# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## General Description

The MAX19692 12-bit, 2.3Gsps digital-to-analog converter (DAC) enables direct digital synthesis of high-frequency and wideband signals in baseband and higher Nyquist zones. It has been optimized for wideband communications and radar applications. It has excellent spurious and noise performance and can be used for synthesis of wideband signals in the frequency range from DC to more than 2 GHz . The 2.3Gsps update rate allows digital generation of signals with more than 1 GHz bandwidth. The selectable frequency response enables signal output with high SNR and excellent gain flatness in the first three Nyquist zones, reducing the number of upconversion stages needed in a radio transmitter. With its unique ability to generate broadband signals over a wide frequency range, the MAX19692 enables ultra-high data rate wireless modems and multistandard software radio transmitters.
The MAX19692 features an update rate up to 2.3Gsps, and has four 12-bit multiplexed low-voltage differential signaling (LVDS) input ports that each operate up to 575 MHz . The device accepts a clock at the DAC update rate that can be either a sine wave or a square wave. The input data rate is $1 / 4$ the DAC update rate. The MAX19692 provides an LVDS data clock output to simplify interfacing to FPGA or ASIC devices.
The MAX19692 has three frequency response output modes:

- Non-Return-to-Zero (NRZ) mode is the most common in the industry and provides highest dynamic range and output power in the 1st Nyquist zone.
- Return-to-Zero (RZ) mode trades off SNR for improved gain flatness in the 1st, 2nd, and 3rd Nyquist zones.
- Radio Frequency (RF) mode provides higher SNR and excellent dynamic performance in the 2nd and 3rd Nyquist zones.
The MAX19692 is a current-steering DAC with an integrated, self-calibrated $50 \Omega$ differential output termination to ensure optimum dynamic performance. The MAX19692 operates from 3.3V and 1.8 V power supplies and consumes 760 mW at 1.0 Gsps .


## Applications

| Radar Waveform and | Direct Digital Synthesis |
| :--- | :--- |
| LO Signal Synthesis | Automatic Test |
| Digital IF Generation in | Equipment |
| X-Band Transmitters | Direct Digital Generation |
| Arbitrary Waveform | of Wideband RF Signals |
| Generators | Up to 2 GHz |

Pin Configuration appears at end of data sheet.

- Industry-Leading Dynamic Performance

SFDR $=68 \mathrm{dBc}$ at fout $=1200 \mathrm{MHz}$
Noise Density $=-162 \mathrm{dBm} / \mathrm{Hz}$ at 200MHz

- 1GHz Signal Bandwidth
- Frequency Response Modes: NRZ, RZ, RF
- High SNR and Exceptional Gain Flatness in Nyquist Zones 1, 2, 3
- 4:1 Multiplexed LVDS Inputs (Up to 575MHz Each)
- Internal $50 \Omega$ Differential Output Termination
- Low Power: 760 mW (fclk $=1000 \mathrm{MHz}$ )
- Compact $11 \mathrm{~mm} \times 11 \mathrm{~mm}, 169$ CSBGA Package
- Evaluation Kit Available (Order MAX19692EVKIT)

Ordering Information

| PART | TEMP RANGE | PACKAGE | PKGCODE |
| :---: | :---: | :---: | :---: |
| MAX19692EXW-D $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 169 CSBGA | X16911-1 |  |

Functional Diagram


# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## ABSOLUTE MAXIMUM RATINGS

| EF | -0.3 V to +3.9V |
| :---: | :---: |
| $V_{\text {DD1.8, }}$ AVCLK to GND, DACREF | 0.3V to +2.1V |
| REFIO, FSADJ to GND, DACREF | -0.3V to (AVDD3.3 + 0.3V) |
| OUTP, OUTN to GND, DACREF | -0.3V to (AV ${ }^{\text {D } 3.3+1.0 \mathrm{~V})}$ |
| CREF to GND, DACREF. | -0.3V to (VDD1.8 + 0.3V) |
| DELAY, CLKDIV, RZ, RF, REFRES, |  |
| CAL to GND, DACREF | -0.3V to (AVDD3.3 + 0.3V) |
| CLKP, CLKN to GND, DACREF | -0.3V to (AVCLK + 0.3V) |
| DAP0-DAP11, DBP0-DBP11, |  |
| DCPO-DCP11 to GND, DACREF | ..--0.3V to (VDD1.8 + 0.3V) |
| DDP0-DDP11 to GND, DACREF. | -0.3V to (VDD1.8 + 0.3V) |
| N0-DAN11, DBN0-DBN11, |  |
| DCN0-DCN11 to GND, DACR | .-0.3V to (VDD1.8 + 0.3V) |

Note 1: Thermal resistance based on a 4.5 in $\times 5.5$ in multilayer board.

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS

(AVDD3.3 $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {DD1 }} .8=A V_{C L K}=1.8 \mathrm{~V}$, RREFRES $=500 \Omega$, RSET $=2 \mathrm{k} \Omega, \mathrm{V}_{\text {REFIO }}=$ external 1.25 V , CAL on, NRZ mode, transformercoupled differential output, IOUT $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 2)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| STATIC PERFORMANCE |  |  |  |  |  |  |
| Resolution |  |  |  | 12 |  | Bits |
| Integral Nonlinearity | INL | Measured differentially |  | $\pm 1.3$ |  | LSB |
| Differential Nonlinearity | DNL | Measured differentially |  | $\pm 0.9$ |  | LSB |
| Offset Voltage Error | OS | Measured differentially, no external load resistors | -0.5 | $\pm 0.1$ | +0.5 | \%FS |
| Offset Drift |  |  |  | $\pm 10$ |  | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Full-Scale Output Current | Iout | (Note 3) | 8 |  | 20 | mA |
| Output-Current Gain Error | GE |  | -4 |  | +4 | \%FS |
| Output-Voltage Gain Drift |  | Internal reference |  | -0.003 |  | $\mathrm{dB} /{ }^{\circ} \mathrm{C}$ |
|  |  | External reference |  | -0.0025 |  |  |
| Maximum Output Power | Pout | Differential, into $50 \Omega$ load |  | -2.6 |  | dBm |
| Output Resistance | Rout | Differential, CAL $\geq 0.7 \times$ AVDD3.3 (Note 4) | 44 | 48 | 52 | $\Omega$ |
| DYNAMIC PERFORMANCE (Note 5) |  |  |  |  |  |  |
| Minimum Output Update Rate | fCLK |  |  |  | 10 | MHz |
| Maximum Output Update Rate | fCLK | $1.8 \mathrm{~V} \leq \mathrm{V}_{\text {DD } 1.8} \leq 1.9 \mathrm{~V}$ | 2300 |  |  | MHz |
| Wideband NoiseSpectral Density |  | $\mathrm{fCLK}=1000 \mathrm{MHz}$, fout $=200 \mathrm{MHz},-12 \mathrm{dBFS}$ |  | -162 |  | $\mathrm{dBm} / \mathrm{Hz}$ |

# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## ELECTRICAL CHARACTERISTICS (continued)

$\left(A V_{D D 3.3}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD1} 1.8}=A \mathrm{~V}_{\text {CLK }}=1.8 \mathrm{~V}\right.$, RREFRES $=500 \Omega$, RSET $=2 \mathrm{k} \Omega$, $\mathrm{V}_{\text {REFIO }}=$ external $1.25 \mathrm{~V}, \mathrm{CAL}$ on, NRZ mode, transformercoupled differential output, lout $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 2)

| PARAMETER | SYMBOL |  | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Spurious-Free Dynamic Range within Nyquist Zone of fout | SFDR | $\mathrm{f}_{\mathrm{CLK}}=500 \mathrm{MHz}$ | fout $=50 \mathrm{MHz}$, -6dBFS, NRZ mode |  | 73 |  | dBc |
|  |  |  | fout $=100 \mathrm{MHz},-6 \mathrm{dBFS}$, NRZ mode |  | 74 |  |  |
|  |  |  | fout $=200 \mathrm{MHz},-6 \mathrm{dBFS}$, NRZ mode |  | 70 |  |  |
|  |  |  | fout $=400 \mathrm{MHz},-6 \mathrm{dBFS}$, RF mode |  | 71 |  |  |
|  |  |  | fout $=600 \mathrm{MHz}$, -6dBFS, RF mode |  | 73 |  |  |
|  |  | fCLK $=1000 \mathrm{MHz}$ | fout $=200 \mathrm{MHz},-6 \mathrm{dBFS}$, NRZ mode |  | 75 |  |  |
|  |  |  | $\begin{aligned} & \text { fout }=409 \mathrm{MHz},-0.1 \mathrm{dBFS}, \\ & \text { NRZ mode, } \mathrm{T}_{\mathrm{A}} \geq+25^{\circ} \mathrm{C} \end{aligned}$ | 60 | 68 |  |  |
|  |  |  | $\text { fout }=409 \mathrm{MHz},-0.1 \mathrm{dBFS} \text {, }$ NRZ mode | 56 | 68 |  |  |
|  |  |  | fout $=800 \mathrm{MHz}$, -6dBFS, RF mode |  | 67 |  |  |
|  |  |  | fout $=1200 \mathrm{MHz},-6 \mathrm{dBFS}$, RF mode |  | 65 |  |  |
|  |  | $\text { fCLK }=2000 \mathrm{MHz},$ <br> NRZ mode | fout $=100 \mathrm{MHz},-6 \mathrm{dBFS}$ |  | 71 |  |  |
|  |  |  | fout $=200 \mathrm{MHz},-6 \mathrm{dBFS}$ |  | 68 |  |  |
|  |  |  | fout $=400 \mathrm{MHz},-6 \mathrm{dBFS}$ |  | 70 |  |  |
|  |  |  | fout $=800 \mathrm{MHz},-6 \mathrm{dBFS}$ |  | 58 |  |  |
|  |  | $\begin{aligned} & \text { fCLK }=2300 \mathrm{MHz} \text {, } \\ & \text { NRZ mode } \end{aligned}$ | fout $=92 \mathrm{MHz}$, OdBFS | 60 | 71 |  |  |
| 2-Tone IMD | TTIMD | $\begin{aligned} & \text { fCLK }=1000 \mathrm{MHz} \text {, } \\ & \text { NRZ mode } \end{aligned}$ | fout $1=200 \mathrm{MHz},-7 \mathrm{dBFS}$ | -72 |  |  | dBc |
|  |  |  | fout2 $=201 \mathrm{MHz},-7 \mathrm{dBFS}$ |  |  |  |  |
|  |  | $\text { fCLK }=1000 \mathrm{MHz},$ <br> RF mode | fout1 $=1300 \mathrm{MHz},-7 \mathrm{dBFS}$ | -66 |  |  |  |
|  |  |  | fout2 $=1301 \mathrm{MHz},-7 \mathrm{dBFS}$ |  |  |  |  |
| Minimum Output Bandwidth | BW-3dB | (Note 6) |  | 1500 |  |  | MHz |
| REFERENCE |  |  |  |  |  |  |  |
| Internal Reference Voltage Range | Vrefio |  |  | 1.1 | 1.2 | 1.3 | V |
| Reference Input Compliance Range | VREFIOCR |  |  | 0.50 |  | 1.25 | V |
| Reference Input Resistance | Rrefio |  |  |  | 10 |  | k $\Omega$ |
| Reference Voltage Drift | TCOREF |  |  |  | 50 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| ANALOG OUTPUT TIMING (Note 7) |  |  |  |  |  |  |  |
| Output Fall Time | tFALL | 90\% to 10\% |  |  | 270 |  | ps |
| Output Rise Time | trise | 10\% to 90\% |  |  | 270 |  | ps |
| Settling Time | $t_{s}$ | Settling to 0.1\% |  |  | 3.5 |  | ns |
|  |  | Settling to 0.025\% |  |  | 4.5 |  |  |
| Output Propagation Delay | tpD | (Note 8) |  |  | 0.9 |  | ns |

## 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response

## ELECTRICAL CHARACTERISTICS (continued)

$\left(\operatorname{AV}\right.$ DD3.3 $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {DD1 }} .8=A V_{C L K}=1.8 \mathrm{~V}$, RREFRES $=500 \Omega$, RSET $=2 \mathrm{k} \Omega$, $\mathrm{V}_{\text {REFIO }}=$ external $1.25 \mathrm{~V}, \mathrm{CAL}$ on, NRZ mode, transformercoupled differential output, lout $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 2)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TIMING CHARACTERISTICS |  |  |  |  |  |  |
| Data to Clock Setup Time | tsetup | Referenced to rising edge of data clock (Note 9) | 1.6 |  |  | ns |
| Data to Clock Hold Time | thold | Referenced to rising edge of data clock (Note 9) | -0.8 |  |  | ns |
| Data Latency |  | (Note 10) |  | 14 |  | Clock cycles |

LVDS LOGIC INPUTS (DAP11-DAP0, DAN11-DAN0, DBP11-DBP0, DBN11-DBN0, DCP11-DCP0, DCN11-DCN0, DDP11-DDP0, DDN11-DDN0)

| Differential Input <br> Logic-High | $\mathrm{V}_{\mathrm{IH}}$ |  | 100 |  |  | mV |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Differential Input Logic-Low | VIL |  |  |  | -100 | mV |
| Common-Mode Voltage Range | VCOM |  | 1.125 |  | 1.375 | V |
| Differential Input <br> Resistance | RIN |  | 85 |  | 125 | $\Omega$ |
| Input Capacitance | CIN |  |  | 1.5 |  | pF |
| CMOS LOGIC INPUTS (RZ, RF, CLKDIV, DELAY) |  |  |  |  |  |  |
| Input Logic-High | $\mathrm{V}_{\mathrm{IH}}$ |  | AVDD3. 3 |  |  | V |
| Input Logic-Low | VIL |  | $\begin{gathered} 0.3 \times \\ \text { AVDD3.3 } \end{gathered}$ |  |  | V |
| Input Leakage Current | IIN |  | -15 |  | +15 | $\mu \mathrm{A}$ |
| Input Capacitance | CIN |  |  | 3 |  | pF |
| CLOCK INPUTS (CLKP, CLKN) |  |  |  |  |  |  |
| Minimum Differential Input Voltage Swing (Note 11) | VCLK | $\mathrm{fCLK} \leq 1.5 \mathrm{GHz}$ | 0.6 |  |  | $V_{\text {P-P }}$ |
|  |  | $\mathrm{fCLK}=2.3 \mathrm{GHz}$, see Figure 6 for dependence on fCLK | 2.0 |  |  |  |
| Maximum Differential Voltage Swing | VCLK | (Note 11) | 2.5 |  |  | VP-P |
| Differential Input Slew Rate | SRCLK |  | 6000 |  |  | V/us |
| Common-Mode Voltage Range | VCOMCLK |  | 0.55 | AVCLK/3 | 0.65 | V |
| Input Resistance | RCLK | Differential | 100 |  |  | $\Omega$ |
| Input Capacitance | CCLK |  | 2 |  |  | pF |

# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## ELECTRICAL CHARACTERISTICS (continued)

(AVDD3.3 $=3.3 \mathrm{~V}, \mathrm{~V}_{\text {DD1 }} 8=A V_{\text {CLK }}=1.8 \mathrm{~V}$, RREFRES $=500 \Omega$, RSET $=2 \mathrm{k} \Omega$, $\mathrm{V}_{\text {REFIO }}=$ external 1.25 V , CAL on, NRZ mode, transformercoupled differential output, IOUT $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 2)

| PARAMETER | SYMBOL | CONDITIONS | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DATA CLOCK OUTPUTS (DATACLKP, DATACLKN) |  |  |  |  |  |  |
| Differential Output | VDCLK | With $100 \Omega$ differential termination | $\pm 0.25$ | $\pm 0.35$ | $\pm 0.45$ | V |
| Output Rise and Fall Time | $t_{R}, t_{F}$ | With $100 \Omega$ differential termination |  | 0.5 |  | ns |
| Common-Mode Voltage Range | VCOM |  | 1.125 | 1.25 | 1.375 | V |
| Output Resistance | RCLK | Differential |  | 100 |  | $\Omega$ |
| POWER SUPPLIES |  |  |  |  |  |  |
| Analog-Supply Voltage Range | AV ${ }_{\text {DD3 } 3}$ |  | 3.1 | 3.3 | 3.5 | V |
| 1.8V Supply Voltage Range | VDD1.8 | $10 \mathrm{MHz} \leq$ fCLK $<2.0 \mathrm{GHz}$ (Note 9) | 1.7 | 1.8 | 1.9 | V |
|  |  | $2.0 \mathrm{GHz} \leq$ fCLK $\leq 2.3 \mathrm{GHz}$ | 1.8 |  | 1.9 |  |
| Clock-Supply Voltage Range | AV ${ }_{\text {cli }}$ | $10 \mathrm{MHz} \leq$ f $\mathrm{CLK}<2.0 \mathrm{GHz}$ (Note 9) | 1.7 | 1.8 | 1.9 | V |
|  |  | $2.0 \mathrm{GHz} \leq$ fCLK $\leq 2.3 \mathrm{GHz}$ | 1.8 |  | 1.9 |  |
| Analog Supply Current | IAVDD3.3 | $\mathrm{f}_{\text {CLK }}=1000 \mathrm{MHz}$, fout $=10 \mathrm{MHz}$, AOUT $=0 \mathrm{dBFS}$ |  | 107 | 117 | mA |
| Digital Supply Current | IVDD1. 8 | fCLK $=1000 \mathrm{MHz}$, fout $=10 \mathrm{MHz}$, AOUT $=0 \mathrm{dBFS}$ |  | 61 | 76 | mA |
| Clock Supply Current | IAvCLK | $\mathrm{f}_{\text {CLK }}=1000 \mathrm{MHz}$, fout $=10 \mathrm{MHz}$, AOUT $=0 \mathrm{dBFS}$ |  | 164 | 191 | mA |
| Total Power Dissipation | Pdiss | $\mathrm{f}_{\text {CLK }}=1000 \mathrm{MHz}$, fout $=10 \mathrm{MHz}$, AOUT $=0 \mathrm{dBFS}$ |  | 760 | 870 | mW |

Note 2: All specifications are $100 \%$ tested at $\mathrm{T}_{\mathrm{A}} \geq+25^{\circ} \mathrm{C}$. Specifications at $\mathrm{T}_{\mathrm{A}}<+25^{\circ} \mathrm{C}$ are guaranteed by design and characterization.
Note 3: Nominal full-scale current lout $=32 \times$ IREF.
Note 4: ROUT can be set to $50 \Omega$ as described in the Output Resistor Calibration section.
Note 5: $\quad$ CLK input $=+10 \mathrm{dBm}, \mathrm{AC}$-coupled sine wave.
Note 6: Excludes impulse-response dependent rolloff inherent in the DAC. Measured single-ended into $50 \Omega$ termination resistor.
Note 7: Measured differentially into a $50 \Omega$ termination resistor.
Note 8: Excludes data latency.
Note 9: Guaranteed by design and characterization.
Note 10: DA_P/DA_N to DAC output.
Note 11: Differential voltage swing defined as $\left|\mathrm{V}_{\mathrm{P}}\right|+\left|\mathrm{V}_{\mathrm{N}}\right|$.


## 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response

$\left(A V_{D D 3.3}=3.3 \mathrm{~V}, A V_{D D 1.8}=\operatorname{DVDD}=A V_{C L K}=1.8 \mathrm{~V}, \operatorname{RREFRES}=500 \Omega, \operatorname{RSET}=2 \mathrm{k} \Omega, \mathrm{V}_{\text {REFIO }}=\right.$ external $1.25 \mathrm{~V}, \mathrm{CAL}$ on, transformercoupled differential output, lout $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)



SFDR vs. OUTPUT FREQUENCY fCLK $=1500 \mathrm{MHz}$, RZ MODE




SFDR vs. OUTPUT FREQUENCY fCLK $=\mathbf{2 3 0 0 M H z}$, RZ MODE


SFDR vs. OUTPUT FREQUENCY
fCLK $=1500 \mathrm{MHz}$, NRZ MODE


SFDR vs. OUTPUT FREQUENCY
fCLK $=1000 \mathrm{MHz}$, RZ MODE


SFDR vs. OUTPUT FREQUENCY fcLK $=500 \mathrm{MHz}$, RZ MODE


# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## Typical Operating Characteristics (continued)

$\left(A V_{D D 3.3}=3.3 \mathrm{~V}, A V_{D D 1.8}=\mathrm{DV}_{\mathrm{DD}}=A \mathrm{~V}_{\mathrm{CLK}}=1.8 \mathrm{~V}\right.$, RREFRES $=500 \Omega$, RSET $=2 \mathrm{k} \Omega$, $\mathrm{V}_{\text {REFIO }}=$ external 1.25 V , CAL on, transformer-





SFDR vs. OUTPUT FREQUENCY


SFDR vs. OUTPUT FREQUENCY
fCLK $=1000 \mathrm{MHz}$, RZ MODE


SFDR vs. OUTPUT FREQUENCY
fcLK $=500 \mathrm{MHz}$, RF MODE


SFDR vs. OUTPUT FREQUENCY fcLk $=\mathbf{2 0 0 0 M H z}$, RF MODE


SFDR vs. OUTPUT FREQUENCY
fCLK $=\mathbf{5 0 0 M H z}$, RF MODE


## 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response

$\qquad$
$\left(A V_{D D 3.3}=3.3 \mathrm{~V}, A V_{D D 1.8}=\mathrm{DV}_{\mathrm{DD}}=A \mathrm{~V}_{\mathrm{CLK}}=1.8 \mathrm{~V}\right.$, RREFRES $=500 \Omega$, RSET $=2 \mathrm{k} \Omega$, $\mathrm{V}_{\text {REFIO }}=$ external 1.25 V , CAL on, transformercoupled differential output, IOUT $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)



TWO-TONE IMD vs. OUTPUT FREQUENCY fcLK = 1000MHz, 1 MHz SPACING, RF MODE



TWO-TONE IMD vs. OUTPUT FREQUENCY fcLK $=500 \mathrm{MHz}, \mathbf{1 M H z}$ SPACING, NRZ MODE


TWO-TONE IMD vs. OUTPUT FREQUENCY fcLK $=1000 \mathrm{MHz}, 1 \mathrm{MHz}$ SPACING, RF MODE


SFDR vs. OUTPUT AMPLITUDE fCLK $=1000 \mathrm{MHz}$, fout $=\mathbf{8 0 0 M H z}$


TWO-TONE IMD vs. OUTPUT FREQUENCY fCLK $=1000 \mathrm{MHz}, 1 \mathrm{MHz}$ SPACING, NRZ MODE


CLK FEEDTHROUGH vs. CLK FREQUENCY fout $=200 \mathrm{MHz}$, AOUT $=-1 \mathrm{dBFS}$, NRZ MODE


# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## Typical Operating Characteristics (continued)

$\left(A V_{D D 3.3}=3.3 \mathrm{~V}, A V_{D D 1.8}=D V_{D D}=A V_{C L K}=1.8 \mathrm{~V}\right.$, RREFRES $=500 \Omega, \operatorname{RSET}=2 \mathrm{k} \Omega, \mathrm{V}_{\text {REFIO }}=$ external $1.25 \mathrm{~V}, \mathrm{CAL}$ on, transformercoupled differential output, lout $=20 \mathrm{~mA}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted.)


SFDR SPECTRAL PLOT, 3rd NYQUIST ZONE fCLK $=1000 \mathrm{MHz}$, fout $=1290 \mathrm{MHz}$, AOUT $=-3 \mathrm{dBFS}$, RF MODE


SFDR SPECTRAL PLOT
fCLK $=1600 \mathrm{MHz}$, fout $=700 \mathrm{MHz}$, AOUT = -3dBFS, NRZ MODE


SFDR vs. TEMPERATURE


TWO-TONE IMD SPECTRAL PLOT $\mathrm{fCLK}=1600 \mathrm{MHz}$, fout $=695 \mathrm{MHz}$, fout2 $=\mathbf{7 0 5 M H z}$


SFDR vs. TEMPERATURE (AVDD3.3, 1.8V SUPPLIES) fCLK $=\mathbf{2 0 0 0} \mathbf{M H z}$, fout $=\mathbf{4 0 0 M H z}$, NRZ MODE


SFDR vs. TEMPERATURE (AVDD3.3, 1.8V SUPPLIES)


SFDR vs. TEMPERATURE (AVDD3.3, 1.8V SUPPLIES)


## 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response

INTERNAL REFERENCE (REFIO)
VOLTAGE vs. TEMPERATURE


DIFFERENTIAL NONLINEARITY


INTEGRAL NONLINEARITY
vs. DIGITAL CODE


SUPPLY CURRENT vs. CLK FREQUENCY fout $=100 \mathrm{MHz}$, A OUT $^{\text {= OdBFS, NRZ MODE }}$


# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

Pin Description

| PIN | NAME | FUNCTION |
| :---: | :---: | :---: |
| A1 | REFIO | Reference Input/Output. Output pin for the internal 1.2V-bandgap reference. REFIO has a $10 \mathrm{k} \Omega$ series resistance and can be driven using an external reference. Connect a $1 \mu$ F capacitor between REFIO and DACREF. |
| A2 | FSADJ | Full-Scale Adjust Input. Sets the full-scale output current of the DAC. For a 20 mA fullscale output current, connect a $2 \mathrm{k} \Omega$ resistor between FSADJ and DACREF. |
| A3 | DACREF | Current-Set Resistor Return Path. For a 20 mA full-scale output current, connect a $2 k \Omega$ resistor between FSADJ and DACREF. DACREF is internally connected to AGND. DO NOT CONNECT TO EXTERNAL GROUND. |
| A4, A5, A7, A9 | AVDD3.3 | Analog 3.3V Supply Voltage. Accepts a 3.1 V to 3.5 V supply voltage range. Connect 47 nF bypass capacitors between each $A V_{D D 3} 3$ pin and AGND. |
| A6 | OUTP | Positive Terminal of Differential DAC Output. OUTP has a calibrated internal $25 \Omega$ resistor to AVDD3.3. |
| A8 | OUTN | Negative Terminal of Differential DAC Output. OUTN has a calibrated internal $25 \Omega$ resistor to AVDD3.3. |
| A10, B10, C2, C3, C10, E1-E4, E10-E13, F13 | VDD1.8 | Analog 1.8 V Supply Voltage. Accepts a 1.7 V to 1.9 V supply voltage range. Connect 47 nF bypass capacitors between each VDD1.8 pin and GND. |
| A11, A13, B5-B9, B11, C4-C9, C11, D1-D11, D13, E5-E9, G13, M13 | GND | Ground. Connect to ground plane with minimum inductance. |
| A12, B12, C12, D12 | AVCLK | Clock 1.8 V Supply Voltage. Accepts a 1.7 V to 1.9 V supply voltage range. Connect 47 nF bypass capacitors between AV CLK and GND. |
| B1 | CREF | Noise Bypass Pin. A $1 \mu$ F capacitor between the CREF and DACREF band limits the phase noise of the MAX19692. |
| B2 | REFRES | Calibration Reference Resistor Input. Connect a $500 \Omega$ resistor between REFRES and AV ${ }_{\text {DD3.3. }}$ The internal analog output resistors are calibrated to this external resistor. |
| B3 | RZ | Return-to-Zero (RZ) Mode-Select Input. <br> RZ = 0 (and RF = 0): Normal DAC (NRZ) operation (default). <br> $R Z=1$ (and RF = 0): Return-to-zero (RZ) DAC operation. <br> $R Z$ is a 3.3 V CMOS logic input with an internal pulldown resistor. |
| B4 | RF | Radio Frequency (RF) Mode-Select Input. <br> RF = 0: NRZ or RZ DAC operation. <br> $R F=1$ (and RZ = 0): RF DAC operation. <br> RF is a 3.3 V CMOS logic input with internal pulldown resistor. |
| C13 | CLKP | LVDS-Compatible Converter Clock Input. There is an internal $100 \Omega$ termination resistor between CLKP and CLKN. |
| B13 | CLKN | LVDS-Compatible Converter Clock Input. There is an internal $100 \Omega$ termination resistor between CLKP and CLKN. |
| C1 | CAL | DAC Output Resistance Calibration Input. <br> Calibration of the internal output resistors is initiated by a rising edge on CAL. <br> $C A L=1$ : Output resistors are calibrated. <br> $C A L=0$ : Output resistors are uncalibrated. <br> CAL is a 3.3 V CMOS input with an internal pulldown resistor. Leakage current is less than $\pm 15 \mu \mathrm{~A}$. |

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## Pin Description (continued)

| PIN | NAME | FUNCTION |
| :---: | :---: | :--- |
| F6-F3, F1, F2, H6-H1 | DAP11-DAP0 | Positive Terminals of A-Channel LVDS Data Inputs. DAP11 is MSB. <br> Offset binary format. |
| G6-G3, G1, G2, J6-J1 | DAN11-DAN0 | Negative Terminals of A-Channel LVDS Data Inputs |
| K1-K4, M1-M4, K5, M5, <br> K6, M6 | DBP11-DBP0 | Positive Terminals of B-Channel LVDS Data Inputs. DBP11 is MSB. <br> Offset binary format. |
| L1-L4, N1-N4, L5, N5, L6, N6 | DBN11-DBN0 | Negative Terminals of B-Channel LVDS Data Inputs |
| M7, K7, M8, K8, M9-M12, <br> K9, K10, K11, L12 | DCP11-DCP0 | Positive Terminals of C-Channel LVDS Data Inputs. DCP11 is MSB. <br> Offset binary format. |
| N7, L7, N8, L8, N9-N12, <br> L9, L10, L11, K12 | DCN11-DCN0 | Negative Terminals of C-Channel LVDS Data Inputs |
| G7, J7, J12-J8, G12-G8 | DDP11-DDP0 | Positive Terminals of D-Channel LVDS Data Inputs. DDP11 is MSB. <br> Offset binary format. |
| F7, H7, H12-H8, F12-F8 | DDN11-DDN0 | Negative Terminals of D-Channel LVDS Data Inputs |
| J13 | DATACLKP | Positive Terminal of LVDS Data Output Clock |
| H13 | DATACLKN | Negative Terminal of LVDS Data Output Clock <br> K13Data Clock Delay Mode Input. <br> Adjusts the delay of the output data clock. <br> DELAY = 0: No delay added. <br> DELAY = 1: Add delay of 1/2 input data period (2 DAC clock cycles). <br> DELAY is a 3.3V CMOS input with an internal pulldown resistor. |
| L13 | CLKDIV | Data Clock Divide Mode Input. <br> CLKDIV = 1: Data clock rate = input data rate / 2 (fCLK / 8). <br> CLKDIV = 0: Data clock rate = input data rate / 4 (fCLK / 16). <br> CLKDIV is a 3.3V CMOS input with an internal pulldown resistor. |
| N13 | N.C. | No Connection. This pin should be left unconnected. |

## Detailed Description

The MAX19692 is a high-performance, high-speed, 12-bit current-steering DAC with an integrated $50 \Omega$ differential output termination. The DAC is capable of operating with clock speeds up to 2.3 GHz . The converter consists of an edge-triggered 4:1 input data multiplexer followed by a current-steering circuit. This circuit is capable of generating differential full-scale currents in the 8 mA to 20 mA range. Internal $25 \Omega$ resistors on each output, in combination with an external termination, convert the differential current into a voltage. The internal resistors are terminated to the 3.3 V analog supply, $\mathrm{AV}_{\mathrm{D}}$ 3.3. The internal termination resistors can be calibrated to an external $500 \Omega$ precision resistor. A calibration cycle can be run every time the converter is powered up, or at any other time. An integrated 1.2V-bandgap reference, control amplifier, and user-selectable external resistor determine the data converter's full-scale range. The converter features selectable frequency response to allow application-dependent optimization of output power and gain flatness. Three responses can be selected: non-return-to-zero (NRZ), return-to-zero (RZ), or radio frequency (RF).

Reference Input/Output
The MAX19692 supports operation with the on-chip 1.2Vbandgap reference or an external reference voltage source. REFIO serves as the input for an external, lowimpedance reference source, and as the output if the DAC is operating with the internal reference. For stable operation with the internal reference, REFIO should be decoupled to DACREF with a $1 \mu$ F capacitor. REFIO must be buffered with an external amplifier if heavier loading is required, due to its $10 \mathrm{k} \Omega$ series resistance.
The MAX19692's reference circuit (Figure 1) employs a control amplifier, designed to regulate the full-scale current IOUT for the differential current outputs of the DAC. The output current can be calculated as follows:

$$
\text { IOUT }=32 \times \operatorname{IREF} \times 4095 / 4096
$$

where IREF is the reference output current (IREF = $V_{\text {REFIO }} /$ RSET) and IOUT is the full-scale output current of the DAC. Located between FSADJ and DACREF, RSET is typically set to $2 k \Omega$, which results in a full-scale current of 20 mA if the internal reference is used.

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## Analog Outputs

The MAX19692 is a differential current-steering DAC with built-in self-calibrated output termination resistors to optimize performance. The outputs are terminated to AVDD3.3, and are calibrated to provide a $50 \Omega$ differential output resistance. In addition to the signal current, a constant 10 mA current sink is connected to each DAC output. Typically, the outputs should be used with a


Figure 1. Reference Architecture, Internal Reference Configuration
$50 \Omega$ transformer. If the transformer is center tapped, it is recommended that the center tap be connected to $A V_{D D 3.3 \text {. If the transformer is not center tapped, bias }}$ tees or RF chokes can be used to pull up the outputs. Figure 2 shows an equivalent circuit of the internal output structure of the MAX19692.
The termination resistors, $\mathrm{RT}_{\mathrm{T}}$, are calibrated to $23.5 \Omega$. $R_{M}=R_{M 1}+R_{M 2}+R_{M 3}$ is resistance associated with the DAC output traces and bond wires, and is not calibrated. The output resistance is equal to $2 R_{T}+2 R_{M}$, and is nominally $50 \Omega$. The MAX19692 is normally used with an external differential $50 \Omega$ load, RL. For this case, the peak differential output voltage is calculated as:

$$
V_{\text {OUT }}=I_{\text {OUT }} \times \frac{R_{L} R_{T}}{R_{L}+2 R_{M}+2 R_{T}}
$$

where IOUT is the full-scale current, which is typically set to 20 mA . With $R_{L}=50 \Omega, R_{\top}=23.5 \Omega$, and $R_{M}=1.5 \Omega$, VOUT $=0.235 \mathrm{~V}$ is found. This corresponds to an output power of -2.6 dBm . As shown in Figure 2, the output circuit has some resistive, capacitive, and inductive elements. These elements limit the output bandwidth to 2 GHz with a resistive differential $50 \Omega$ load.

## Output Resistor Calibration

The integrated termination resistors, Rt, must be calibrated to have an accurately known DAC output resistance and an accurately known DAC output voltage.


Figure 2. Equivalent Output Circuit

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The termination resistors are calibrated to the external reference resistor, RREFRES, which should be connected between REFRES (pin B2) and AVDD3.3. RREFRES is nominally $500 \Omega$. A plot showing the typical relation between the DAC output resistance and Rrefres is shown in Figure 3.
The calibration cycle is initiated with a rising edge on the CAL pin. The CAL pin must be asserted after the supply voltages and the reference voltage have reached steady state. Input data should not be switching while calibration is running. The duration of the calibration cycle is shorter than 65,536 DAC clock cycles-which is less than $65.6 \mu \mathrm{~s}$ if the converter is operated with a 1 GHz clock rate. The CAL pin must be held high for the output resistors to remain calibrated. If the clock is stopped, or if power is cycled, a new calibration cycle must be run.


## DAC Impulse/Frequency <br> Response Selection

The MAX19692 has three impulse/frequency response modes. These are set with the RZ and RF input pins as described in Table 1.
The impulse responses of the three operating modes are shown in Figure 4. The sample period is equal to $T$. The default operating mode of the MAX19692 is NRZ mode. The sinc $(\operatorname{sine}(x) / x)$ response has zeros at every multiple of the DAC update frequency fCLK $=1 / \mathrm{T}$. Using this impulse response, the frequency response of the DAC has the familiar sinc shape:

$$
A_{\text {NRZ }}=A_{0}\left[\frac{\sin \left(\pi f_{\mathrm{OUT}} T\right)}{\pi \mathrm{f}_{\mathrm{OUT}}{ }^{T}}\right]
$$

where fout is the DAC output frequency, $T=1 /$ fcLK is the period of the DAC clock, and $A_{0}$ is the peak low-frequency output amplitude.
In RZ mode, the DAC output has a $50 \%$ duty cycle. The DAC output stays at midscale for the remaining $50 \%$ of the clock cycle. The resulting frequency response is:

$$
A_{R Z}=\frac{A_{0}}{2}\left[\frac{\sin \left(\pi f_{O U T} T / 2\right)}{\pi f_{O U T} T / 2}\right]
$$

Table 1. RZ and RF Input Truth Table

| $\mathbf{R Z}$ | RF | FREQUENCY RESPONSE MODE |
| :---: | :---: | :---: |
| 0 | 0 | NRZ |
| 1 | 0 | RZ |
| 0 | 1 | RF |
| 1 | 1 | Do not use |

Figure 3. Output Resistance vs. REFRES Resistor


Figure 4. Impulse Responses in (a) NRZ Mode, (b) RZ Mode, and (c) RF Mode

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Figure 5. Amplitude Responses for NRZ Mode (Solid Line), RZ Mode (Dash-Dot Line), and RF Mode (Dashed Line). Excludes output bandwidth limitation.

This frequency response is flatter than the NRZ response in the three first Nyquist zones, particularly in the 2nd and 3rd Nyquist zones-making this DAC usable for outputting wideband signals in the 2nd and 3rd Nyquist zones.
The third mode of operation is the RF mode. In this mode, the DAC output response is inverted in the second half of the clock cycle, resulting in a doublet pulse at the output of the DAC in every clock cycle. The resulting DAC frequency response is:

$$
A_{R F}=A_{0}\left[\frac{\sin \left(\pi f_{\mathrm{OUT}} \mathrm{~T} / 2\right)}{\pi \mathrm{f}_{\mathrm{OUT}}{ }^{\top} / 2} \times \sin \left(\pi \mathrm{f}_{\mathrm{OUT}} \mathrm{~T} / 2\right)\right]
$$

The RF mode increases the DAC output power in the second and third Nyquist zones and attenuates it in the first Nyquist zone.
The frequency responses for the three modes of operation are plotted in Figure 5.
NRZ mode provides the highest power in the first Nyquist zone. RZ mode provides the flattest frequency response in the first and third Nyquist zones, and RF mode provides superior output power in the second and third Nyquist zones, as well as the flattest gain in the second Nyquist zone.


Figure 6. Recommended Clock Amplitude

## Clock Inputs

The MAX19692 features a flexible differential clock input (CLKP, CLKN) operating from a separate supply (AVCLK) to achieve the best possible jitter performance. The two clock inputs can be driven from a single-ended or a differential clock source. A sine wave or a square wave can be used. For single-ended operation, CLKP should be driven by a logic source, while CLKN should be bypassed to GND with a $0.1 \mu \mathrm{~F}$ capacitor.
Driving the clocks differentially is recommended for optimum jitter performance. Choose a clock amplitude that is as large as possible (without the clock voltage at the CLKN and CLKP pins going more than 200mV below ground or above the AVCLK supply voltage) to minimize jitter. This results in the most accurate duty cycle-and hence the most accurate gain in RZ and RF modes. For an AC-coupled, differential sine-wave clock, the clock amplitude should not be higher than 2.5 V peak-to-peak ( 12 dBm if terminated in $50 \Omega$ ). The typical performance plots in this data sheet have generally been measured using a 10 dBm (2VP-P) clock amplitude.
The MAX19692 can be used with a sinusoidal clock amplitude as low as 0.6VP-p below 1.5 Gsps . For higher update rates, the clock amplitude should stay within the operating region specified in Figure 6.
The CLKP and CLKN pins are internally biased to 0.6 V with resistors. This allows the user to AC-couple clock sources directly to the device without external resistors to define the DC level.

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Figure 7. Typical Clock Application Circuit


Figure 8. Clock Application Circuit with Improved Symmetry

The MAX19692 has an internal $100 \Omega$ termination resistor between CLKP and CLKN. An extra $100 \Omega$ differential termination resistor should be added if using a $50 \Omega$ clock source. See Figure 7 for a convenient and quick way to apply a differential signal created from a singleended source and a wideband transformer.
The clock circuit in Figure 7 has some amplitude asymmetry at update rates above 1Gsps, due to transformer loss. This may cause performance degradation for some operating conditions. A clock interface circuit with improved symmetry using three balun transformers is shown in Figure 8. This clock interface circuit provides symmetric and balanced clock signals for frequencies up to the maximum update rate of the MAX19692.
An equivalent circuit model for the clock inputs is shown in Figure 9.

## Clock Duty Cycle

The duty cycle of the converter clock should be close to $50 \%$. If an AC-coupled sine-wave clock is used, the clock duty cycle is automatically close to $50 \%$. If a squarewave clock is used, this is not necessarily the case.
Keeping the clock duty cycle close to $50 \%$ is particularly important when operating in RZ and RF modes.
When operating in RZ mode, clock duty-cycle deviation from $50 \%$ distorts the converter's frequency response. A clock duty cycle above 50\% increases the converter's output power at low frequencies, and lowers the frequency of the zero in the frequency response func-tion-effectively producing a frequency response between that of NRZ and RZ modes.
When operating in RF mode, a clock duty cycle higher or lower than $50 \%$ increases the output amplitude at low frequencies in the first Nyquist zone and slightly lowers the output amplitude in the second and third Nyquist zones.

## Data Inputs

Data inputs (DAP[11:0], DAN[11:0], DBP[11:0], DBN[11:0], DCP[11:0], DCN[11:0], DDP[11:0], DDN[11:0]) have LVDS receivers followed by edgetriggered flip flops. Four 12-bit buses accept data in offset binary format. The LVDS inputs feature on-chip termination with differential $100 \Omega$ resistors. A 1.25 V common-mode level with $a \pm 400 \mathrm{mV}$ differential swing can be applied to these inputs. See Figure 10 for an equivalent circuit of the LVDS inputs.

# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 



Figure 9. Clock Input Equivalent Circuit


Figure 10. LVDS Input Equivalent Circuit

## Data-Timing Relationships

The timing of the LVDS inputs is defined with respect to the LVDS output DATACLK (DATACLKP - DATACLKN). The LVDS data inputs are latched at $1 / 4$ the input clock frequency. The DATACLK output frequency is divided by another factor of $4($ CLKDIV $=0)$ or by $2($ CLKDIV $=1)$.
Define the $0^{\circ}$ point of DATACLK as the rising edge.
For the case of CLKDIV $=1$, data are latched at $0^{\circ}$ and $180^{\circ}$ of DATACLK, and setup and hold times must be satisfied for both these points in time.

For the case of CLKDIV = 0, data are latched at $0^{\circ}, 90^{\circ}$ $180^{\circ}$, and $270^{\circ}$ of DATACLK. Setup and hold times must be satisfied for all four of these points in time.
A delay set by the DELAY pin can skew DATACLK by $1 / 2$ period of the input data period, as shown in Figure 11. This eases interfacing to an FPGA where the clock to Q delay of the LVDS outputs is not adjustable. The clock driving the data input register is not delayed with the DELAY pin. The setup and hold times are always referred to the case when DELAY $=0$. Data-timing relationships are shown in Figure 12.

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Figure 11. Effect of Setting DELAY $=1$ on Data Clock Output


Figure 12. Setup (ts) and Hold Time (tH) for Data Input Interface

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Figure 13. Possible Output Circuits for MAX19692

## Applications Information <br> Differential Coupling Using RF Transformers

The differential voltage existing between OUTP and OUTN can be converted to a single-ended voltage using a transformer or a differential amplifier configuration. Using a differential transformer-coupled output, in which the output power is limited to -2.6 dBm , can optimize the dynamic performance. It is recommended that the DAC outputs are pulled up to 3.3 V . The use of bias tees, as shown in Figure 13, is recommended for optimal performance. RF chokes can be used rather than bias tees if an isolation transformer is used. Not pulling up the outputs to 3.3 V is also possible, but may result in some degradation of dynamic performance in some applications. Two output circuits are shown in Figure 13. The circuit shown in Figure 13(a) has less than 3dB loss (in addition to the sinc attenuation built into the DAC) from approximately

(b) $\quad{ }^{*} n=80 R n=16$ AS SET BY CLKDIV.

Figure 14. Data Source to DAC Interfacing
4 MHz to 700 MHz . The circuit shown in Figure 13(b)-that is used on the MAX19692 evaluation kit-has less than 3 dB loss at frequencies up to approximately 1150 MHz . To achieve the maximum bandwidth, it is important to minimize the inductance in the ground lead on the secondary side of the transformers. It is recommended to use a very short trace and multiple vias for the connection to the ground plane.

Data Synchronization
The DAC clock is running at four times the data rate of the data interface to the MAX19692. An LVDS level data clock output (DATACLKP, DATACLKN) is provided to help the user synchronize the data source and the DAC. The output data clock frequency can be set to $1 / 2$ the input data rate or $1 / 4$ the input data rate. When the DAC is running at full speed, this allows the data clock to be interfaced directly to FPGAs without using an external clock divider. For example, if the DAC is updating at 2.3 Gsps , the input data rate is 575 Mwps . If the DAC is interfaced to an FPGA, one could run the data clock at $1 / 4$ the data input rate; hence the data output clock frequency would be 143.75 MHz .

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If the system clock is running at the DAC update rate, the scheme in Figure 14(a) can be used. In this case, the system is clocked using the data clock output from the DAC. The delays of the data and the clock depend upon line lengths and loading. Hence, clock deskewing using a phase-locked loop may be necessary to make this system work properly at speed. When CLKDIV $=0$, the data clock output can be phase-shifted by $45^{\circ}$ using the DELAY pin. When CLKDIV = 1, the data clock output can be phase-shifted by $90^{\circ}$ using the DELAY pin.
An alternative solution is shown in Figure 14(b). In this case, the system clock distribution is running at the data clock rate. A low-jitter, low-phase-noise phaselocked loop is used to generate the high-speed DAC clock. Using the data clock for feedback into the PLL ensures synchronization between data and clock.
If more than one MAX19692 is used in a system, and the relative phases need to be defined, the divided data clock of each DAC should be phase locked to a system clock running at data-rate / 4 or data-rate / 2, which is equal to the input clock rate divided by 8 or 16 .

## Grounding, Bypassing, Power-Supply, and Board Layout Considerations

Grounding and power-supply decoupling can strongly influence the performance of the MAX19692. Unwanted digital crosstalk may couple through the input, reference, power supply, and ground connections, affecting dynamic performance. Proper grounding and powersupply decoupling guidelines for high-speed, high-frequency applications should be closely followed. This reduces EMI and internal crosstalk that can significantly affect the dynamic performance of the MAX19692.
Use of a multilayer PC board with separate ground and power-supply planes is required. It is recommended that the analog output and the clock input are run as controlled-impedance microstrip lines on the top layer of the board, directly above a ground plane, and that no vias are used for the clock input (CLKP, CLKN) and the analog output (OUTP, OUTN) signals. Depending on the length of the traces, and the operating condition, a low-loss dielectric material (such as ROGERS RO4003) as the top layer dielectric may be advisable. The data clock (DATACLKP, DATACLKN) must be routed so its coupling into the clock input and the DAC output is minimized.
Digital input signals should be run as controlled-impedance strip lines between ground planes. Digital signals should be kept as far away from sensitive analog inputs, reference input sense lines, common-mode inputs, and clock inputs as practical. It is particularly important to
minimize coupling between digital signals and the clock to optimize dynamic performance for high output frequencies. A symmetric design of the clock input and analog output lines is critical to minimize distortion and optimize the DAC's dynamic performance.
Digital signal paths should be kept short and run lengths matched to avoid propagation delay and dataskew mismatches.
The MAX19692 supports three separate power-supply inputs for analog 3.3V (AVDD3.3), switching (VDD1.8), and clock (AVCLK) circuits. Each AVDD3.3, VDD1.8, and $A V_{C L K}$ input should at least be decoupled with a separate 47 nF capacitor as close to the pin as possible and their opposite ends with the shortest possible connection to the corresponding ground plane, to minimize loop inductance. All three power-supply voltages should also be decoupled at the point they enter the PC board with tantalum or electrolytic capacitors. Ferrite beads with additional decoupling capacitors forming a pi-network could also improve performance.
The power-supply inputs VDD1.8 and AVCLK of the MAX19692 allow a $1.8 \mathrm{~V} \pm 0.1 \mathrm{~V}$ supply voltage range for update rates $<2.0 \mathrm{Gsps}$. A range of 1.8 V to 1.9 V should be used for 2.0Gsps to 2.3Gsps. The analog powersupply input $A V_{D D 3} 3$ allows a $3.3 \mathrm{~V} \pm 0.2 \mathrm{~V}$ supply voltage range. To optimize the dynamic performance of the MAX19692 over temperature at the highest update rates, it is important that the difference between VDD1.8 and $A V_{D D 3.3}$ is at least 1.4 V . If $\mathrm{V}_{\text {DD1 }} 1.8$ is 1.9 V and AVDD3.3 is 3.1 V , dynamic performance at these update rates will degrade at higher temperatures, as shown in the Typical Operating Characteristics.
The MAX19692 is packaged in a 169 CSBGA package with 0.8 mm ball pitch (package code: X16911-1), providing design flexibility, thermal efficiency, and a small footprint for the DAC.

## Static Performance Parameter Definitions

Integral Nonlinearity (INL)
Integral nonlinearity is the deviation of the values on an actual transfer function from either a best straight-line fit (closest approximation to the actual transfer curve) or end-point fit (a line drawn between the end points of the transfer function, once offset and gain errors have been nullified). For a DAC, the deviations are measured at every individual step. The MAX19692 INL is specified using the end-point method.

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## Differential Nonlinearity (DNL)

Differential nonlinearity is the difference between an actual step height and the ideal value of 1 LSB . A DNL error specification greater than-1 LSB guarantees a monotonic transfer function.

Offset Error
The offset error is the difference between the ideal and the actual offset current. For a DAC, the offset point is the average value at the output for the two midscale digital input codes with respect to the full scale of the DAC. This error affects all codes by the same amount.

## Gain Error

A gain error is the difference between the ideal and the actual full-scale output voltage on the transfer curve, after nullifying the offset error. This error alters the slope of the transfer function and corresponds to the same percentage error in each step.

## Dynamic Performance Parameter Definitions

## Settling Time

The settling time is the amount of time required from the start of a transition until the DAC output settles its new output value to within the specified accuracy.

## Noise Spectral Density

The DAC output noise is the sum of the quantization noise and other noise sources. Noise spectral density is the noise power in a 1 Hz bandwidth.

Spurious-Free Dynamic Range (SFDR)
SFDR is the ratio of the RMS amplitude of the carrier frequency (maximum signal components) to the RMS value of the largest distortion component. SFDR is usually measured in dBc with respect to the carrier frequency amplitude or in dBFS with respect to the DAC's full-scale range. Depending on its test condition, SFDR is observed within a predefined window or to Nyquist.

## Two-/Four-Tone

Intermodulation Distortion (IMD)
The two-/four-tone IMD is the ratio expressed in dBc (or dBFS) of the worst 3rd-order (or higher) IMD products to any output tone.

## 12－Bit，2．3Gsps，Multi－Nyquist DAC with Selectable Frequency Response

Pin Configuration

| TOP VIEW | 11131 |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|  | REFIO <br> A1 <br> A1 ； | FSADJ A2 ： | DACREF <br> ：A3 ； | AVDD3．3 <br> （A4 | AV ${ }_{\text {DD3．}}$ <br> A5 | $\begin{aligned} & \text { OUTP } \\ & \hline \text { A6 } \end{aligned}$ | AV ${ }^{\text {DD3 }} 3$ <br> A7 | OUTN | AV ${ }_{\text {DD3．}}$ <br> A9 | $V_{\text {DD1．}}$ <br> A10 | $\begin{aligned} & \text { GND } \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{AV} \mathrm{CLK} \\ & \hline \mathrm{~A} 2 \mathrm{C} \end{aligned}$ |  |
| B | $\begin{aligned} & \text { CREF } \\ & \hdashline B 1 \end{aligned}$ | REFRES <br> B2 | $\begin{gathered} R Z \\ \hdashline B 3 \\ \end{gathered}$ | $\begin{gathered} \text { RF } \\ \hdashline \end{gathered}$ | $\begin{aligned} & \text { GND } \\ & \hdashline-B 5 \\ & \hdashline \end{aligned}$ | $\begin{gathered} \text { GND } \\ \hdashline \\ \hline \end{gathered}$ | $\begin{aligned} & \text { GND } \\ & \hline B 7 \\ & \end{aligned}$ | $\begin{aligned} & \text { GND } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { GND } \\ & \hdashline B 9 \end{aligned}$ | $V_{\text {DD1．}} 8$ <br> B10 | GND | $\begin{aligned} & \mathrm{AV} \mathrm{CLK} \\ & -\mathrm{B} 12 \end{aligned}$ | $\begin{aligned} & \text { CLKN } \\ & \\ & \hline \text { B13 } \end{aligned}$ |
| C | $\begin{gathered} \text { CAL } \\ \hdashline \mathrm{C1} \end{gathered}$ | VDD1．8 C2 ： | $\begin{aligned} & V_{D D 1.8} \\ & C-C 3 \end{aligned}$ | $\begin{gathered} \text { GND } \\ \cdots \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline-C 5 \\ \hdashline \end{gathered}$ | GND <br> C6 | GND <br> C7 | $\begin{gathered} \text { GND } \\ \hdashline-1 \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline \\ \hdashline \end{gathered}$ | $V_{\text {DD1．}} 8$ <br> C10 | $\begin{aligned} & \text { GND } \\ & \cdots \\ & \hdashline-11 ; \end{aligned}$ | $\begin{aligned} & \mathrm{AV} \mathrm{CLK} \\ & \mathrm{CC12} \end{aligned}$ | $\begin{aligned} & \text { CLKP } \\ & \hdashline \end{aligned}$ |
| D | $\begin{aligned} & \text { GND } \\ & \hdashline-D 1 \end{aligned}$ | GND D2 ： | $\begin{gathered} \text { GND } \\ \hdashline-D 3 \\ \hdashline \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline D 4 \\ \hdashline \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline-D 5 \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline D 6 \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline D 7 \\ \hdashline \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline-D 8 \\ \hdashline \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline-D 9 \\ \hdashline \end{gathered}$ | $\begin{gathered} \text { GND } \\ \cdots \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline-11 \end{gathered}$ | AVCLK D12 | $\begin{gathered} \text { GND } \\ \hdashline-D 13 \\ \hdashline \end{gathered}$ |
| E | VDD1．8 E1 | VD1． 8 E2 ； | VDD1．8 | VDD1．8 | $\begin{gathered} \text { GND } \\ \hdashline \mathrm{ES} \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline \text { E6 } \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline E 7 \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline E 8 \end{gathered}$ | $\begin{gathered} \text { GND } \\ \hdashline \end{gathered}$ | $V_{D D 1.8}$ <br> ！E10 | VDD1．8 <br> E11 | $V_{\text {DD1．8 }}$ （E12） | VDD1．8 （E13） |
| F | $\begin{aligned} & \text { DAP7 } \\ & \hline \text { F1 } \end{aligned}$ | $\begin{aligned} & \text { DAP6 } \\ & \hdashline-F 2 \end{aligned}$ | $\begin{aligned} & \text { DAP8 } \\ & \hdashline \\ & \hdashline \end{aligned}$ | $\begin{gathered} \text { DAPG } \\ \hdashline \text { F4 } \end{gathered}$ | $\begin{aligned} & \text { DAP10 } \\ & \end{aligned}$ | DAP11 <br> F6 | DDN11 F7 ： | $\begin{gathered} \text { DDNO } \\ \hdashline-\cdots 8 \\ \hdashline- \end{gathered}$ | $\begin{gathered} \text { DDN1 } \\ \hdashline-F 9 \end{gathered}$ | $\begin{aligned} & \text { DDN2 } \\ & \hline-\mathrm{F} 10 \end{aligned}$ | $\begin{aligned} & \text { DDN3 } \\ & \hline-N 11 \end{aligned}$ | $\begin{aligned} & \text { DDN4 } \\ & \hline-N 12 \vdots \end{aligned}$ | VDD1．8 （F13！ |
| G | $\begin{aligned} & \text { DAN7 } \\ & \hdashline \text { G1 } \end{aligned}$ | DAN6 G2 ： | $\begin{aligned} & \text { DAN8 } \\ & \hdashline G 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { DANS } \\ & \hline \text { G4 } \end{aligned}$ | DAN10 G5 | DAN11 <br> G6 | DDP11 G7 | $\begin{gathered} \text { DDPO } \\ \hdashline \text { G8 } \end{gathered}$ | $\begin{aligned} & \text { DDP1 } \\ & \hdashline-G 9 \\ & \hdashline \end{aligned}$ | $\begin{aligned} & \text { DDP2 } \\ & \hline-\quad \text { G10 } \end{aligned}$ | $\begin{aligned} & \text { DDP3 } \\ & \text { G-G11 } \end{aligned}$ | $\begin{gathered} \text { DDP4 } \\ 1 \text { G12 } \end{gathered}$ | $\begin{gathered} \text { GND } \\ \cdots \end{gathered}$ |
| H | $\begin{aligned} & \text { DAPO } \\ & \hdashline ⿴ 囗 十 力 \end{aligned}$ | $\begin{aligned} & \text { DAP1 } \\ & \hdashline ⿴ 囗 ⿱ 一 一 口 \end{aligned}$ | $\begin{gathered} \text { DAP2 } \\ \hdashline \end{gathered}$ | $\begin{aligned} & \text { DAP3 } \\ & \hline \text { H4 } \end{aligned}$ | $\begin{aligned} & \text { DAP4 } \\ & \end{aligned}$ | $\begin{aligned} & \text { DAP5 } \\ & \hdashline H 6 \end{aligned}$ | DDN10 H7 －－ | $\begin{aligned} & \text { DDN5 } \\ & \hdashline \\ & \hdashline \end{aligned}$ | $\begin{aligned} & \text { DDN6 } \\ & \hdashline-10 \end{aligned}$ | $\begin{aligned} & \text { DDN7 } \\ & 1 \text { H10 } \end{aligned}$ | DDN8 <br> ！ H 11 | $\begin{aligned} & \text { DDN9 } \\ & 1 \text { H12 } \end{aligned}$ | DATACLKN （H13） |
| J | $\begin{gathered} \text { DANO } \\ \hdashline, ~ \end{gathered}$ | $\begin{aligned} & \text { DAN1 } \\ & \hdashline \mathrm{J} 2 \end{aligned}$ | $\begin{gathered} \text { DAN2 } \\ \hdashline, ~ \end{gathered}$ | $\begin{aligned} & \text { DAN3 } \\ & \hdashline, ~ \end{aligned}$ | DAN4 J5 ； | $\begin{aligned} & \text { DAN5 } \\ & \hdashline, ~ \end{aligned}$ | $\begin{gathered} \text { DDP10 } \\ \hdashline J 7 \\ \hdashline \end{gathered}$ | $\begin{aligned} & \text { DDP5 } \\ & \hdashline, ~ \end{aligned}$ | $\begin{array}{r} \text { DDP6 } \\ \hdashline J 9 \end{array}$ | $\begin{gathered} \text { DDP7 } \\ \hdashline 100 \end{gathered}$ | DDP8 <br> （J11） | $\begin{gathered} \text { DDP9 } \\ \hdashline-J 12 \end{gathered}$ | DATACLKP （J13） |
| K | $\begin{aligned} & \text { DBP11 } \\ & \hdashline \text { K1 } \end{aligned}$ | $\begin{aligned} & \text { DBP10 } \\ & \hdashline \text { K2 } \end{aligned}$ | $\begin{aligned} & \text { DBP9 } \\ & \hdashline \text { K3 } \end{aligned}$ | $\begin{aligned} & \text { DBP8 } \\ & \hdashline K 4 \end{aligned}$ | $\begin{aligned} & \text { DBP3 } \\ & \hdashline K 5 \end{aligned}$ | $\begin{aligned} & \text { DBP1 } \\ & \hdashline \text { K6 } \\ & \hdashline \end{aligned}$ | DCP10 <br> K7 | $\begin{aligned} & \text { DCP8 } \\ & \hdashline K 8 \end{aligned}$ | $\begin{aligned} & \text { DCP3 } \\ & \hdashline K 9 \end{aligned}$ | $\begin{aligned} & \text { DCP2 } \\ & \hline \text { K10 } \end{aligned}$ | $\begin{aligned} & \text { DCP1 } \\ & \hdashline \text { K11 } \end{aligned}$ | $\begin{aligned} & \text { DCNO } \\ & \hdashline \text { K12 } \end{aligned}$ | $\begin{aligned} & \text { DELAY } \\ & \hdashline \mathrm{K} 13 \end{aligned}$ |
| L | DBN11 <br> L1 | DBN10 <br> L2 |  | $\begin{gathered} \text { DBN8 } \\ \hdashline-\mathrm{L4} \\ \hline \end{gathered}$ | $\begin{gathered} \text { DBN3 } \\ \hdashline-1 . \end{gathered}$ | $\begin{aligned} & \text { DBN1 } \\ & \hdashline 16 \\ & \hdashline \end{aligned}$ | DCN10 L7 | $\begin{gathered} \text { DCN8 } \\ \hline 18 \end{gathered}$ | $\begin{gathered} \text { DCN3 } \\ \hdashline \\ \hline \end{gathered}$ | DCN2 | $\begin{aligned} & \text { DCN1 } \\ & \hdashline-L 11 \\ & \hdashline \end{aligned}$ | $\begin{aligned} & \text { DCPO } \\ & \hdashline-L 12 \end{aligned}$ | $\begin{aligned} & \text { CLKDIV } \\ & \text { LLI3 } \end{aligned}$ |
| M | $\begin{aligned} & \text { DBP7 } \\ & \hdashline M 1 \end{aligned}$ | DBP6 <br> （M2； | $\begin{aligned} & \text { DBP5 } \\ & \text { M3 } \end{aligned}$ | $\begin{aligned} & \text { DBP4 } \\ & \hline \text { M4 } \end{aligned}$ | $\begin{aligned} & \text { DBP2 } \\ & \hdashline M 5 \end{aligned}$ | $\begin{aligned} & \text { DBPO } \\ & \hdashline M 6 \end{aligned}$ | $\begin{aligned} & \text { DCP11 } \\ & \text { M7 } \end{aligned}$ | $\begin{aligned} & \text { DCP9 } \\ & \hdashline, ~ M 8: ~ \end{aligned}$ | $\begin{aligned} & \text { DCP7 } \\ & \hline \text { Mg } \end{aligned}$ | $\begin{aligned} & \text { DCP6 } \\ & \text { M10 } \end{aligned}$ | $\begin{aligned} & \text { DCP5 } \\ & \hline \text { M11 } \end{aligned}$ | $\begin{aligned} & \text { DCP4 } \\ & \hdashline \text { M12 } \end{aligned}$ | $\begin{aligned} & \text { GND } \\ & \hdashline \text { M13 } \end{aligned}$ |
| N | $\begin{aligned} & \text { DBN7 } \\ & \hdashline \text { N1 } \end{aligned}$ | $\begin{aligned} & \text { DBN6 } \\ & \hdashline \text { N2 } \end{aligned}$ | $\begin{aligned} & \text { DBN5 } \\ & \hdashline \text { N3 } \\ & \hdashline \end{aligned}$ | $\begin{aligned} & \text { DBN4 } \\ & \hdashline N 4 \\ & \hdashline \end{aligned}$ | $\begin{aligned} & \text { DBN2 } \\ & \hdashline \cdots \end{aligned}$ | $\begin{aligned} & \text { DBNO } \\ & \hdashline \text { N6 } \\ & \hline \end{aligned}$ | $\begin{gathered} \text { DCN11 } \\ \hdashline N 7 \end{gathered}$ | $\begin{gathered} \text { DCN9 } \\ \hdashline \text { N8 } \\ \hdashline \end{gathered}$ | $\begin{aligned} & \text { DCN7 } \\ & \hdashline, ~ \end{aligned}$ | $\begin{aligned} & \text { DCN6 } \\ & \vdots, \ldots \\ & \hdashline 10 \vdots \end{aligned}$ | $\begin{aligned} & \text { DCN5 } \\ & \hdashline \mathbf{N 1 1} ; \end{aligned}$ | $\begin{aligned} & \text { DCN4 } \\ & \cdots \\ & \hdashline 12 \end{aligned}$ | $\begin{aligned} & \text { N.C. } \\ & \hdashline \text { N13 } \end{aligned}$ |

The MAX19692 is packaged in an $11 \mathrm{~mm} \times 11 \mathrm{~mm}, 169$ CSBGA package（package code X16911－1）．Ball pitch is 0.8 mm ．

# 12-Bit, 2.3Gsps, Multi-Nyquist DAC with Selectable Frequency Response 

## Package Information

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information go to www.maxim-ic.com/packages.)


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