47-16 AUSTEL PLACE
2100 S. O BAY ST.
P O BOX 500
2530 CRESCENT DR.
701 SONORA AVENUE

89663 REESE, J. RAMSEY, INC.
93907 CAMCAR SCREW AND MFG. CO.
95987 WECKESSER CO., INC.
99934
RENBRANDT INC.
P. o. BOX 1360

71 MURRAY STREET
600 18TH AVE.
4444 WEST IRVING PARK RD.
6 PARMELEE STREET
PORTLAND, OR 97214
HARRISBURG, PA 17105 MARKHAM, ONTARIO, CANADA NEW CUMBERLAND, PA 17070 INDIANAPOLIS, IN 46227 SPRING MILLS, PA 16875 HARTFORD, CT 06101 ELK GROVE VILLAGE, IL 60007 CINCINNATI, OH 45206 HARTFORD, CT 06110 CRYSTAL LAKE, IL 60014

ELGIN, IL 60120
LONG ISLAND CITY, NY 11101
MILWAUKEE, WI 53207
BEAVERTON, OR 97077
BROADVIEW, IL 60153
GLENDALE, CA 91201
Statesville, nc 28677
NEW YORK, NY 10007
ROCKFORD, IL 61101
CHICAGO, IL 60641
BOSTON, MA 02118

Fig. \&


Fig. \&


Fig. \&
Index Tektronix Serial/Model No
No. Part No. Eff Dscon

| $1-81$ | $337-1146-00$ | B010100 B069999 | 1 SHIELD, ELEC:RIGHT SIDE |
| :--- | :--- | :--- | :--- |
|  | $337-1146-01$ | B070000 | 1 SHIELD,ELEC:RIGHT SIDE |
| -82 | $348-0115-00$ |  | 1 GROMMET, PLASTIC: U-SHP,0.548 X0. 462 INCH |
| -83 | $337-1045-00$ |  | 1 SHIELD, ELEC:INPUT |

-83 337-1045-00
Name \& Description Qty 123451 SHIELD, ELEC:RIGHT SIDESHIELD, ELEC:RIGHT SIDE1 SHIELD, ELEC:INPUT

Mfr
Code Mfr Part Number

80009 337-1146-00
80009 337-1146-01
80009 348-0115-00
80009 337-1045-00

Fig. \&
Index Tektronix Serial/Model No.

| Qty | 12345 Name \& Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: |
| 1 | EXTENSION SHAFT:0.08/0.125 DIA $\times 5.594 " \mathrm{~L}$ | 80009 | 384-0255-00 |
| 1 | EXTENSION SHAFT:9.5 INCH LONG | 80009 | 384-0306-00 |
| 1 | EXTENSION SHAFT:11.062 INCH LONG | 80009 | 384-0444-00 |
| 1 | GUIDE, SHAFT:FOR 0.125 OD SHAFT, PLASTIC | 80009 | 351-0159-00 |
| 1 | SCR,TPG,THD CTG:4-24 X 0.25 INCH,PNH STL | 83385 | OBD |
| 2 | CONTACT, ELEC: 0.577 "L, 18-20 AWG WIRE | 22526 | 46221 |
| 2 | CONTACT, ELEC: 0.577 "L, $28-32$ AWG WIRE | 22526 | 46241 |
| 2 | CONN BODY, PL, EL: 2 WIRE BLACK | 80009 | 352-0198-00 |
| 2 | CONTACT, ELEC: 0.315 INCH LONG,18 TO 20 Awg | 00779 | 61508-2 |
| 2 | CONTACT, ELEC : 0.315 INCH LONG, 28 TO 32 AWg | 00779 | 61615-1 |
| 2 | CONN BODY,PL,EL:2 WIRE BLACK | 80009 | 352-0169-00 |
| 1 | WIRING HARNESS, :MAIN | 80009 | 179-1407-00 |
| 4 | CONNECTOR, TERM. 0 : $48 \mathrm{LI} \mathrm{L}, 22-26 \mathrm{AWG}$ WIRE | 22526 | 75691-005 |
| 27 | CONTACT, ELEC:0.315 L, 22-26 AWG WIRE | 00779 | 61507-1 |
| 1 | FUSEHOLDER : TEFLON | 80009 | 352-0136-00 |
|  | (ATtaching Parts) |  |  |
| 2 | SCREW, MACHINE:4-40 x 0.25 INCH, PNH STL | 83385 | OBD |
| 2 | NUT, PLAIN, EXT W:4-40 x 0.25 INCH,STL | 78189 | 211-041800-00 |
| 1 | COVER,CKT CARD:PLASTIC <br> (AtTACHING PARTS) | 80009 | 200-0902-00 |
| 1 | SCREW,MACHINE:4-40 X 0.25 INCH, PNH STL | 83385 | OBD |
| 2 | COV, TRANSISTOR:0.438 DIA X 0.47 INCH H | 80009 | 200-0687-01 |
| 1 | RESISTOR,VAR: (SEE R540 EPL) $\underset{\text { (ATTACHING PARTS) }}{ }$ |  |  |
| 1 | BRKT, COMP MTG: | 80009 | 407-0554-00 |
| 1 | WASHER,LOCK:INTL, 0.26 ID X 0.40" OD,STL | 78189 | 1214-05-00-0541C |
| 1 | NUT, PLAIN, HEX. : $0.25-32 \times 0.312$ INCH, BRS | 73743 | 2x20224-402 |
| 1 | CPLG, SHAFT, RGD $=0.128$ ID $\times 0.312$ OD $\times 0.5$ "L | 80009 | 376-0029-00 |
| 2 | - . SETSCREW:4-40 x 0.094 INCH, HEX SOC STL | 000BK | OBD |
| 1 | CKT BOARD ASSY:BANDWIDTH <br> (ATtACHING PARTS) | 80009 | 670-1013-00 |
| 4 | SCREW, EXT, RLV B:4-40 $\times 0.375$ INCH, SST | 80009 | 211-0155-00 |
| 4 | SPRING,HLCPS $: 0.251$ OD X $0.375 " \mathrm{~L}$,SST WIRE | 80009 | 211-1140-00 |
| 5 | INSULATOR,STDF : CONNECTOR,DELRIN | 80009 | 351-0155-00 |
| 5 | TERMINAL, PIN: 0.365 L x $0.25 \mathrm{PH}, \mathrm{BRZ}, \mathrm{GOLD}$ PL | 22526 | 47357 |
| 18 | SOCKET, PIN TERM: FOR 0.025 INCH SQUARE PIN | 00779 | 85861-2 |
| 18 | SOCKET, PIN TERM: FOR 0.025 INCH SQUARE PIN | 00779 | 86250-2 |
| 18 | SOCKET, PIN TERM: FOR 0.025 INCH SQUARE PIN | 22526 | 48059 |
| 3 | SOCKET, PLUG-IN:3 PIN,ROUND | 80009 | 136-0183-00 |
| 3 | SOCKET, PLUG-IN:3 PIN,SQUARE | 71785 | 133-23-11-034 |
| 24 | CONTACT, ELEC:CKT BD SW, SPR, CU BE | 80009 | 131-0604-00 |
| 2 | CONTACT, ELEC: GROUNDING | 80009 | 131-0840-00 |
| 1 | DRUM ASSY, CAM S: LOW FREQUENCY <br> (ATTACHING PARTS) | 80009 | 105-0415-00 |
| 4 | SCR,ASSEM WSHR:4-40 X 0.312 INCH,PNH BRS | 83385 | OBD |
| 1 | COVER, CAM SW: (ATTACHING PARTS) | 80009 | 200-0996-00 |
| 2 | SCREW, MACHINE $: 2-56 \times 0.188$ INCH, PNH STL | 83385 | OBD |
| 2 | WASHER,LOCK:INTL, 0.092 ID X 0.18"OD, STL | 78189 | 1202-00-00-0541C |
| 1 | BRACKET, CAM SW: | 80009 | 407-0714-00 |
| 2 | SPRING,FLAT:RED COLORED | 80009 | 214-1126-02 |
| 1 | ROLIER, DETENT:0.125 DIA X 0.125 INCH L | 80009 | 214-1127-00 |
| 1 | BEARING, CAM SW: FRONT <br> (ATtAChing parts) | 80009 | 401-0058-00 |
| 1 | RING,RETAINING:FOR 0.25 INCH SHAFT | 79136 | 5103-25-MD-R |

[^3]Fig. \&
Index

| $2-45$ | $105-0112-00$ |
| :--- | :--- |
|  | $213-0075-00$ |
| -46 | $210-0405-00$ |
| -47 | $210-0406-00$ |
| -48 | $401-0061-00$ |
|  | $105-0466-00$ |
| -49 | $211-0116-00$ |
| -50 | $200-0995-00$ |
|  |  |
| -51 | $211-0022-00$ |
| -52 | $210-0001-00$ |
| -53 | $407-0714-00$ |
| -54 | $214-1126-01$ |


| Qty | 12345 Name \& Description | Code | Mfr Part Number |
| :---: | :---: | :---: | :---: |
| 1 | - DRUM,CAM SW: |  | 105-0112-00 |
| 2 | - . SETSCREW:4-40 x 0.094 INCH, HEX SOC STL | O00Bk | OBD |
| 1 | . . NUT, PLAIN, HEX. : $2-56 \times 0.188$ INCH, BRS | 73743 | 2x12157-402 |
| 2 | . . NUT, PLAIN, HEX. : 4-40 $\times 0.188$ INCH, BRS | 73743 | 2x12161-402 |
| 1 | . . BEARING,CAM SW:REAR | 80009 | 401-0061-00 |
| 1 | - DRUM ASSY,CAM S:LOW FREQENCY (ATTACHING PARTS) | 80009 | 105-0466-00 |
| 4 | . SCR,ASSEM WSHR:4-40 X 0.312 INCH,PNH BRS | 83385 | OBD |
| 1 | - Cover,cam SW: | 80009 | 200-0995-00 |
| 2 | . SCREW, MACHINE: ${ }^{\text {(ATTACHING PARTS) }} \mathbf{2 - 5 6} \times 0.188$ INCH,PNH STL | 83385 | OBD |
| 2 | . WASHER,LOCK:INTL,0.092 ID X 0.18"OD,STL | 78189 | 1202-00-00-0541C |
| 1 | - BRACKET,CAM SW: | 80009 | 407-0714-00 |
| 1 | - SPRING,FLAT:GREEN COLORED | 80009 | 214-1126-01 |
| 1 | - SPRING,FLAT: RED COLORED | 80009 | 214-1126-02 |
| 1 | . ROLLER,DETENT:0.125 DIA X 0.125 INCH L | 80009 | 214-1127-00 |
| 1 | - . BEARING, CAM SW:FRONT <br> (ATTAChing Parts) | 80009 | 401-0058-00 |
| 1 | . . RING, RETAINING:FOR 0.25 INCH SHAFT | 79136 | 5103-25-MD-R |
| 1 | - . DRUM, CAM SW: | 80009 | 105-0109-00 |
| 2 | . . . SETSCREW : 4-40 x 0.094 INCH, HEX SOC STL | 0008K | OBD |
| 1 | . . NUT, PLAIN, HEX. : $2-56$ X 0.188.INCH, BRS | 73743 | 2x12157-402 |
| 2 | . . NUT, PLAIN, HEX. : 4-40 x 0.188 INCH, BRS | 73743 | 2x12161-402 |
| 1 | -. BEARING, CAM SW : REAR | 80009 | 401-0061-00 |
| 1 | RESISTOR,VAR: (SEE R535,S535 EPL) (ATTACHING PARTS) |  |  |
| 1 | NUT, PLAIN, HEX. 0 : $0.25-32 \times 0.312$ INCH, BRS | 73743 | 2x20224-402 |
| 1 | WASHER, LOCK: INTL, 0.26 ID X 0.40" OD, STL | 78189 | 1214-05-00-0541C |
| 1 | BRKT, CMPNT MTG: | 80009 | 407-0553-00 |
| 1 | CKT BOARD ASSY:MAIN | 80009 | 670-1014-00 |
| 1 | CKT BOARD ASSY :MAIN | 80009 | 670-1014-01 |
| 1 | CKT BOARD ASSY :MAIN | 80009 | 670-1014-03 |
| 1 | CKT BOARD ASSY :MAIN | 80009 | 670-1014-04 |
| 1 | CKT BOARD ASSY :MAIN | 80009 | 670-1014-05 |
| 1 | CKT BOARD ASSY:MAIN (ATTACHING PARTS) | 80009 | 670-1014-06 |
| 1 | SCR,ASSEM WSHR:4-40 $\times 0.312$ INCH, PNH BRS | 83385 | OBD |
| 1 | SCREW, MACHINE:6-32 $\times 0.625$ INCH, PNH STL | 83385 | OBD |
| 1 | NUT, PLAIN, EXT W:4-40 x 0.25 INCH,STL | 78189 | 211-041800-00 |
| 1 | NUT, PLAIN, EXT W:6-32 X 0.312 INCH,STL | 83385 | OBD |
| 1 | WSHR,LOOP CLAMP:FOR 0.50" WIDE CLAMP,STL | 95987 | C191 |
| 1 | CLAMP, LOOP:0.188 INCH DIA | 95987 | 3-16-6B |
| 1 | CLAMP,IOOP:0.25 INCH DIA | 95987 | 1-4 6R |
| 1 | NUT, PLAIN, HEX. $00.375-32 \times 0.50$ INCH, STL | 73743 | 3145-402 |
| 1 | WASHER,FLAT:0.39 ID X 0.562 INCH OD,STL | 89663 | 644R |
| 1 | - SHAFT, EXTENSION:11.125 INCH LONG,PLASTIC | 80009 | 384-0448-00 |
| 1 | - CPLG, Shaft, FLEX: | 99934 | A-201-165 |
| 4 | - . SETSCREW:6-32 X 0.125 INCH,HEX.SOC STL | 70276 | OBD |
| 18 | - CONTACT,ELEC:0.71 INCH LONG | 22526 | 47351 |
| 15 | - INSULATOR, STDF : |  | 342-0050-00 |
| 22 | - INSULATOR, STDF : CONNECTOR, DELRIN | 80009 | 351-0155-00 |
| 4 | . SOCKET,PLUG-IN: 6 CONTACT,ROUND | 71785 | 133-96-12-062 |
| 4 | - CLIP, ELECTRICAL:FOR 0.25 INCH DIA FUSE | 80009 | 344-0154-00 |
| 4 | - SOCKET,PLUG-IN: 3 PIN,ROUND | 80009 | 136-0183-00 |
| 2 | - LINK, TERM. CONNE:0.086 DIA X 2.375 INCH L | 55210 | L-2007-1 |
| 1 | - SHIELD, ELEC: | 80009 | 337-1266-02 |
| 4 | - TERM. ,TEST PT:BRS CD PL | 80009 | 214-0579-00 |
| 1 | . SOCKET,PLUG-IN: 6 CONTACT,ROUND | 71785 | 133-96-92-067 |

$\mathrm{I}_{\text {Replace only with part bearing the same color as the original part in your instrument. }}$

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| PART NUMBER | FSCM | NATIONAL sTOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| :---: | :---: | :---: | :---: | :---: | :---: |
| BE2035 | 01121 | 5905-00-958-3830 | CEATO-1241.F | 75042 | 5905-00-1.53-4435 |
| BB2235 | 01.21 | 5905-00-403-8837 | CEATO-1272F | 75042 | 5905-00-105-9724 |
| BB2415 | 01121 | 5905-00-961-7730 | CEATO-1500F | 75042 | 5905-00-917-0576 |
| BB3915 | 01121 | 5905-00-407-0085 | CEATO-1,501F | 75042 | 5905-00-109-9848 |
| BB51.15 | 01121 | 5905-00-234-4374 | CEATO-1,541F | 75042 | 5905-01-026-5084 |
| CB1015 | 01.21 | 5905-00-102-5294 | CEATO-20ROF | 75042 | 5905-00-177-7172 |
| CB1035 | 01,121 | 5905-00-909-3885 | CEATO-2000F | 75042 | 5905-00-998-1796 |
| CB1045 | 03121 | 5905-00-959-1202 | CEATO-2001F | 75042 | 5905-00-922-9920 |
| CB1055 | 01121 | 5905-00-1116-8554 | CEATO-2051F | 75042 | 5905-00-724-5717 |
| CB1235 | 01121 | 5905-00-989-7943 | CEATO-2261F | 75042 | 5905-00-102-6001 |
| CB1545 | 01.21 | 5905-00-904-5696 | CEATO-2491F | 75042 | 5905-00-021-6494 |
| CB1855 | 01721 | 5905-00-800-8068 | CEATO-2493F | 75042 | 5905-00-051-1879 |
| CB2025 | 01121 | 5905-00-102-5289 | CEATO-3010F | 75042 | 5905-00-078-1,549 |
| CB2045 | 01121 | 5905-00-136-71,03 | CEATO-3012F | 75042 | 5905-01-017-8107 |
| CB2225 | 01121 | 5905-00-909-3940 | CEATO-3320F | 75042 | 5905-00-021-6496 |
| CB3635 | 01.21 | 5905-00-136-8430 | CEATO-3652F | 75042 | 5905-00-419-2676 |
| CB3645 | 01121. | 5905-00-141-0741 | CEATO-3742F | 75042 | 5905-00-441-7812 |
| CB3915 | 01121 | 5905-00-907-4118 | CEATO-4021F | 75042 | 5905-00-922-9923 |
| CB4335 | 01221 | 5905-00-122-0004 | CEATO-4530F | 75042 | 5905-00-433-7389 |
| C34735 | 01121 | 5905-00-960-0126 | CEATO-4990F | 75042 | 5905-00-922-9924 |
| CB5105 | 01121 | 5905-00-909-3834 | CEATO-4991F | 75042 | 5905-00-922-9925 |
| CB5125 | 01,121 | 5905-00-911-3754 | CEATO-5622F | 75042 | 5905-00-997-9579 |
| CB5135 | 01122 | 5905-00-136-3890 | CEATO-8060F | 75042 | 5905-00-233-5377 |
| CB5625 | 01122 | 5905-00-909-3862 | EB5625 | 01121 | 5905-00-121-91.10 |
| CB7535 | 01121 | 5905-00-916-7268 | SE365 | 03508 | 5961-00-222-6190 |
| CEATO-1002F | 75042 | 5905-00-904-4409 | SS22650 | 07263 | 5961-00-488-9927 |
| CEATO-1003F | 75042 | 5905-00-484-7475 | SV2511 | 01121 | 5905-00-414-1101 |
| CEATO-1012D | 75042 | 5905-00-105-9709 |  |  |  |
| CEATO-1012F | 75042 | 5905-00-893-1242 | SZ50646 | 04713 | 5961-00-237-2353 |
| CEATO-1201F | 75042 | 5905-00-994-8457 | WA1GO40S202UA | 01,121 | 5905-00-400-3541 |

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| PART NUMBER | FSCM | NATIONAL STOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1,N4152 | 07910 | 5961-00-899-8924 | 152-0185-00 | 80009 | 5961-00-936-7604 |
| 1N5567B | 99942 | 5961-00-254-1621 | 152-0212-00 | 80009 | 5961-00-237-2353 |
| 1N963B | 04713 | 5961-00-998-3666 | 152-0280-00 | 80009 | 5961-00-436-2890 |
| 1214-05-00-0541C | 78189 | 5310-00-193-6731 | 152-0323-00 | 80009 | 5961-00-222-6190 |
| 129-0053-00 | 80009 | 5940-00-835-2060 | 152-0405-00 | 80009 | 5961-00-254-1621 |
| 131-0566-00 | 80009 | 5940-00-242-0676 | 189-4-5 | 74970 | 5910-00-958-31.53 |
| 131-0589-00 | 80009 | 5999-00-275-0213 | 189-509-5 | 74970 | 5910-00-247-8600 |
| 131-0590-00 | 80009 | 5999-00-551-9434 | 189-6-5 | 74970 | 5910-00-834-4931 |
| 131-0604-00 | 80009 | 5999-00-1.73-9923 | 2N5308 | 03508 | 5961-00-1,46-8295 |
| 131-0608-00 | 80009 | 5999-00-551-9433 | 2N5859 | 04713 | 5961-00-448-6717 |
| 131-0622-00 | 80009 | 5999-01-022-6616 | 2X12161-402 | 73743 | 531.0-00-407-4600 |
| 131-0679-00 | 80009 | 5935-00-236-7554 | 2X20224-402 | 73743 | 5310-00-158-5262 |
| 131-0707-00 | 80009 | 5999-00-396-6331 | 200-0103-00 | 80009 | 5999-00-914-3308 |
| 131-0792-00 | 80009 | 5999-01-023-1578 | 210-0046-00 | 80009 | 5310-00-841-8117 |
| 133-23-11-034 | 71785 | 5935-00-067-73111 | 210-0259-00 | 80009 | 5940-00-474-9824 |
| 133-96-12-062 | 71785 | 5935-00-814-2209 | 21,0-0457-00 | 80009 | 5310-00-841-81,06 |
| 136-0183-00 | 80009 | 5935-00-938-4734 | 210-0583-00 | 80009 | 5310-00-006-8168 |
| 136-0220-00 | 80009 | 5935-00-067-7311 | 21.0-0586-00 | 80009 | 5310-00-836-3520 |
| 136-0235-00 | 80009 | 5935-00-81,4-2209 | 210-0940-00 | 80009 | 5310-00-158-5237 |
| 136-0263-03 | 80009 | 5999-00-394-0381 | 21,04-04-00-2520N | 78189 | 5940-00-847-3138 |
| 150-0046-00 | 80009 | 6240-00-933-5822 | 211-0101-00 | 80009 | 5305-00-492-2145 |
| 150-0048-01 | 80009 | 6240-00-060-2941 | 211-011,6-00 | 80009 | 5305-00-005-8245 |
| 150-0057-01 | 80009 | 6240-00-183-0669 | 213-0020-00 | 80009 | 5305-00-005-8247 |
| 150D396X9010B2 | 56289 | 5910-00-833-5175 | 21,3-01.53-00 | 80009 | 5305-00-283-1909 |
| 150D475X9035B2 | 56289 | 5910-00-177-4300 | 214-0579-00 | 80009 | 5940-00-935-8313 |
| 151-021,9-00 | 80009 | 5961-00-488-9927 | 214-1,127-00 | 80009 | 3110-00-442-8406 |
| 151-0228-00 | 80009 | 5961-00-401-6210 | 214-3136-00 | 80009 | 5930-01-020-6724 |
| 151-0260-00 | 80009 | 5961-00-493-1102 | 214-11139-02 | 80009 | 5360-00-480-3639 |
| 151-0261-00 | 80009 | 5961-00-689-1455 | 21,4-1.139-03 | 80009 | 5360-00-447-8721 |
| 151-1027-00 | 80009 | 5961-00-438-6453 | 21,4-11,90-00 | 80009 | 6625-01-066-3336 |

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| PART NUMBER | FSCM | NATIONAL STOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 28JR168-3 | 24931 | 5935-00-236-7554 | 310-0583-00 | 80009 | 5905-00-969-8991 |
| 281~0081-00 | 80009 | 5910-00-834-4931 | 311-0467-00 | 80009 | 5905-00-472-7323 |
| 281-0092-00 | 80009 | 5910-00-403-8872 | 311-0532-00 | 80009 | 5905-00-472-7773 |
| 281-0093-00 | 80009 | 5910-00-983-2623 | 311,-0605-00 | 80009 | 5905-00-481-8441 |
| 281-0114-00 | 80009 | 5910-00-065-9821. | 311-0609-00 | 80009 | 5905-00-431-2984 |
| 281-0122-00 | 80009 | 5910-00-013-9658 | 31,1-0635-00 | 80009 | 5905-00-497-4330 |
| 281-0528-00 |  | 5910-00-765-0380 | 3111-0704-00 | 80009 | 5905-00-498-13330 |
| 281-0534-00 | 80009 | 5910-00-978-2441 | 312,-0827-00 | 80009 | 5905-00-414-1,101 |
| 281-0544-00 | 80009 | 5910-00-725-1700 | 311-1258-00 | 80009 | 5905-00-434-541,4 |
| 281-0613-00 | 80009 | 591,0-00-018-1241 | 3112-1260-00 | 80009 | 5905-00-434-541,6 |
| 283-0000-00 | 80009 | 591,0-00-688-8702 | 311-1261-00 | 80009 | 5905-00-433-4372 |
| 283-0002-00 | 80009 | 5910-00-721-2030 | 31.5-0101-00 | 80009 | 5905-00-102-5294 |
| 283-0058-00 | 80009 | 5910-00-089-7509 | 31.5-01,03-00 | 80009 | 5905-00-434-5442 |
| 283-0059-00 | 80009 | 5910-00-932-71.3 | 315-01,04-00 | 80009 | 5905-00-434-5443 |
| 283-0080-00 | 80009 | 5910-00-931-7067 | 315-01,23-00 | 80009 | 5905-00-445-3826 |
| 283-0092-00 | 80009 | 5910-00-848-6590 | 315-0151-00 | 80009 | 5905-00-577-9598 |
| 283-0113-00 | 80009 | 5910-00-436-71,54 | 315-0202-00 | 80009 | 5905-00-445-3739 |
| 283-0594-00 | 80009 | 5910-00-066-0061 | 315-0204-00 | 80009 | 5905-00-445-3762 |
| 283-0604-00 | 80009 | 5910-00-064-9433 | 315-0222-00 | 80009 | 5905-00-436-9299 |
| 283-0617-00 | 80009 | 5910-00-491-2367 | 315-0473-00 | 80009 | 5905-00-437-01,64 |
| 285-0627-00 | 80009 | 5910-00-014-6565 | 315-0510-00 | 80009 | 5905-00-437-0272 |
| 285-0702-00 |  | 5910-00-243-2218 | 3115-0512-00 | 80009 | 5905-00-437-0283 |
| 285-0703-00 | 80009 | 5910-00-947-6978 | 315-0562-00 | 80009 | 5905-00-437-0423 |
| 3-1.6-6B | 95987 | 5340-00-437-4927 | 321-0098-01 | 80009 | 5905-00-441-7807 |
| 301-000C0J0339C | 72982 | 5910-00-978-2441 | 321,-01, 4 -00 | 80009 | 5905-00-405-7804 |
| 301-000U2M0820K | 72982 | 5910-00-765-0380 | 321-0126-00 | 80009 | 5905-00-998-1796 |
| 301-0470-00 | 80009 | 5905-00-464-1844 | 321-0127-01 | 80009 | 5905-00-879-7833 |
| 307-0181-00 | 80009 | 5905-00-551-9251 | 321-0147-00 | 80009 | 5905-00-405-7785 |
| 308-0495-00 | 80009 | 5905-00-401-6651 | 321-0164-00 | 80009 | 5905-00-922-9924 |

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| PART NUMBER | FSCM | NATIONAL STOCK NUMBER | PART NUMBER | FSCM | NATIONAL STOCK NUMBER |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 321-0184-00 | 80009 | 5905-00-405-7962 | 376-0029-00 | 80009 | 3010-00-498-7454 |
| 321-0197-00 | 80009 | 5905-00-434-5060 | 410 P 111 | 56289 | 5910-00-243-2218 |
| 321-0210-00 | 80009 | 5905-00-109-9848 | 46221 | 22526 | 5999-01-023-1578 |
| 321-0222-00 | 80009 | 5905-00-426-7707 | 46241 | 22526 | 5999-01-022-6616 |
| 321-0227-00 | 80009 | 5905-00-426-7720 | 47350 | 22526 | 5999-00-275-021.3 |
| 321-0231-00 | 80009 | 5905-00-021-6494 | 4735? | 22526 | 5999-00-551-9433 |
| 321-0260-00 | 80009 | 5905-00-922-9925 | 47439 | 22526 | 5999-00-396-6331 |
| 321-0289-00 | 80009 | .5905-00-434-5068 | 538-0111E2P094R | 72982 | 5910-00-993-2624 |
| 321-0299-00 | 80009 | 5905-00-105-9724 |  |  |  |
| 321-0335-00 | 80009 | 5905-00-426-7771 | 62-56-3 | 80740 | 5905-00-497-4330 |
| 321-0344-00 | 80009 | 5905-00-441-7812 | 683AS15 | 08806 | 6240-00-062-61.73 |
| 321-0385-00 | 80009 | 5905-00-426-7847 | 811-546E1032 | 72982 | 5910-00-721-2030 |
| 321-0614-00 | 80009 | 5905-00-893-1242 | 8131N147W5R273K | 72982 | 5910-00-089-7509 |
| 321-0763-07 | 80009 | 5905-00-441-7810 | 86250-2 | 00779 | 5999-00-394-0381 |
| 321-1068-01 | 80009 | 5905-00-441-7828 |  |  |  |
| 321-1166-01 | 80009 | 5905-00-441-7829 |  |  |  |
| 321-1231-01 | 80009 | 5905-00-441-7826 |  |  |  |
| 344-0154-00 | 80009 | 5999-00-465-9987 |  |  |  |
| 348-0115-00 | 80009 | 5325-00-232-9217 |  |  |  |
| 348-0235-00 | 80009 | 5999-00-434-2894 |  |  |  |
| 352-0067-00 | 80009 | 6250-00-089-7366 |  |  |  |
| 352-0068-00 | 80009 | 6625-00-980-9301 |  |  |  |
| 352-0136-00 | 80009 | 5920-00-401-6790 |  |  |  |
| 352-0169-00 | 80009 | 5935-00-597-5054 |  |  |  |
| 352-0198-00 | 80009 | 5935-00-597-5055 |  |  |  |
| 355-0507-00 | 80009 | 5307-00-529-8873 |  |  |  |
| 358-0216-00 | 80009 | 5355-00-016-8665 |  |  |  |
| 366-1057-00 | 80009 | 5355-00-765-3932 |  |  |  |
| 366-1077-00 | 80009 | 5355-00-419-4045 |  |  |  |

## CALIBRATION TEST EQUIPMENT REPLACEMENT

## Calibration Test Equipment Chart

This chart compares TM 500 product performance to that of older Tektronix equipment. Only those characteristics where significant specification differences occur, are listed. In some cases the new instrument may not be a total functional replacement. Additional support instrumentation may be needed or a change in calibration procedure may be necessary.

| Comparison of Main Characteristics |  |  |
| :---: | :---: | :---: |
| DM 501 replaces 7D13 |  |  |
| PG 501 replaces 107 | PG 501 - Risetime less than 3.5 ns into $50 \Omega$. <br> PG 501-5 V output pulse; 3.5 ns Risetime. <br> PG 501-Risetime less than $3.5 \mathrm{~ns} ; 8 \mathrm{~ns}$ Pretrigger pulse delay. <br> PG $501- \pm 5 \mathrm{~V}$ output. <br> PG 501 - Does not have Paired, Burst, Gated, or Delayed pulse mode; $\pm 5 \mathrm{~V}$ dc Offset. Has $\pm 5 \mathrm{~V}$ output. | 107 - Risetime less than 3.0 ns into $50 \Omega$. <br> 108-10 V output pulse; 1 ns Risetime. <br> 111 - Risetime $0.5 \mathrm{~ns} ; 30$ to 250 ns Pretrigger Pulse delay. <br> $114- \pm 10 \mathrm{~V}$ output. Short proof output. <br> 115 - Paired, Burst, Gated, and Delayed pulse mode; $\pm 10 \mathrm{~V}$ output. Short-proof output. |
| PG 502 replaces 107 | PG 502-5 V output <br> PG 502 - Risetime less than $1 \mathrm{~ns} ; 10 \mathrm{~ns}$ Pretrigger pulse delay. <br> PG 502- $\pm 5$ V output <br> PG 502 - Does not have Paired, Burst, Gated, Delayed \& Undelayed pulse mode; Has $\pm 5 \mathrm{~V}$ output. <br> PG 502 - Does not have Paired or Delayed puise. Has $\pm 5 \mathrm{~V}$ output. | 108-10 V output. <br> 111 - Risetime $0.5 \mathrm{~ns} ; 30$ to 250 ns Pretrigger pulse delay. <br> $114- \pm 10$ V output. Short proof output. <br> 115 - Paired, Burst, Gated, Delayed \& Undelayed pulse mode; $\pm 10 \mathrm{~V}$ output. Short-proof output. <br> 2101 - Paired and Delayed pulse; 10 V output. |
| PG 506 replaces 106 $067-0502-01$ | ```PG 506 - Positive-going trigger output signal at least 1 V ; High Amplitude out- put, 60 V . PG 506 - Does not have chopped feature.``` | 106 - Positive and Negative-going trigger output signal, 50 ns and 1 V ; High Amplitude output, 100 V . <br> 1502-01 - Comparator output can be alternately chopped to a reference voltage. |
| $\begin{array}{r} \hline \text { SG } 503 \text { replaces } 190, \\ 190 \mathrm{~A}, 190 \mathrm{~B} \\ 191 \\ 067-0532-01 \end{array}$ | SG 503 - Amplitude range 5 mV to 5.5 V p-p. <br> SG 503 - Frequency range 250 kHz to 250 MHz . <br> SG 503 - Frequency range 250 kHz to 250 MHz . | 190B - Amplitude range 40 mV to 10 V p-p. <br> 191 - Frequency range 350 kHz to 100 MHz . <br> 532-01 - Frequency range 65 MHz to 500 MHz . |
| TG 501 replaces 180 , 180A <br> 181 <br> 184 <br> 2901 | TG 501 - Marker outputs, 5 (sec 10 1 ns. Sinewave available at 5,2 , and 1 ns . Trigger output - slaved to marker output from 5 sec through 100 ns . One time-mark can be generated at a time. <br> TG 501 - Marker outputs[ 5 secto 1 ns. Sinewave available at 5,2 , and 1 ns . <br> TG 501 - Marker outputs, 5 sect to 1 ns. Sinewave available at 5,2 , and 1 ns . Trigger output - slaved to marker output from 5 sec through 100 ns . One time-mark can be generated at a time. <br> TG 501 - Marker outputs. 5 secto 1 ns . Sinewave available at 5,2 , and 1 ns . Trigger output - slaved to marker output from 5 sec through 100 ns . One time-mark can be generated at a time. | 180A - Marker outputs, 5 secto 1us. <br> Sinewave available at 20, 10, and 2 ns . Trigger pulses 1, 10, $100 \mathrm{~Hz} ; 1,10$, and 100 kHz . Multiple time-marks can be generated simultaneously. <br> 181 - Marker outputs, $1,10,100,1000$, and $10,000 \mu \mathrm{~s}$, plus 10 ns sinewave. <br> 184 - Marker outputs 5 sectio 2 ns. Sinewave available at $50,20,10,5$, and 2 ns . Separate trigger pulses of 1 and $.1 \mathrm{sec} ; 10,1$, and .1 ms ; 10 and $1 \mu \mathrm{~s}$. Marker amplifier provides positive or negative time marks of 25 V min. Marker intervals of 1 and .1 sec; 10, 1 , and .1 ms ; 10 and $1 \mu \mathrm{~s}$. <br> 2901 - Marker outputs, 5 sectio $0.1 \mu \mathrm{~s}$. Sinewave available to 50,10 , and 5 ns . Separate trigger pulses, from $5 \mathrm{sec} 100.1 \mu \mathrm{~s}$. Multiple time-marks can be generated simultaneously. |

NOTE: All TM $\mathbf{5 0 0}$ generator outputs are short-proof. All TM 500 plug-in instruments require TM 500-Series Power Module.

## APPENDI X A

## REFERENCES

| DA Pam 310-4 | I ndex of Techni cal Publ i cations: Techni cal Manual s, Techni cal Bul Ietins, Supply Manual s (Types 7, 8, and 9), Supply Bulletins, and Lubrication Orders. |
| :---: | :---: |
| DA Pam 316-7 | US Army Equi pnent Index of Mbdification Whrk Orders. |
| TM 43-0118 | Fi eld Instructions for Painting and Preserving El ectronics Command Equi pnent Incl udi ng Canoflauge Pattern Painting of El ectrical Equi pnent Shel ters. |
| TM 38-750 | The Army Mai itenance Managenent System (TAMM). |
| TM 750-244-2 | Procedures for Destruction of El ectronics Materiel to Prevent Enemy Use (El ectroni cs Command). |

APPENDI X D

## MAI NTENANCE ALLOCATI ON

## Section I. I NTRODUCTI ON

## D.1. General

Thi s appendix provi des a summary of the maintenance operations for AM6786/U. It authorizes categories of maintenance for specific mai ntenance functions on repai rable items and components and the tools and equi pment required to perform each function. This appendix may be used as an aid in pl anni ng mai ntenance operations.

D-2. Mai nt enance Function
Maintenance functions will be limited to and defined as follows:
To determine the servi ceability of an item by comparing its physical, mechanical, and/or electrical characteristics with established standards through examination.
b. Test. To verify serviceability and to detect incipient failure by measuring the mechanical or el ectrical characteristics of an item and com paring those characteristics with prescribed standards.
c. Service. Operations required periodically to keep an item in proper operating condition, i.e., to cl ean (decontaminate), to preserve, to drain, to paint, or to replenish fuel, lubricants, hydraulic fluids, or compressed ai $r$ supplies.
d. Adjust. To maintain, within prescribed limits, by bringing into proper or exact position, or by setting the operating characteristics to the specified parameters.

To adjust specified variable el ements of an item to bring about opt $\frac{\text { e. Al i gn. }}{1 \text { mim or desi red performance. }}$
f. Calibrate. To determine and cause corrections to be made or to be adjusted on instruments or test measuring and di agnostic equipment used in precision measurement. Consists of comparisons of two instruments, one of whi ch is a certified standard of known accuracy, to detect and adjust any di screpancy in the accuracy of the instrument being compared.

Instal|. The act of emplacing, seating, or fixing into position an item part, nodule (component or assenbly) in a manner to allow the proper functioning of the equi pment or system
h. Repl ace. The act of substituting a serviceable like type, part, subassentbly, or module (component or assentbly) for an unservi ceable "count er part.
i. Repair. The application of mai ntenance services (inspect, test, servi ce, adjust, al ign, calibrate, repl ace) or other mai ntenance actions (wel di ng, grinding, riveting, strai ghtening, facing, remachining, or resurfacing) to restore serviceability to an item by correcting specific damage, fault, malfunction, or failure in a part, subassembly, module (component or assenbly), end item or system
L. Overhaul. That maintenance effort (service/action) necessary to restore an itemto a completely serviceable/operational condition as prescribed by maintenance standards (i.e., DMNR) in appropriate technical publications. Overhaul is normally the hi ghest degree of mai ntenance performed by the Army. Overhaul does not normally return an item to like new condition.
k. Rebuild. Consists of those services/actions necessary for the restoration of unservi ceable equi pment to a like new condition in accordance with original manufacturing standards. Rebuild $s$ the highest degree of materiel mai ntenance applied to Army equi prent. The rebuild operation includes the act of returning to zero those age measurements (hours, miles, etc.) considered in classifying Army equi pments/components.

## D. 3. Col umm Entries

a. Col um 1. Group Number. Col um 1 lists group numbers, the purpose of whi ch is to identify components, assemblies, subassemblies, and modules with the next hi gher assembly.
b. Col um 2, Component / Assentbly. Col um 2 contai ns the noun names of components, assemblies, subassemblies, and modul es for which mai ntenance is aut horized.
C. Col um 3, Maintenance Functions. Col um 3 lists the functions to be performed on the itemlisted in colum 2. When itens are listed without maintenance functions, it is sol ely for purpose of having the group numbers in the MAC and RPSTL coi nci de.
d. Col umm 4, Maintenance Cat egory. Col um 4 specifies, by the listing of a "work time" figure in the appropriate subcol um(s), the lowest level of maintenance authorized to perform the function listed in col um 3. This figure represents the active time required to perform that maintenance function at the indicated category of maintenance. If the number or complexity of the tasks within the listed maintenance function vary at different maintenance categories, appropriate "work time" figures will be shown for each category. The number of task-hours specified by the "work time" figure represents the average time required to restore an item (assentloly, subassently, component, module, end item or system) to a serviceable condition under typical field operating conditions. This time includes preparation time, troubl eshooting time, and quality assurance/quality control time in addition to the time required to perform the specific tasks identified for the maintenance functions authorized in the mai ntenance allocation chart. Subcol ums of col umm 4 are as follows:

## C - Operator/Crew

O - Organi zational
F - Direct Support
H - General Support
D - Depot
e. Col um 5, Tools and Equi pment. Col umm 5 specifies by code, those tomon tool sets (not indivdual tools) and special tools, test, and support equi prent required to perform the designated function.
f. Col umm 6, Remarks. Col um 6 contai ns an al phabetic code whi ch I eads to the remark in section IV, Remarks, whi ch is pertinent to the item opposite the particular code.
D.4. Tool and Test Equi pment Requirements (Sect. III)
a. Tool or Test Equi pment Reference Code. The numbers in this col umm coi nci de with the numbers used in the tools and equi prent col um of the MAC. The numbers indicate the applicable tool or test equi pment for the maintenance functions.
b. Maintenance Category. The codes in this col um indicate the maintenance category allocated the tool or test equi pment.
c. Nomenclature. Thi s col um lists the noun name and nomenclature of the tools and test equi pment required to perform the mai ntenance functions,
d. National / NATO St ock Number. Thi s col um lists the Nati onal / NATO stock number of the specific tool or test equi pment.
e. Tool Number. This col um lists the manufacturer's part number of the tool followed by the Federal Supply Code for manufacturers.

D-5. Remarks (Sect. IV)
a. Reference Code. This code refers to the appropriate item in section II, col un 6 .
b. Remarks. This col um provi des the requi red expl anat ory inf or mation necessary to clarify itens appearing in section ll.

## SECTION II MAINTENANCE ALLOCATION CHART <br> FOR

DIFFERENTIAL AMPLIFIER AM-6786/


DIFFEREMTIAL AMPLIFIER AM-6786/U



[^0]:    ${ }^{1}$ The DC plus peak AC voltages on the test points with respect to the chassis potential of the Type 7A22 should be limited to the levels listed in Sertion l under Maximum Common-mode Input Voltage characteristics. Higher levels will degrade the common-mode rejection ratio and exceed the inpul voltage rating of the unit.

[^1]:    $1_{\text {Furnished }}$ as a unit with S 535

[^2]:    $1_{\text {Replaceable only }}$ under Circuit Board Assembly 670-1050-XX
    2 See Mechanical Parts List for replacement parts.
    ${ }^{3}$ Replaceable only under Circuit Board Assembly 670-1051-xX.
    ${ }_{4}$ Furnished as a unit with R535.
    ${ }^{5}$ Furnished as a unit with R430.

[^3]:    $1_{\text {Replace only }}$ with part bearing the same color as the original part in your instrument.

